Appendix F:

Geologic and Geotechnical Report

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GEOLOGIC AND GEOTECHNICAL ENGINEERING REPORT
PROPOSED ADDITION, FOUR NEW BUILDINGS, RETAINING WALLS, AND SWIMMING POOL

LOT 1, TRACT 23823

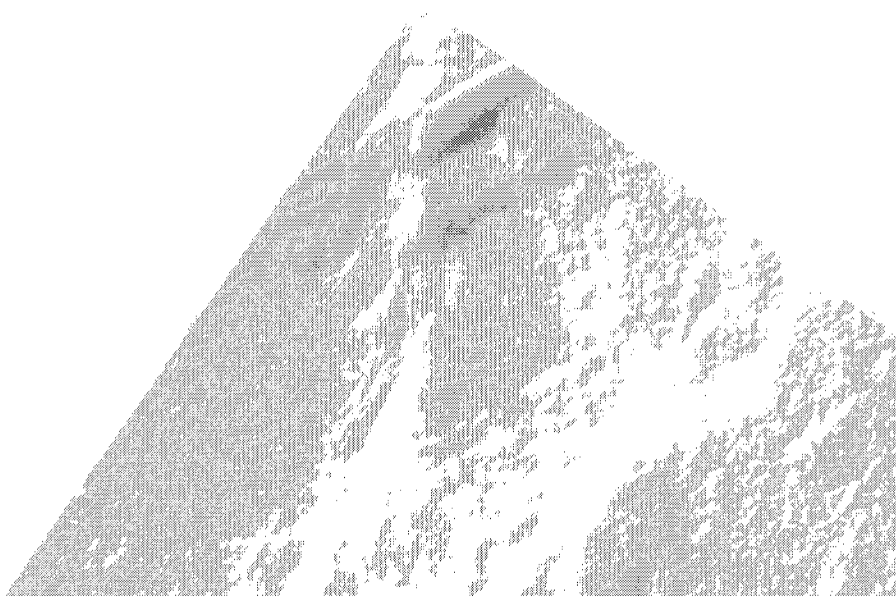
3900 STANSBURY AVENUE

SHERMAN OAKS, CALIFORNIA

FOR THE BUCKLEY SCHOOL

THE J. BYER GROUP, INC. PROJECT NUMBER JB 19376-B

JUNE 6, 2006



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INTRODUCTION

Per your written authorization, The J. Byer Group has prepared this report to summarize findings of our geologic and geotechnical engineering exploration performed at the site. The purpose of this study is to evaluate the nature, distribution, engineering properties, relative stability, and geologic structure of the earth materials underlying the site with respect to constructing additions, four new buildings, retaining walls, and a swimming pool.

INTENT

It is the intent of this report to assist in the design and completion of the proposed projects. The recommendations are intended to reduce geotechnical risks affecting the projects. The professional opinions and advice presented in this report are based upon commonly accepted standards and are subject to the general conditions described in the NOTICE section of this report.

EXPLORATION

The scope of the recent exploration was determined from a site observation by John Byer and review of the new Master Plan Design prepared by Jeffrey M. Kalban & Associates. Exploration was conducted using techniques normally applied to this type of project in this setting. This report is limited to the area of the exploration as shown on the enclosed Geologic Map and cross sections. Conditions affecting portions of the property outside the area explored are beyond the scope of this report.

The original exploration was conducted on September 27, October 1, and October 6, 2003. The recent testing was done on December 22, 2005. The combined exploration includes 10 hand dug test pits and 19, eight inch hollow-stem auger borings. Soil samples were obtained from the test pits and borings and returned to our soils engineering laboratory for testing and analysis. The borings and test pits were logged by the undersigned engineering geologist, project geologist, and our project engineer.

Office tasks included review of laboratory testing, review of the City of Los Angeles, Department of Building and Safety (LADBS), grading records for the subject property, preparation of the Geologic Map, preparation of Sections A through F and I, and engineering analysis of the existing slopes and proposed structures. A description of the earth materials can be found on the enclosed Log of Test Pits and Log of Borings. Appendix I contains a discussion of the laboratory testing procedures and results.

The proposed project, surface geologic conditions, test pit and boring locations are shown on the Geologic Map. Subsurface distribution of the earth materials, projected geologic structure, and the proposed projects are shown on Sections A through F and I.

RESEARCH - PRIOR WORK

LADBS files contain numerous reports which were prepared for the property dating back to 1968. These reports provide geotechnical and geologic information with respect to development of the school and the site conditions at each of the existing structures. Copies of the reports, which describe geologic and geotechnical conditions for the buildings and the city approval letters are attached to this report as Appendix II. The Geologic Map indicates the date that the building sites were developed and shows the approximate limits of the grading as determined from the previous reports. The data contained in the previous reports was reviewed and considered as part of our work on this project.

PROPOSED DEVELOPMENT

Information concerning the proposed project was provided by Jeffrey M. Kalban & Associates. It is proposed to construct four new buildings at the school facility. The three new academic buildings and a library/tech center will be located on the lower portion of the campus. The proposed Main Academic Building will consist of two stories of classrooms and offices over two levels of partial subterranean parking. The Academic Building West will be two stories. The Library/Tech Center Building will be two stories and a basement. The Aquatic Center Building will be two stories and will be located on the north portion of the athletic field. The swimming pool is to be located to the southeast of the Aquatic Center Building. The addition is planned for the north side of the Academic Building South.

SITE DESCRIPTION

The subject property is located on the north flank of the Santa Monica Mountains, south of Ventura Boulevard and east of Beverly Glen Boulevard (33.1401°N Latitude, 118.4436°W Longitude). Access is provided by Stansbury Avenue, which leads up to the school from the north. Several interior roads allow traffic to proceed through the school. Parking is provided by the main lot near Stansbury Avenue. The property consists of a north draining canyon, which has periodically been filled with compacted and uncompacted soil imported to the property. Natural slopes ascend from the graded areas to the west up to Camino De La Cumbre Avenue at an average 2:1 slope gradient. Natural slopes ascend above the east side of the canyon between 275 feet high at a 1.8:1 gradient and 325 feet high at an overall 2:1 slope gradient. These natural slopes are underlain by bedrock and show no signs of past instability or soil erosion. The slopes are covered with a thick growth of native brush. Secondary drainage swales enter the property from the east and carry natural runoff to the property. Drainage from the south is collected in an existing storm drain and directed north to the storm drain system. Drainage within the graded portion of the school site is collected in numerous surface drains and catch basins and transferred to the storm drainage system.

GROUNDWATER

The majority of the borings did not encounter groundwater. The bedrock formation is generally tight and not a groundwater producer. Water was noticed in Boring 1 at a depth of 55 feet and in Boring 13 at a depth 56½ feet. The groundwater apparently is perched on the top of the bedrock and is seeping along the bedrock/alluvium contact. It is the opinion of The J. Byer Group that groundwater will not be a factor in the construction of the proposed buildings and additions to the school. It should be noted that seasonal fluctuations in groundwater levels may occur due to variations in climate, irrigation, and other factors not evident at the time of the exploration. Fluctuations in groundwater levels may also occur across the site.

EARTH MATERIALS

Compacted Fill

Several generations of compacted fill are present at the school dating back to the original grading performed in 1968. The fill consists of soil imported to the site and compacted under the site observation of Advanced Foundation Engineers and Converse, Davis and Associates. Copies of the Compaction Reports and city approval letters can be found in Appendix II. The fill locations are shown on the Geologic Map.

Fill

Fill was imported to the property to generate a level area at the front for the parking lot and in the southern portion of the property for the athletic field. This fill was not compacted and was not tested by a geotechnical engineer. The fill exposed in Boring 1 consists of an upper layer of clayey sand that is brown, moist, medium dense, and contains some gravel. At a depth of about 14 feet, the fill changes to a dark gray clayey sand that is moist and dense. The fill contains small pebbles of slate that are rounded. The imported clayey sand fill with slate chips is relatively consistent throughout the property. The fill is 25 feet thick in Boring 1, which is at the north end of the school. The fill thins to less than 20 feet to the south, east, and west. Fill was found in Borings 10, 11, and 12 in the south-central portion of the school to a depth of 24 feet in Boring 11. The fill in Boring 11 also contained some construction debris and rubble. Fill underlies the athletic field to a depth of 43 feet as indicated in Boring 13. The fill consists of clayey sand that is reddish brown to dark gray and contains small slate gravel.

Alluvium

Natural alluvial soils underlie the fill and consist of an upper layer of silty clay that is brown, moist, firm, and very porous. The alluvium becomes coarser with depth and grades to light brown silty sand with gravel. It contains large gravel and some small cobbles with depth. The alluvium extends to a depth of 59 feet below grade in Boring 1. The alluvial section becomes thinner to the south where borings encountered bedrock at 43 feet below the surface. The alluvium in Boring 14, which is at the southern end of the school, was found to terminate at 28 feet below grade.

Soil

Natural residual soil blankets the ascending slopes around the property and was encountered in Borings 7 through 10. The soil consists of clayey sand that is dark brown, damp, dense, porous, and contains numerous shale fragments.

Bedrock

Bedrock underlying the property consists of diatomaceous siltstone with interbedded sandstone which is part of the Miocene Modelo Formation. The bedrock is well exposed on cut slopes along Camino De La Cumbre Avenue as well as natural outcrops within the school property. The diatomaceous siltstone and sandstone is well bedded, light gray to tan, and moderately hard.

GEOLOGIC STRUCTURE

Bedding planes within the bedrock strike nearly east-west and dip 25 to 30 degrees to the north. The bedding planes mapped are consistent from the north end of the campus to the south. The geologic structure is also consistent with regional trends. The geologic structure of the bedrock is favorably oriented with respect to gross geologic stability of the site.

GENERAL SEISMIC CONSIDERATIONS

The subject property and all of southern California are located in an active seismic region (CBC Seismic Zone IV). Moderate to strong earthquakes can occur on numerous local faults. The United States Geological Survey, California Geological Survey, private consultants, and universities have been studying earthquakes in southern California for several decades. Early studies were directed toward earthquake prediction and estimation of the effects of strong ground shaking. Studies indicate that earthquake prediction is not practical and not sufficiently accurate to benefit the general public. Governmental agencies are shifting their focus to earthquake resistant structures as opposed to prediction. The purpose of the code seismic design parameters is to prevent collapse during strong ground shaking. Cosmetic damage should be expected.

Within the past 35 years, southern California and vicinity have experienced an increase in seismic activity beginning with the San Fernando earthquake in 1971. In 1987, a moderate earthquake struck the Whittier area and was located on a previously unknown fault. Ground shaking from this event caused substantial damage to the City of Whittier, and surrounding cities.

The January 17, 1994, Northridge Earthquake was initiated along a previously unrecognized fault below the San Fernando Valley. The energy released by the earthquake propagated to the southeast, northwest, and northeast in the form of shear and compression waves, which caused the strong ground shaking in portions of the San Fernando Valley, Simi Valley, City of Santa Clarita, and City of Santa Monica.

Southern California faults are classified as active or potentially active. Faults from past geologic periods of mountain building that do not display any evidence of recent offset are considered "potentially active." Faults that have historically produced earthquakes or show evidence of movement within the past 11,000 years are known as "active faults." No known active faults cross the subject property.

The nearest known potentially active fault is located approximately 3½ kilometers to the south (Santa Monica-Hollywood Fault). From a Building Code (Chapter 16) standpoint, the nearby Santa Monica-Hollywood Fault is classified as a Type "B" fault. The following table lists the applicable CBC seismic coefficients for the project:

BUILDING CODE SEISMIC COEFFICIENTS	
Earth Materials	Compacted Fill/Alluvium
Soil Profile Type	S_D
Seismic Coefficient (C_a)	$0.44N_a$
Seismic Coefficient (C_v)	$0.64N_v$
Near-Source Factor (N_a)	1.15
Near-Source Factor (N_v)	1.4

The principal seismic hazard to the subject property and proposed project is strong ground shaking from earthquakes produced by local faults. Modern, well-constructed buildings are designed to resist ground shaking through the use of shear panels and reinforcement. Additional precautions may be taken to protect personal property and reduce the chance of injury, including strapping water heaters and securing furniture. It is likely that the subject property will be shaken by future earthquakes produced in southern California. However, secondary effects such as surface rupture, lurching, liquefaction, consolidation, ridge shattering, and landsliding should not occur at the subject property.

Liquefaction

The California Geologic Survey has not mapped the site within an area of historic liquefaction. A high groundwater table is not present below the site and the earth materials are fine grained and not subject to liquefaction.

SLOPE STABILITY

Gross Stability

Slopes on the subject property include a natural slope in bedrock that is 275 feet high at 1.8:1 gradient (see Section I). The gross and seismic stability of the slope was analyzed using Bishop's method with a software program by Taga, Copyright 1983.

The analysis shows that the natural ascending slope is grossly stable with a factor of safety in excess of 1.5. The calculations use the shear tests of samples believed to represent the weakest bedrock encountered during exploration. The cross section used is the most critical for the slopes analyzed.

Surficial Stability

Based upon the enclosed calculations, it is reasonable to assume that the natural residual soil is surficially stable. The method of analysis used is the "parallel seepage model" recommended by the American Society of Civil Engineers and the Building and Safety Advisory Committee (August 16, 1978). The assumptions of this method are a uniform planar slope, uniform soil density and shear strength, and uniform seepage parallel to the slope. The validity of the analysis depends, in part, on how closely the assumptions model the field conditions.

For surficial deposits overlying natural slopes, it is the opinion of The J. Byer Group, Inc. that the assumptions of the "parallel seepage model" are not completely satisfied. Thus, though the calculation shows that the surficial materials on the site are stable with a factor of safety in excess of 1.5, the mitigating measures recommended in the "Conclusions and Recommendations" of this report should be implemented during development of the site.

ENVIRONMENTAL GEOLOGY

1. Purpose

The purpose of this section is to provide data for support of the environmental impact report being prepared for the Buckley School improvements. The "Conclusions and Recommendations" section of this report discusses the technical issues with respect to constructing new facilities at the Buckley School. General geologic conditions are discussed in this report, but are summarized in this section.

2. Regional Geology

The subject property is located on the enclosed Regional Geologic Map, which shows the north flank of the Santa Monica Mountains and the southern edge of the San Fernando Valley. This area of the Santa Monica Mountains is underlain by sedimentary bedrock formations consisting of Miocene sandstone and shales, which strike nearly east-west and dip to the north at 25 to 30 degrees. Geologic conditions discovered during our exploration are consistent with regional trends. The north draining canyons contain natural alluvium, which has washed into the canyons from the side walls. The alluvium consists of a mixture of sand, silt, and clay, along with gravel and cobbles of the bedrock. At the subject property, the alluvium has been covered with a layer of fill imported to the site and placed for support of structures and to gain additional level area. There are no landslides indicated from our exploration and none are shown on the Regional Geologic Map. Development of the school facility should have a minimal impact on the existing geologic conditions provided the conclusions and recommendations of this study are incorporated into the building plans and implemented during development of the structures.

3. Site Seismicity

The subject property is NOT located within an Alquist-Priolo special study zone. No known active faults pass through the school property. The computer program EQSEARCH is a database of historical earthquakes, including the 1994 Northridge, 1992 Landers, 1987 Whittier, and 1971 San Fernando. The peak ground acceleration is calculated for each earthquake and is shown on the following table.

HISTORICAL EARTHQUAKES		
Earthquake	Year	Calculated Ground Acceleration (% g)
San Fernando	1971	0.104
Whittier	1987	0.059
Landers	1992	0.017
Northridge	1994	0.335

The 1994 Northridge Earthquake is the most significant historic event and occurred on a "blind" fault located below the San Fernando Valley approximately 6½ miles northwest of the school. It generated a ground acceleration of 0.335g. The site is NOT within an area of liquefaction potential, but portions of the ascending slope are in a seismic landslide hazard zone, as shown on the enclosed Seismic Hazard Map. Calculations performed on the slopes above the school indicate that the natural slopes in bedrock are grossly and seismically stable (Calculation Sheets 1-6). The Northridge Earthquake did cause damage to the elementary school building on the northwest corner of the school. The area was developed in 1968 by placing compacted fill over the existing grade. The previous geotechnical engineer did not recognize the need to remove and recompact the upper four feet of the existing alluvium, which is porous and subject to collapse upon saturation or earthquake loading. This is a local condition and the building was repaired by placing underpinning piles into the bedrock. A copy of the report describing the repair can be found in Appendix II.

4. Soil Stability

Natural ascending slopes surround the school and are underlain by natural soil over shale bedrock. The natural slopes on the subject property do not show any signs of surficial slope failures or erosion. A surficial failure did occur offsite in response to the record rainfall of the 2004/2005 rainy season. The failure occurred on the slope west of Camino De La Cumbre, near the rear gate of the school. Concentrated drainage from Beverly Ridge Drive residential development flowed over the descending slope causing erosion. The eroded material moved downslope across the small street, Camino de La Solana, and came to rest on Camino De La Cumbre. The mud was removed from the street. Natural drainages enter the property from the east and can be sources of eroded soil material. Erosion control is recommended for those areas where concentrated offsite flows can carry mud and water onto the school site.

5. Mineral Resources

The Miocene shale at the site does not contain any mineral resources. The shale layers do contain some fish fossils. These fossils are scattered throughout the formation and are not unique or rare.

6. Seismic Safety

The proposed school project is not located in an area where seismic safety is an issue with respect to development of the new buildings. The site is not subject to fault displacement. Ground shaking from local earthquakes will occur at the site. However, modern, well designed buildings are resistant to ground shaking. Liquefaction is not a hazard at the subject property. Seismic settlement of the school building at the northwest corner of the school did occur as the result of shaking from the Northridge Earthquake. The building has been repaired by underpinning. None of the other structures were adversely affected by the strong seismic waves. There are no bodies of water surrounding the school site. Inundation due to tsunami, seiches, and mudflow is not a hazard.

7. Geologic and Geotechnical Conditions

Based upon our exploration and testing there are no landslides within the property. No offsite landslides were discovered during our exploration. The subject property is protected from flooding by a large storm drain system. Subsidence of the older portion of the school did occur in the past due to strong ground shaking from the Northridge Earthquake. Subsidence of the remaining portion of the school should not occur as the buildings were placed on certified compacted fill pads tested by a geotechnical engineer. Subsidence of the open space fill areas may occur, but will not affect any structure. The earth materials underlying the school are not subject to lateral spreading. The earth materials are capable of supporting the proposed school buildings. The conclusions and recommendations contained in the following sections of this report should be included in the plans. There will be no impacts on mineral resources.

The expansion potential of the fill on the site was tested using the procedures outlined in ASTM D 4829-03. The results of the testing range from an expansion index of 18 to 42. These test results are in the very low to low range.

The data and conclusions of this exploration, testing, and report are subject to review by geotechnical engineers and engineering geologists employed by LADBS.

CONCLUSIONS AND RECOMMENDATIONS

General Findings

The conclusions and recommendations of this exploration are based upon 19 borings, 10 test pits, field geologic mapping, research of previous reports, consultation with Jeffrey M. Kalban & Associates, and over 30 years experience providing similar studies on similar sites. It is the finding of The J. Byer Group, Inc. that construction of the proposed buildings, addition, and swimming pool is feasible from a geologic and soils engineering standpoint provided the advice and recommendations contained in this report are included in the plans and are implemented during construction. The following section is a discussion of the general site conditions as they pertain to the existing and proposed buildings.

The recommended bearing material for the proposed buildings, additions, and swimming pool is the bedrock. Due to the depth of fill and alluvium underlying portions of the site it will be necessary to utilize a deepened foundation system consisting of friction piles and grade beams. Where bedrock is at the finished grade of the proposed buildings, a conventional foundation system may be utilized.

It is proposed to re-grade the access road from the entrance to the athletic field. This will require cut and fill grading along the alignment of the road. In some areas the grade will be raised seven feet. The road alignment is underlain by fill and alluvium over bedrock. The existing fill is not certified. Due to the depth of the existing fill and an existing storm drain, it is not practical to remove and recompact the existing fill. In order to place new fill over uncertified fill it will be necessary to obtain a modification from the Building Code.

Excavation Characteristics

The test pits and borings did not encounter hard, cemented bedrock. Some of the existing fill contains construction debris including concrete and asphalt. The deeper sections of the alluvium contain cemented cobbles and boulders which could impede drilling progress. The diatomaceous siltstone bedrock is moderately hard and can be excavated with conventional drilling equipment. However, cemented layers are known to occur within this bedrock formation at random locations and depths and may be encountered during foundation excavation.

SWIMMING POOL

The proposed swimming pool will be located in an area of deep fill and alluvium. The swimming pool should utilize a free-standing design and be supported on a deepened foundation system extending into the bedrock.

FOUNDATION DESIGN

General Conditions

The following foundation recommendations are minimum requirements. The structural engineer may require footings that are deeper, wider, or larger in diameter, depending on the final loads. Foundation design may change depending upon the final location of the buildings and the elevations of the finished grades.

Spread Footings

Conventional spread footings may be used to support future buildings provided they are founded in bedrock. The use of conventional spread footings will depend upon the building location and the elevations of the finished floors. Continuous footings should be a minimum of 12 inches in width. Pad footings should be a minimum of 24 inches square. The following chart contains the recommended design parameters.

Bearing Material	Minimum Embedment Depth of Footing (Inches)	Vertical Bearing (psf)	Coefficient of Friction	Passive Earth Pressure (pcf)	Maximum Earth Pressure (psf)
Bedrock	12	2,000	0.4	400	4,000

Increases in the bearing value are allowable at a rate of 20 percent for each additional foot of footing width or depth to a maximum of 4,000 pounds per square foot. For bearing calculations, the weight of the concrete in the footing may be neglected.

The bearing values shown above are for the total of dead and frequently applied live loads and may be increased by one third for short duration loading, which includes the effects of wind or seismic forces. When combining passive and friction for lateral resistance, the passive component should be reduced by one third.

All continuous footings should be reinforced with a minimum of four #4 steel bars; two placed near the top and two near the bottom of the footings. Footings should be cleaned of all loose soil, moistened, free of shrinkage cracks and approved by the geologist prior to placing forms, steel or concrete.

Deepened Foundations - Friction Piles

Drilled, cast-in-place concrete friction piles are recommended to support buildings in areas of old fill. Piles should be a minimum of 24 inches in diameter and a minimum of eight feet into bedrock. Piles may be assumed fixed at eight feet into alluvium or four feet into bedrock. The piles may be designed for a skin friction of 600 pounds per square foot for the bedrock and 300 pounds per square foot for the alluvium. Foundation piles should be tied in two horizontal directions with grade beams.

Shoring Piles

Shoring will be required for excavations along the south and west side of the proposed Main Academic Building. The excavations will be up to 20 feet high and expose fill. Cast-in-place concrete shoring piles may be utilized to support these temporary excavations. Soldier piles should be a minimum of 24 inches in diameter and a minimum of eight feet into bedrock below the base of the future excavations. Piles may be assumed fixed four feet into bedrock below the base of the excavations. The piles may be designed for a skin friction of 600 pounds per square foot for that portion of pile in contact with the bedrock. Shoring piles should be spaced a maximum of 10 feet on center. Shoring piles may be designed for an equivalent fluid pressure of 43 pounds per cubic foot per the enclosed calculation sheet #9. The fluid pressure should be multiplied by the pile spacing. Lagging between the shoring piles may be required for piles supporting existing fill. The shoring piles should be designed for the full anticipated lateral pressure. However, the pressure on the lagging will be less due to arching in the soils. Lagging should be designed for the recommended earth pressure, but may be limited to a maximum value of 400 pounds per square foot.

Lateral Design

The friction value is for the total of dead and frequently applied live loads and may be increased by one third for short duration loading, which includes the effects of wind or seismic forces. Resistance to lateral loading may be provided by passive earth pressure within the firm alluvium or bedrock.

For alluvium, passive earth pressure may be computed at 200 pounds per cubic foot. For bedrock, passive earth pressure may be computed at 400 pounds per cubic foot. The maximum allowable earth pressure is 4,000 pounds per square foot. For design of isolated piles, the allowable passive and maximum earth pressures may be increased by 100 percent. Piles spaced more than 2½ pile diameters on center may be considered isolated.

Foundation Settlement

Settlement of the foundation system is expected to occur on initial application of loading. A settlement of ¼ to ½ inch may be anticipated. Differential settlement should not exceed ¼ inch.

Toe of Slope Clearance

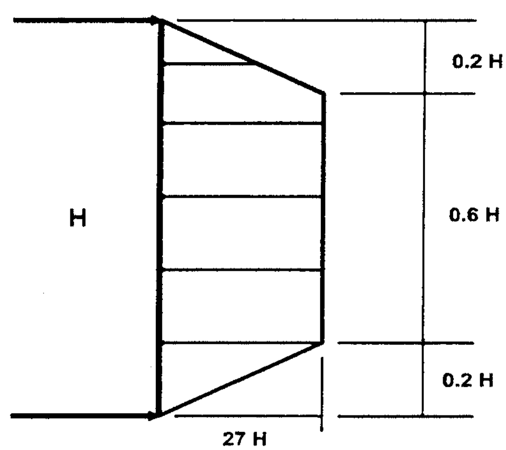
The Building Code requires a level setback between the toe of an ascending slope and the wall of the proposed structure of one half the slope height to a maximum 15 feet clearance for slopes steeper than 3:1. For swimming pools the setback is one fourth the slope height to a maximum 7.5 feet clearance for slopes steeper than 3:1. For retained slopes, the face of the retaining wall is considered the toe of the slope. Building Code setbacks will be evaluated on a building by building basis depending upon their location.

RETAINING WALLS

General Design

Basement and cantilevered retaining walls are planned for the proposed project. The basement walls will be up to 25 feet high. Cantilevered retaining walls may be up to 15 feet high. Cantilevered retaining walls with a level to 2:1 backslope should be designed for an equivalent fluid pressure of 43 pounds per cubic foot. Restrained retaining walls for basements, where deflection at the top of the wall is limited, should be designed to resist a trapezoidal distribution of pressure. The maximum earth pressure is 27H pounds per square foot, where H is the height of the retaining wall in feet. The design earth pressure assumes a subdrain and that excess hydrostatic pressures are not developed.

TRAPEZOIDAL DISTRIBUTION OF PRESSURE



Backfill

Retaining wall backfill should be compacted to a minimum of 90 percent of the maximum density as determined by ASTM D 1557-02, or equivalent. Where access between the retaining wall and the temporary excavation prevents the use of compaction equipment, retaining walls should be backfilled with ¾ inch crushed gravel to within two feet of the ground surface. Where the area between the wall and the excavation exceeds 18 inches, the gravel must be vibrated or wheel-rolled, and tested for compaction. The upper two feet of backfill above the gravel should consist of a compacted fill blanket to the surface. Retaining wall backfill should be capped with a paved surface drain.

Foundation Design

Retaining wall footings may be sized per the "Deepened Foundations" and "Spread Footings" sections of this report.

Freeboard

Retaining walls surcharged by a sloping condition should be provided with a minimum of 18 inches of freeboard for slough protection. An open "V" drain should be placed behind the wall so that all upslope flows are directed around the structure.

Temporary Excavations

Temporary excavations will be necessary to construct some of the proposed buildings. Excavations for the main Academic Building will be up to 20 feet. The existing fill can be cut vertically for a height of five feet. Slopes in excess of five feet should be trimmed to a 1:1 gradient. For excavations along the south and west sides of the main Academic Building trimming is not feasible.

These excavations may be supported by shoring designed for an equivalent fluid pressure of 43 pounds per cubic foot per the enclosed Calculation Sheet #9. For bedrock slopes, vertical excavations up to eight feet may be planned with natural soil above trimmed back to a 1:1 gradient.

FLOOR SLABS

Portions of the Library/Tech Center Building, Academic Building West, and addition to the Academic Building South will be constructed in areas of existing uncertified fill, floor slabs should be designed to bridge between the pile foundations. For portions of the building where the finished grade will be below the existing fill, the floor slab can be supported on the firm alluvium or bedrock. The upper portion of the alluvium is porous and may require removal and recompaction for slab support. The main academic building will be constructed on certified compacted fill. The floor slabs may be supported on grade, reinforced with #4 bars on 16 inch centers, each way and protected by a plastic vapor barrier.

PAVING

Paving sections utilizing flexible A/C paving should be designed per the following table. As an alternative to flexible paving, rigid concrete may be utilized. The concrete should be a minimum of four inches thick and be reinforced with #4 steel bars placed on 16 inch centers each way. The upper 24 inches of soils below the base coarse or subgrade should be removed, moistened as required to obtain optimum moisture content, and recompacted to 90 percent of the maximum dry density, as determined by ASTM D 1557-02. Trench backfill below paving, should be compacted to 90 percent of the maximum dry density. Irrigation water should be prevented from migrating under paving. The following table shows the recommended pavement sections:

Service	Pavement Thickness (Inches)	Base Course (Inches)
Passenger Cars and Light Trucks (T.I. = 4)*	3	4
Medium to Heavy Trucks (T.I. = 5)*	4	6

*T.I. - Traffic Index

Base course should be compacted to a minimum of 95 percent of maximum density

DRAINAGE

Control of site drainage is important for the performance of the proposed project. Pad and roof drainage should be collected and transferred to the street or existing storm drain system in non-erosive drainage devices. Drainage should not be allowed to pond on the pad or against any foundation or retaining wall. Drainage should not be allowed to flow uncontrolled over any descending slope. Planters located within retaining wall backfill should be sealed to prevent moisture intrusion into the backfill. Planters located next to raised floor type construction also should be sealed to the depth of the footings or grade beams. Drainage control devices require periodic cleaning, testing and maintenance to remain effective.

WATERPROOFING

Interior and exterior retaining walls are subject to moisture intrusion, seepage, and leakage and should be waterproofed. Waterproofing paints, compounds, or sheeting can be effective if properly installed. Equally important is the use of a subdrain that daylights to the atmosphere. The subdrain should be covered with ¾ inch crushed gravel to help the collection of water. Yard areas above the wall should be sealed or properly drained to prevent moisture contact with the wall or saturation of wall backfill.

Construction of raised floor buildings where the grade under the floor has been lowered for joist clearance can also lead to moisture problems. Surface moisture can seep through the footing and pond in the underfloor area. Positive drainage away from the footings, waterproofing the footings, compaction of trench backfill and subdrains can help to reduce moisture intrusion.

PLAN REVIEW

Formal plans ready for submittal to the Building Department should be reviewed by The J. Byer Group. Any change in scope of the project may require additional work.

SITE OBSERVATIONS DURING CONSTRUCTION

The Building Department requires that the geotechnical company provide site observations during construction. The observations include foundation excavations, keyways for fill, benching, pool excavations, temporary slopes and permanent cut slopes. All fill that is placed should be tested for compaction and approved by the soils engineer prior to use for support of engineered structures. LADBS requires that all retaining wall subdrains be observed by a representative of the geotechnical company and the City Inspector.

Please advise The J. Byer Group, Inc. at least 24 hours prior to any required site visit. The agency approved plans and permits should be at the job site and available to our representative. The project consultant will perform the observation and post a notice at the job site of his visit and findings. This notice should be given to the agency inspector.

CONSTRUCTION SITE MAINTENANCE

It is the responsibility of the contractor to maintain a safe construction site. When excavations exist on a site, the area should be fenced and warning signs posted. All pile excavations must be properly covered and secured. Soil generated by foundation and subgrade excavations should be either removed from the site or properly placed as a certified compacted fill. Soil must not be spilled over any descending slope. Workers should not be allowed to enter any unshored trench excavations over five feet deep.

GENERAL CONDITIONS

This report and the exploration are subject to the following NOTICE. Please read the NOTICE carefully, it limits our liability.

NOTICE

In the event of any changes in the design or location of any structure, as outlined in this report, the conclusions and recommendations contained herein may not be considered valid unless the changes are reviewed by us and the conclusions and recommendations are modified or reaffirmed after such review.

The subsurface conditions, excavation characteristics, and geologic structure described herein and shown on the enclosed cross sections have been projected from excavations on the site as indicated and should in no way be construed to reflect any variations that may occur between these excavations or that may result from changes in subsurface conditions.

Fluctuations in the level of groundwater may occur due to variations in rainfall, temperature, irrigation, and other factors not evident at the time of the measurements reported herein. Fluctuations also may occur across the site. High groundwater levels can be extremely hazardous. Saturation of earth materials can cause subsidence or slippage of the site.

If conditions encountered during construction appear to differ from those disclosed herein, notify us immediately so we may consider the need for modifications. Compliance with the design concepts, specifications, and recommendations requires geotechnical review during the course of construction.

THE EXPLORATION WAS PERFORMED ONLY ON A PORTION OF THE SITE, AND CANNOT BE CONSIDERED AS INDICATIVE OF THE PORTIONS OF THE SITE NOT EXPLORED.

This report is issued and made for the sole use and benefit of the client, is not transferable and is as of the exploration date. Any liability in connection herewith shall not exceed the fee for the exploration. No warranty, expressed or implied, is made or intended in connection with the above exploration or by the furnishing of this report or by any other oral or written statement.

THIS REPORT WAS PREPARED ON THE BASIS OF THE PRELIMINARY DEVELOPMENT PLAN FURNISHED. FINAL PLANS SHOULD BE REVIEWED BY THIS OFFICE AS ADDITIONAL GEOTECHNICAL WORK MAY BE REQUIRED.

The J. Byer Group appreciates the opportunity to provide our service on this project. Any questions concerning the data or interpretation of this report should be directed to the undersigned.

Respectfully submitted,
THE J. BYER GROUP, INC.

James E. Tucker
R. G. 6628

John W. Byer
E. G. 883

Robert I. Zweigler
E. G. 1210/G. E. 2120

REGISTERED PROFESSIONAL ENGINEER
ROBERT I. ZWEIGLER
No. 2120
Exp. 6-30-06
GEOTECHNICAL
STATE OF CALIFORNIA

JET:JWB:RIZ:flh:mh
S:\FINAL\REPORTS\19376_The_Buckley_School_Geologic_and_Geotechnical_Report.wpd

Enc: Appendix I - Laboratory Testing (2 Pages)
Shear Test Diagrams (5 Pages)
Consolidation Curves (29 Pages)
Vicinity Map
Regional Geologic Map
Seismic Hazard Zones Map
Log of Test Pits dated December 3, 2003 (4 Pages)
Log of Borings 1-19 (37 Pages)
Figure 3.3 - Seismic Hazard Zone Map - Peak Ground Acceleration
Figure 3.4 - Seismic Hazard Zone Map - Predominant Earthquake
EQFAULT Summary (2 Pages)
Section I Calculation Sheets #1 - 6 (6 Pages)
Section I-I
Slope Stability Map
Calculation Sheets #7, 8, and 9 (3 Pages)

Enc. (Continued)
Appendix II - Previous Work (94 Pages)
Sections A, B, C, D, E and F (4 Sheets)

In Pocket: Geologic Map

xc: (4) Addressee
(1) Englekirk & Sabol
(2) Project Development Group, Attention: James J. Shelton, Jr.
(5) Bruce A. Miller
(3) Jeffrey M. Kalban & Associates
(1) PCR Services Corporation, Attention: Stephanie Eyestone-Jones

APPENDIX I

LABORATORY TESTING

Undisturbed and bulk samples of the fill, soil, alluvium, and bedrock were obtained from the test pits and borings and transported to the laboratory for testing and analysis. The samples were obtained by driving a ring lined barrel sampler conforming to ASTM D 3550-01 with successive drops of the sample hammer. Experience has shown that sampling causes some disturbance of the sample, however the test results remain within a reasonable range. The samples were retained in brass rings of 2.50 inches outside diameter and 1.00 inches in height. The central portions of the samples were stored in close fitting, waterproof containers for transportation to the laboratory.

Moisture-Density

The dry density of the samples was determined using the procedures outlined in ASTM D 2937-00. The moisture content of the samples was determined using the procedures outlined in ASTM D 2216-98. The results are shown on the Log of Test Pits and Log of Borings.

Maximum Density

The maximum dry density and optimum moisture content of the future compacted fill was determined by remolding bulk samples using the procedures outlined in ASTM D 1557-00, a five-layer standard.

Boring/ Test Pit	Depth (Feet)	Soil Type	Maximum Density (pcf)	Optimum Moisture %	Expansion Index
TP2	2 - 4	Medium Brown Clayey Sand with Slate Chips	129.0	10.5	18 - Very Low
TP3	5 - 6	Gray Brown Clayey Sand with Shale Chips	108.0	19.5	42 - Low
B1	4 - 5	Dark Brown Clayey Sand	113.0	17.5	29 - Low

APPENDIX I (Continued)

Shear-Tests

Shear tests were performed on samples of existing fill, soil, alluvium, and bedrock using the procedures outlined in ASTM D 3080-98 and a strain controlled, direct shear machine manufactured by Soil Test, Inc. The rate of deformation was 0.025 inches per minute. The samples were tested in an artificially saturated condition. Following the shear test, the moisture content of the samples was determined to verify saturation. The results are plotted on the "Shear Test Diagrams."

Consolidation

Consolidation tests were performed on insitu samples of the fill and alluvium using the procedures outlined in ASTM D 2435-96. Results are graphed on the "Consolidation Curves."

SHEAR DIAGRAM #1

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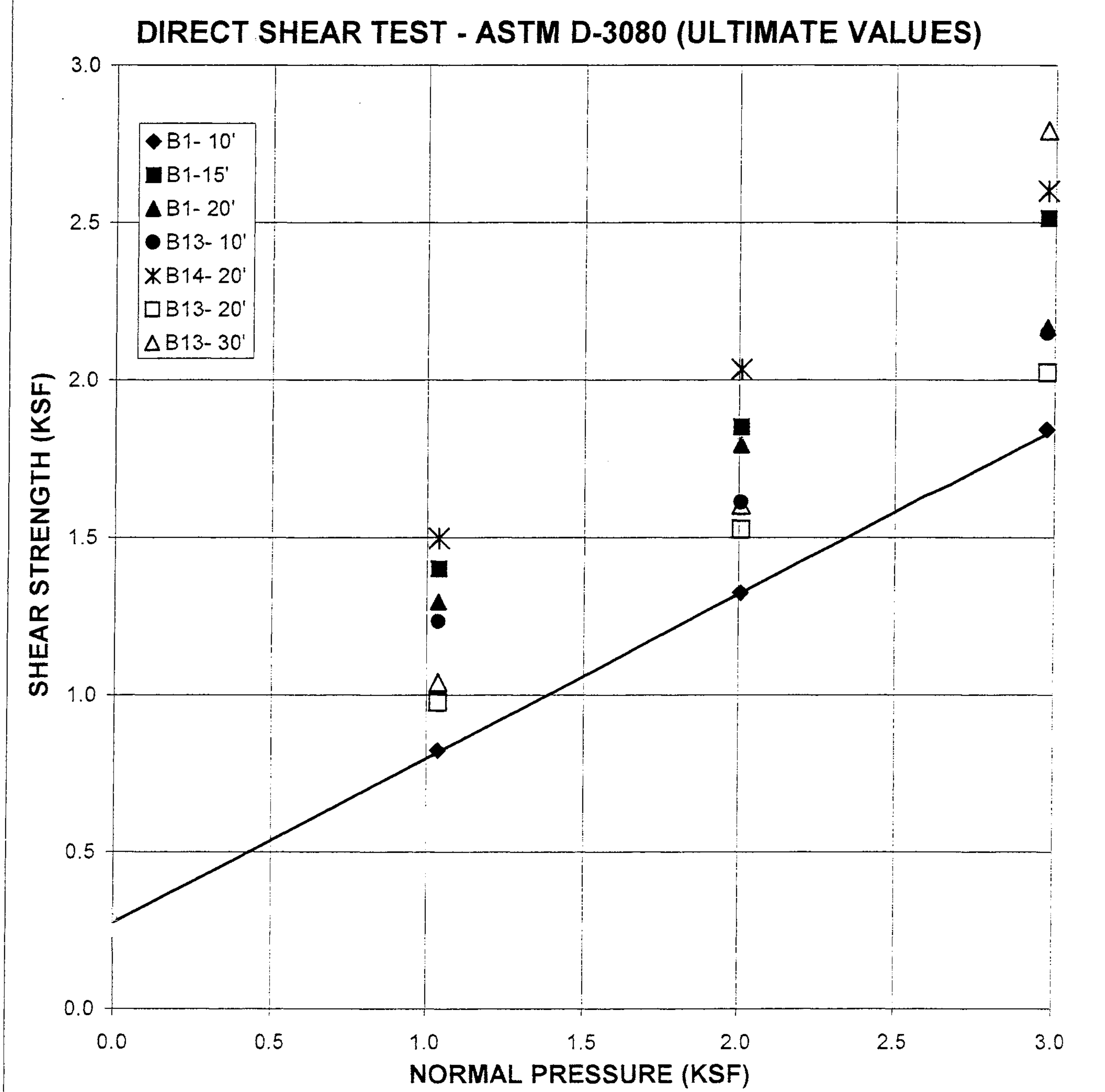
JB: 19376-B CONSULTANT JWB
CLIENT: BUCKLEY SCHOOL

EARTH MATERIAL: FILL

Phi Angle =	27.5 degrees	Average Moisture Content	25.6%
Cohesion =	255 psf	Average Dry Density (pcf)	98.0
		Percent Saturation	98.6%



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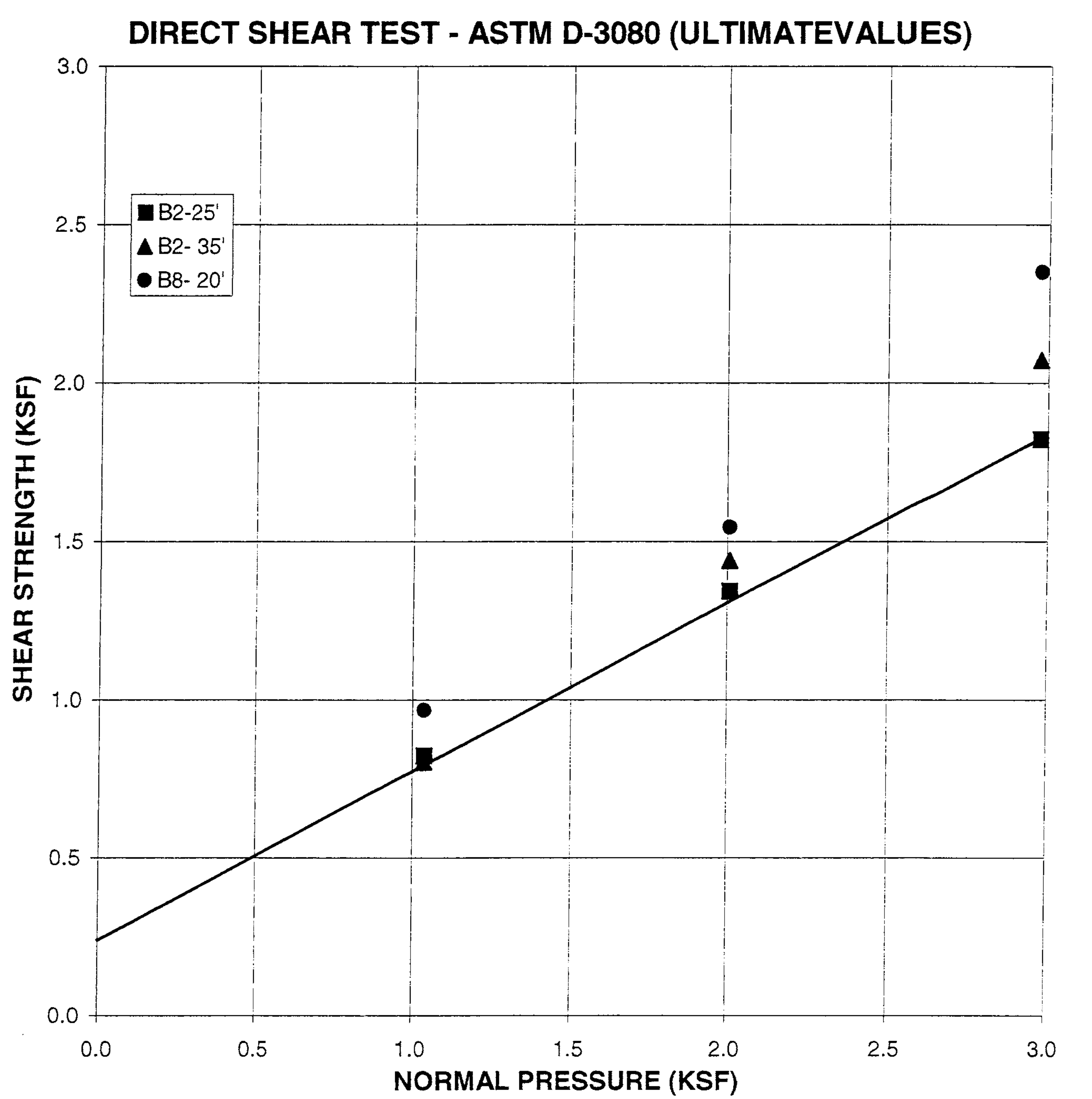
SHEAR DIAGRAM #2

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **BUCKLEY SCHOOL**

EARTH MATERIAL: **ALLUVIUM**

Phi Angle =	**28 degrees**	**Average Moisture Content**	**28.4%**
Cohesion =	**257 psf**	**Average Dry Density (pcf)**	**91.7**
		Percent Saturation	**93.8%**



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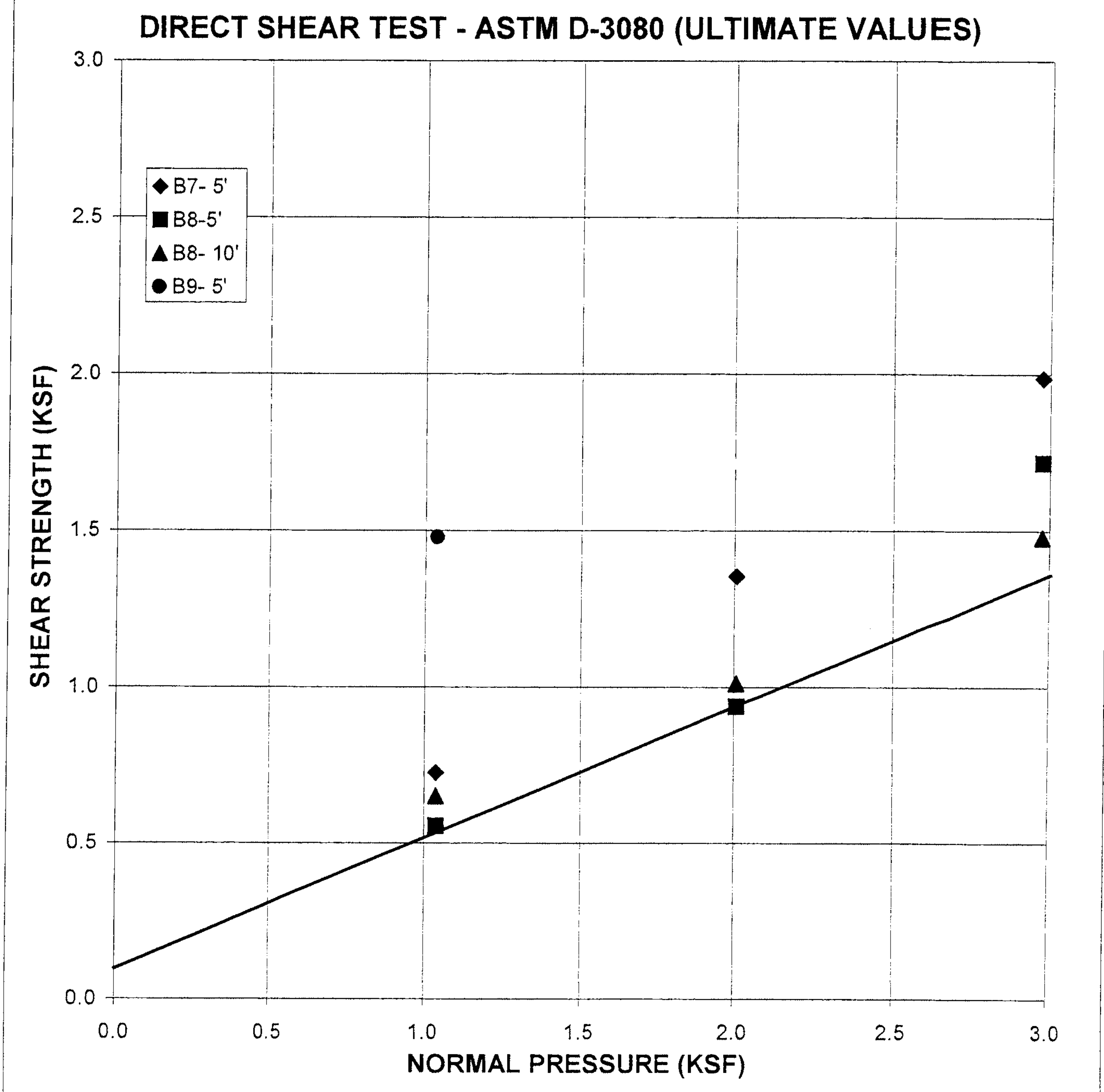
SHEAR DIAGRAM #3

JB: 19376-B CONSULTANT JWB
CLIENT: BUCKLEY SCHOOL

EARTH MATERIAL: SOIL

Phi Angle =	**22 degrees**	**Average Moisture Content**	**44.3%**
Cohesion =	**250 psf**	**Average Dry Density (pcf)**	**76.0**
		Percent Saturation	**99.7%**



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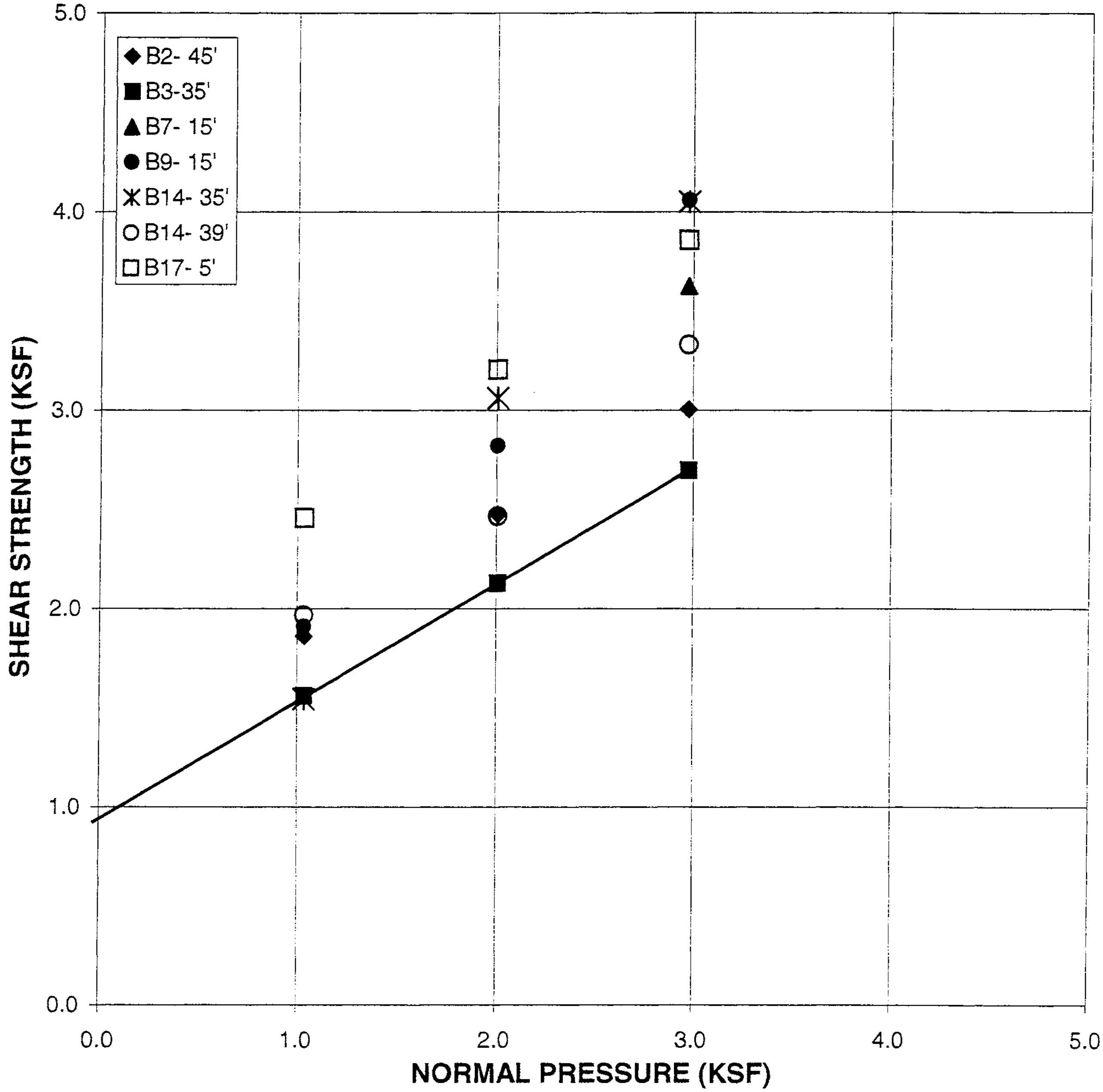
SHEAR DIAGRAM #4

JB: **19376-B** CONSULTANT **JWB**
CLIENT: **BUCKLEY SCHOOL**

EARTH MATERIAL: **BEDROCK**

Phi Angle =	**30 degrees**	**Average Moisture Content**	**50.7%**
Cohesion =	**951 psf**	**Average Dry Density (pcf)**	**70.0**
		Percent Saturation	**98.5%**

DIRECT SHEAR TEST - ASTM D-3080 (ULTIMATEVALUES)



SHEAR DIAGRAM #5

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(818) 549-9959 Tel (818) 543-3747 FAX

JB: 19376-B CONSULT: JWB
CLIENT: BUCKLEY SCHOOL

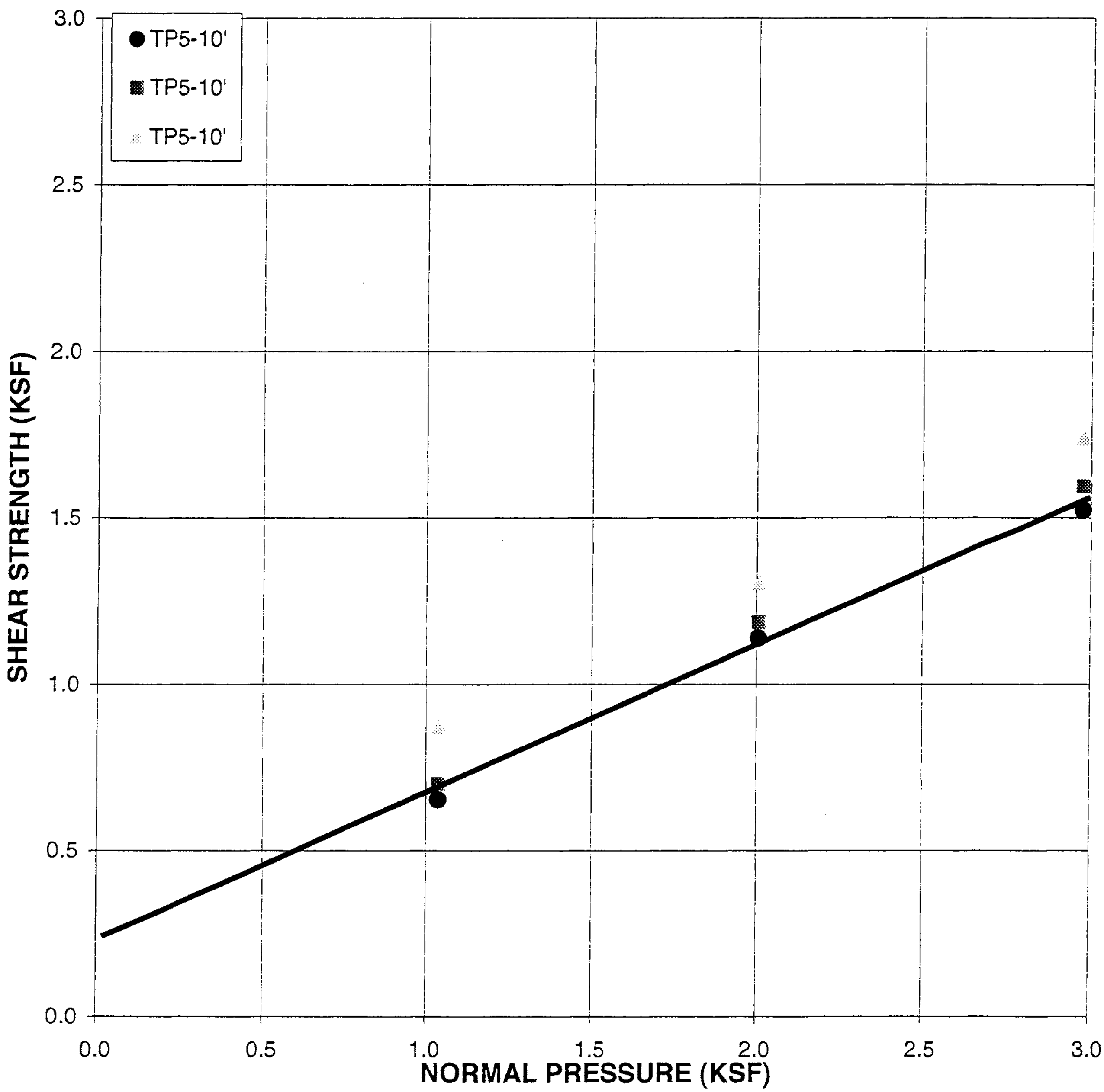
EARTH MATERIAL: BEDDING

SAMPLES REPEATEDLY SHEARED TO DETERMINE THE RESIDUAL SHEAR STRENGTH

Phi Angle = 24 degrees
Cohesion = 186 psf

Average Moisture Content	**52.1%**
Average Dry Density (pcf)	**68.3**
Percent Saturation	**95.9%**

DIRECT SHEAR TEST - ASTM D-3080 (RESIDUAL VALUES)



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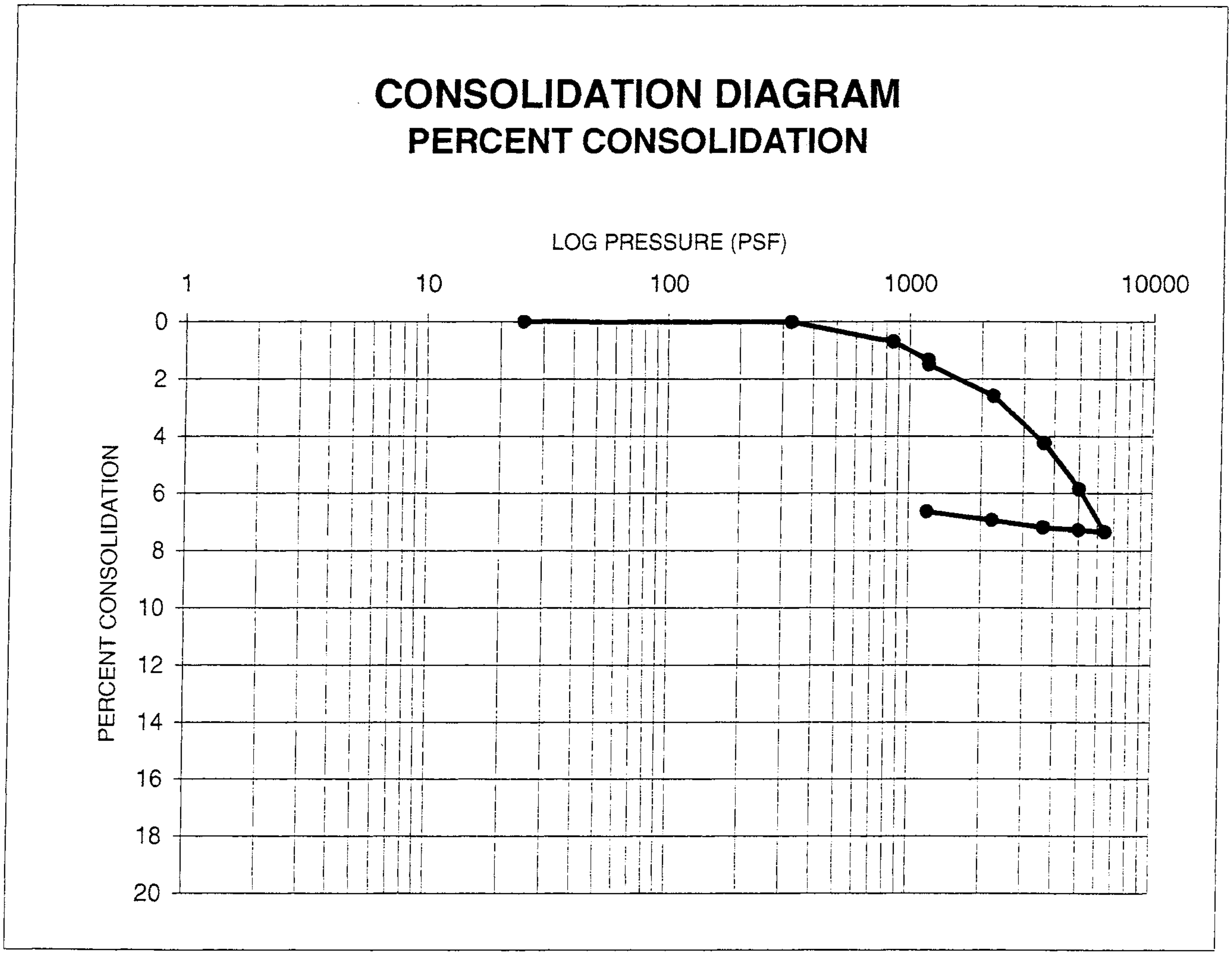
CONSOLIDATION DIAGRAM #1

JB: **19376-B** CONSULTANT: **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B1 - 25'	Specific Gravity:	2.65
Dry Weight (pcf):	89.0	Initial Void Ratio:	0.86
Initial Moisture:	21.9%	Water Added At (psf):	1206.0
Initial Saturation:	67.6%	Consolidation Coef. (Cc):	0.2050



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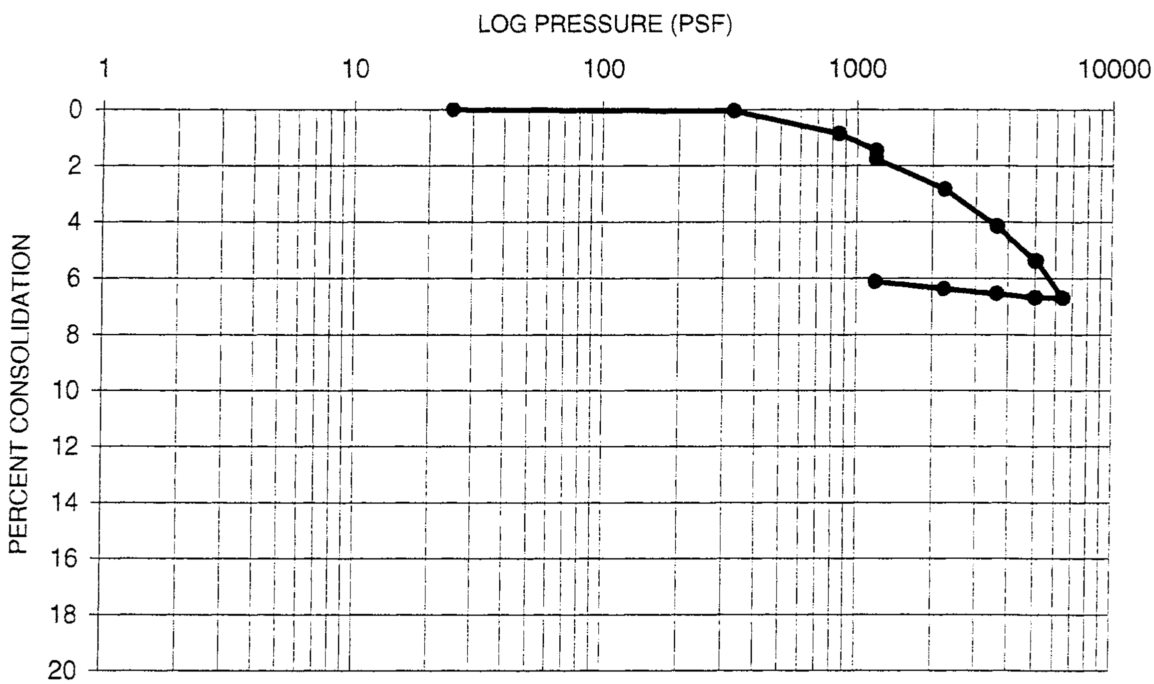
CONSOLIDATION DIAGRAM #2

JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B1-35'	Specific Gravity:	2.65
Dry Weight (pcf):	97.7	Initial Void Ratio:	0.69
Initial Moisture:	10.6%	Water Added At (psf):	1203.0
Initial Saturation:	40.6%	Consolidation Coef. (Cc):	0.1520

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



CONSOLIDATION DIAGRAM #3

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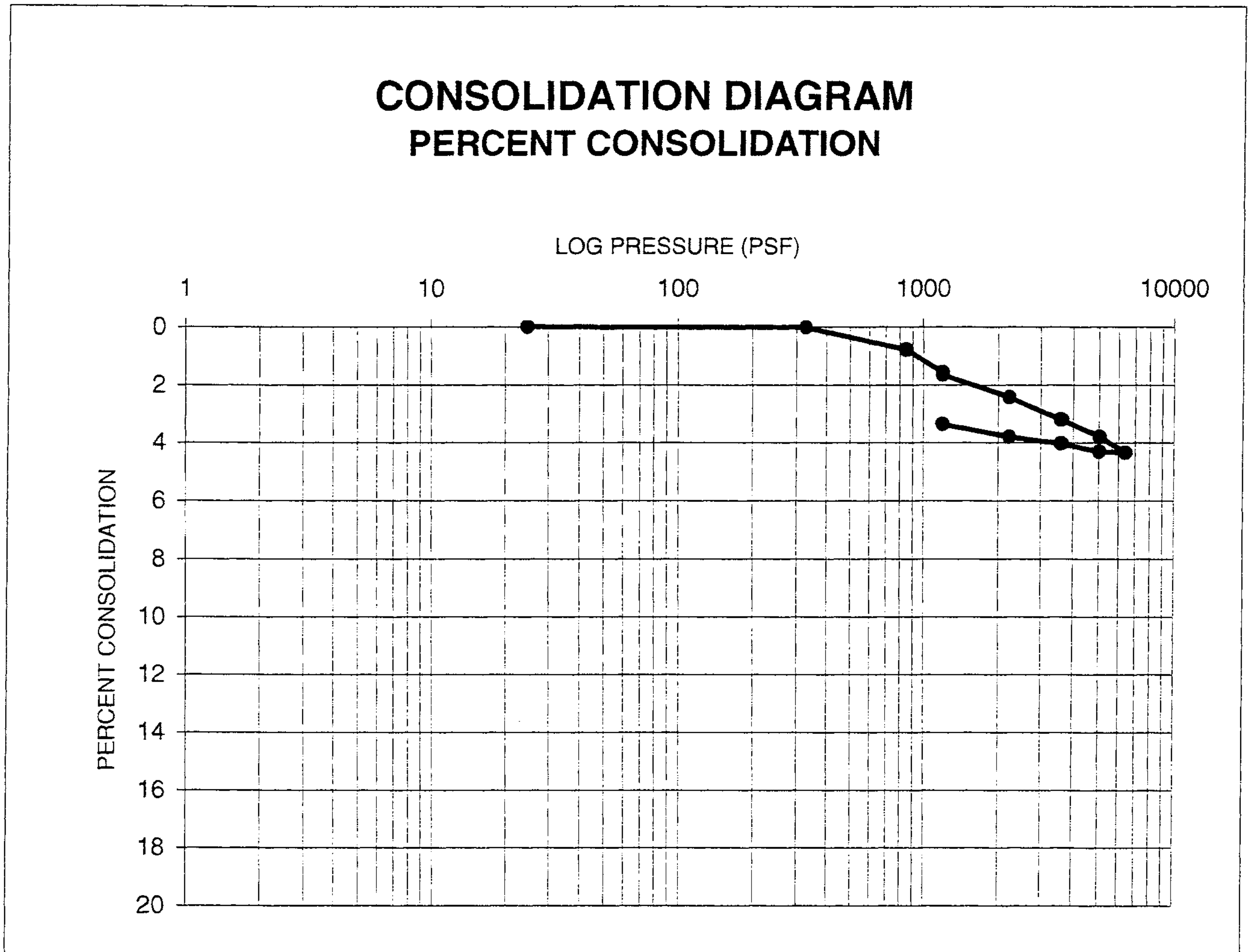
JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	ALLUVIUM		
Sample Location:	B1 - 40'	Specific Gravity:	2.65
Dry Weight (pcf):	87.1	Initial Void Ratio:	0.90
Initial Moisture:	19.9%	Water Added At (psf):	1203.0
Initial Saturation:	58.8%	Consolidation Coef. (Cc):	0.0823



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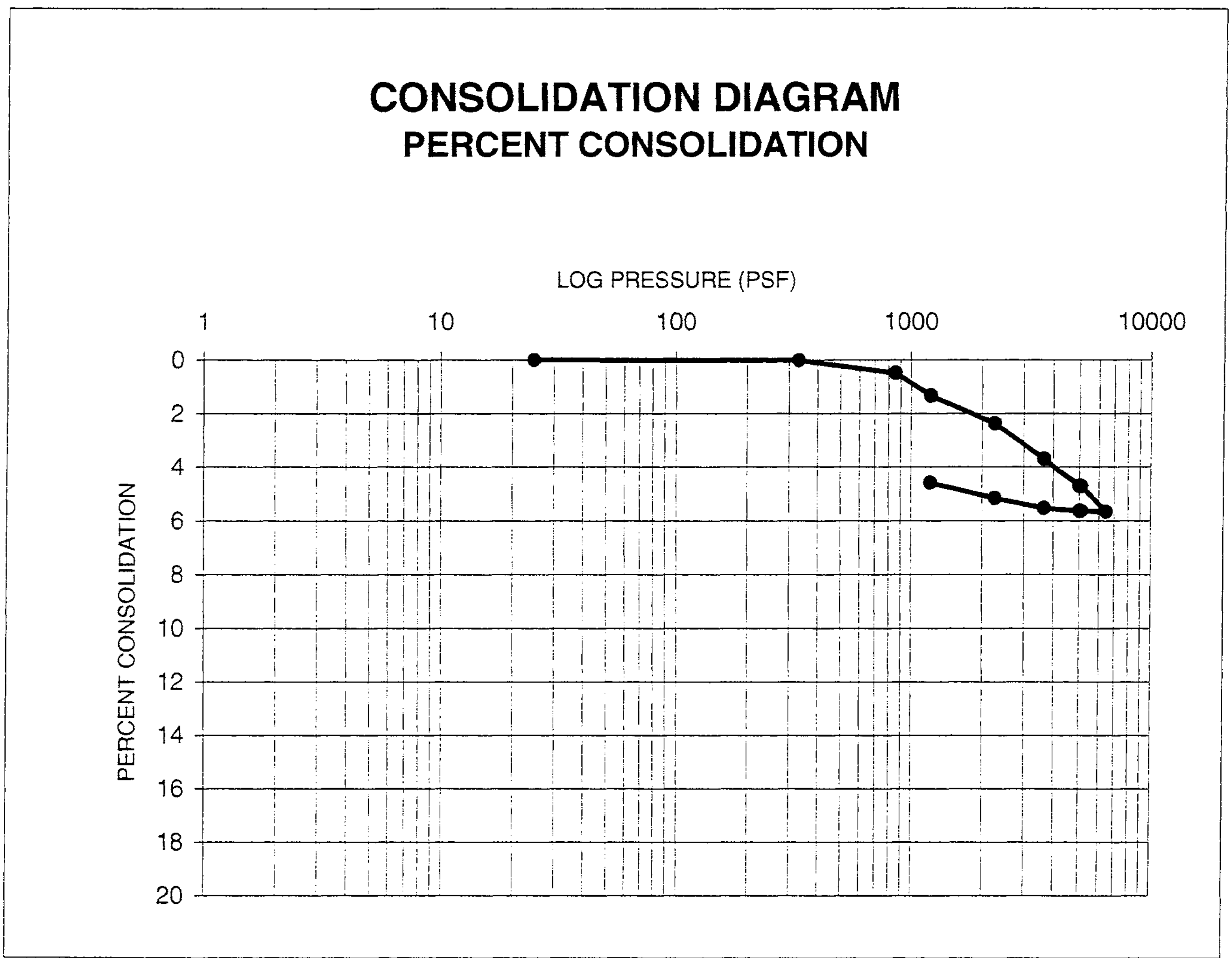
CONSOLIDATION DIAGRAM #4

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	ALLUVIUM		
Sample Location:	B1 - 45'	Specific Gravity:	2.65
Dry Weight (pcf):	84.9	Initial Void Ratio:	0.95
Initial Moisture:	33.6%	Water Added At (psf):	1216.0
Initial Saturation:	94.0%	Consolidation Coef. (Cc):	0.1447



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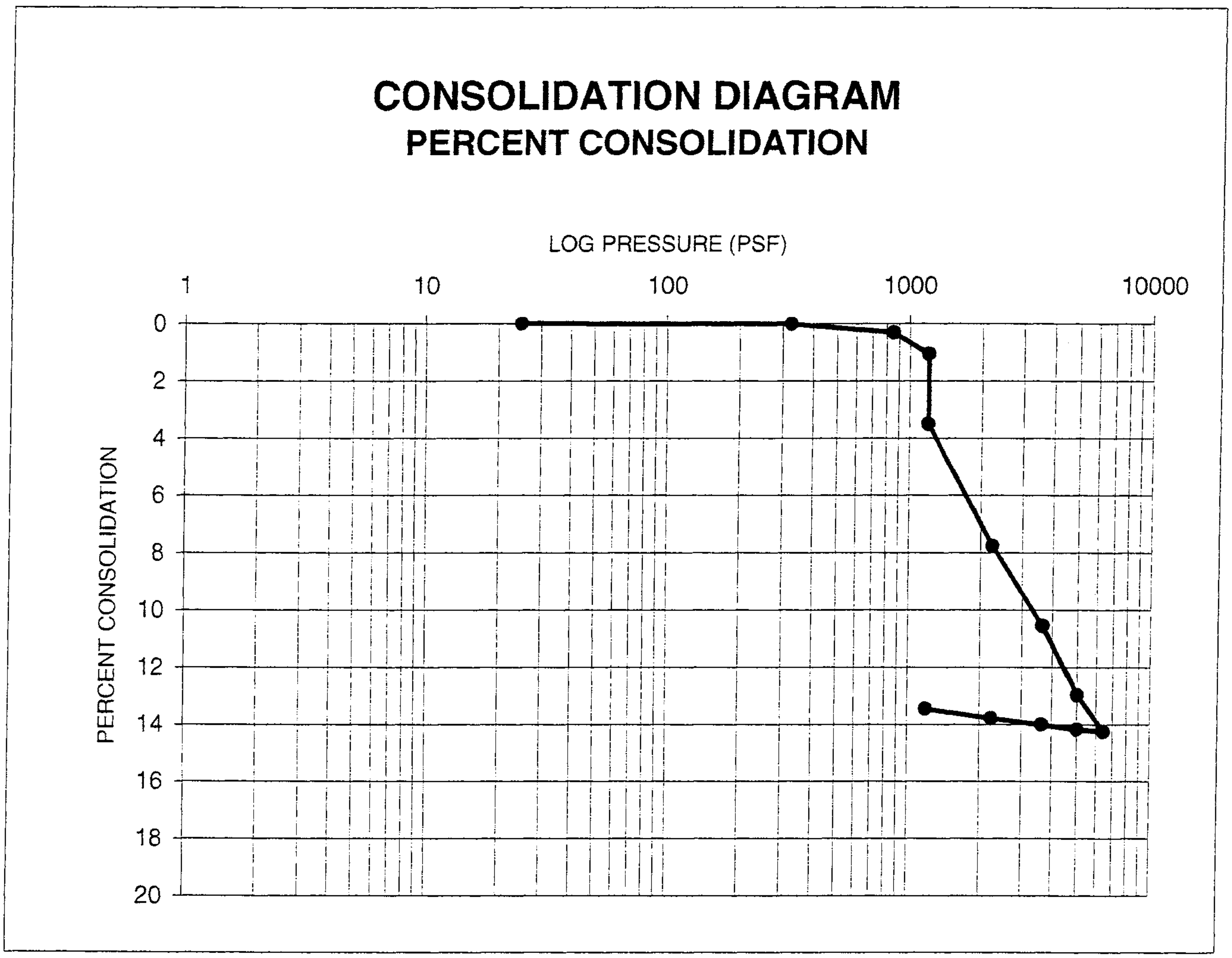
CONSOLIDATION DIAGRAM #5

JB: **19376-B** CONSULTANT: **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B2 - 20'	Specific Gravity:	2.65
Dry Weight (pcf):	82.7	Initial Void Ratio:	1.00
Initial Moisture:	23.1%	Water Added At (psf):	1206.0
Initial Saturation:	61.2%	Consolidation Coef. (Cc):	0.2901



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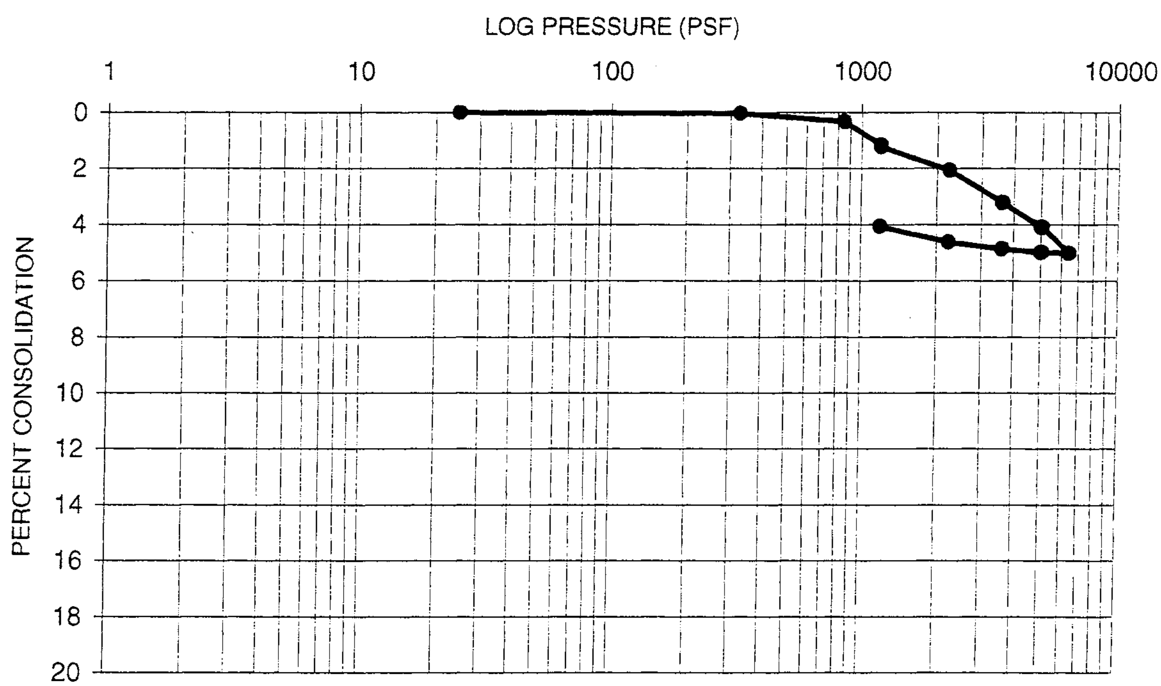
CONSOLIDATION DIAGRAM #6

JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B2-30'	Specific Gravity:	2.65
Dry Weight (pcf):	86.8	Initial Void Ratio:	0.91
Initial Moisture:	17.3%	Water Added At (psf):	1203.0
Initial Saturation:	50.6%	Consolidation Coef. (Cc):	0.1278

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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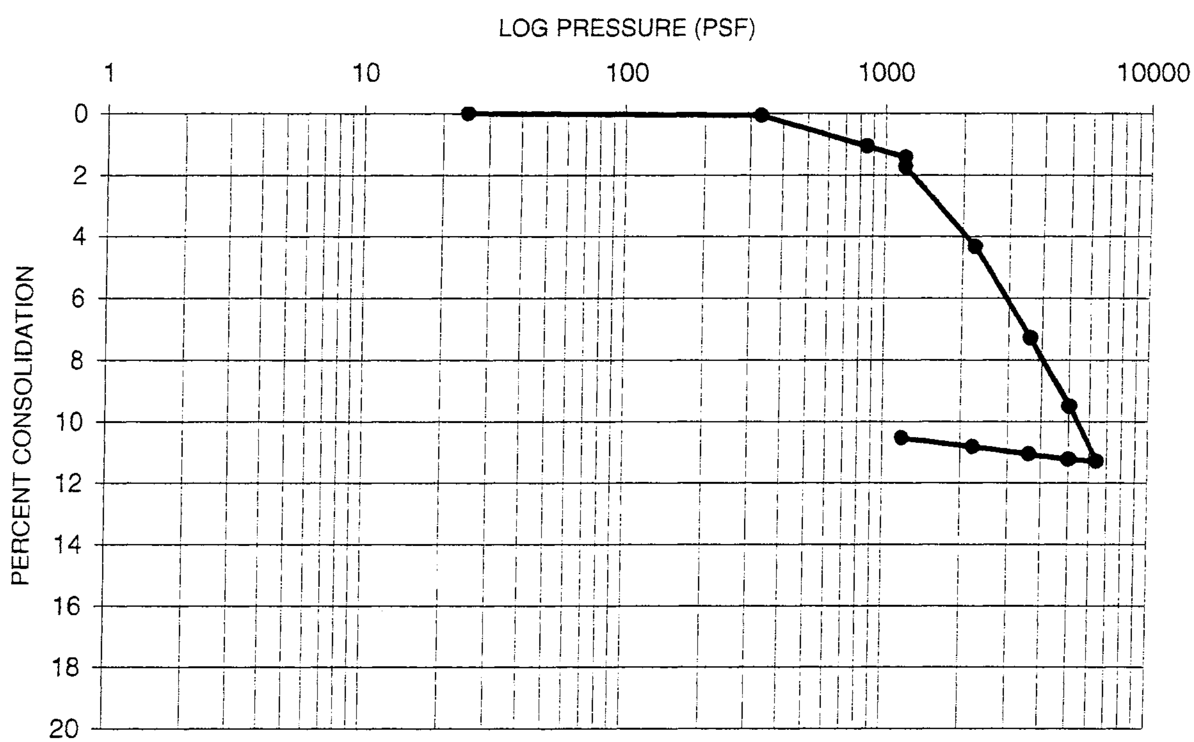
CONSOLIDATION DIAGRAM #7

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	ALLUVIUM		
Sample Location:	B4 - 15'	Specific Gravity:	2.65
Dry Weight (pcf):	84.4	Initial Void Ratio:	0.96
Initial Moisture:	24.7%	Water Added At (psf):	1203.0
Initial Saturation:	68.2%	Consolidation Coef. (Cc):	0.3048

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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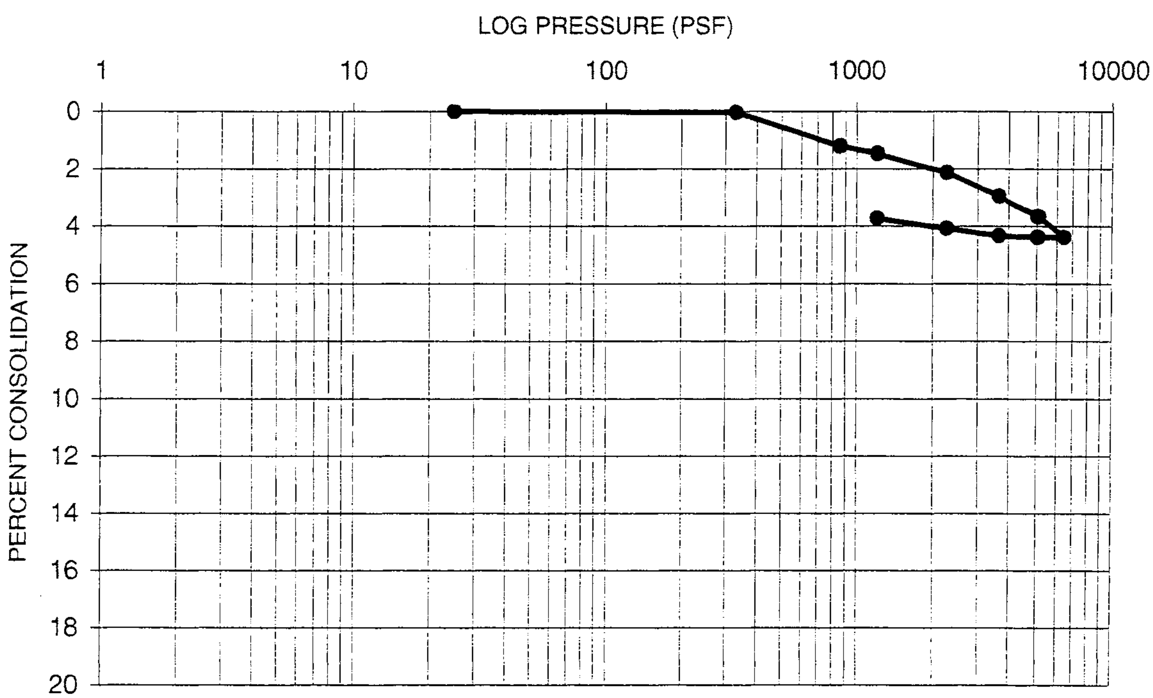
CONSOLIDATION DIAGRAM #8

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	ALLUVIUM		
Sample Location:	B6 - 20'	Specific Gravity:	2.65
Dry Weight (pcf):	91.6	Initial Void Ratio:	0.80
Initial Moisture:	26.8%	Water Added At (psf):	1216.0
Initial Saturation:	88.3%	Consolidation Coef. (Cc):	0.0940

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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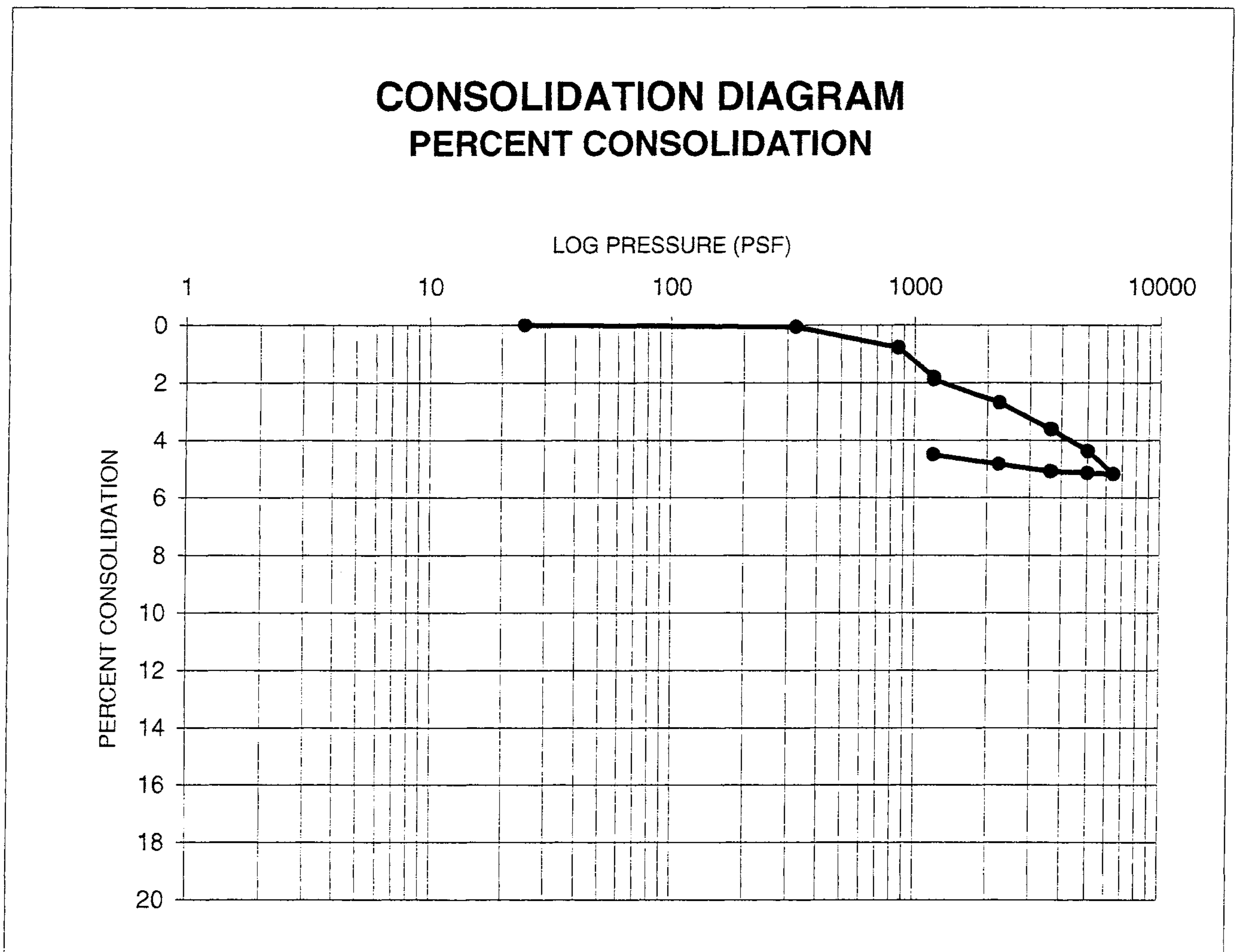
CONSOLIDATION DIAGRAM #9

JB: **19376-B** CONSULTANT: **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B6 - 25'	Specific Gravity:	2.65
Dry Weight (pcf):	92.4	Initial Void Ratio:	0.79
Initial Moisture:	26.8%	Water Added At (psf):	1206.0
Initial Saturation:	90.0%	Consolidation Coef. (Cc):	0.1021



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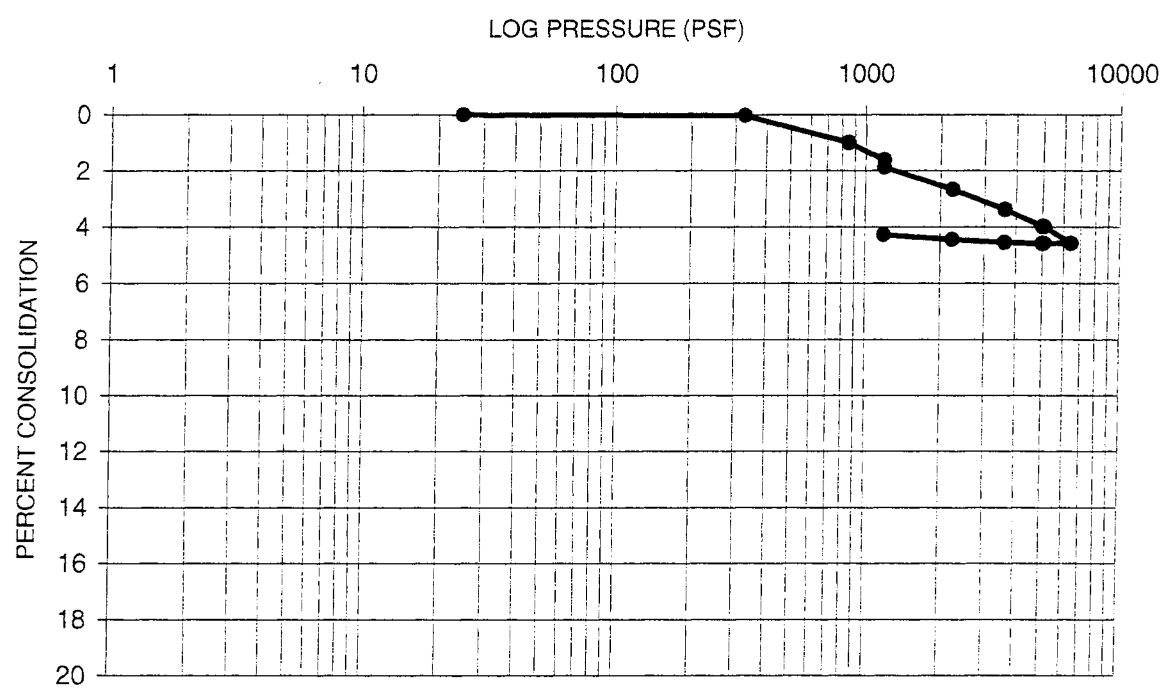
CONSOLIDATION DIAGRAM #10

JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B6-30'	Specific Gravity:	2.65
Dry Weight (pcf):	91.9	Initial Void Ratio:	0.80
Initial Moisture:	24.4%	Water Added At (psf):	1203.0
Initial Saturation:	80.8%	Consolidation Coef. (Cc):	0.0788

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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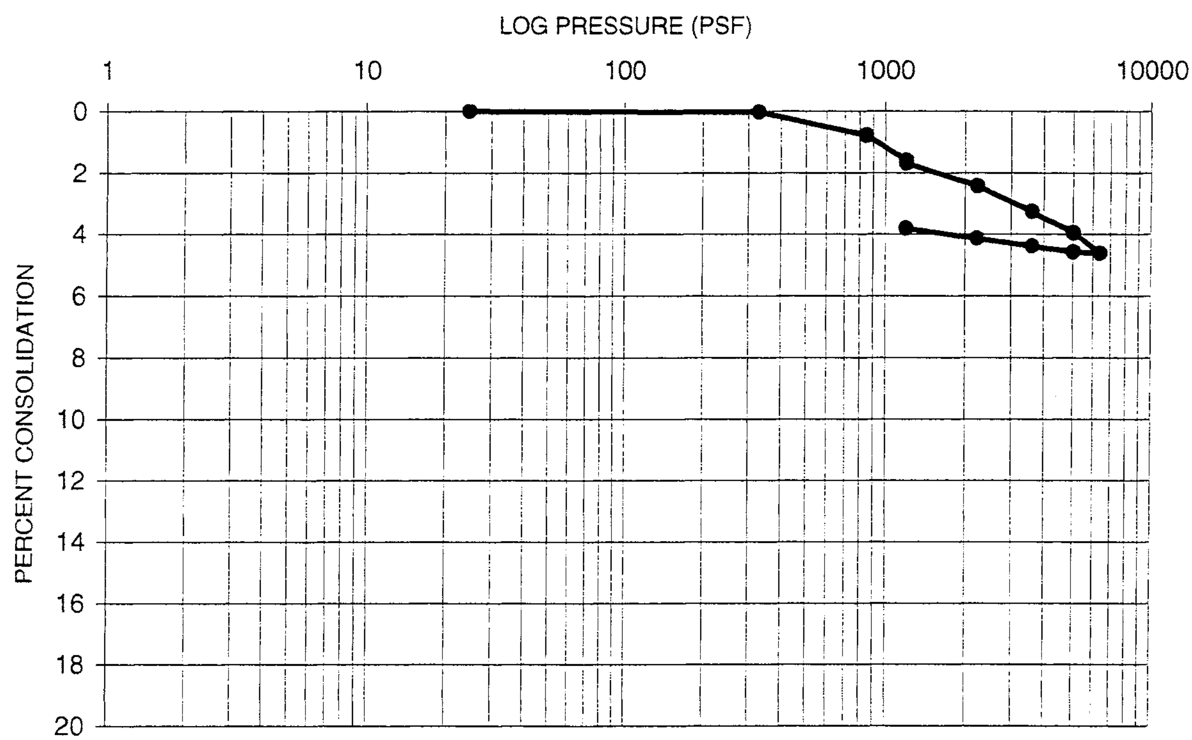
CONSOLIDATION DIAGRAM #11

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	ALLUVIUM		
Sample Location:	B6 - 35'	Specific Gravity:	2.65
Dry Weight (pcf):	96.7	Initial Void Ratio:	0.71
Initial Moisture:	24.7%	Water Added At (psf):	1203.0
Initial Saturation:	92.2%	Consolidation Coef. (Cc):	0.0859

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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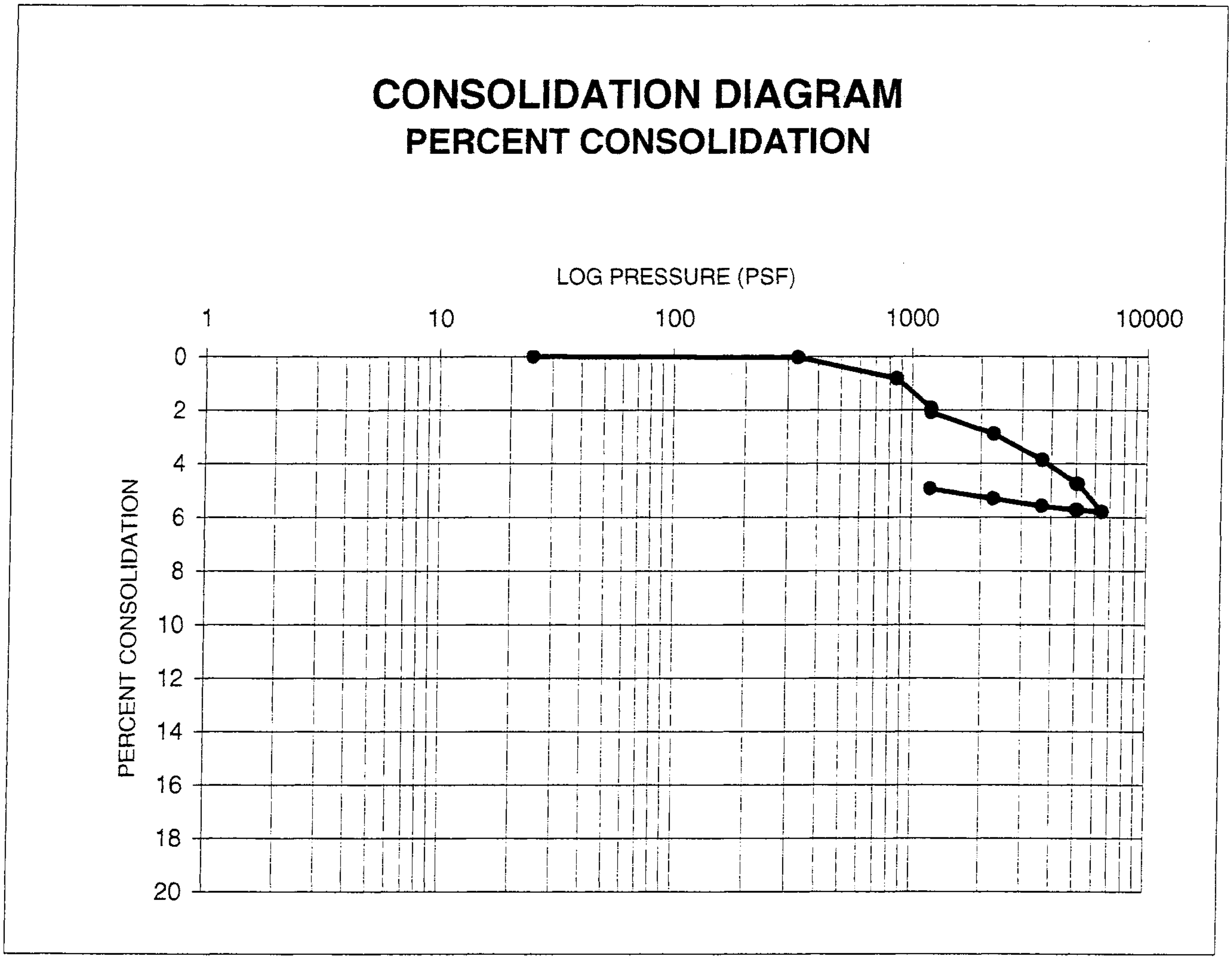
CONSOLIDATION DIAGRAM #12

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	FILL		
Sample Location:	B11 - 10'	Specific Gravity:	2.65
Dry Weight (pcf):	106.6	Initial Void Ratio:	0.55
Initial Moisture:	15.3%	Water Added At (psf):	1216.0
Initial Saturation:	73.6%	Consolidation Coef. (Cc):	0.1053



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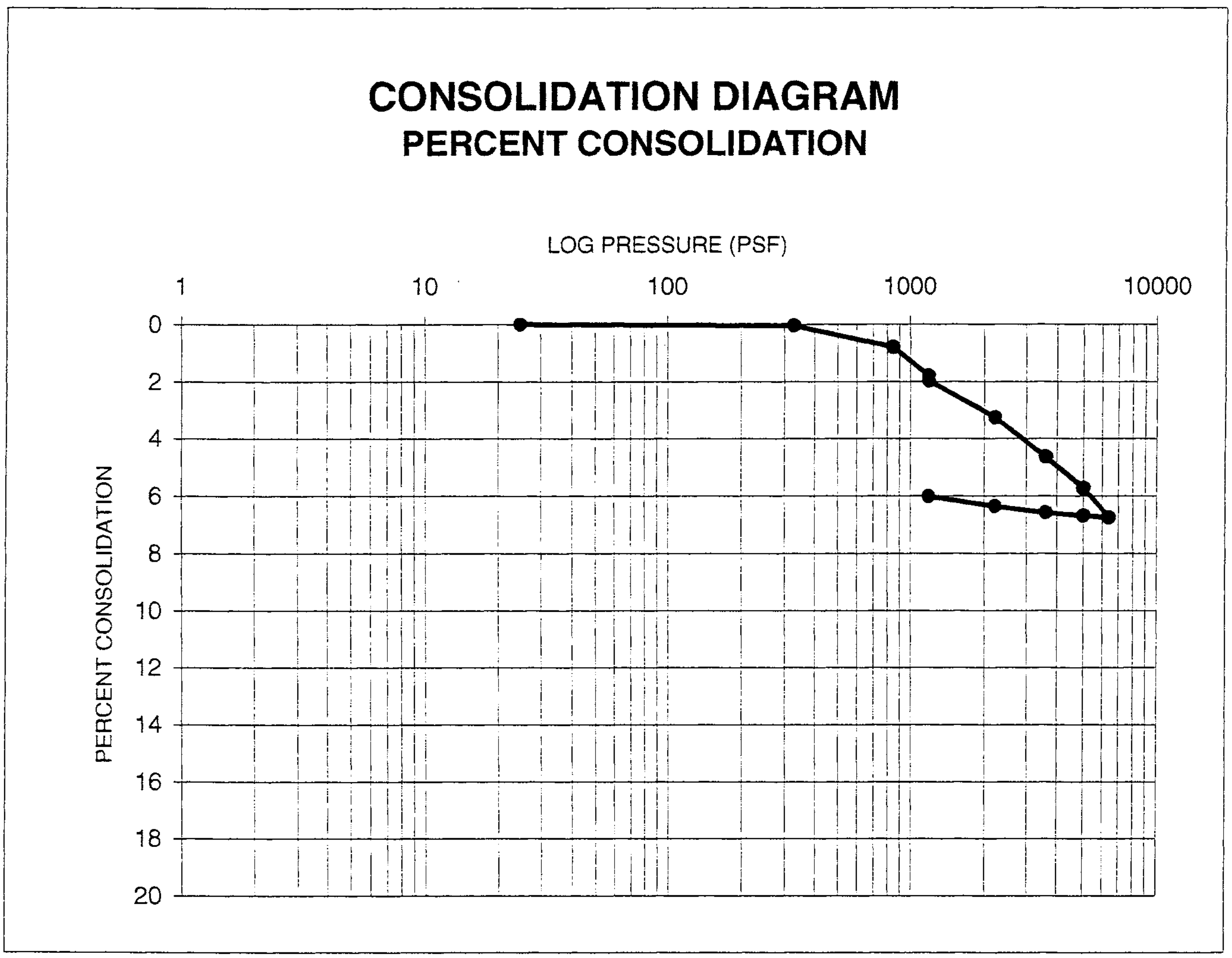
CONSOLIDATION DIAGRAM #13

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	FILL		
Sample Location:	B11 - 15'	Specific Gravity:	2.65
Dry Weight (pcf):	113.3	Initial Void Ratio:	0.46
Initial Moisture:	12.2%	Water Added At (psf):	1203.0
Initial Saturation:	70.4%	Consolidation Coef. (Cc):	0.1158



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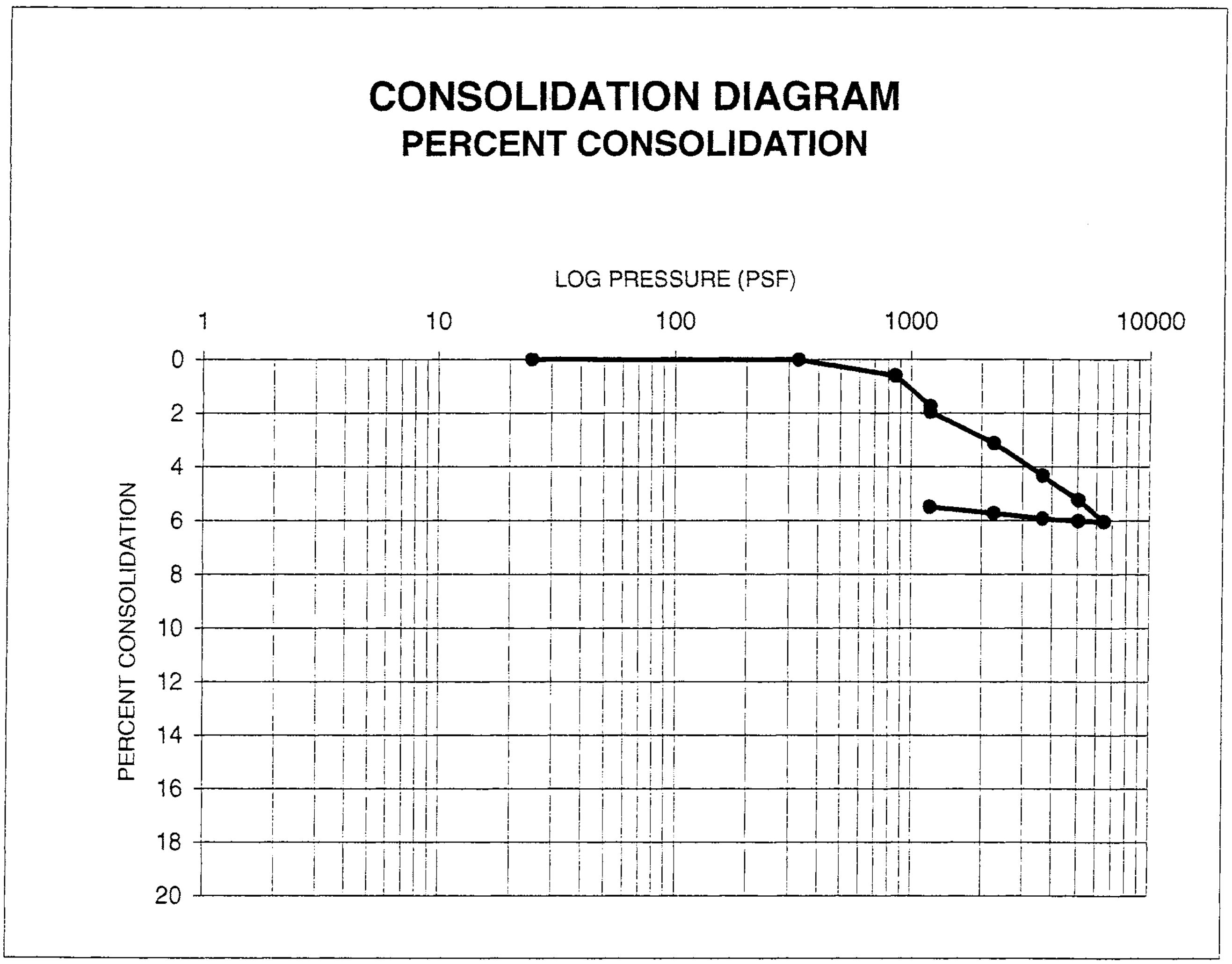
CONSOLIDATION DIAGRAM #14

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	FILL		
Sample Location:	B11 - 20'	Specific Gravity:	2.65
Dry Weight (pcf):	107.0	Initial Void Ratio:	0.55
Initial Moisture:	20.3%	Water Added At (psf):	1216.0
Initial Saturation:	98.6%	Consolidation Coef. (Cc):	0.1017



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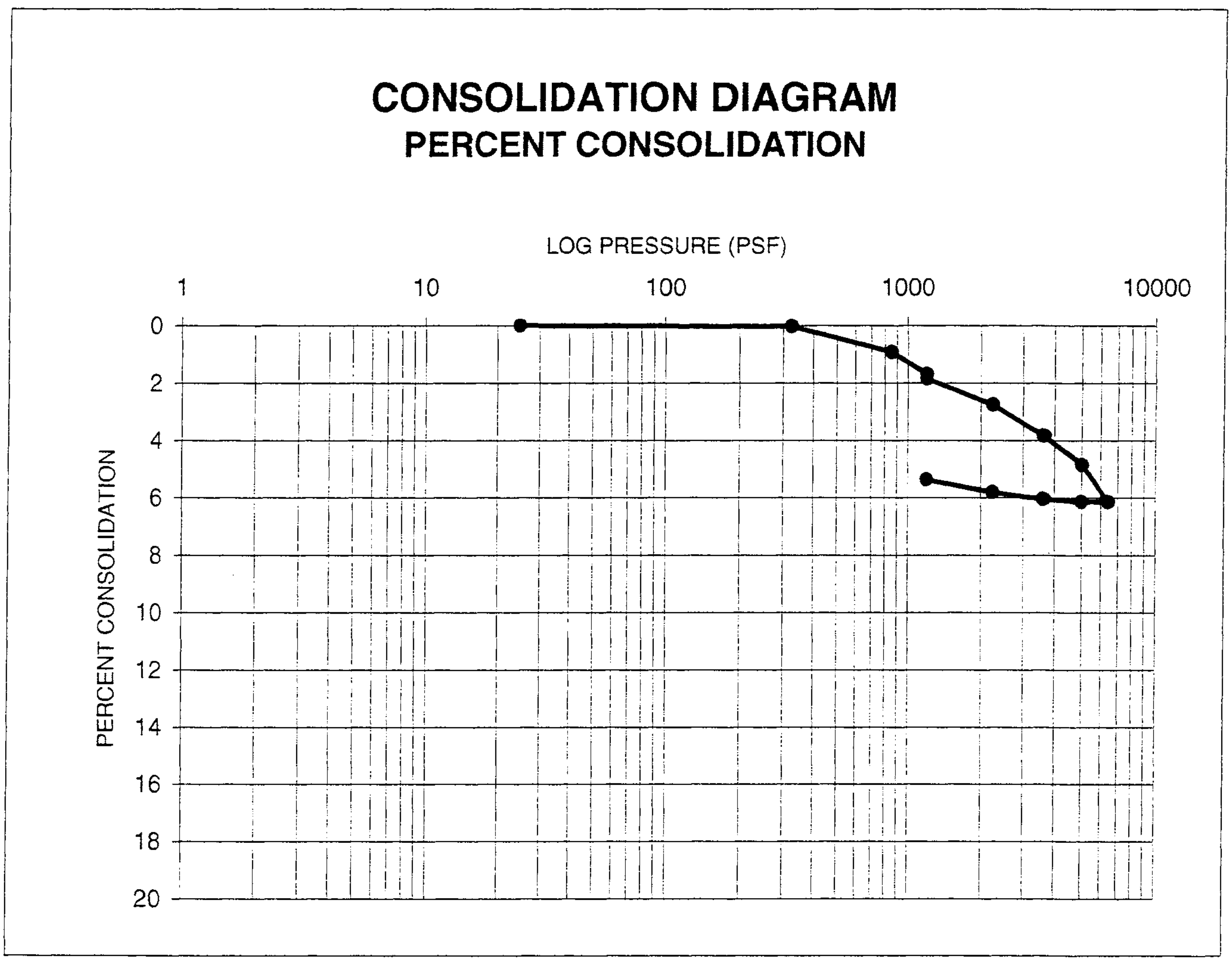
CONSOLIDATION DIAGRAM #15

JB: **19376-B** CONSULTANT: **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B11- 25'	Specific Gravity:	2.65
Dry Weight (pcf):	82.4	Initial Void Ratio:	1.01
Initial Moisture:	28.4%	Water Added At (psf):	1206.0
Initial Saturation:	74.8%	Consolidation Coef. (Cc):	0.1594



CONSOLIDATION DIAGRAM #16

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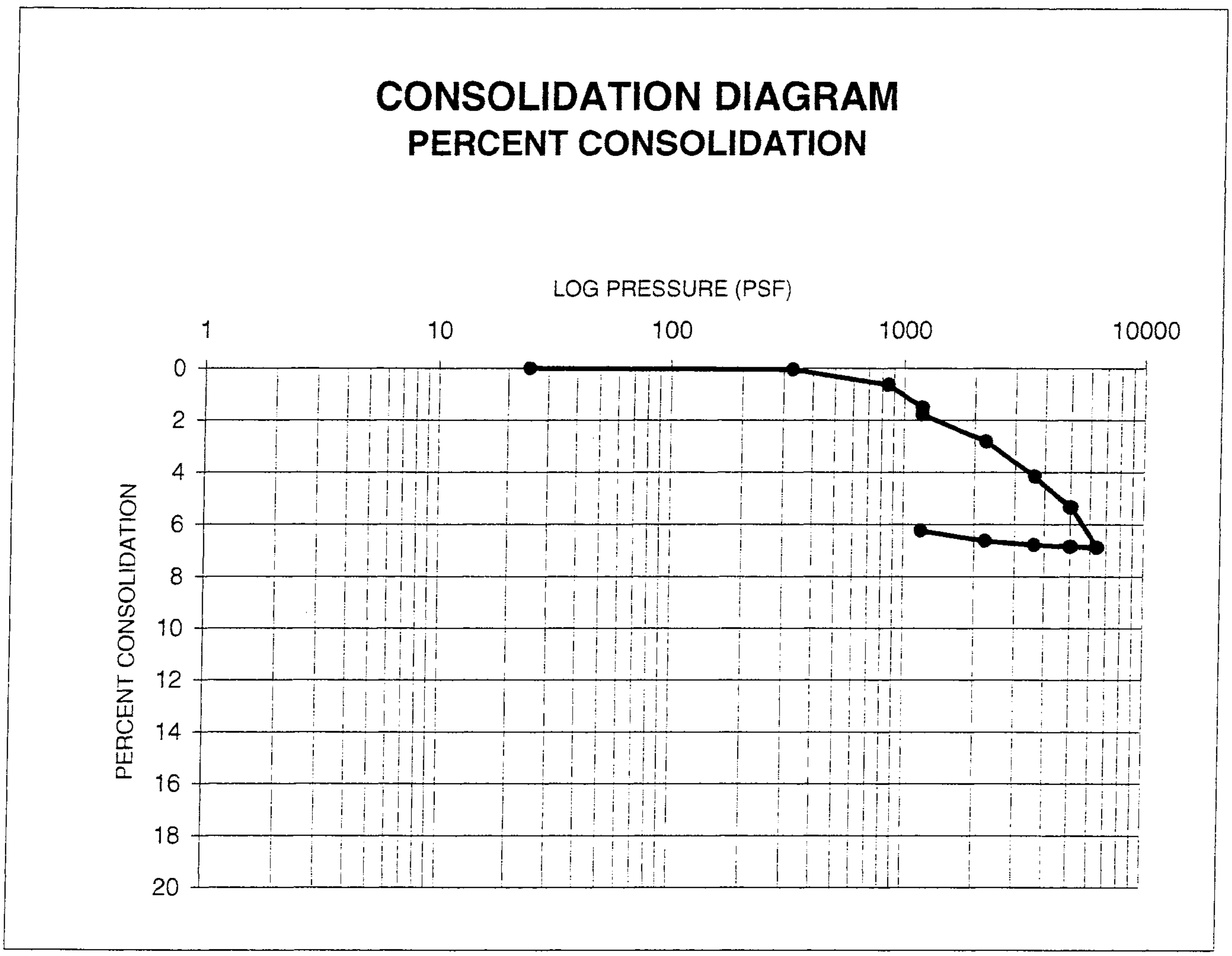
JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B11-30'	Specific Gravity:	2.65
Dry Weight (pcf):	83.4	Initial Void Ratio:	0.98
Initial Moisture:	30.1%	Water Added At (psf):	1203.0
Initial Saturation:	81.1%	Consolidation Coef. (Cc):	0.1894



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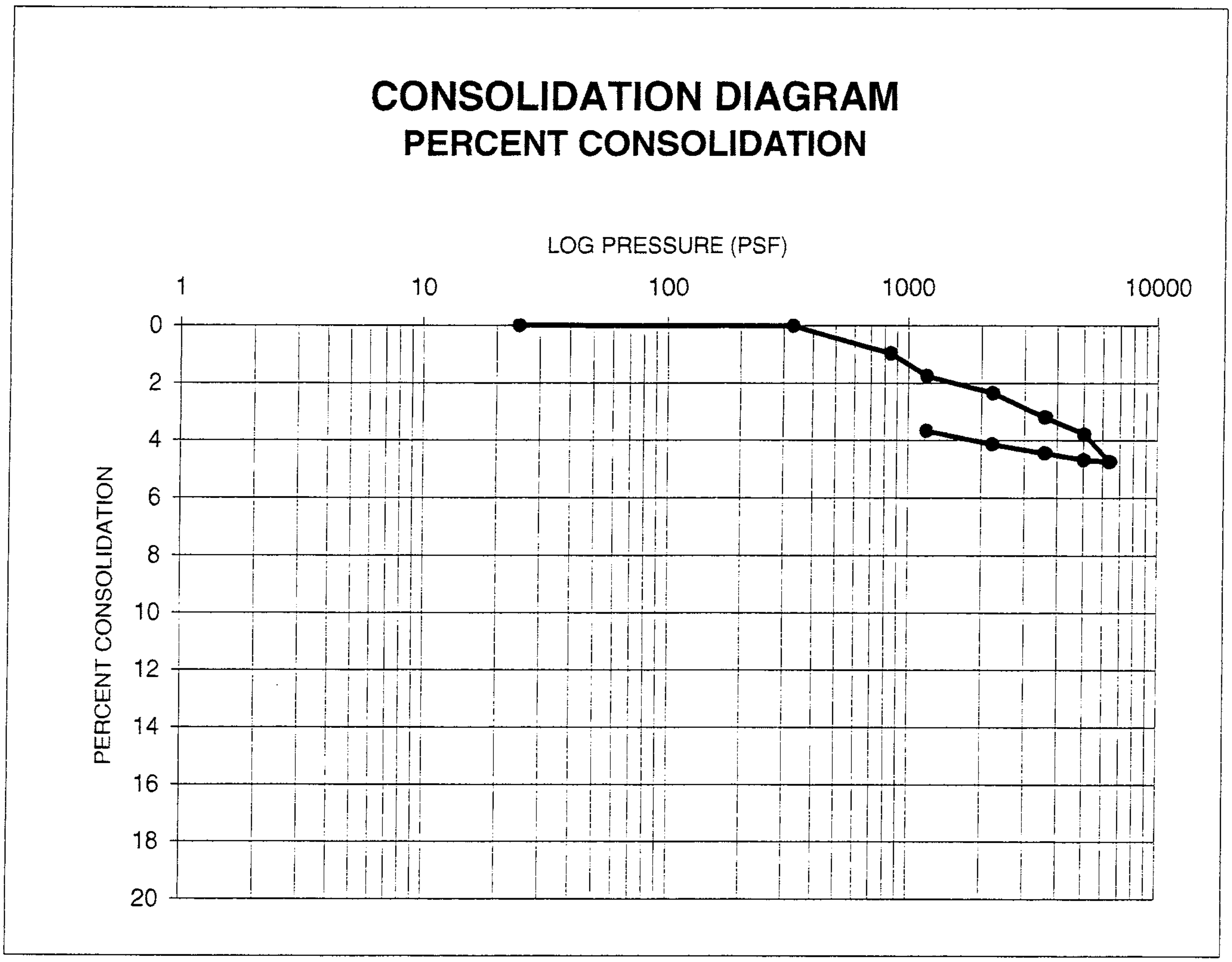
CONSOLIDATION DIAGRAM #17

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B11 - 35'	Specific Gravity:	2.65
Dry Weight (pcf):	86.9	Initial Void Ratio:	0.90
Initial Moisture:	28.9%	Water Added At (psf):	1203.0
Initial Saturation:	84.7%	Consolidation Coef. (Cc):	0.1050



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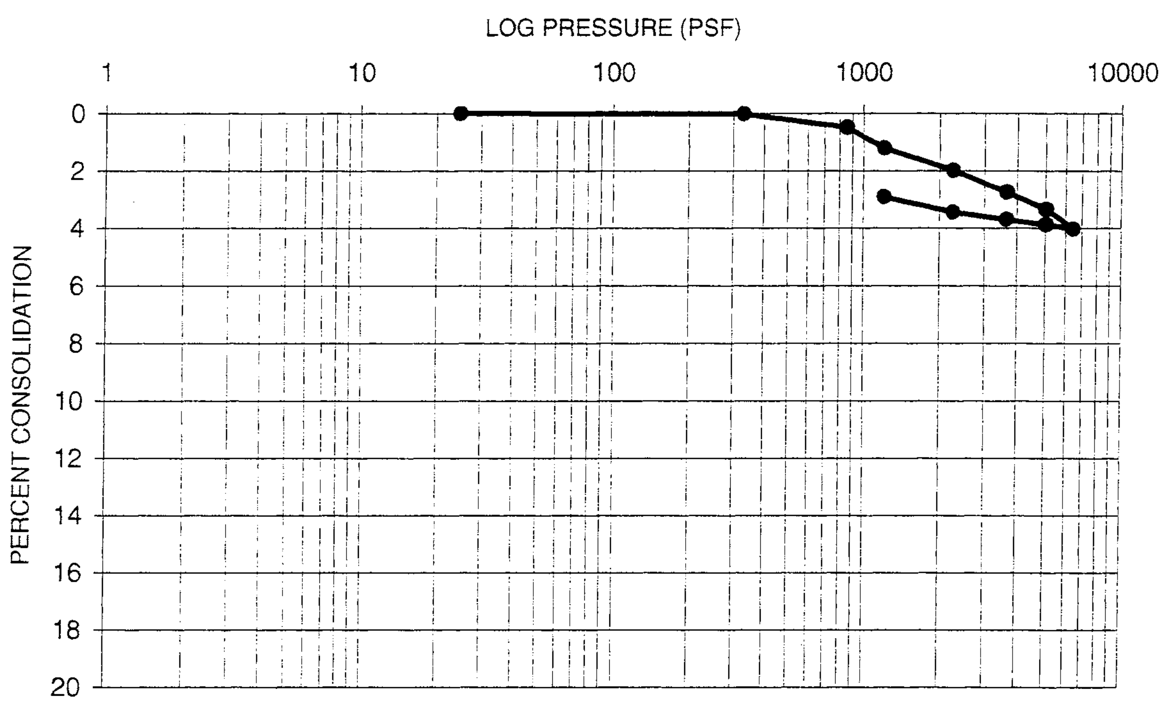
CONSOLIDATION DIAGRAM #18

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B12 - 20'	Specific Gravity:	2.65
Dry Weight (pcf):	74.3	Initial Void Ratio:	1.22
Initial Moisture:	35.3%	Water Added At (psf):	1216.0
Initial Saturation:	76.4%	Consolidation Coef. (Cc):	0.1045

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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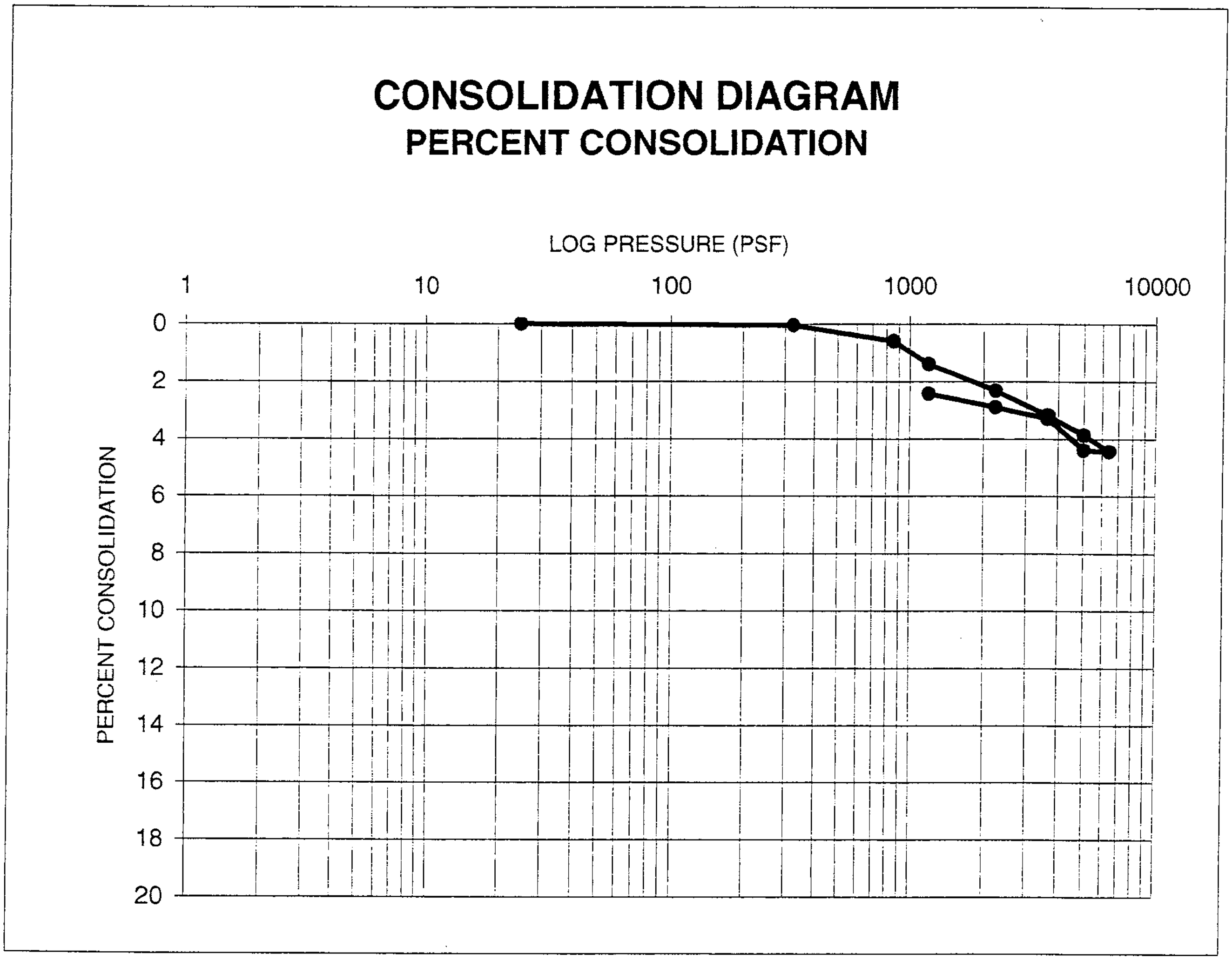
CONSOLIDATION DIAGRAM #19

JB: **19376-B** CONSULTANT: **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B12- 25'	Specific Gravity:	2.65
Dry Weight (pcf):	73.3	Initial Void Ratio:	1.26
Initial Moisture:	44.8%	Water Added At (psf):	1206.0
Initial Saturation:	94.4%	Consolidation Coef. (Cc):	0.1090



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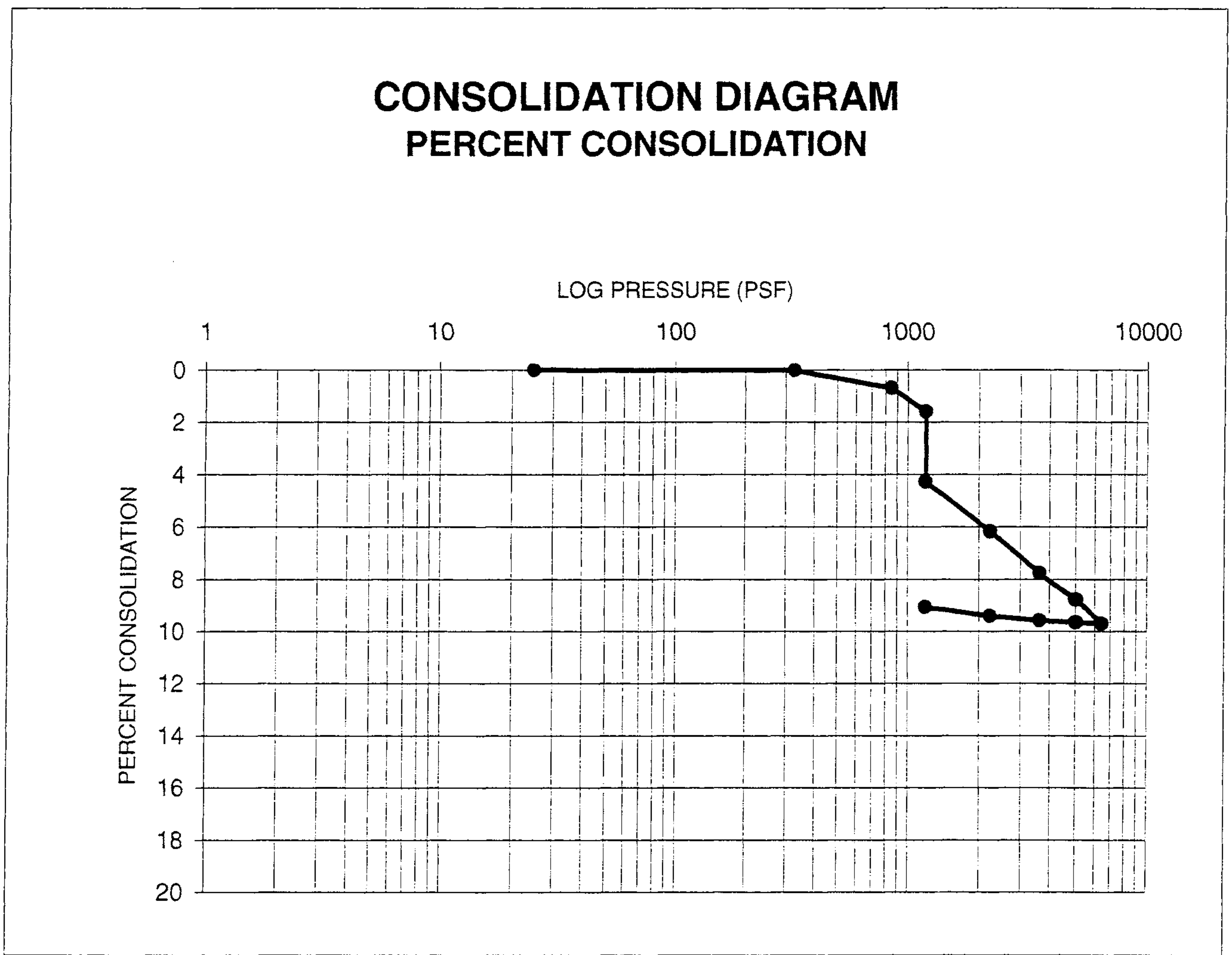
CONSOLIDATION DIAGRAM #20

JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B8-15'	Specific Gravity:	2.65
Dry Weight (pcf):	100.9	Initial Void Ratio:	0.64
Initial Moisture:	10.0%	Water Added At (psf):	1203.0
Initial Saturation:	41.5%	Consolidation Coef. (Cc):	0.1272



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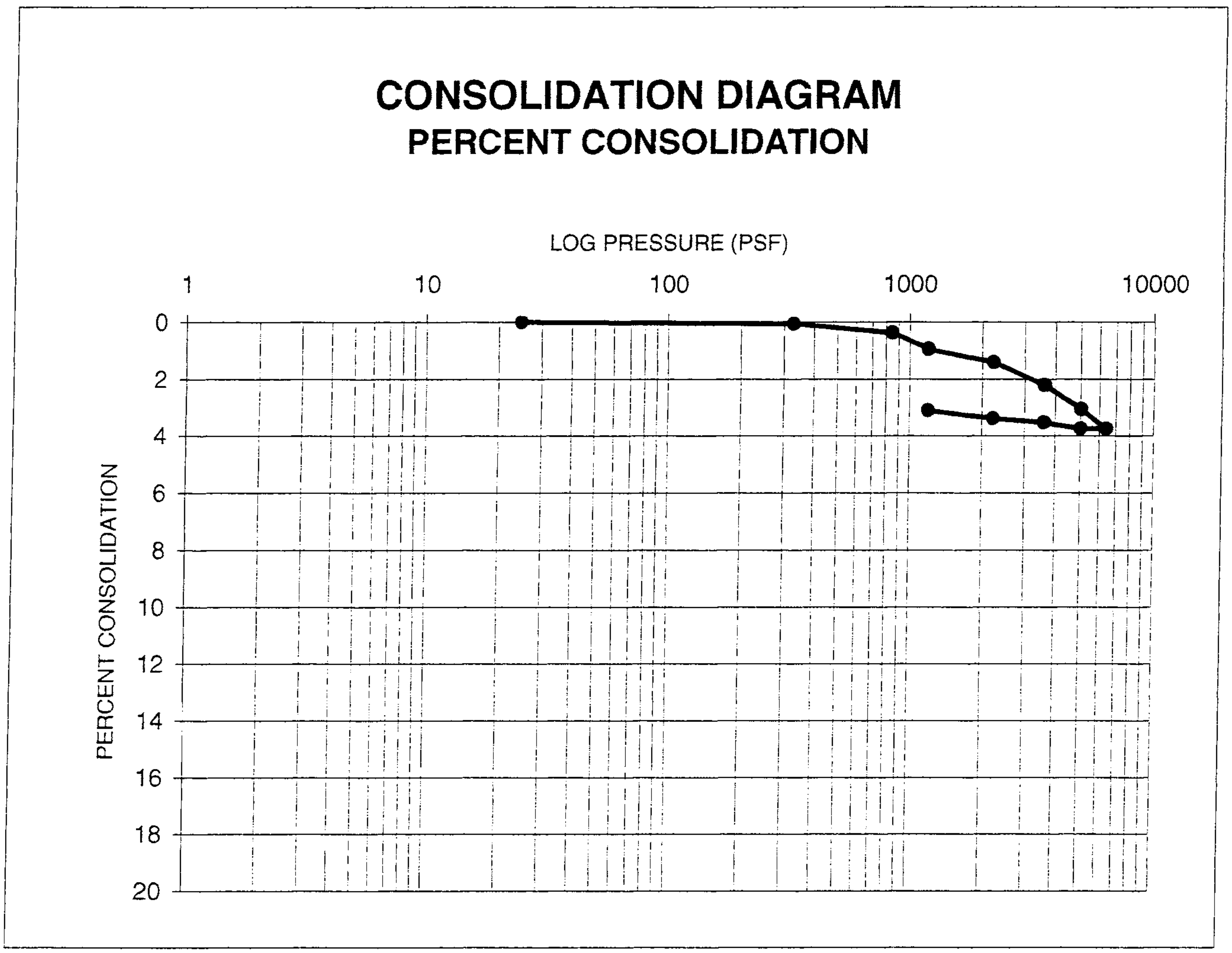
CONSOLIDATION DIAGRAM #21

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B13 - 45'	Specific Gravity:	2.65
Dry Weight (pcf):	67.7	Initial Void Ratio:	1.44
Initial Moisture:	62.6%	Water Added At (psf):	1203.0
Initial Saturation:	114.9%	Consolidation Coef. (Cc):	0.1335



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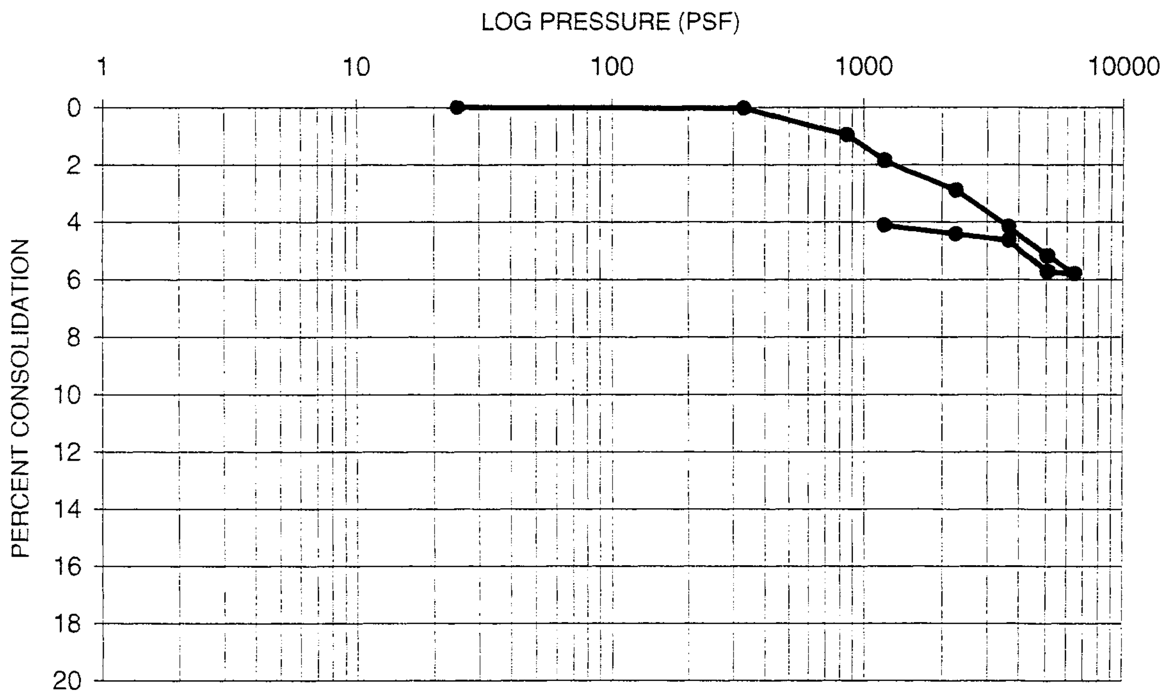
CONSOLIDATION DIAGRAM #22

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Alluvium		
Sample Location:	B13 - 55'	Specific Gravity:	2.65
Dry Weight (pcf):	76.0	Initial Void Ratio:	1.18
Initial Moisture:	43.1%	Water Added At (psf):	1216.0
Initial Saturation:	97.1%	Consolidation Coef. (Cc):	0.1411

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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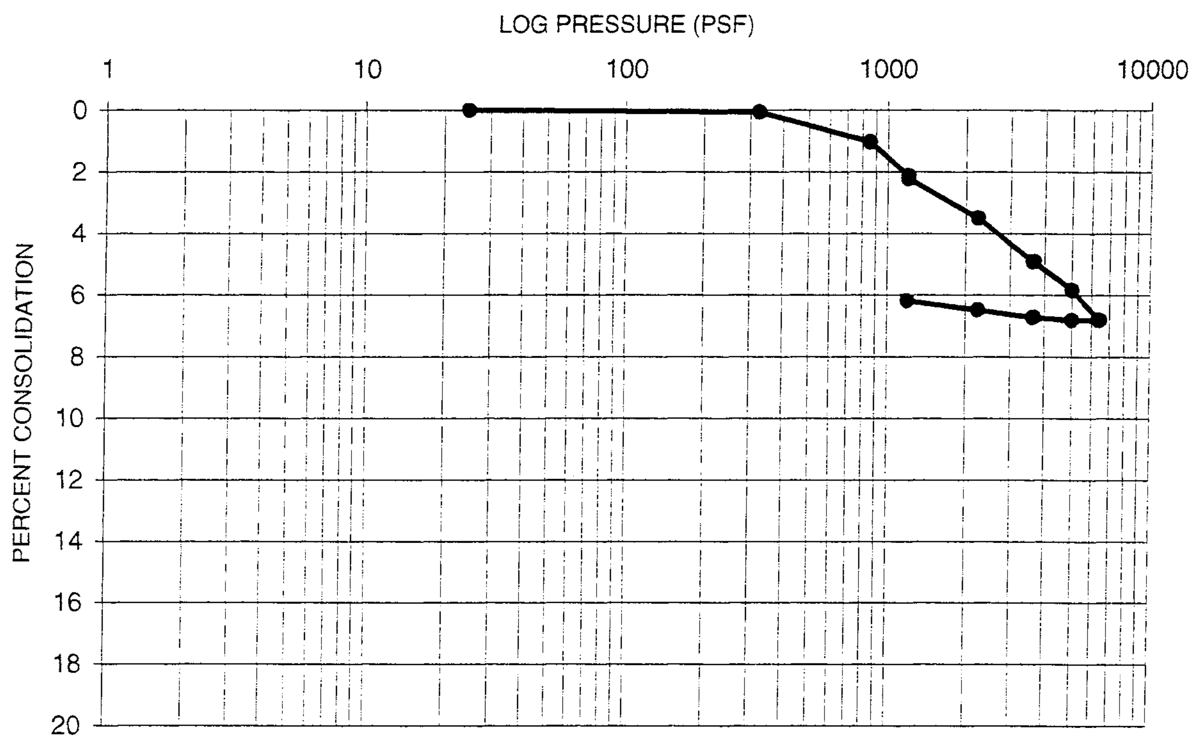
CONSOLIDATION DIAGRAM #23

JB: **19376-B** CONSULTANT: **JWB**

CLIENT: **Buckley School**

Earth Material:	Fill		
Sample Location:	B14 - 10'	Specific Gravity:	2.65
Dry Weight (pcf):	105.1	Initial Void Ratio:	0.57
Initial Moisture:	23.5%	Water Added At (psf):	1206.0
Initial Saturation:	108.6%	Consolidation Coef. (Cc):	0.1155

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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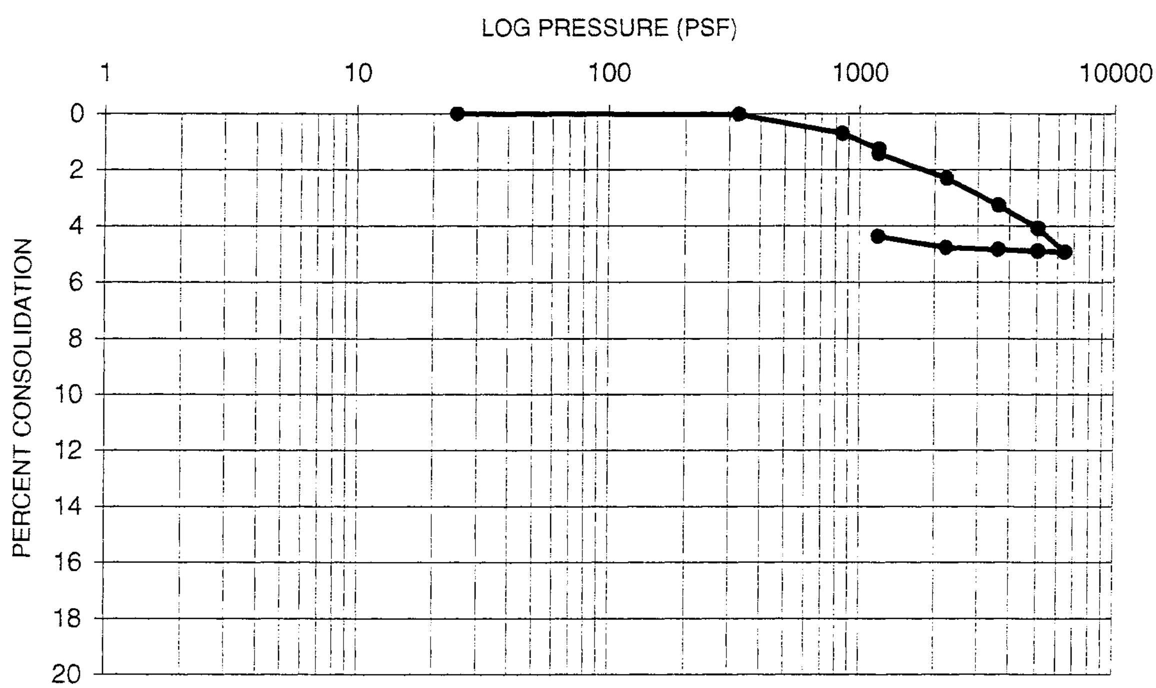
CONSOLIDATION DIAGRAM #24

JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Fill		
Sample Location:	B14-15'	Specific Gravity:	2.65
Dry Weight (pcf):	99.4	Initial Void Ratio:	0.66
Initial Moisture:	23.5%	Water Added At (psf):	1203.0
Initial Saturation:	93.9%	Consolidation Coef. (Cc):	0.1004

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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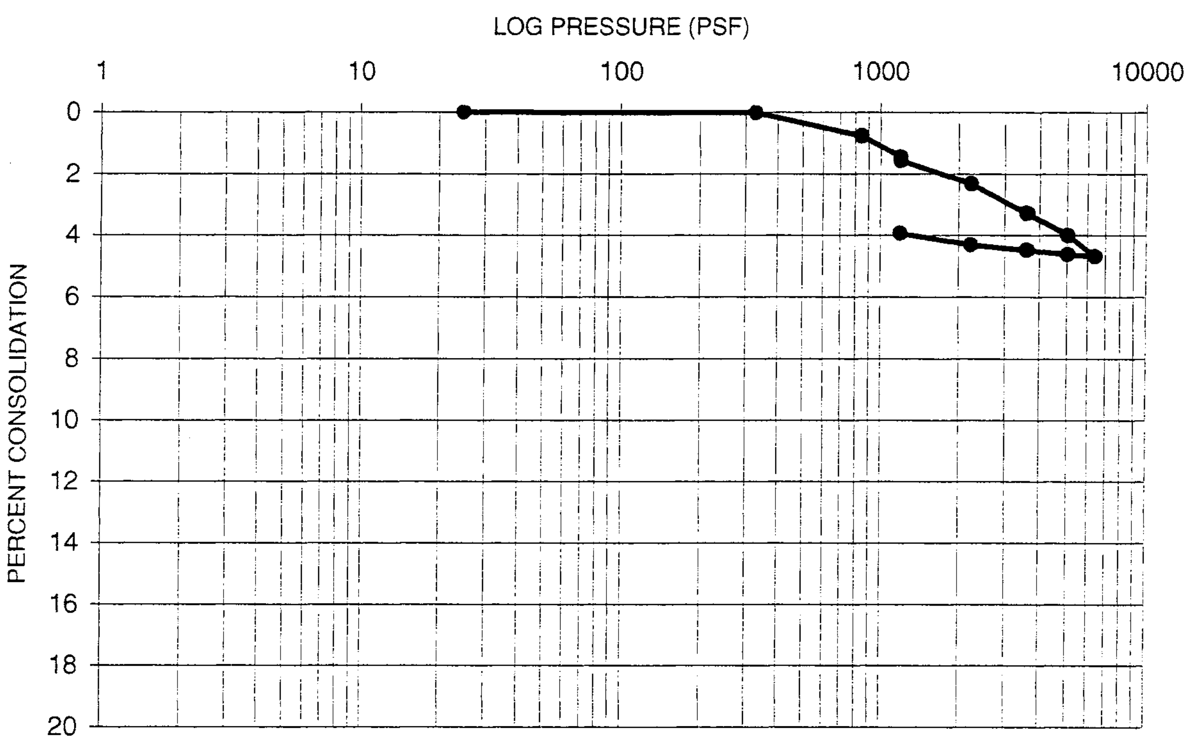
CONSOLIDATION DIAGRAM #25

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Fill		
Sample Location:	B14 - 20'	Specific Gravity:	2.65
Dry Weight (pcf):	93.7	Initial Void Ratio:	0.77
Initial Moisture:	16.3%	Water Added At (psf):	1203.0
Initial Saturation:	56.4%	Consolidation Coef. (Cc):	0.0938

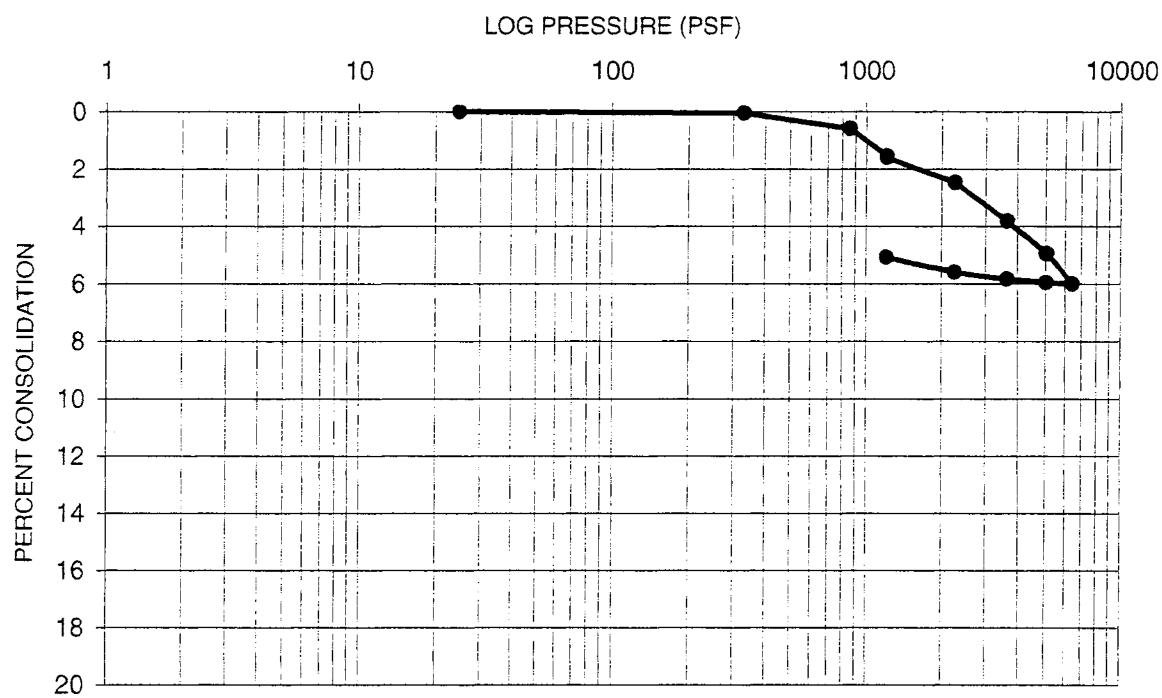
CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



THE J. BYER GROUP, INC.	CONSOLIDATION DIAGRAM #26
A GEOTECHNICAL CONSULTING FIRM	JB: **19376-B** CONSULTANT **JWB**
1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206 (818) 549-9959 FAX: (818) 543-3747	CLIENT: **Buckley School**

Earth Material:	ALLUVIUM		
Sample Location:	B14 - 25'	Specific Gravity:	2.65
Dry Weight (pcf):	87.1	Initial Void Ratio:	0.90
Initial Moisture:	28.4%	Water Added At (psf):	1216.0
Initial Saturation:	83.7%	Consolidation Coef. (Cc):	0.1524

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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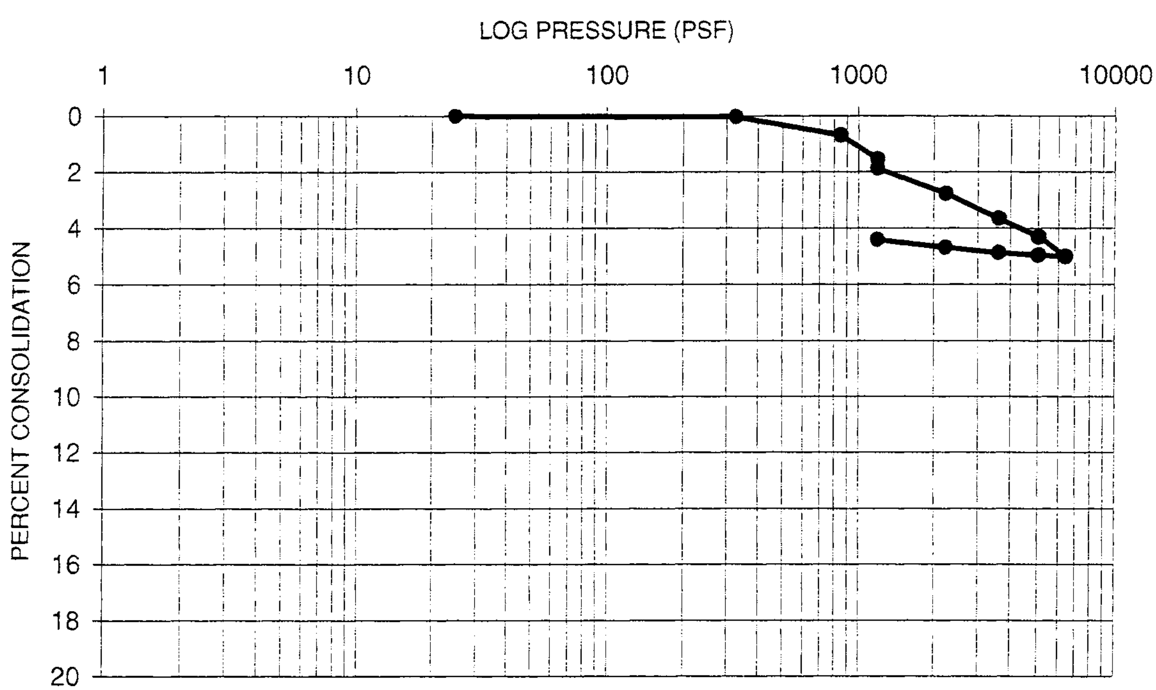
CONSOLIDATION DIAGRAM #27

JB: **19376 - B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Fill		
Sample Location:	B16-5'	Specific Gravity:	2.65
Dry Weight (pcf):	96.1	Initial Void Ratio:	0.72
Initial Moisture:	23.6%	Water Added At (psf):	1203.0
Initial Saturation:	86.8%	Consolidation Coef. (Cc):	0.0878

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION



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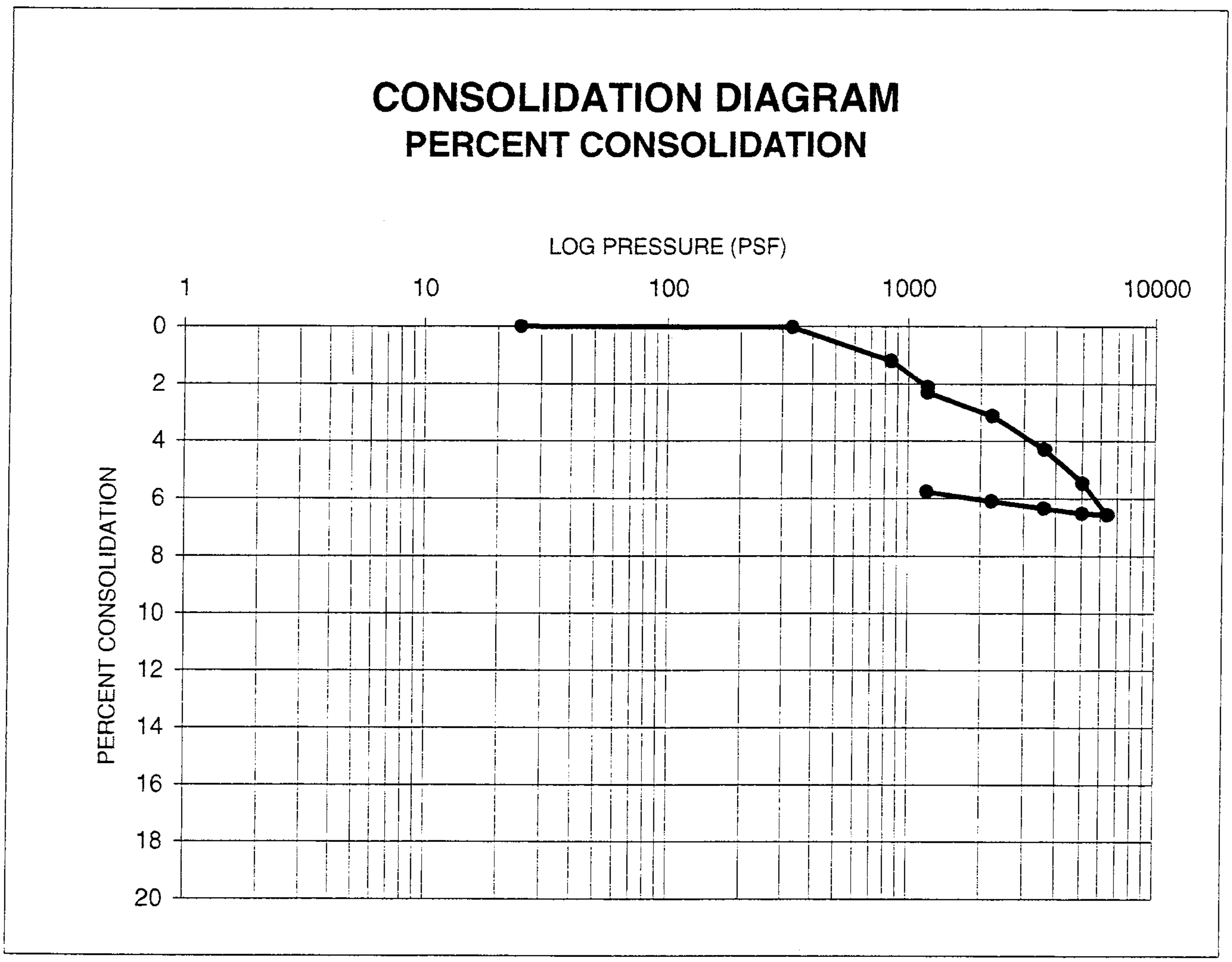
CONSOLIDATION DIAGRAM #28

JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Fill		
Sample Location:	B16 - 10'	Specific Gravity:	2.65
Dry Weight (pcf):	92.3	Initial Void Ratio:	0.79
Initial Moisture:	20.6%	Water Added At (psf):	1203.0
Initial Saturation:	69.0%	Consolidation Coef. (Cc):	0.1443



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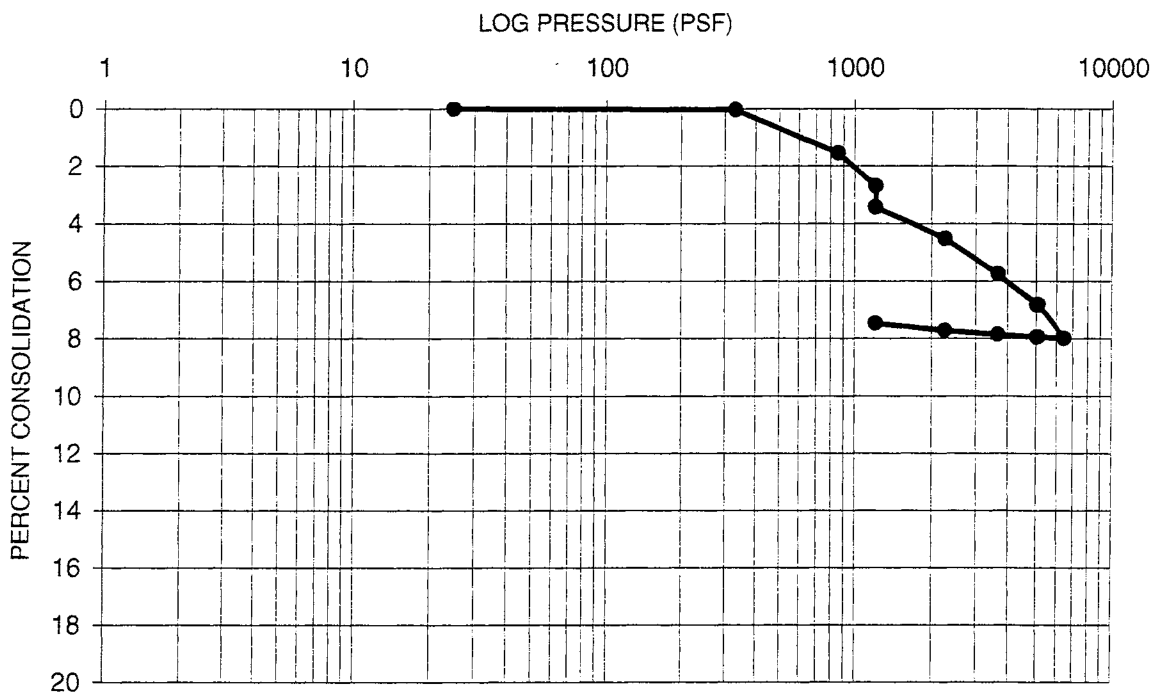
CONSOLIDATION DIAGRAM #29

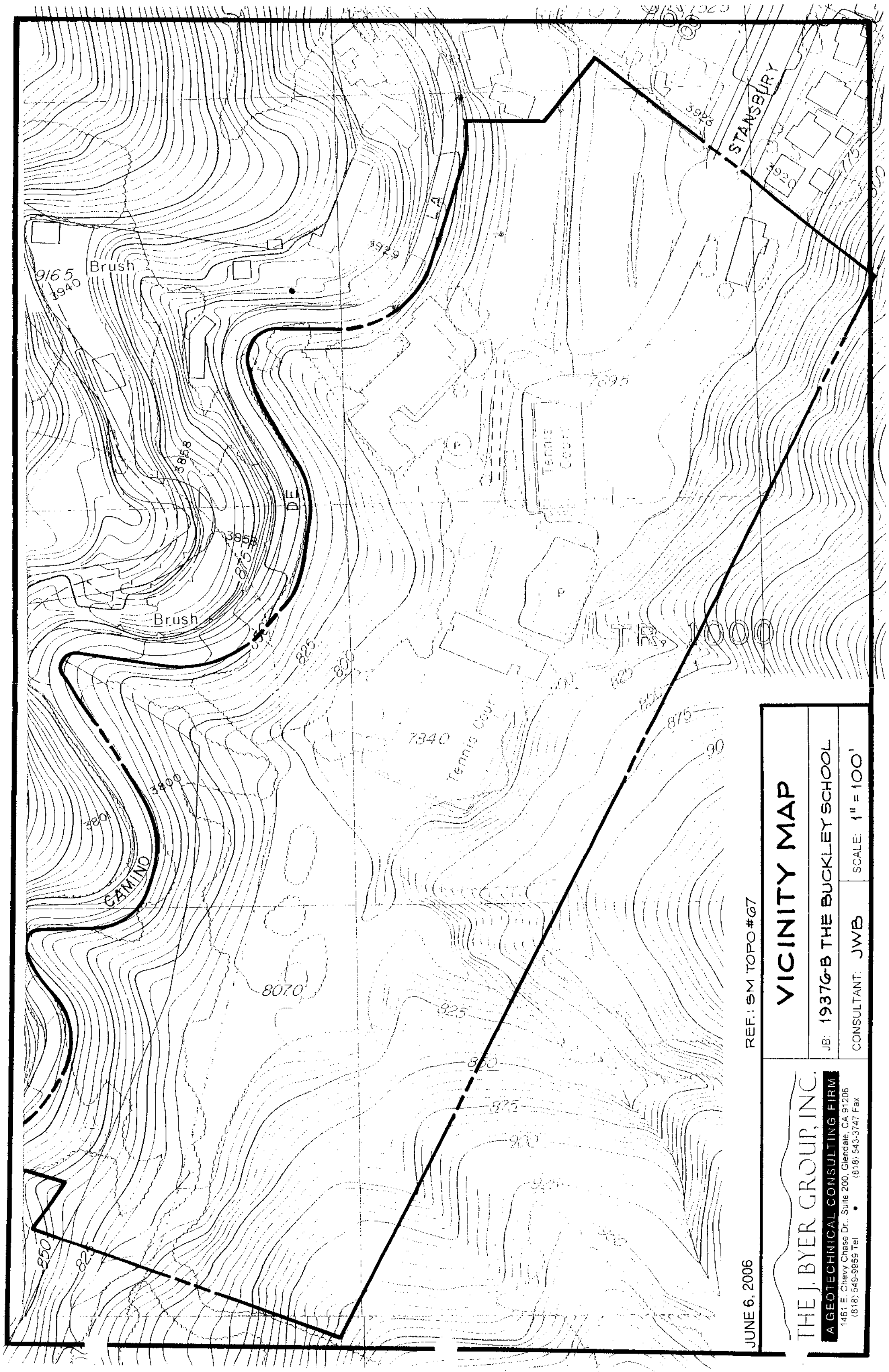
JB: **19376-B** CONSULTANT **JWB**

CLIENT: **Buckley School**

Earth Material:	Fill		
Sample Location:	B16 - 15'	Specific Gravity:	2.65
Dry Weight (pcf):	109.6	Initial Void Ratio:	0.51
Initial Moisture:	9.4%	Water Added At (psf):	1216.0
Initial Saturation:	48.9%	Consolidation Coef. (Cc):	0.1211

CONSOLIDATION DIAGRAM
PERCENT CONSOLIDATION




VICINITY MAP
JB: 1937G-B THE BUCKLEY SCHOOL
CONSULTANT: JWB
SCALE: 1" = 100'
REF: SM TOPO #G7
JUNE 6, 2006
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
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(818) 549-9959 Tel • (818) 543-3747 Fax
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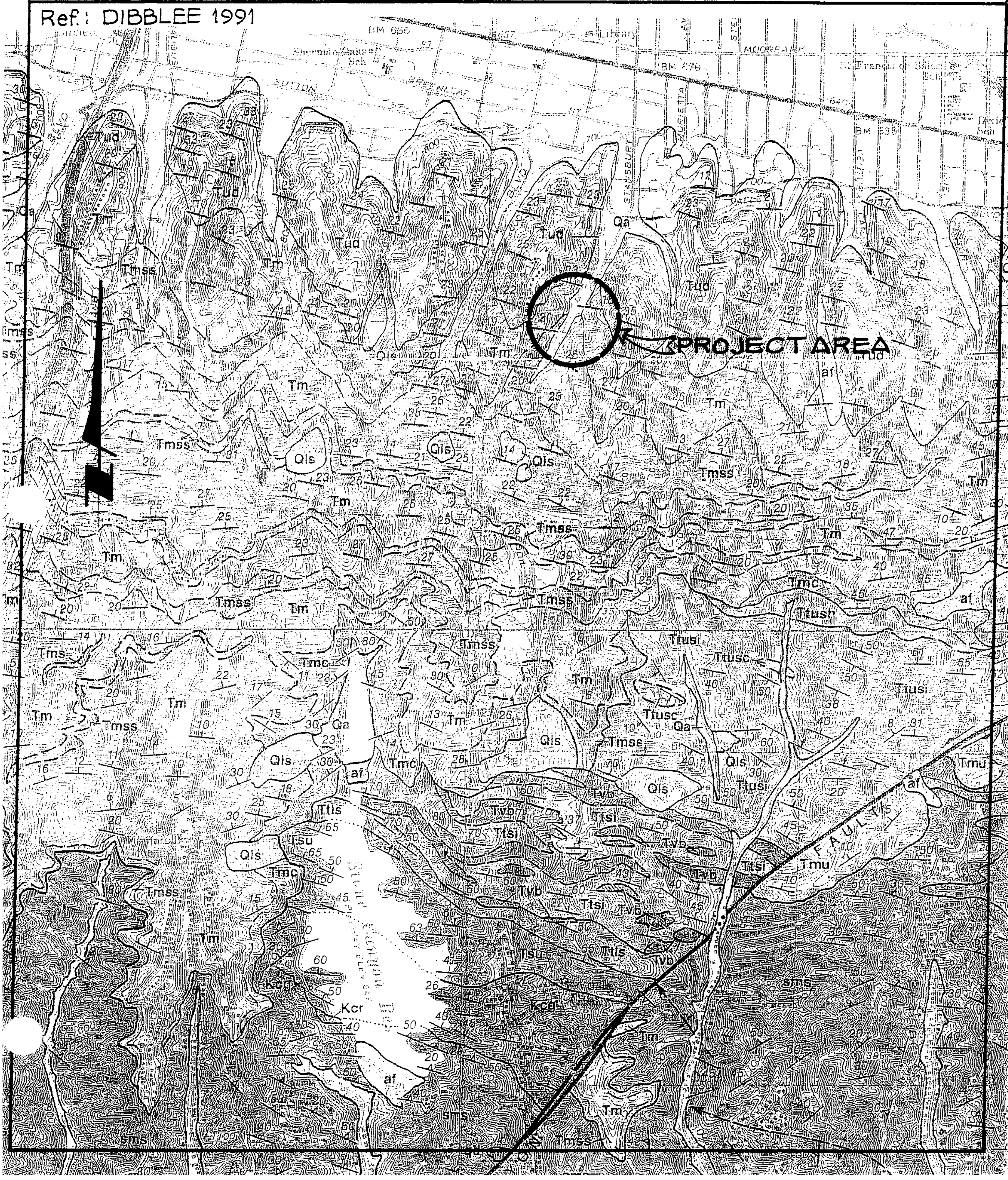
REGIONAL GEOLOGIC MAP

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JWB | SCALE: 1" = 2000'



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SEISMIC HAZARD ZONES MAP

JB 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JWB APPROX.SCALE: 1"=500'

REFERENCE: CALIFORNIA GEOLOGICAL SURVEY; *SEISMIC HAZARD ZONES VAN NUYS QUADRANGLE, LOS ANGELES COUNTY, CALIFORNIA*, OFFICIAL MAP, DATED FEBRUARY 1, 1998.

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LOG OF TEST PITS

JB: 19376-B CLIENT: BUCKLEY SCHOOL

GEOLOGIST: JC/JWB DATE LOGGED: 9/27/03

REPORT DATE: 12/3/03

TEST PIT #1 Elevation: 788 Feet Surface Conditions: Planted Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
2 5	18.0 17.5	113.6 113.4	0 - 8	FILL:	Clayey Sand, reddish brown, very moist, medium dense, slate chips, roots
10	20.5	104.6	8 - 11		Silty Sand, brownish gray, very moist, medium dense to dense, with shale chips
					wet at 8 feet

*End at *11 Feet; No Water; No Caving; Fill to Total Depth.*

TEST PIT #2 Elevation: 792 Feet Surface Conditions: Grass

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
2	17.3	112.3	0 - 4	FILL:	Clayey Sand, reddish brown, very moist to saturated, medium dense to dense, black slate chips, roots, debris
5	19.3	103.1	4 - 6		Clayey Sand, brownish gray, wet, soft, shale debris, brick fragments
10	15.9	109.8	6 - 10		Silty Sand, brownish bray, very moist, slightly to medium dense
					brick debris at 9 feet

End at 10 Feet; No Water; No Caving; Fill to Total Depth.

TEST PIT #3 *Elevation: 790 Feet* Surface Conditions: Planter

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
2	14.1	105.0	0 - 4	FILL:	Clayey Sand, gray brown, very moist, dense, slate chips, roots, debris
5 10	22.1 16.7	99.5 83.7	4 - 12		Clayey Sand, brownish-gray, very moist, dense, shale chips, brick debris, roots
			12 - 13		large brick blocks
15	22.7	89.4	13 - 16		glass fragments

End at 16 Feet; No Water; No Caving; Fill to Total Depth.

NOTE: The stratification depths shown on the Log of Test Pits are approximate and are based upon visual classification of samples and cuttings. The actual depths may vary. Variations between test pits may also occur.

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LOG OF TEST PITS

JB: 19376-B CLIENT: BUCKLEY SCHOOL

GEOLOGIST: JC/JWB DATE LOGGED: 9/27/03

REPORT DATE: 12/3/03

TEST PIT #4 Elevation: 789 Feet Surface Conditions: Soil Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
2	10.6	107.7	0 - 2½	FILL:	Silty Sand, brownish gray, moist, medium dense to dense, roots, shale fragments, porous
5	28.3	80.2	2½ - 8		Silty Sand, reddish-brown, very moist, medium dense to dense, shale fragments, slate chips
			8 - 9		concrete, pipe, and glass bottle
10	22.1	83.1	9 - 11		Silty Sand, brown, very moist, slightly dense, gravel, rock chips

End at 11 Feet; No Water; No Caving; Fill to Total Depth.

TEST PIT #5 Elevation: 798 Feet Surface Conditions: Natural Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
2 5	17.2 15.8	60.9 63.9	0 - 6	SOIL:	Silty Sand, brownish gray, slightly moist, medium dense, roots, shale fragments, porous
10	28.1	68.3	6 - 11	BEDROCK:	Diatomaceous Shale, light brown, soft, well bedded Bedding: N55W; 27N

End at 11 Feet; No Water; No Caving; No Fill.

TEST PIT #6 Elevation: 795 Feet Surface Conditions: Natural Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
			0 - 4½	SOIL:	Silty Sand, brownish gray, slightly moist, medium dense, roots, porous, shale fragments
			4½ - 6½	BEDROCK:	Diatomaceous Shale, light brown, slightly hard, well bedded Bedding: N88W; 31N

End at 6½ Feet; No Water; No Caving; No Fill.

NOTE: The stratification depths shown on the Log of Test Pits are approximate and are based upon visual classification of samples and cuttings. The actual depths may vary. Variations between test pits may also occur.

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LOG OF TEST PITS

JB: 19376-B CLIENT: BUCKLEY SCHOOL

GEOLOGIST: JC/JWB DATE LOGGED: 9/27/03

REPORT DATE: 12/3/03

TEST PIT #7 Elevation: 820 Feet Surface Conditions: Natural Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
			0 - 3	**SOIL:**	Silty Sand, brownish gray, slightly moist, medium dense, porous, shale fragments
			3 - 5½	**BEDROCK:**	Diatomaceous Shale, brown, soft, well bedded Bedding: N60W; 34N

End at 5½ Feet; No Water; No Caving; No Fill.

TEST PIT #8 Elevation: 785 Feet Surface Conditions: Natural Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
2	13.2	77.9	0 - 4	**SOIL:**	Silty Sand, brownish gray, damp, medium dense, shale fragments, roots, porous
			4 - 6½	**BEDROCK:**	Diatomaceous Shale, light brown, soft, well bedded Bedding: N60W; 27N

End at 6½ Feet; No Water; No Caving; No Fill.

TEST PIT #9 ***Elevation: 784 Feet*** Surface Conditions: Natural Slope, Minor Vegetation

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
			0 - 8	**SOIL:**	Silty Sand, brownish gray, slightly moist, slightly to medium dense, shale fragments
			8 - 10	**BEDROCK:**	Diatomaceous Shale, light brown, white, soft, well bedded Bedding: N89W; 32N

End at 10 Feet; No Water; No Caving; No Fill.

NOTE: The stratification depths shown on the Log of Test Pits are approximate and are based upon visual classification of samples and cuttings. The actual depths may vary. Variations between test pits may also occur.

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LOG OF TEST PITS

JB: 19376-B CLIENT: BUCKLEY SCHOOL

GEOLOGIST: JC/JWB DATE LOGGED: 9/27/03

REPORT DATE: 12/3/03

TEST PIT #10 Elevation: 802 Feet Surface Conditions: Natural Slope

SAMPLE DEPTH (feet)	MOISTURE CONTENT (%)	DRY DENSITY (pcf)	DEPTH INTERVAL (feet)	EARTH MATERIAL	LITHOLOGIC DESCRIPTION
			0 - 6½	**SOIL:**	Silty Sand, brownish gray, very moist, medium dense, porous, roots, shale fragments
			6½ = 8	**BEDROCK:**	Diatomaceous Shale, light brown, soft, well bedded Bedding: N75W; 32N

End at 8 Feet; No Water; No Caving; No Fill.

NOTE: The stratification depths shown on the Log of Test Pits are approximate and are based upon visual classification of samples and cuttings. The actual depths may vary. Variations between test pits may also occur.

JB No: 19376-B

Log of Boring: 1

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	Saturation %	Remarks
	0	*FILL:* Silty Clay, brown, moist, firm								
777.0	1									
776.0	2									
775.0	3									
774.0	4	Clayey Sand, mottled brown, moist, medium dense, some gravel								
773.0	5			----	R	17	22.9	89.9		
772.0	6									
771.0	7									
770.0	8									
769.0	9	Layers of Gravelly Clay, Silty Sand, Silty Clay, mottled brown, gray, reddish brown, moist, firm to medium dense								
768.0	10			----	R	14	43.7	73.6		
767.0	11									
766.0	12									
765.0	13									
764.0	14	Gravelly Sand, dark gray, moist, dense, clay binder								
763.0	15			----	R	35	11.8	122.1		
762.0	16									
761.0	17									
760.0	18									
759.0	19									
758.0	20	Clayey Sand, dark gray, moist, dense								
757.0	21			----	R	23	31.0	85.6		
756.0	22									
755.0	23									
754.0	24									
753.0	25									

Surface: Asphalt Parking - 3 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 778 Feet

Drill Date: September 27, 2003

Sheet: 1 of 3

JB No: 19376-B

Log of Boring: 1

Client: THE BUCKLEY SCHOOL **Logged By:** JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	Saturation %	Remarks
		ALLUVIUM: Silty Clay, brown, moist, firm, very porous, small rock chips								
752.0	26									
751.0	27									
750.0	28									
749.0	29									
748.0	30	Sandy Silt, gray brown, damp, soft, porous, some decomposed wood, small rockchips		----	R	12	23.0	74.7		
747.0	31									
746.0	32									
745.0	33									
744.0	34									
743.0	35	Sandy layers		----	R	16	10.6	97.7		
742.0	36									
741.0	37									
740.0	38	Silty Sand, light brown, damp, slightly dense, porous, small gravel								
739.0	39									
738.0	40									
737.0	41			----	R	17	19.9	87.2		
736.0	42									
735.0	43									
734.0	44									
733.0	45	Clayey Sand, light brown, moist, slightly dense, porous, small rock chips		----	R	16	33.6	84.9		
732.0	46									
731.0	47									
730.0	48									
729.0	49									
728.0	50									

Surface: Asphalt Parking - 3 Inches AC/3 Inches Base
Size: 8 Inch
Drill Method: Hollow-Stem Auger Drill Rig
Elevation: 778 Feet
Drill Date: September 27, 2003
Sheet: 2 of 3

JB No: 19376-B

Log of Boring: 1

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	Saturation %	Remarks
		very moist, more gravel to 1 inch diameter, less porous								
727.0	51									
726.0	52									
725.0	53									
724.0	54									
723.0	55	wet - seep at 55 feet		----	R	39	----	----		No Recovery
722.0	56	Sandy Gravel, brown, saturated, dense, rocks to 3 inches								
721.0	57									
720.0	58									
719.0	59	*BEDROCK:* Diatomaceous Siltstone and Sandstone, gray, moist, soft, well bedded, friable								
718.0	60			----	R	22	39.2	81.2		
717.0	61	End at 61 Feet; Seep at 55 Feet; Fill to 25 Feet.								
716.0	62									
715.0	63									
714.0	64									
713.0	65									
712.0	66									
711.0	67									
710.0	68									
709.0	69									
708.0	70									
707.0	71									
706.0	72									
705.0	73									
704.0	74									
703.0	75									

Surface: Asphalt Parking - 3 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 778 Feet

Drill Date: September 27, 2003

JB No: 19376-B

Log of Boring: 2

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
776		Ground Surface								
	0	*FILL:* Clayey Sand, brown, moist, medium dense, layers of Sand								
775	1									
774	2									
773	3									
772	4									
771	5									
770	6	Gravelly Clay with Slate chips, blue gray, moist, very firm								
769	7									
768	8									
767	9									
766	10									
765	11									
764	12									
763	13									
762	14	rocky layer								
761	15	Gravelly Clay, dark gray, moist, firm, no slate								
760	16									
759	17									
758	18	*ALLUVIUM:* Clayey Sand, brown, moist, slightly dense, porous, rock chips								
757	19									
756	20									

Surface: Asphalt Parking - 3 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 776 Feet

Drill Date: September 27, 2003

JB No: 19376-B

Log of Boring: 2

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
				----	R	10	23.1	82.7		
755	21									
754	22									
753	23									
752	24									
751	25	Gravelly Sand, light brown, damp, medium dense		----	R	15	11.3	96.4		
750	26									
749	27									
748	28	Clayey Sand, gray brown, moist, medium dense, porous								
747	29	layers of Silty Sand, light brown, damp, dense								
746	30			----	R	14	17.3	86.8		
745	31									
744	32									
743	33									
742	34									
741	35	Clayey Sand, light brown, moist, medium dense, porous, few rock chips		----	R	17	20.6	94.3		
740	36									
739	37									
738	38									
737	39									
736	40									

Surface: Asphalt Parking - 3 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 776 Feet

Drill Date: September 27, 2003

Sheet: 2 of 3

JB No: 19376-B

Log of Boring: 2

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
735	41	*BEDROCK:* Diatomaceous Siltstone with Sandstone, light brown, moist, soft, bedded		----	R	17	33.1	86.9		
734	42									
733	43									
732	44	moderately hard								
731	45			----	R	31	38.0	85.8		
730	46	End at 46 Feet; No Water; Fill to 18 Feet. End of Borehole								
729	47									
728	48									
727	49									
726	50									
725	51									
724	52									
723	53									
722	54									
721	55									
720	56									
719	57									
718	58									
717	59									
716	60									

Surface: Asphalt Parking - 3 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 776 Feet

Drill Date: September 27, 2003

Sheet: 3 of 3

JB No: 19376-B

Log of Boring: 3

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (Subsurface Profile)	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
781		Ground Surface								
781–769	0–12	*FILL:* Clayey Sand, dark brown, damp, medium dense, slate gravel								
769–766	12–15	*ALLUVIUM:* Sandy Silt, dark gray brown, moist, firm, rock chips								
766	15	light brown, damp, porous		----	R	10	31.3	63.3		
764	17	Clayey Sand, light brown, very moist, medium dense								

Surface: Asphalt Parking - 3 Inches AC

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 781 Feet

Drill Date: September 27, 2003

Sheet: 1 of 2

JB No: 19376-B

Log of Boring: 3

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
760	21									
759	22									
758	23									
757	24									
756	25	*BEDROCK:* Diatomaceous Siltstone with Sandstone, brown and light gray, moist, medium hard, well bedded, tight, no open fractures		----	R	50	53.7	67.5		
755	26									
754	27									
753	28									
752	29									
751	30									
750	31									
749	32									
748	33									
747	34									
746	35			----	R	50 7"	44.3	66.3		
745	36									
744	37									
743	38									
742	39	End at 40 Feet; No Water; Fill to 12 Feet.		----	R	50 7"	58.1	66.4		
741	40									

Surface: Asphalt Parking - 3 Inches AC

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 781 Feet

Drill Date: September 27, 2003

Sheet: 2 of 2

JB No: 19376-B

Log of Boring: 4

Client: THE BUCKLEY SCHOOL **Logged By:** JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
780		Ground Surface								
	0	*FILL:* Clayey Sand, brown, moist, medium dense								
779	1									
778	2									
777	3									
776	4									
775	5									
774	6	Clayey Sand, dark gray brown, very moist, medium dense, some debris								
773	7									
772	8									
771	9	Clayey Silt, dark brown, moist, firm								
770	10			----	R	15	23.0	98.9		
769	11									
768	12									
767	13									
766	14	*ALLUVIUM:* Clayey Sand, dark brown, moist, medium dense, porous								
765	15			----	R	10	24.7	84.3		
764	16									
763	17									
762	18									
761	19									
760	20									

Surface: Asphalt Drive - 3 Inches AC/5 Inches Gravel

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 780 Feet

Drill Date: September 27, 2003

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

JB No: 19376-B

Log of Boring: 4

Client: THE BUCKLEY SCHOOL *Logged By:* JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

SUBSURFACE PROFILE				SAMPLE						Remarks
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	
		Gravelly Clay, dark gray brown, moist, very firm, rock fragments to 2 inches		----	R	23	28.3	97.8		
759	21									
758	22	Clayey Sand, brown, moist, medium dense, porous, rock chips and some gravel								
757	23									
756	24									
755	25									
754	26									
753	27									
752	28									
751	29									
750	30			----	R	30	25.8	95.0		
749	31	Gravelly Clay layer, large rock fragments								
748	32									
747	33									
746	34									
745	35	Sandy Gravel, light brown, moist, dense, hard drilling, shale fragments over 3 inches, coarse sand matrix		----	R	46	24.4	94.5		
744	36									
743	37									
742	38									
741	39									
740	40									

Surface: Asphalt Drive - 3 Inches AC/5 Inches Gravel
Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig
Elevation: 780 Feet

Drill Date: September 27, 2003
Sheet: 2 of 3

JB No: 19376-B

Log of Boring: 4

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	Symbol	USCS (SAMPLE)	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		Clayey Gravel, light brown, moist, dense, shale fragments		----	R	25	25.5	96.4		
739	41									
738	42									
737	43									
736	44									
735	45			----	R	38	17.8	96.7		
734	46									
733	47									
732	48	*BEDROCK:* Diatomaceous Siltstone and Sandstone, gray, moist, moderately hard, well bedded, tight								
731	49									
730	50			----	R	50 9"	45.3	73.3		
729	51	End at 51 Feet; No Water; Fill to 14 Feet. End of Borehole								
728	52									
727	53									
726	54									
725	55									
724	56									
723	57									
722	58									
721	59									
720	60									

Surface: Asphalt Drive - 3 Inches AC/5 Inches Gravel

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 780 Feet

Drill Date: September 27, 2003

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

JB No: 19376-B

Log of Boring: 5

Client: THE BUCKLEY SCHOOL *Logged By:* JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

SUBSURFACE PROFILE				SAMPLE						Remarks
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	
771		Ground Surface								
	0	*FILL:* Gravelly Sand, gray brown, moist, dense, slate gravel, clay binder								
770	1									
769	2									
768	3									
767	4									
766	5									
765	6									
764	7									
763	8									
762	9									
761	10	Refusal at 10 Feet; Hard Rock?, FIll to Total Depth.								
760	11	End of Borehole								
759	12									
758	13									
757	14									
756	15									
755	16									
754	17									
753	18									
752	19									
751	20									

Surface: Asphalt Parking
Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig
Elevation: 771 Feet

Drill Date: September 27, 2003
Sheet: 1 of 1

JB No: 19376-B

Log of Boring: 6

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						Remarks
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	
779	0	Ground Surface								
	0	*FILL:* Clayey Sand, brown, moist, medium dense								
775	4	dark brown layer								
774	5	Gravelly Sand, brown, moist, dense, some clay		----	R	22	12.1	115.8		
770	9	Clayey Silt, dark gray brown, very moist, firm								
769	10			----	R	19	31.1	91.6		
764	15	sample disturbed		----	R	17	24.0	77.6		
760	19	*ALLUVIUM:* Sandy Silt, dark gray, moist, soft to firm, few rock chips								
759	20									

Surface: Asphalt Road - 3 Inches AC/6 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 779 Feet

Drill Date: September 27. 2003

Sheet: 1 of 3

JB No: 19376-B

Log of Boring: 6

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
				----	R	15	26.8	91.6		
758	21									
757	22									
756	23									
755	24									
754	25	Clayey Sand, dark and light brown, moist, medium dense, numerous rock chips in layers		----	R	13	26.8	92.4		
753	26									
752	27									
751	28									
750	29									
749	30	Silty Sand, brown and light brown, moist, medium dense		----	R	21	24.4	91.8		
748	31									
747	32									
746	33									
745	34	Gravel layer, Clayey Sand layers								
744	35			----	R	26	24.7	96.7		
743	36									
742	37									
741	38									
740	39									
739	40									

Surface: Asphalt Road - 3 Inches AC/6 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 779 Feet

Drill Date: September 27, 2003

Sheet: 2 of 3

JB No: 19376-B

Log of Boring: 6

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		Gravelly Sand, gray and brown, moist, medium dense, gravel to 3 inches		----	R	27	21.1	98.5		
738	41									
737	42									
736	43									
735	44									
734	45	Sampler on rock		----	R	17 9"	----	----		No Recovery
733	46	End at 46 Feet; Refusal - Hard Rock, Fill to 19 Feet. End of Borehole								
732	47									
731	48									
730	49									
729	50									
728	51									
727	52									
726	53									
725	54									
724	55									
723	56									
722	57									
721	58									
720	59									
719	60									

Surface: Asphalt Road - 3 Inches AC/6 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 779 Feet

Drill Date: September 27, 2003

JB No: 19376-B

Log of Boring: 7

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	USCS (SAMPLE)	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
787.0	1	*FILL:* Silty Sand, brown, damp, medium dense, with shale fragments							
786.0	2	*SOIL:* Clayey Sand, dark brown, damp, dense, porous, shale fragments							
785.0	3								
784.0	4								
783.0	5		----	R	19	17.1	92.0		
782.0	6								
781.0	7								
780.0	8								
779.0	9								
778.0	10	*ALLUVIUM:* Clayey Sand, brown, damp, medium dense, large shale fragments	----	R	50 10"	30.7	71.9		
777.0	11								
776.0	12	*BEDROCK:* Diatomaceous Siltstone and Sandstone, tan, damp, well bedded, moderately hard							
775.0	13								
774.0	14								
773.0	15		----	R	50 11"	32.4	72.0		
772.0	16	End at 16 Feet; No Water; Fill to 2 Feet.							
771.0	17								
770.0	18								
769.0	19								
768.0	20								
767.0	21								
766.0	22								
765.0	23								
764.0	24								
763.0	25								

Surface: Asphalt Drive - 3 Inches AC/5 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 788 Feet

Drill Date: October 6, 2003

Sheet: 1 of 1

Log of Boring: 8

JB No: 19376-B

Client: THE BUCKLEY SCHOOL *Logged By:* JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		FILL: Silty Sand, brown, damp, medium dense, brick fragment, slate chips, shale fragments, rubble								
785.0	1									
784.0	2									
783.0	3									
782.0	4									
781.0	5	*SOIL:* Clayey Sand, brownish gray, damp, medium dense, porous		----	R	18	25.1	77.7		
780.0	6									
779.0	7									
778.0	8									
777.0	9									
776.0	10			----	R	13	16.7	83.8		
775.0	11									
774.0	12	hard drilling								
773.0	13									
772.0	14									
771.0	15	*ALLUVIUM:* Clayey Sand, light brown, damp, medium dense, porous, with shale chips		----	R	18	10.0	91.8		
770.0	16									
769.0	17									
768.0	18									
767.0	19									
766.0	20	brown, damp, dense, porous, shale chips (hard drilling)		----	R	28	23.1	84.4		
765.0	21	hard drilling								
764.0	22									
763.0	23									
762.0	24									
761.0	25									

Surface: Asphalt Pavement - 4 Inches AC/5 Inches Base Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig Elevation: 786 Feet

Drill Date: October 6, 2003 Sheet: 1 of 2

JB No: 19376-B

Log of Boring: 8

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
760.0	26									
759.0	27									
758.0	28									
757.0	29									
756.0	30	Clayey Sand, light brown, damp, dense, large shale fragments		----	R	31	34.6	86.0		
755.0	31									
754.0	32									
753.0	33									
752.0	34									
751.0	35			----	R	25	42.3	77.9		
750.0	36									
749.0	37									
748.0	38									
747.0	39	*BEDROCK:* Diatomaceous Shale, brown-gray, moist, well bedded, moderately hard								
746.0	40			----	R	49	55.4	76.8		
745.0	41	End at 41 Feet; No Water; Fill to 5 Feet.								
744.0	42									
743.0	43									
742.0	44									
741.0	45									
740.0	46									
739.0	47									
738.0	48									
737.0	49									
736.0	50									

Surface: Asphalt Pavement - 4 Inches AC/5 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 786 Feet

Drill Date: October 6, 2003

JB No: 19376-B

Log of Boring: 9

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
796.0	0	*FILL:* Clayey Sand, brown, damp, dense, rubble, shale fragments, roots								
794.0	2			----	R	18	20.2	104.1		
793.0	3	*SOIL:* Clayey Sand, brown gray, damp, medium dense, shale chips, roots								
791.0	5			----	R	24	51.3	69.0		
790.0	6	Sandstone and Shale fragments								
786.0	10			----	R	50 9"	----	----		No Recovery
783.0	13	*BEDROCK:* Diatomaceous Siltstone, light brown, moist, well bedded, moderately hard								
781.0	15			----	R	45	59.5	66.2		
780.0	16	End at 16 Feet; No Water; Fill to 3 Feet.								

Surface: Asphalt Pavement - 3 Inches AC/4 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 796 Feet

Drill Date: October 6, 2003

Sheet: 1 of 1

JB No: 19376-B

Log of Boring: 10

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	Symbol	USCS (SAMPLE)	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
829.0–825.0	0–4	*FILL:* Clayey Sand, dark gray, moist, medium dense, gravel								
825.0–819.0	4–10	*SOIL:* Sandy Clay, brown, moist, firm, rock fragments								
819.0–813.0	10–16	*BEDROCK:* Diatomaceous Siltstone and Sandstone, brown-gray, moist, moderately hard, minor fractures, bedded								
819.0	10			----	R	50 10"	13,5	93.5		
814.0	15			----	R	36	40.9	81.2		
813.0	16	End at 16 Feet; No Water; Fill to 4 Feet.								

Elevation scale: 828.0, 827.0, 826.0, 825.0, 824.0, 823.0, 822.0, 821.0, 820.0, 819.0, 818.0, 817.0, 816.0, 815.0, 814.0, 813.0, 812.0, 811.0, 810.0, 809.0, 808.0, 807.0, 806.0, 805.0, 804.0

Depth scale: 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25

Surface: Asphalt Parking - 4 Inches AC/6 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 829 Feet

Drill Date: October 6, 2003

Sheet: 1 of 1

JB No: 19376-B

Log of Boring: 11

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	Symbol	USCS (SAMPLE)	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		FILL: Clayey Sand, reddish-brown, damp, medium dense, some rubble, blue slate chips								
829.0	1									
828.0	2									
827.0	3									
826.0	4									
825.0	5	Clayey Sand, brownish-gray, damp, medium dense, some rubble, brick fragments								
824.0	6									
823.0	7									
822.0	8									
821.0	9									
820.0	10	sample barrel on concrete		----	R	25	15.3	106.6		
819.0	11	Clayey Sand, dark gray, damp, dense, rubble, slate chips, twigs								
818.0	12									
817.0	13									
816.0	14	Clayey Sand, dark gray, damp, medium dense to dense, asphalt rubble, slate chps								
815.0	15			----	R	20	12.2	113.3		
814.0	16									
813.0	17									
812.0	18									
811.0	19									
810.0	20	Clayey Sand, brown, damp, medium dense to dense, rubble, slate chips								
809.0	21			----	R	20	20.3	107.0		
808.0	22	hard drilling at 22 to 24 feet (possible rock)								
807.0	23									
806.0	24									
805.0	25									

Surface: Asphalt Pavement/Parking - 5 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 830 Feet

Drill Date: October 1, 2003

JB No: 19376-B

Log of Boring: 11

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	Saturation %	Remarks
804.0	26									
803.0	27									
802.0	28									
801.0	29									
800.0	30	Silty Sand, brown, damp, medium dense to dense, small rock/gravel, more coarse, shale chips		----	R	17	30.1	83.4		
799.0	31									
798.0	32									
797.0	33									
796.0	34	Clayey Sand, brown, damp, medium dense to dense, porous, large amounts of shale fragments								
795.0	35			----	R	20	28.9	86.8		
794.0	36									
793.0	37									
792.0	38									
791.0	39									
790.0	40			----	R	50 7"	----	----		No Recovery
789.0	41									
788.0	42									
787.0	43	*BEDROCK:* Diatomaceous Siltstone/Sandstone, brown and gray, moderately hard, minor fractures, weathered, well bedded								
786.0	44									
785.0	45			----	R	50 11"	28.3	87.3		
784.0	46	End at 46 Feet; No Water; Fill to 24 Feet.								
783.0	47									
782.0	48									
781.0	49									
780.0	50									

Surface: Asphalt Pavement/Parking - 5 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 830 Feet

Drill Date: October 1, 2003

Log of Boring: 12

JB No: 19376-B

Client: THE BUCKLEY SCHOOL *Logged By:* JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
822		Ground Surface								
	0	*FILL:* Clayey Sand, brown, damp, medium dense, some rubble, asphalt, gravel								
817	5			----	R	28	16.2	105.6		
816	6	Clayey Sand, dark brown, damp, dense, small gravel (slate)								
812	10	Clayey Sand, dark gray brown, moist, medium dense, gravel, sandstone fragment in sample tip		----	R	45	13.0	113.0		
807	15	Clayey Sand, gray and brown layers, moist, medium dense, gravel		----	R	31	19.4	97.1		
802	20									

Surface: Asphalt Parking - 4 Inches AC/3 Inches Base	Size: 8 Inch
Drill Method: Hollow-Stem Auger Drill Rig	Elevation: 822 Feet
Drill Date: October 1, 2003	Sheet: 1 of 2

JB No: 19376-B

Log of Boring: 12

Client: THE BUCKLEY SCHOOL *Logged By:* JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
801	21	*ALLUVIUM:* Gravelly Clay, tan, damp, firm, small fragments of shale, sandstone, siltstone		----	R	48	35.3	74.3		
797	25	rock in sample tip		----	R	40	44.8	73.2		
792	30	*BEDROCK:* Diatomaceous Siltstone and Sandstone, gray and brown, damp, soft as rock, well bedded, tight		----	R	50	32.2	82.2		
791	31	End at 31 Feet; No Water; Fill to 20 Feet. End of Borehole								

Elevation scale: 801, 800, 799, 798, 797, 796, 795, 794, 793, 792, 791, 790, 789, 788, 787, 786, 785, 784, 783, 782

Depth scale: 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40

Surface: Asphalt Parking - 4 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 822 Feet

Drill Date: October 1, 2003

JB No: 19376-B

Log of Boring: 13

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	Saturation %	Remarks
840.0–834.0	0–6	*FILL:* Clayey Sand, brown, damp, medium dense, rubble, brick fragments, slate chips								
834.0–830.0	6–10	Clayey Sand, reddish-brown, damp, medium dense, slate chips, rubble, shale fragments								
830.0	10	Clayey Sand, reddish brown, damp, medium dense, shale fragments, slate chips, rubble, roots		----	R	11	17.7	108.0		
824.0	16	Clayey Sand, dark gray, damp, medium dense, slate chips, rubble								
~819.4	~20.6			----	R	15	21.5	103.1		
818.0	22	color change to very dark gray-green								

Surface: Grass Field

Drill Method: Hollow-Stem Auger Drill Rig

Drill Date: October 6, 2003

Size: 8 Inch

Elevation: 840 Feet

JB No: 19376-B

Log of Boring: 13

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
814.0	26									
813.0	27									
812.0	28									
811.0	29									
810.0	30	Clayey Sand, brown, damp, medium dense, slate chips, rubbie		----	R	17	15.6	114.0		
809.0	31									
808.0	32									
807.0	33	Clayey Sand, dark gray, moist, medium dense, rubble, slate chips								
806.0	34									
805.0	35									
804.0	36									
803.0	37	hard drilling								
802.0	38									
801.0	39									
800.0	40	Clayey Sand, gray-green, damp, medium dense, shale fragments, rubble		----	R	16	28.0	91.7		
799.0	41									
798.0	42									
797.0	43	*ALLUVIUM:* Clayey sand, light brown, light gray, damp, dense, large shale fragments								
796.0	44									
795.0	45			----	R	33	52.6	67.7		
794.0	46									
793.0	47									
792.0	48									
791.0	49									
790.0	50									

Surface: Grass Field

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 840 Feet

Drill Date: October 6, 2003

Log of Boring: 13

JB No: 19376-B

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
789.0	51									
788.0	52									
787.0	53									
786.0	54									
785.0	55	Clayey Sand, brown, damp, medium dense, rock fragments		----	R	23	43.1	76.0		
784.0	56	water at 56.5 Feet								
783.0	57									
782.0	58									
781.0	59									
780.0	60									
779.0	61									
778.0	62									
777.0	63									
776.0	64									
775.0	65	Gravelly Sand, Clayey Sand mix, brown and gray, wet, dense, large shale fragments		----	R	25	23.6	96.1		
774.0	66	End at 66 Feet; Water at 56.5 Feet, Fill to 43 Feet.								
773.0	67									
772.0	68									
771.0	69									
770.0	70									
769.0	71									
768.0	72									
767.0	73									
766.0	74									
765.0	75									

Surface: Grass Field

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 840 Feet

Drill Date: October 6, 2003

Sheet: 3 of 3

JB No: 19376-B

Log of Boring: 14

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		FILL: Silty Sand, brown, damp, medium dense, some gravel								
836.0	1									
835.0	2									
834.0	3									
833.0	4	Clayey Sand, brown, saturated, soft, slate chips, roots								
832.0	5			----	R	3	26.7	98.1		
831.0	6									
830.0	7									
829.0	8									
828.0	9									
827.0	10	Clayey Sand, reddish-brown, saturated, soft, slate chps, wood fragments		----	R	10	18.6	109.5		
826.0	11									
825.0	12									
824.0	13									
823.0	14									
822.0	15	Clayey Sand, dark gray, damp, medium dense, slate chips, granite fragments		----	R	15	23.5	99.4		
821.0	16									
820.0	17									
819.0	18									
818.0	19	Clayey Sand, light brown, damp, moist, medium dense, slate chips, shale chips								
817.0	20									
				----	R	14	16.3	93.7		
816.0	21									
815.0	22									
814.0	23	*ALLUVIUM:* Clayey Sand, dark green/blue, very moist, medium dense, fragment of Sandstone								
813.0	24									
812.0	25									

Surface: Dirt Field

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 837 Feet

Drill Date: October 1, 2003

JB No: 19376-B

Log of Boring: 14

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
811.0	26									
810.0	27									
809.0	28	*BEDROCK:* Diatomaceous Siltstone and Sandstone, brown, gray layers, moderately hard, well bedded								
808.0	29									
807.0	30			----	R	26	45.8	77.7		
806.0	31									
805.0	32									
804.0	33									
803.0	34									
802.0	35	Diatomaceous Siltstone and Sandstone, brown, gray layers, moderately hard, fractured, well bedded		----	R	50 11"	25.6	89.7		
801.0	36									
800.0	37									
799.0	38									
798.0	39			----	R	50 6"	32.9	82.7		
797.0	40	Diatomaceous Siltstone and Sandstone, brown and gray, moderately hard, minor fractures, bedded								
796.0	41	End at 40 Feet; No water; Fill to 23 Feet.								
795.0	42									
794.0	43									
793.0	44									
792.0	45									
791.0	46									
790.0	47									
789.0	48									
788.0	49									
787.0	50									

Surface: Dirt Field

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 837 Feet

Drill Date: October 1, 2003

JB No: 19376-B

Log of Boring: 15

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
	0	*FILL:* Clayey Sand, reddish-brown, damp, medium dense, some rubble, slate chips and shale fragments							
837.0	1								
836.0	2								
835.0	3								
834.0	4								
833.0	5								
832.0	6	Clayey Sand, brown, damp, medium dense to dense, shale fragments, rubble							
831.0	7								
		ALLUVIUM: Clayey Sand, brown, damp, medium dense, rock fragments							
830.0	8								
829.0	9								
828.0	10		----	R	18	28.6	80.2		
827.0	11								
826.0	12								
825.0	13								
824.0	14								
823.0	15	Clayey Sand, brown, damp, medium dense, large shale fragments, porous	----	R	14	32.1	71.9		
822.0	16								
821.0	17								
820.0	18								
819.0	19								
818.0	20		----	R	14	26.3	83.1		
817.0	21								
816.0	22	hard drilling at 22 feet, rocky layer							
815.0	23	*BEDROCK:* Diatomaceous Siltstone and Sandstone, brown and gray, moderately hard, fractured, bedded							
814.0	24								
813.0	25								

Surface: Asphalt Driveway - 4 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 838 Feet

Drill Date: October 6, 2003

JB No: 19376-B

Log of Boring: 15

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
812.0	26	End at 26 Feet; No water; Fill to 7.5 Feet								
811.0	27									
810.0	28									
809.0	29									
808.0	30									
807.0	31									
806.0	32									
805.0	33									
804.0	34									
803.0	35									
802.0	36									
801.0	37									
800.0	38									
799.0	39									
798.0	40									
797.0	41									
796.0	42									
795.0	43									
794.0	44									
793.0	45									
792.0	46									
791.0	47									
790.0	48									
789.0	49									
788.0	50									

Surface: Asphalt Driveway - 4 Inches AC/3 Inches Base

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 838 Feet

Drill Date: October 6, 2003

JB No: 19376-B

Log of Boring: 16

Client: THE BUCKLEY SCHOOL   Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
843		Ground Surface								
	0	FILL: Clayey Sand, brown, moist, medium dense, some rock fragments								
842	1	concrete in sample								
841	2									
840	3									
839	4									
838	5			----	R	26	23.6	96.1		
837	6	light brown and dark brown layers, medium dense to dense								
836	7									
835	8									
834	9									
833	10	Clayey Sand, dark gray brown, very moist, medium dense, gravel and rock fragments		----	R	18	20.6	92.3		
832	11									
831	12									
830	13									
829	14									
828	15	more gravel and rocks, less dense, more moisture		----	R	16	9.4	109.6		
827	16									
826	17									
825	18	rocky layers, hard drilling								
824	19									
823	20									

Surface: Soil   Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig   Elevation: 843 Feet

Drill Date: October 6. 2003

JB No: 19376-B

Log of Boring: 16

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE						Remarks
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	
	20.5			----	R	19	21.0	104.9		
822	21									
821	22									
820	23									
819	24	fill contains cobbles of granite								
818	25	hard drilling		----	R	21	2.4	106.0		
817	26									
816	27									
815	28	*BEDROCK:* Siltstone and Sandstone, light and dark brown, damp, moderately hard, well bedded								
814	29									
813	30			----	R	50 10"	25.0	84.9		
812	31									
811	32	refusal - too hard to drill End at 32 Feet; No Water; Fill to 28 Feet.								
810	33	End of Borehole								
809	34									
808	35									
807	36									
806	37									
805	38									
804	39									
803	40									

Surface: Soil

Size: 8 Inch

Drill Method: Hollow-Stem Auger Drill Rig

Elevation: 843 Feet

Drill Date: October 6, 2003

JB No: 19376-B

Log of Boring: 17

Client: THE BUCKLEY SCHOOL

Logged By: JWB

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		SUBSURFACE PROFILE	SAMPLE						
843.0–841.0	0–3	*FILL:* Silty Sand, light brown, damp, dense, rubble, brick and shale fragments, roots							
841.0–839.0	3–5	*SOIL:* Clayey Sand, light brown, damp, dense, white diatomaceous shale fragments							
839.0–835.0	5–9	*BEDROCK:* Diatomaceous Sandstone and Siltstone, brownish-gray, damp, moderately hard, fractured, roots	----	R	50 10"	27.1	89.9		
835.0–833.0	9–11	Diatomaceous Sandstone and Siltstone, brownish-gray, damp, moderately hard, well bedded, cemented limestone layers	----	R	50 5"	27.1	86.6		
833.0	11	End at 11 Feet; No Water; Fill to 3 Feet.							

Elevation scale: 843.0 to 819.0; Depth scale: 1 to 25.

Surface: Dirt/Grassy Surface

Drill Method: Hollow-Stem Auger Drill Rig

Drill Date: October 6, 2003

Size: 8 Inch

Elevation: 844 Feet

Sheet: 1 of 1

JB No: 19376-B

Log of Boring: 18

Client: THE BUCKLEY SCHOOL

Logged By: JET

Site Location: 3900 Standebury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
	0	*FILL:* Silty Clay, dark brown, very moist, slightly firm to soft								
781.5	2.5	10 inch rock fragments								
779.0	5	Clayey Silt, dark brown to brown, moist, firm, some gravel		----	R	16	21.9	101.4	91.9	
774.0	10	dark gray, stiff		----	R	20	26.2	93.9	91.1	
769.0	15	SandySilt, gray-brown, moist, firm, some clay		----	R	17	22.6	94.1	79.3	
764.0	20	*ALLUVIUM:* Sandy Silt/Silty Sand, light gray, light brown, slightly moist, dense, some gravel		----	R	20	27.7	83.6	75.2	

Elevation scale: 783.0, 782.0, 781.0, 780.0, 779.0, 778.0, 777.0, 776.0, 775.0, 774.0, 773.0, 772.0, 771.0, 770.0, 769.0, 768.0, 767.0, 766.0, 765.0, 764.0, 763.0, 762.0, 761.0, 760.0, 759.0

Depth scale: 1–25

Surface: Asphalt

Drill Method: Hollow-Stem Auger Drill Rig

Drill Date: December 22, 2005

Size: 8 Inch Diameter

Elevation: 784 Feet

JB No: 19376-B

Log of Boring: 18

Client: THE BUCKLEY SCHOOL **Logged By:** JET

Site Location: 3900 Standebury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

Elevation	Depth	Description (SUBSURFACE PROFILE)	Symbol	USCS (SAMPLE)	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
758.0	26	Silty Sand, gray, slightly moist, dense, some gravel		----	R	44	26.3	94.5	93.0	
757.0	27									
756.0	28									
755.0	29									
754.0	30	Gravelly Sand, tan, gray, slightly moist, dense, rock fragments to 4 inches		----	R	51	15.8	89.6	49.5	
753.0	31									
752.0	32									
751.0	33									
750.0	34									
749.0	35	Sandy Gravel, gray-brown, gray, tan, slightly moist to dry, dense to very dense		----	R	71	13.8	99.8	55.5	
748.0	36									
747.0	37									
746.0	38									
745.0	39	*BEDROCK:* Siltstone, Claystone, tan, light gray, soft to moderately hard, thinly bedded		----	R	21	33.8	85.9	97.0	
744.0	40									
743.0	41									
742.0	42	Refusal at 42 Feet; No Water; Fill to 20 Feet.								
741.0	43									
740.0	44									
739.0	45									
738.0	46									
737.0	47									
736.0	48									
735.0	49									
734.0	50									

Surface: Asphalt Size: 8 Inch Diameter

Drill Method: Hollow-Stem Auger Drill Rig Elevation: 784 Feet

Drill Date: December 22, 2005 Sheet: 2 of 2

JB No: 19376-B

Log of Boring: 19

Client: THE BUCKLEY SCHOOL

Logged By: JET

Site Location: 3900 Stansbury Avenue, Sherman Oaks

The J. Byer Group, Inc.
1461 E. Chevy Chase Dr., Ste 200
Glendale, CA. 91206
(818) 549-9959

SUBSURFACE PROFILE				SAMPLE							
Elevation	Depth	Description	Symbol	USCS	Type	Blow Count	Moisture Content (%)	Dry Density	% Saturation	Remarks
		FILL: Silty Sand, dark brown, slightly moist to moist								
790.0	1									
789.0	2									
788.0	3									
787.0	4									
786.0	5			----	R	21	13.2	112.0		
785.0	6									
784.0	7									
783.0	8									
782.0	9									
781.0	10	End at 10Feet; No Water; Fill to Total Depth Unable to Continue Due to Utility Line								
780.0	11									
779.0	12									
778.0	13									
777.0	14									
776.0	15									
775.0	16									
774.0	17									
773.0	18									
772.0	19									
771.0	20									
770.0	21									
769.0	22									
768.0	23									
767.0	24									
766.0	25									

Surface: Asphalt

Drill Method: Hollow-Stem Auger Drill Rig

Drill Date: December 22, 2005

Size: 8 Inch Diameter

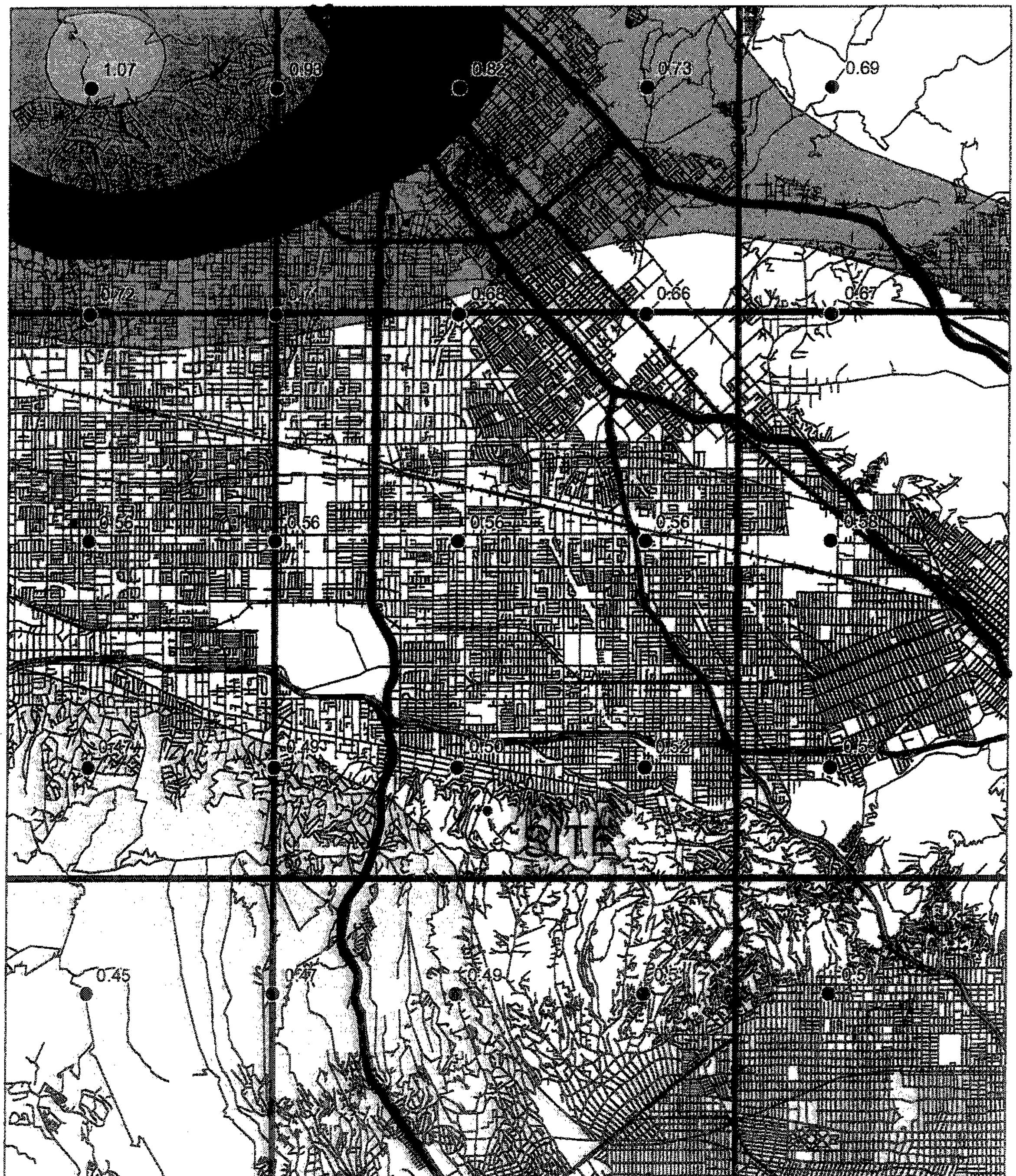
Elevation: 791 Feet

VAN NUYS 7.5 MINUTE QUADRANGLE AND PORTIONS OF ADJACENT QUADRANGLES

10% EXCEEDANCE IN 50 YEARS PEAK GROUND ACCELERATION (g)

1998

ALLUVIUM CONDITIONS



Base map modified from MapInfo Street Works ©1998 MapInfo Corporation

0 2.5 5

Kilometers

Department of Conservation
Division of Mines and Geology

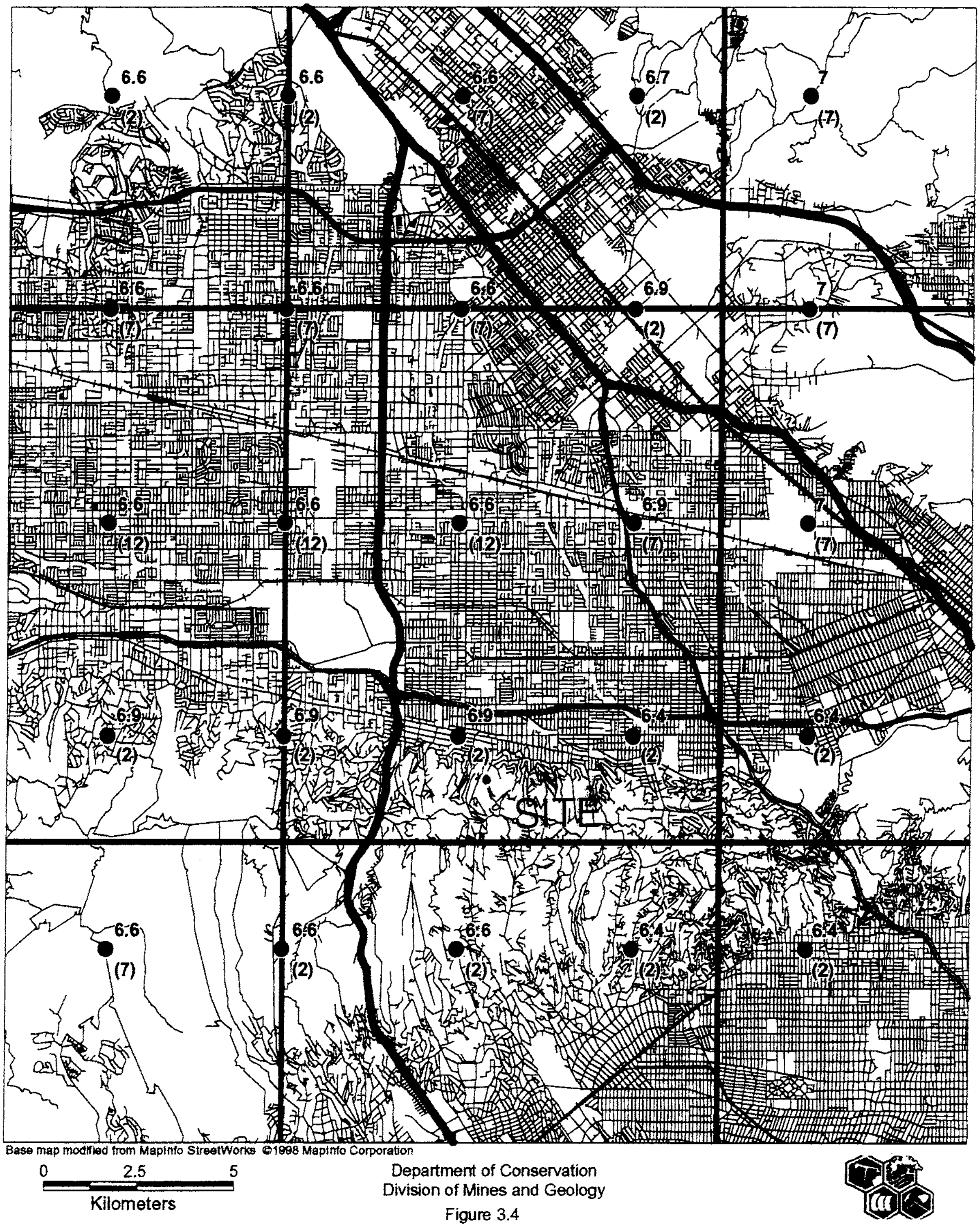
Figure 3.3

VAN NUYS 7.5 MINUTE QUADRANGLE AND PORTIONS OF ADJACENT QUADRANGLES

10% EXCEEDANCE IN 50 YEARS PEAK GROUND ACCELERATION

1998

PREDOMINANT EARTHQUAKE
Magnitude (Mw)
(Distance (km))



Base map modified from MapInfo StreetWorks ©1998 MapInfo Corporation

Department of Conservation
Division of Mines and Geology
Figure 3.4

EQFAULT SUMMARY

DETERMINISTIC SITE PARAMETERS

ABBREVIATED FAULT NAME	APPROXIMATE DISTANCE mi (km)	ESTIMATED MAX. EARTHQUAKE EVENT: MAXIMUM EARTHQUAKE MAG.(Mw)	PEAK SITE ACCEL. g	EST. SITE INTENSITY MOD.MERC.
HOLLYWOOD	4.2(6.8)	6.4	0.437	X
SANTA MONICA	4.4(7.1)	6.6	0.455	X
NEWPORT-INGLEWOOD (L.A.Basin)	8.6(13.9)	6.9	0.278	IX
MALIBU COAST	8.9(14.4)	6.7	0.290	IX
NORTHRIDGE (E. Oak Ridge)	9.0(14.5)	6.9	0.365	IX
VERDUGO	9.3(15.0)	6.7	0.279	IX
SIERRA MADRE (San Fernando)	12.7(20.5)	6.7	0.204	VIII
RAYMOND	12.7(20.5)	6.5	0.178	VIII
PALOS VERDES	13.4(21.6)	7.1	0.209	VIII
SANTA SUSANA	13.9(22.4)	6.6	0.173	VIII
COMPTON THRUST	14.1(22.7)	6.8	0.222	IX
SIERRA MADRE	14.2(22.8)	7.0	0.222	IX
SAN GABRIEL	15.5(25.0)	7.0	0.168	VIII
ELYSIAN PARK THRUST	16.2(26.1)	6.7	0.177	VIII
ANACAPA-DUME	17.6(28.3)	7.3	0.215	VIII
HOLSER	19.0(30.5)	6.5	0.112	VII
OAK RIDGE (Onshore)	23.1(37.1)	6.9	0.119	VII
SIMI-SANTA ROSA	23.4(37.6)	6.7	0.101	VII
CLAMSHELL-SAWPIT	24.0(38.7)	6.5	0.083	VII
WHITTIER	26.7(42.9)	6.8	0.077	VII
SAN CAYETANO	28.5(45.9)	6.8	0.085	VII
SAN JOSE	32.5(52.3)	6.5	0.057	VI
SAN ANDREAS - Mojave	33.7(54.3)	7.1	0.072	VII
SAN ANDREAS - 1857 Rupture	33.7(54.3)	7.8	0.122	VII
CHINO-CENTRAL AVE. (Elsinore)	38.8(62.5)	6.7	0.053	VI
CUCAMONGA	38.8(62.5)	7.0	0.067	VI
SAN ANDREAS - Carrizo	39.0(62.7)	7.2	0.065	VI
SANTA YNEZ (East)	40.1(64.5)	7.0	0.054	VI
VENTURA - PITAS POINT	42.6(68.6)	6.8	0.051	VI
OAK RIDGE(Blind Thrust Offshore)	46.0(74.1)	6.9	0.057	VI
CHANNEL IS. THRUST (Eastern)	47.3(76.2)	7.4	0.081	VII
M.RIDGE-ARROYO PARIDA-SANTA ANA	48.0(77.3)	6.7	0.040	V
MONTALVO-OAK RIDGE TREND	48.3(77.8)	6.6	0.042	VI
NEWPORT-INGLEWOOD (Offshore)	48.5(78.1)	6.9	0.039	V
ELSINORE-GLEN IVY	50.2(80.8)	6.8	0.034	V
RED MOUNTAIN	52.2(84.0)	6.8	0.039	V
SAN ANDREAS - San Bernardino	53.7(86.4)	7.3	0.047	VI
SAN ANDREAS - Southern	53.7(86.4)	7.4	0.051	VI
SAN JACINTO-SAN BERNARDINO	54.0(86.9)	6.7	0.029	V
GARLOCK (West)	54.1(87.1)	7.1	0.040	V

DETERMINISTIC SITE PARAMETERS

ABBREVIATED FAULT NAME	APPROXIMATE DISTANCE mi (km)	ESTIMATED MAX. EARTHQUAKE EVENT MAXIMUM EARTHQUAKE MAG.(Mw)	PEAK SITE ACCEL. g	EST. SITE INTENSITY MOD.MERC.
PLEITO THRUST	54.7(88.1)	7.2	0.051	VI
BIG PINE	56.8(91.4)	6.7	0.027	V
CLEGHORN	57.3(92.2)	6.5	0.023	IV
SANTA CRUZ ISLAND	62.2(100.1)	6.8	0.031	V
CORONADO BANK	67.1(108.0)	7.4	0.038	V
NORTH FRONTAL FAULT ZONE (West)	68.8(110.7)	7.0	0.032	V
WHITE WOLF	69.0(111.0)	7.2	0.038	V
SAN JACINTO-SAN JACINTO VALLEY	69.5(111.9)	6.9	0.024	V
ELSINORE-TEMECULA	71.5(115.0)	6.8	0.022	IV
SANTA YNEZ (West)	72.1(116.1)	6.9	0.023	IV
NORTH CHANNEL SLOPE	72.2(116.2)	7.1	0.033	V
HELENDALE - S. LOCKHARDT	78.1(125.7)	7.1	0.025	V
GARLOCK (East)	82.7(133.1)	7.3	0.027	V
LENWOOD-LOCKHART-OLD WOMAN SPRGS	83.7(134.7)	7.3	0.026	V
SANTA ROSA ISLAND	84.1(135.3)	6.9	0.023	IV
ROSE CANYON	91.0(146.4)	6.9	0.017	IV
SAN JACINTO-ANZA	91.6(147.4)	7.2	0.022	IV
NORTH FRONTAL FAULT ZONE (East)	93.9(151.1)	6.7	0.017	IV
GRAVEL HILLS - HARPER LAKE	95.4(153.6)	6.9	0.016	IV
ELSINORE-JULIAN	97.4(156.7)	7.1	0.018	IV
PINTO MOUNTAIN	98.6(158.7)	7.0	0.017	IV
So. SIERRA NEVADA	99.1(159.5)	7.1	0.022	IV
LOS ALAMOS-W. BASELINE	99.4(160.0)	6.8	0.017	IV

-END OF SEARCH- 63 FAULTS FOUND WITHIN THE SPECIFIED SEARCH RADIUS.

THE HOLLYWOOD FAULT IS CLOSEST TO THE SITE.
IT IS ABOUT 4.2 MILES (6.8 km) AWAY.

LARGEST MAXIMUM-EARTHQUAKE SITE ACCELERATION: **0.4554 g**

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* *                                       * *
* *    --------------------------------   * *
* *     TSTAB  slope stability analysis   * *
* *        Revision 2.52 - 01/06/86       * *
* *    --------------------------------   * *
* *                                       * *
* *    TAGA Engineering Software Services * *
* *         Berkeley, California USA      * *
* *                                       * *
* *   IBM PC & 8086/8088 MS-DOS Version by * *
* *                                       * *
* * Design Professionals Management Systems * *
* *         Kirkland, Washington USA      * *
* *                                       * *
* *      copyright (c) 1983,84,85 TAGA    * *
* *      copyright (c) 1983,84,85 DPMS    * *
* *                                       * *
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*********************************************************************
  CALCULATE THE GROSS STABILITY OF SECTION I
*********************************************************************

*****************************************
  ANALYSIS BY BISHOP'S SIMPLIFIED METHOD
*****************************************

**************
  INPUT DATA
**************

 CONTROL DATA,
      AUTOMATIC SEARCH FOR CRITICAL CIRCLE
      NUMBER OF DEPTH LIMITING TANGENTS                  0
      NUMBER OF VERTICAL SECTIONS                       16
      NUMBER OF SOIL LAYER BOUNDARIES                    2
      NUMBER OF POINTS DEFINING COHESION PROFILE         0
      NUMBER OF CURVES DEFINING COHESION ANISOTROPY      0
      NUMBER OF BOUNDARY LINE LOADS                      0
      NUMBER OF BOUNDARY PRESSURE LOADS                  0

      SEISMIC COEFFICIENT                    =        .000
      ATMOSPHERIC PRESSURE                   =    2116.000
      UNIT WEIGHT OF WATER                   =      62.400
      UNIT WEIGHT OF WATER IN TENSION CRACK =      62.400

 SEARCH STARTS AT CENTER ( 600.0, -1400.0), WITH FINAL GRID OF 25.0

 ALL CIRCLES PASS THROUGH THE POINT ( 585.0, -775.0)
```

CALCULATION SHEET #2

GEOMETRY

SECTIONS	-1000.00	15.00	50.00	72.00	160.00	210.00	246.00	280.00
T. CRACKS	-1050.00	-1050.00	-1053.00	-1050.00	-1025.00	-1000.00	-975.00	-950.00
W IN CRACK	-1050.00	-1050.00	-1053.00	-1050.00	-1025.00	-1000.00	-975.00	-950.00
BOUNDARY 1	-1050.00	-1050.00	-1053.00	-1050.00	-1025.00	-1000.00	-975.00	-950.00
BOUNDARY 2	.00	.00	.00	.00	.00	.00	.00	.00

SECTIONS	320.00	368.00	405.00	465.00	510.00	554.00	585.00	602.00
T. CRACKS	-925.00	-900.00	-875.00	-850.00	-825.00	-800.00	-775.00	-770.00
W IN CRACK	-925.00	-900.00	-875.00	-850.00	-825.00	-800.00	-775.00	-770.00
BOUNDARY 1	-925.00	-900.00	-875.00	-850.00	-825.00	-800.00	-775.00	-770.00
BOUNDARY 2	.00	.00	.00	.00	.00	.00	.00	.00

SOIL PROPERTIES

LAYER	DENSITY	COHESION	FRICTION ANGLE	DELTA PHI
1	105.00	951.00	30.00	.00

****
RESULTS
****

NUMBER	TANGENT	RADIUS	(X) CENTER	(Y) CENTER	F.S.
1	-774.8	625.2	600.0	-1400.0	1.549
2	-774.0	626.0	550.0	-1400.0	1.577
3	-774.8	675.2	600.0	-1450.0	1.549
4	-771.6	628.4	650.0	-1400.0	1.608
5	-774.8	575.2	600.0	-1350.0	1.561
6	-774.9	625.1	575.0	-1400.0	1.554
7	**-774.8**	**650.2**	**600.0**	**-1425.0**	**1.548**
8	-773.7	626.3	625.0	-1400.0	1.563
9	-774.8	600.2	600.0	-1375.0	1.553
10	-774.9	650.1	575.0	-1425.0	1.558
11	-774.8	675.2	600.0	-1450.0	1.549
12	-773.8	651.2	625.0	-1425.0	1.554
13	-774.9	675.1	575.0	-1450.0	1.566
14	-773.8	676.2	625.0	-1450.0	1.550
15	-773.7	626.3	625.0	-1400.0	1.563
16	-774.9	625.1	575.0	-1400.0	1.554

F.S. MINIMUM= **1.548** FOR THE CIRCLE OF CENTER (600.0, -1425.0)

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******************************
  LOCATION OF CRITICAL CIRCLE
******************************
```

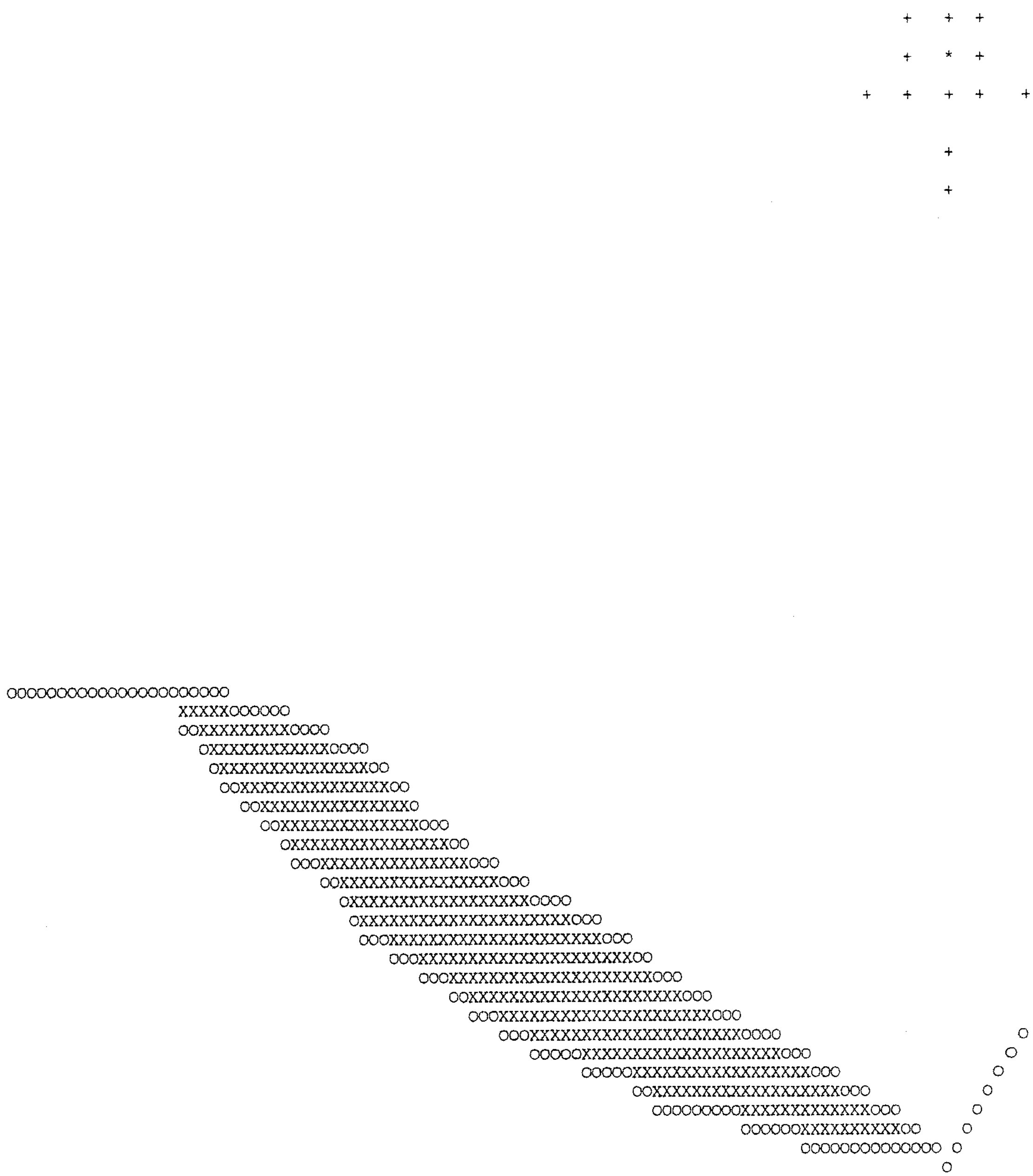

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* *                                       * *
* *    --------------------------------   * *
* *     TSTAB  slope stability analysis   * *
* *        Revision 2.52 - 01/06/86       * *
* *    --------------------------------   * *
* *                                       * *
* *    TAGA Engineering Software Services * *
* *         Berkeley, California USA      * *
* *                                       * *
* *   IBM PC & 8086/8088 MS-DOS Version by * *
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* *         Kirkland, Washington USA      * *
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* *      copyright (c) 1983,84,85 DPMS    * *
* *                                       * *
* ***************************************** *
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```
**********************************************************************
  CALCULATE THE SEISMIC STABILITY OF SECTION I
**********************************************************************

******************************************
  ANALYSIS BY BISHOP'S SIMPLIFIED METHOD
******************************************

**************
  INPUT DATA
**************

 CONTROL DATA,
      AUTOMATIC SEARCH FOR CRITICAL CIRCLE
      NUMBER OF DEPTH LIMITING TANGENTS                0
      NUMBER OF VERTICAL SECTIONS                     16
      NUMBER OF SOIL LAYER BOUNDARIES                  2
      NUMBER OF POINTS DEFINING COHESION PROFILE       0
      NUMBER OF CURVES DEFINING COHESION ANISOTROPY    0
      NUMBER OF BOUNDARY LINE LOADS                    0
      NUMBER OF BOUNDARY PRESSURE LOADS                0

      SEISMIC COEFFICIENT                   =        .150
      ATMOSPHERIC PRESSURE                  =    2116.000
      UNIT WEIGHT OF WATER                  =      62.400
      UNIT WEIGHT OF WATER IN TENSION CRACK =      62.400

 SEARCH STARTS AT CENTER ( 600.0,-1400.0), WITH FINAL GRID OF 25.0

 ALL CIRCLES PASS THROUGH THE POINT ( 585.0, -775.0)
```

GEOMETRY

ECTIONS	-1000.00	15.00	50.00	72.00	160.00	210.00	246.00	280.00
T. CRACKS	-1050.00	-1050.00	-1053.00	-1050.00	-1025.00	-1000.00	-975.00	-950.00
W IN CRACK	-1050.00	-1050.00	-1053.00	-1050.00	-1025.00	-1000.00	-975.00	-950.00
BOUNDARY 1	-1050.00	-1050.00	-1053.00	-1050.00	-1025.00	-1000.00	-975.00	-950.00
BOUNDARY 2	.00	.00	.00	.00	.00	.00	.00	.00

SECTIONS	320.00	368.00	405.00	465.00	510.00	554.00	585.00	602.00
T. CRACKS	-925.00	-900.00	-875.00	-850.00	-825.00	-800.00	-775.00	-770.00
W IN CRACK	-925.00	-900.00	-875.00	-850.00	-825.00	-800.00	-775.00	-770.00
BOUNDARY 1	-925.00	-900.00	-875.00	-850.00	-825.00	-800.00	-775.00	-770.00
BOUNDARY 2	.00	.00	.00	.00	.00	.00	.00	.00

SOIL PROPERTIES

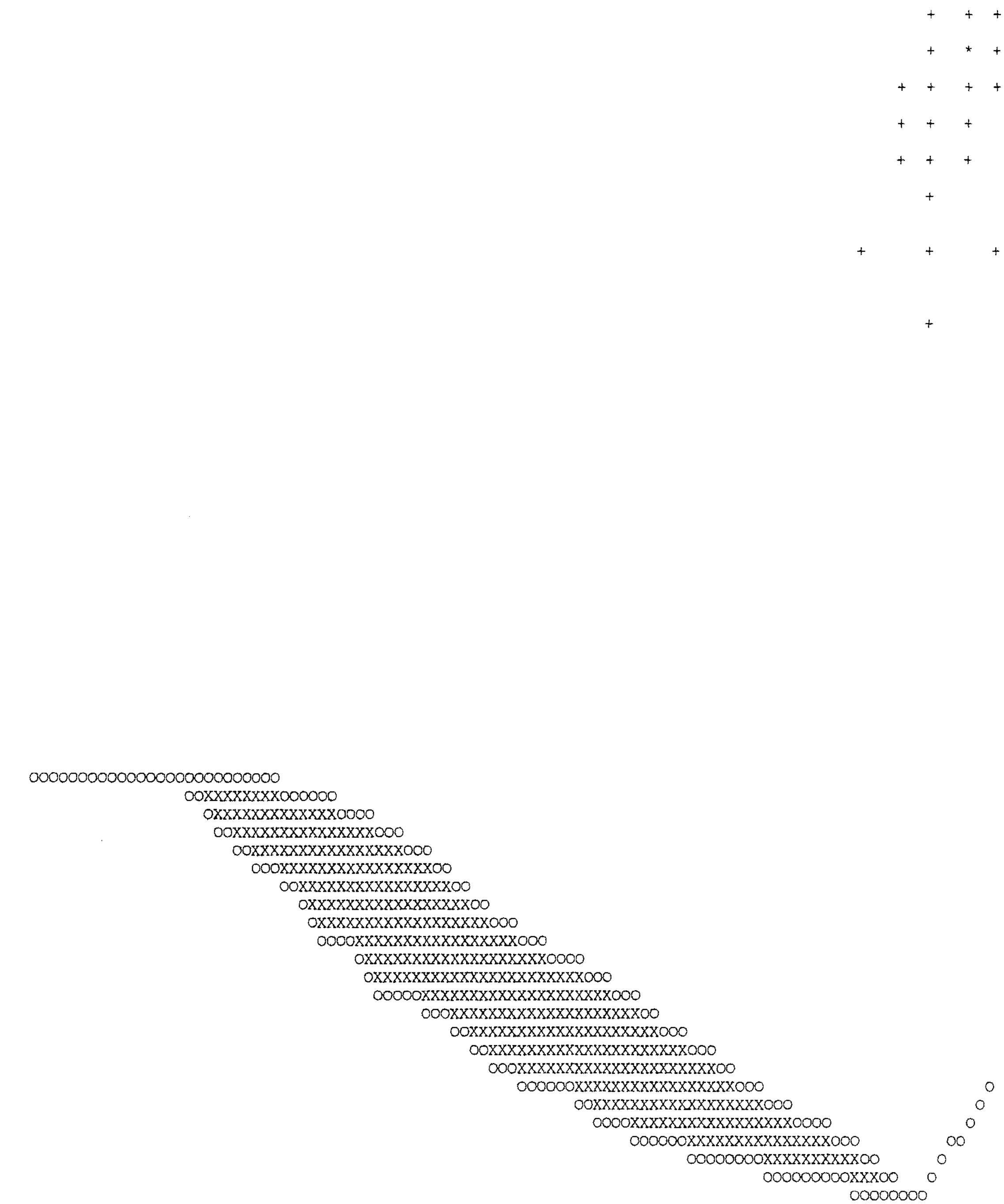
LAYER	DENSITY	COHESION	FRICTION ANGLE	DELTA PHI
1	105.00	951.00	30.00	.00

****
RESULTS
****

NUMBER	TANGENT	RADIUS	(X) CENTER	(Y) CENTER	F.S.
1	-774.8	625.2	600.0	-1400.0	1.157
2	-774.0	626.0	550.0	-1400.0	1.168
3	-774.8	675.2	600.0	-1450.0	1.152
4	-771.6	628.4	650.0	-1400.0	1.209
5	-774.8	575.2	600.0	-1350.0	1.172
6	-774.9	675.1	575.0	-1450.0	1.158
7	-774.8	700.2	600.0	-1475.0	1.151
8	-773.8	676.2	625.0	-1450.0	1.157
9	-774.8	650.2	600.0	-1425.0	1.154
10	-774.9	700.1	575.0	-1475.0	1.162
11	-774.8	725.2	600.0	-1500.0	1.153
12	-773.9	701.1	625.0	-1475.0	1.153
13	-774.9	725.1	575.0	-1500.0	1.168
14	-773.9	726.1	625.0	-1500.0	1.150
15	-773.8	676.2	625.0	-1450.0	1.157
16	-774.9	675.1	575.0	-1450.0	1.158
17	**-773.9**	**751.1**	**625.0**	**-1525.0**	**1.149**
18	-772.1	727.9	650.0	-1500.0	1.160
19	-774.9	750.1	600.0	-1525.0	1.157
20	-774.0	776.0	625.0	-1550.0	1.151
21	-772.2	752.8	650.0	-1525.0	1.155
22	-774.9	775.1	600.0	-1550.0	1.162
23	-772.3	777.7	650.0	-1550.0	1.152
24	-772.1	727.9	650.0	-1500.0	1.160
25	-774.8	725.2	600.0	-1500.0	1.153

F.S. MINIMUM= **1.149** FOR THE CIRCLE OF CENTER (625.0, -1525.0)

****
LOCATION OF CRITICAL CIRCLE
****



JUNE 6, 2006

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

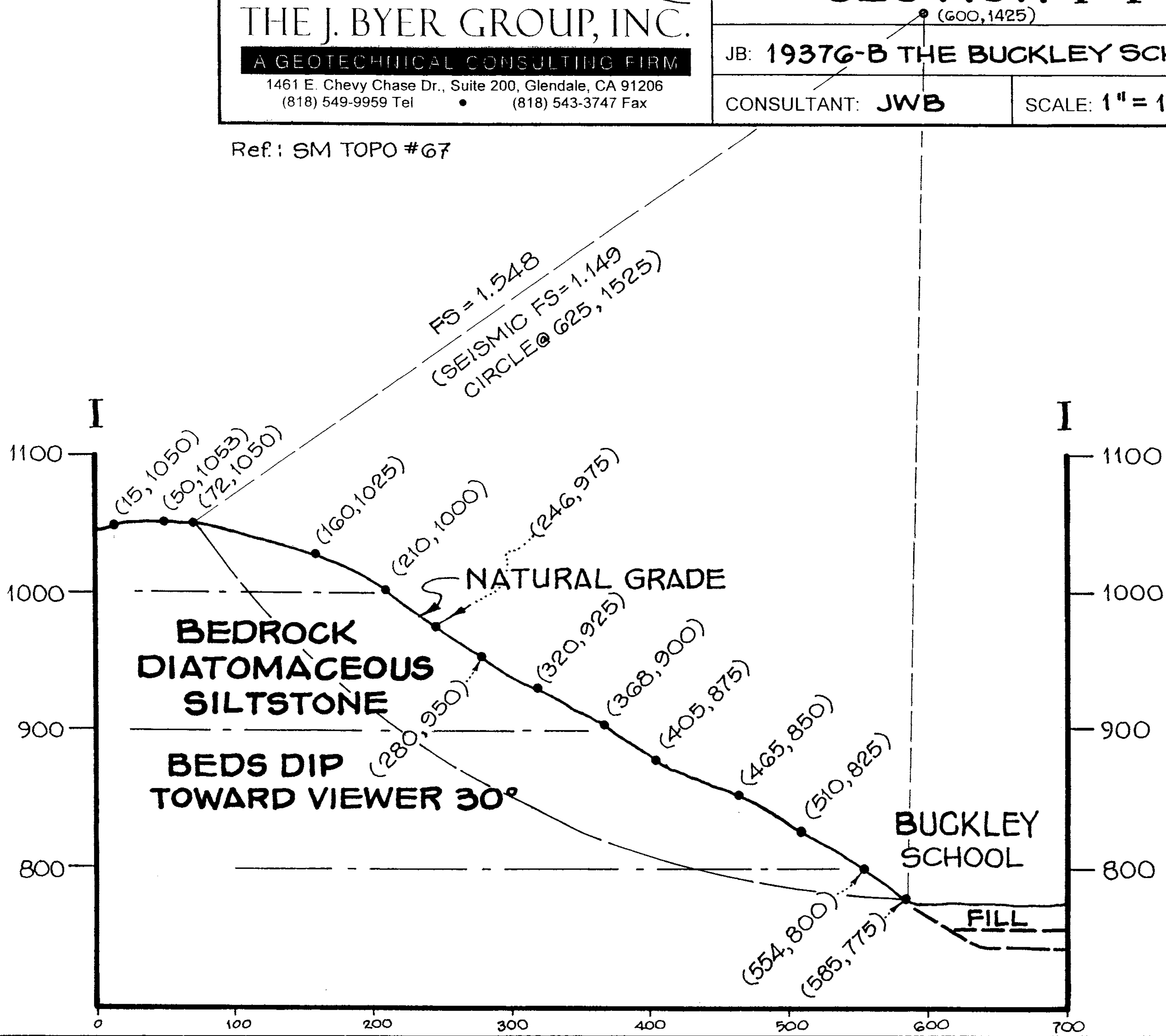
SECTION I-I

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JWB

SCALE: 1" = 100'

Ref.: SM TOPO #67



JUNE 6, 2006

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM

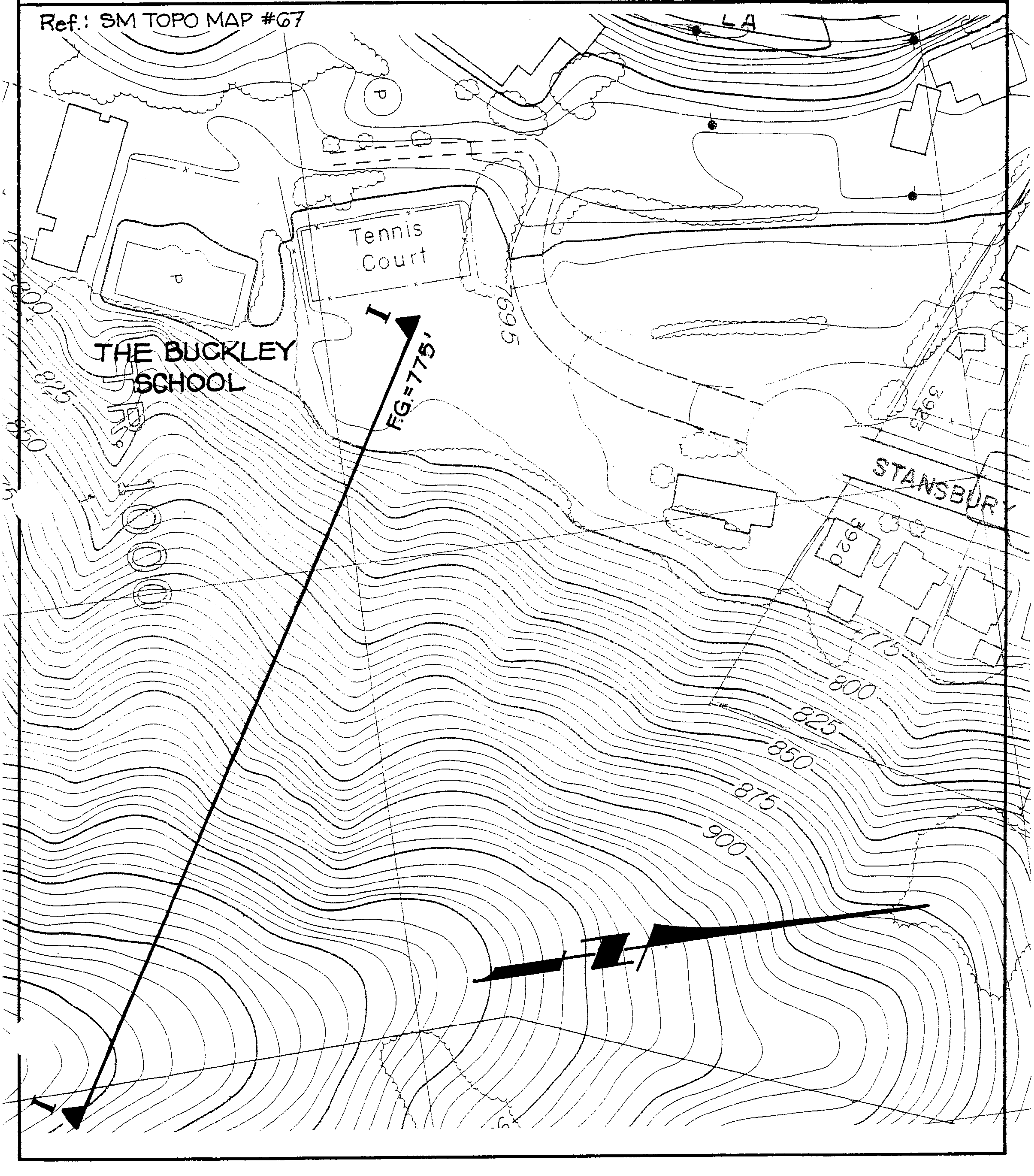
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

SLOPE STABILITY MAP

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JWB | SCALE: 1" = 100'

Ref.: SM TOPO MAP #67



THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM

SURFICIAL STABILITY

JB: **19376-B** CONSULT: **JWB**
CLIENT: **BUCKLEY SCHOOL**

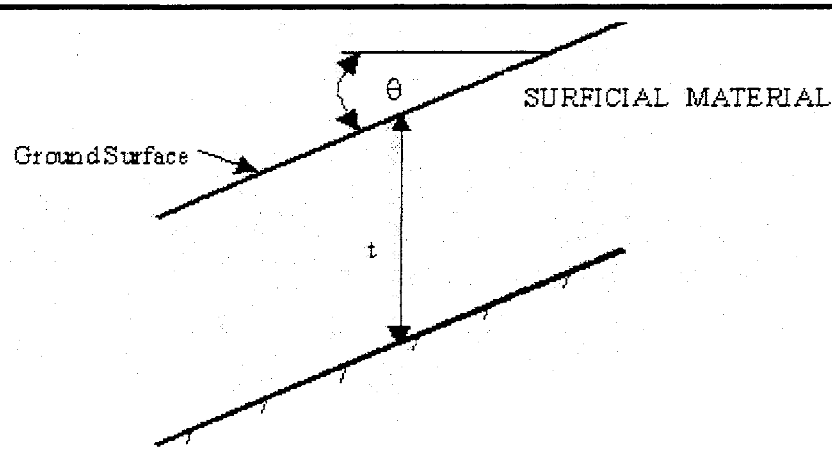
CALCULATION SHEET # 7

CALCULATE THE SURFICIAL STABILITY OF THE EARTH MATERIAL USING THE INFINITE SLOPE ANALYSIS WITH PARALLEL SEEPAGE. THIS METHOD WAS RECOMMENDED BY THE ASCE AND THE BUILDING AND SAFETY ADVISORY COMMITTEE (8/16/78). MODIFIED FROM SKEMPTON & DeLORY, 1957.

CALCULATION PARAMETERS

EARTH MATERIAL: SOIL

COHESION:	250 psf	SHEAR DIAGRAM:	3
PHI ANGLE:	22 degrees	SLOPE ANGLE:	34 degrees
DENSITY:	120 pcf	SATURATION DEPTH (t):	3.0 feet



$$FS = \frac{C + (\gamma_{soil} - \gamma_{water}) \bullet t \bullet \cos^2\theta \tan\Phi}{\gamma_{soil} \bullet t \bullet \cos\Phi \sin\Phi}$$

SAFETY FACTOR = 1.79

CONCLUSIONS:

THE CALCULATION INDICATES THAT UNIFORM SLOPES IN SOIL ARE SURFICIALLY STABLE.

THE J. BYER GROUP, INC.

A GEOTECHNICAL CONSULTING FIRM

RETAINING WALL

JB: **19376-B** CONSULTANT: **JET**
CLIENT: **BUCKLEY SCHOOL**

CALCULATION SHEET # 8

CALCULATE THE DESIGN MINIMUM EQUIVALENT FLUID PRESSURE (EFP) FOR PROPOSED RETAINING WALL SUPPORTING BEDROCK. ASSUME BACKFILL IS SATURATED AND THERE IS NO HYDROSTATIC PRESURE THE RETAINED HEIGHT AND BACKSLOPE AND SURCHARGE CONDITIONS ARE LISTED BELOW. USE THE MONONOBE-OKABE METHOD FOR SEISMIC FORCES.

CALCULATION PARAMETERS

EARTH MATERIAL:	FILL	WALL HEIGHT	25 feet
SHEAR DIAGRAM:	1	BACKSLOPE ANGLE:	0 degrees
COHESION:	255 psf	SURCHARGE:	0 pounds
PHI ANGLE:	27.5 degrees	SURCHARGE TYPE:	U Uniform
DENSITY	120 pcf	INITIAL FAILURE ANGLE:	22 degrees
SAFETY FACTOR:	1.5	FINAL FAILURE ANGLE:	70 degrees
WALL FRICTION	0 degrees	INITIAL TENSION CRACK:	3 feet
CD (C/FS):	170.0 psf	FINAL TENSION CRACK:	50 feet

PHID = ATAN(TAN(PHI)/FS) = 19.1 degrees

HORIZONTAL PSEUDO STATIC SEISMIC COEFFICIENT (k_h) 0 %g

VERTICAL PSEUDO STATIC SEISMIC COEFFICIENT (k_v) 0 %g

CALCULATED RESULTS

CRITICAL FAILURE ANGLE	55 degrees
AREA OF TRIAL FAILURE WEDGE	214.3 square feet
TOTAL EXTERNAL SURCHARGE	0.0 pounds
WEIGHT OF TRIAL FAILURE WEDGE	25720.0 pounds
NUMBER OF TRIAL WEDGES ANALYZED	2352 trials
LENGTH OF FAILURE PLANE	26.2 feet
DEPTH OF TENSION CRACK	3.6 feet
HORIZONTAL DISTANCE TO UPSLOPE TENSION CRACK	15.0 feet
CALCULATED HORIZONTAL THRUST ON WALL	**13409.0 pounds**
CALCULATED EQUIVALENT FLUID PRESSURE	**42.9 pcf**
DESIGN EQUIVALENT FLUID PRESSURE	**43.0 pcf**

THE CALCULATION INDICATES THAT THE PROPOSED RETAINING WALL MAY BE DESIGNED FOR AN EQUIVALENT FLUID PRESSURE OF 43 POUNDS PER CUBIC FOOT.

THE J. BYER GROUP, INC.

A GEOTECHNICAL CONSULTING FIRM

SHORING PILE

JB: **19376-B** CONSULT: **JET**
CLIENT: **BUCKLEY SCHOOL**

CALCULATION SHEET # **9**

CALCULATE THE DESIGN MINIMUM EQUIVALENT FLUID PRESSURE (EFP) FOR PROPOSED SHORING PILES. THE RETAINING HEIGHT AND BACKSLOPE AND SURCHARGE CONDITIONS ARE LISTED BELOW. ASSUME THE BACKFILLL IS SATURATED WITH NO EXCESS HYDROSTATIC PRESSURE. USE THE MONONOBE-OKABE METHOD FOR SEISMIC FORCES.

CALCULATION PARAMETERS

EARTH MATERIAL:	FILL	RETAINED LENGTH	20 feet
SHEAR DIAGRAM:	1	BACKSLOPE ANGLE:	0 degrees
COHESION:	255 psf	SURCHARGE:	0 pounds
PHI ANGLE:	27.5 degrees	SURCHARGE TYPE:	U Uniform
DENSITY	123 pcf	INITIAL FAILURE ANGLE:	30 degrees
SAFETY FACTOR:	1.5	FINAL FAILURE ANGLE:	70 degrees
PILE FRICTION	0 degrees	INITIAL TENSION CRACK:	2 feet
CD (C/FS):	170.0 psf	FINAL TENSION CRACK:	40 feet

PHID = ATAN(TAN(PHI)/FS) = 19.1 degrees

HORIZONTAL PSEUDO STATIC SEISMIC COEFFICIENT (k_h) 0 %g

VERTICAL PSEUDO STATIC SEISMIC COEFFICIENT (k_v) 0 %g

CALCULATED RESULTS

CRITICAL FAILURE ANGLE	55 degrees
AREA OF TRIAL FAILURE WEDGE	133.6 square feet
TOTAL EXTERNAL SURCHARGE	0.0 pounds
WEIGHT OF TRIAL FAILURE WEDGE	16432.4 pounds
NUMBER OF TRIAL WEDGES ANALYZED	1599 trials
LENGTH OF FAILURE PLANE	19.2 feet
DEPTH OF TENSION CRACK	4.3 feet
HORIZONTAL DISTANCE TO UPSLOPE TENSION CRACK	11.0 feet
CALCULATED THRUST ON PILE	**8077.6 pounds**
CALCULATED EQUIVALENT FLUID PRESSURE	**40.4 pcf**
DESIGN EQUIVALENT FLUID PRESSURE	**43.0 pcf**

THE CALCULATION INDICATES THAT THE PROPOSED SHORING PILES MAY BE DESIGNED FOR AN EQUIVALENT FLUID PRESSURE OF 43 POUNDS PER CUBIC FOOT. THE FLUID PRESSURE SHOULD BE MULTIPLIED BY THE PILE SPACING.

APPENDIX II - PREVIOUS WORK

GeoSoils Geotechnical Investigation, prepared by GeoSoils, Inc., dated March 24, 1994 (20 Pages)

LADBS Letter, dated June 20, 1994 (3 Pages)

Converse Compaction Report - Administration Building, dated August 7, 1972, with LADBS Letter (7 Pages)

Converse - Report on Compacted Fill - Classrooms, dated August 14, 1972, with LADBS Letter (8 Pages)

Converse - Report on Field Density Tests - Blanket Fill Slope - Proposed Athletic Field, dated May 24, 1971, with LADBS Letter (7 Pages)

Converse - Report on Compacted Fill - Proposed Library, dated September 25, 1972, with LADBS Letter (9 Pages)

Converse - Final on Pavilion With Map, dated June 8, 1977, with LADBS Letter (12 Pages)

Converse - Report on Compacted Fill - Maintenance Building, dated December 13, 1972 (8 Pages)

Advanced Foundation Engineering - Soil Compaction Tests - Progress Report, dated February 16, 1968 (5 Pages)

Advanced Foundation Engineering - Soil Compaction Tests - Progress Report No. 2, dated April 4, 1968 (8 Pages)

Advanced Foundation Engineering - Soil Compaction Tests - Final Report, dated April 12, 1968, with LADBS Letter (6 Pages)

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MAY 24 1994

DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

GEOTECHNICAL INVESTIGATION
of Elementary School Building
3900 Stansbury Avenue
Portion of Lot 1, Tract 23823
Sherman Oaks, California

for

The Buckley School

W.O. 4213-VN March 24, 1994

March 24, 1994
W.O. 4213-VN

The Buckley School
3900 Stansbury Avenue
Sherman Oaks, California 91413-5949

Subject: Geotechnical Investigation of Elementary School Building
3900 Stansbury Avenue, Portion of Lot 1, Tract 23823
Sherman Oaks, California

Gentlemen:

As requested, GeoSoils, Inc., has completed a geotechnical engineering study to evaluate earth materials present below one of the elementary school buildings. The building was damaged by the January 17, 1994, earthquake. The following tasks were completed as a part of this geotechnical evaluation:

1. Reviewing prior geotechnical reports pertaining to the site. The reports that were reviewed are referenced.

2. Completing a floor level manometer survey to assess damage to the structure. The results of the manometer survey are included in this report as Plate 3.

3. Excavation, logging and sampling of five exploratory borings with a limited access drill rig. Logs of the borings are included as Plates A-1 through A-7. The approximate locations of the borings are shown on the enclosed Boring Location Map, Plate 1. Subsurface interpretations of the earth materials are shown on the Cross-Sections, Plate 2.

4. Laboratory testing of earth materials sampled from the excavations. The results of the laboratory testing are summarized in Appendix A.

5. Engineering analyses of the data and preparation of this report.

SITE LOCATION

The Buckley school is located at the southern terminus of Stansbury Avenue in Sherman Oaks. The school grounds are located in a north/south trending canyon area, which has been modified by mass grading in the past. The subject elementary school building is the first structure on the west side, as you enter the school grounds from Stansbury Avenue.

SITE DESCRIPTION

The subject elementary school building is a single-story, wood frame, slab-on-grade structure. A 10 to 21-foot high, 2:1 gradient manufactured fill slope, descends from the east side of the building site down to the main parking lot. The building is located within five feet of the top of the east-facing fill slope. There is a playground area along the north side of the building. A 15± foot, 2:1 gradient manufactured fill slope descends towards the north below the playground area. There is a block fence located immediately along the top of the fill slope that descends east and north from the playground. Additional structures and an asphalt court area are located at the same grade as the subject building south and west of it.

SITE HISTORY

Preliminary geotechnical studies for the elementary school were completed in 1967 by Advanced Foundation Engineering Incorporated. At the time of that investigation, a graded pad had already existed at the present location of the elementary school. The original graded pad was approximately ten feet lower in elevation than the current pad. Borings excavated in the vicinity of the subject elementary school building indicated that the pad was underlain by artificial fill, natural soil and bedrock. The report recommended removal of old fill and unsuitable natural ground prior to placement of additional fill.

Final reports of grading for the elementary school site were completed by Advanced Foundation Engineering, Inc., in 1968. The reports indicate that a non-structural and a structural fill were placed as a part of the grading. The limits of the structural and non-structural fill are shown on Plate 1. The report indicates that all structural fill was placed on natural soil and compacted to 90 percent relative density Based upon our interpretations, removals of existing materials were made prior to the placement of the fill. The non-structural fill was placed directly on top of existing ground without any removal of existing material.

EARTH MATERIALS

Based upon our interpretations of the referenced materials and our observations made during this investigation, it appears that the subject building is underlain by compacted fill, natural soil and bedrock.

Compacted Fill: (Caf(s))

The entire structure is underlain by compacted fill materials. Depth of compacted fill observed in the borings ranged from 15 to 30 feet in thickness. The fill is comprised predominately of a mixture of silt and clay, with some sand and rock fragments. Final reports of grading indicate that in addition to reuse of on-site materials, additional fill materials were also imported to the site.

Natural Soil/Alluvium

Observations made in the borings indicate that the compacted fill materials were placed on top of natural soil/alluvium. The thickness of the alluvium ranged from 5 to 16 feet in the borings. The natural soil consisted of a mixture of clay, silt and fine sand with scattered rock fragments. Caliche stringers were observed within the natural soil.

Bedrock (Tm):

Bedrock was encountered in all 5 test borings at depths between 20 and 40.5 feet below existing ground surface. The bedrock consist of interbedded diatomaceous siltstones and sandstones.

OBSERVED DISTRESS

The manometer survey indicates that a maximum differential of 6.2 inches exist across the floor slab within the building. The survey suggest that settlement has occurred along the portion of the structure closest to the descending fill slope. Distress to door jambs and windows indicate settlement on the east side of the building. Where floor coverings were removed, several cracks were observed in the floor slab.

In the playground area, on the north side of the building, an open ground fissure traverses in an north/south direction across the playground. The block fence located along the top of the descending fill slope, adjacent to the playground area, was observed to be severely damaged.

CONCLUSIONS

Based upon available data and on the results of our field investigation and laboratory testing, it is our opinion that most of the observed distress appears to have resulted from differential settlement of the fill and alluvial material underneath the structure and possibly slope creep on the east-facing, descending fill slope. This toe of the east-facing, descending fill slope is within the designated non-structural fill material. The vibrations and lateral movements generated during the recent January 17, 1994, earthquake, may have increased and/or hastened local settlement (consolidation) of the underlying fill/alluvium.

The results of the manometer survey indicates a high point at the southwesterly portion of the structure (elevation of +1.4 inches), and a low point at the northeasterly portion of the structure (elevation of -4.8 inches). The northwesterly portion has a manometer elevation of -0.2 inches, while the southeasterly portion has a manometer elevation of -2.0 inches. The manometer data follows the trend of increasing thickness of fill and alluvial material. The thicker the fill and alluvial material, the greater the settlement.

The following factors may have contributed to the distress of the structure.

1. **Loose Compacted Fill and Alluvium**

Our laboratory density tests (see Table I), indicates that the on-site soil materials are loose and has a range of relative compaction of 71 to 86 percent (fill), and 76 to 89 percent (alluvium). It should be noted that the standard of compaction during 1968, when the fill was processed, was lower than todays standard.

The loosely compacted material and the alluvium, which have high consolidation potential, is a major factor which caused the distress of the foundation pad.

2. **Creep and/or Settlement of Adjacent Descending Slope**

The adjacent toe of the descending fill slope is founded within the designated non-structural fill, i.e., the fill slope toe was placed directly on top of the original ground without any removal (reprocessing) of loose soil material. Settlement of the loose original ground will cause settlement and lateral movement (creep) of the fill slope above. We anticipate that settlement and creep of the adjacent fill slope may have also been a contributing factor to the distress of the foundation pad above.

3. **Earthquake Shaking**

We suspect that the vibrations ad lateral movement (shaking) generated during the recent January 17, 1994 earthquake, may have increased and/or hastened local consolidation settlement of the loose fill and alluvium material, causing the building pad to undergo additional differential settlement.

RECOMMENDATIONS

The following can be used for remedial repair of the distressed foundation and pad; 1) soil improvement, and 2) remedial underpinning.

1. **Soil Improvement**

Soil improvement is the collective term for any physical, chemical, or biological method, or any combination of such methods, employed to improve certain properties of a natural or fill soil to make it serve adequately and intended for engineering purposes. For this particular site, compaction grouting, chemical grouting, slurry grouting, and lime injection may be considered to densify and strengthen the site soil, and therefore, reduce the future settlement. However, it is our opinion that grouting will not be effective due to the low permeability of some layers of the soil deposit, i.e., layers of silt and clay material. A reliable company experience with the above methods should be consulted.

2. **Remedial Underpinning**

Underpinning structures involves the introduction of additional support to the foundation of a structure to deepen or increase its bearing capacity. If done because the foundation is inadequate, it is called remedial underpinning.

Based upon our evaluation, remedial underpinning such as cast-in-place piles or caissons, chance anchors, mini-piles or the perma-jack system, will be the most effective method to reduce the future settlement. Reference materials of chance anchors, mini-piles and the perma-jack system are presented in Appendix B. Companies experienced with the above underpinning methods should be consulted. Recommendations for cast-in-place piles or caissons are presented in Appendix C.

3. **Potential Future Distress of Slab-On-Grade**

The remedial underpinning can stabilize the wall frames of the building and has less effect on the slab-on-grade unless the slab is rigidly tied with the wall frames. If the slab-on-grade is not tied with the frame, it may have future distress even after the building load is transferred to the subsurface competent layer. However, after the installation of underpinning structures, the building load will be transmitted to the subsurface competent layer, and the near surface soil in proximity to the underpinning structures will not be subjected to vertical dead load except that from slab-on-grade. Additionally, however saturation of the subgrade material may cause additional settlement. Therefore, we expect that the potential distress of the slab-on-grade is low if the structure strength of the slab is adequate and saturation of the subgrade soil is prevented. Note that because of its loose consistency, the on-site subgrade (fill and alluvium) will continue to settle slowly and the slab-on-grade will be affected by this normal consolidation settlement of the loose subgrade. After releveling the structure, the subgrade area under the slab should be leveled off by either hole grouting through the slab or by complete slab removal then replacement after adding compacted fill to level the subgrade area.

4. **Cosmetic Repairs**

Cosmetic repairs should be made only after the required underpinning has been done and the structure re-leveled.

5. **Drainage**

On-site drainage should be corrected to the extent that no water is allowed to pond next to the structure. Improvement of the drainage may help to mitigate future settlement of the slab-on-grade subgrade by not increasing the on-site soil moisture.

RECOMMENDATIONS FOR REMEDIAL REPAIR

It is our recommendation that remedial underpinning such as cast-in-place piles or caissons, chance anchors, mini-piles or a perma-jack system be employed to mitigate the future settlement of the building. The building load should be transferred to the competent bedrock layer, which ranges from 20 to 25 feet on the west side and is about 38 to 40 feet below the existing ground surface on the east side of the structure. An underpinning contractor should be consulted for the final evaluation of applicable methods and workability. A check of utility line locations will be necessary prior to underpinning and a check of utility line leaks after underpinning and releveling. The soil characteristics at the pile shaft/soil interface will be forwarded once a remedial underpinning method is chosen. It should be noted that no additional soil values are necessary if the perma-jack system is chosen.

LIMITATION

The analyses, conclusions and recommendations contained in this report are based on site conditions as they presently exist, and we further assume that the exploratory borings are representative of subsurface conditions through the site. Since our investigation is based on the site materials observed, selective laboratory testing and engineering analyses, the conclusions and recommendations contained herein are professional opinions. Further, these opinions have been derived in accordance with current standards of practice, and no warranty is expressed or implied.

We appreciate the opportunity to provide this geotechnical engineering service. If you have any questions regarding this report, please do not hesitate to contact us.

Very truly yours,

GEOSOILS, INC.

REGISTERED PROFESSIONAL ENGINEER
WILLIAM A. CIRIDON
No. GE 217
Exp. 3-31-96
GEOTECHNICAL
STATE OF CALIFORNIA

WILLIAM A. CIRIDON
GE 217

MARK A. SWIATEK
CEG 1781

WAC.MAS/mm.A99:4392

Encl: References
Plate 1, Boring Location Map
Plate 2, Cross-Sections
Plate 3, Manometer Survey
Table I, Relative Compaction of On-Site Material
Appendix A, Field Exploration and Laboratory Testing
Plates A-1 through A-7, Boring Logs
Plates SH-1 through SH-4, Shear Test Diagrams
Plates C-1 through C-8, Consolidation Tests
Appendix B, Chance Anchors, Mini-piles and Perma-Jack System
Appendix C, Vertical and Lateral Soil Resistance for Conventional Underpinning Piles/Caissons

cc: (1) Addressee
(1) Ghodsi and Associates, Inc.
(6) RTK and Associates

March 24, 1994
W.O. 4213-VN

REFERENCES

1. Allen W. Hazard, October 25, 1967, "Geologic Examination of Buckley Schools Property, Part of Lot 1108, Tract 1000, City of Los Angeles, at 3190 Stansbury Avenue, Sherman Oaks, California".

2. Advanced Foundation Engineering Incorporated, October 30, 1967, "Foundation Investigation Proposed New Buckley School Complex, 3190 Stansbury Avenue, Sherman Oaks, California".

3. Advanced Foundation Engineering Incorporated, February 16, 1968, "Soil Compaction Tests, Progress Report."

4. Advanced Foundation Engineering Incorporated, April 4, 1968, "Soil Compaction Tests, Progress Report #2."

5. Advanced Foundation Engineering Incorporated, April 12, 1968, "Soil Compaction Test, Final Report on Structural Areas."

6. Advanced Foundation Engineering Incorporated, April 18, 1968, "Supplemental Report to our Final Compaction Report on Structural Areas dated April 12, 1986".

March 24, 1994
W.O. 4213-VN

TABLE II

Relative Compaction of On-Site Material

Boring No. and Depth	On-Site		Maximum Laboratory Dry Density (pcf)	% Relative Compaction	Remarks
	Dry Unit Wt. (pcf)	Moisture (%)			
B-1 @ 2'	---	8.6	122.0	---	Fill
B-1 @ 5'	102.5	12.7	122.0	84.0	Fill
B-1 @ 10'	101.2	17.4	122.0	83.0	Fill
B-1 @ 15'	103.3	13.5	122.0	84.7	Fill
B-1 @ 20'	96.3	9.8	122.0	78.9	Fill
B-1 @ 25'	98.8	12.0	122.0	81.0	Alluvium
B-1 @ 30'	103.9	14.2	122.0	85.2	Alluvium
B-1 @ 35'	106.1	13.6	122.0	87.0	Alluvium
B-2 @ 3'	103.1	18.6	126.0	81.8	Fill
B-2 @ 8'	104.4	18.2	122.0	85.6	Fill
B-2 @ 13'	101.9	21.1	122.0	83.5	Fill
B-2 @ 18'	93.0	24.1	122.0	76.2	Alluvium
B-3 @ 4'	101.7	21.8	126.0	80.7	Fill
B-3 @ 9'	104.2	19.8	126.0	82.7	Fill
B-3 @ 14'	103.1	20.6	122.0	84.5	Fill
B-3 @ 20'	86.2	33.7	122.0	70.7	Fill

TABLE I

Relative Compaction of On-Site Material

Boring No. and Depth	On-Site		Maximum Laboratory Dry Density (pcf)	% Relative Compaction	Remarks
	Dry Unit Wt. (pcf)	Moisture (%)			
B-4 @ 5'	89.2	28.9	122.0	73.1	Fill
B-4 @ 10'	97.0	24.1	122.0	79.5	Fill
B-4 @ 15'	100.7	23.6	122.0	82.5	Fill
B-4 @ 20'	95.9	22.5	122.0	78.6	Alluvium
B-5 @ 3'	94.7	24.2	122.0	77.6	Fill
B-5 @ 8'	88.1	26.7	122.0	72.2	Fill
B-5 @ 13'	96.8	23.2	122.0	79.3	Fill
B-5 @ 18'	105.0	16.3	122.0	86.1	Fill
B-5 @ 25'	102.5	15.5	122.0	84.0	Fill
B-5 @ 30'	108.2	16.1	122.0	88.7	Alluvium
B-5 @ 35'	101.0	21.2	122.0	82.8	Alluvium

BORING LOG

GeoSoils, Inc.

W.O. 4213-VN

PROJECT: BUCKLEY SCHOOL

BORING LOG B-1 SHEET 1 OF 2

DATE EXCAVATED 2-23-94

SAMPLE METHOD: 8-inch ϕ H.S.
140 lbs., 30-inch Drop

☒ Standard Penetration Test
∿ Water Seepage into Hole
▨ Ring Sample

Depth (ft.)	Sample: Bulk	Sample: Undisturbed	Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)	Description of Material
							COMPACTED FILL: (Caf) 0 - 22'
0 - 5	▨	▨	12 22 34	SM/SC	--	8.6	0 - 2', Dark brown, silty fine SAND, moist, loose, some organic roots. @ 2', Light brown, clayey, silty fine to medium SAND with scattered small shale fragments, caliche, moist, medium dense to dense, dark brown, silty fine SAND lenses @ 4 - 5' and loose.
5		▨	5 8 13	SM/SC	102.5	12.7	@ 5', Dark brown, clayey, silty fine to medium SAND scattered with some 1" diameter small rocks, loose, moist, occasionally with sandy clay lenses. @ 8 1/2 - 10', Dark brown, sandy CLAY and clayey fine sand in layers, plastic.
10		▨	14 19 32	CL	101.2	17.4	@ 10', Dark brown, silty, sandy CLAY with scattered rocks up to 2" diameter and sandstone shale fragments, moist, medium stiff to stiff, plastic.
15		▨	15 31 46	CL	103.3	13.5	@ 15', Dark brown, sandy CLAY with scattered rocks (rock greater than 2" diameter, moist, stiff to very stiff.
20		▨	21 27 30	ML/SM	96.3	9.8	@ 20', Tan, brown, silty fine SAND, shale fragments, caliche, oxidized with piece of root, moist.
							ALLUVIUM: (Qal) 22 - 38'
25		▨	10 18 26	ML/SM	98.8	12.0	@ 25', Brown, light gray, fine SAND/SILT shale fragments with organic roots, caliche, moist, stiff, plastic.
30		▨	12 18 22	CL	103.9	14.2	@ 30', Dark brown, sandy CLAY with 1 1/2" diameter light brown, siltstone fragments, stiff to very stiff, caliche, moist. Stiff, plastic.
35		▨	11 22 34	CL	106.1	13.6	@ 35', Dark brown, sandy, silty CLAY, moist, very stiff, caliche, porous.
							BEDROCK: (Tm) 38' - 45'

GeoSoils, Inc. PLATE A-1

BORING LOG

GeoSoils, Inc.

W.O. 4213-VN

PROJECT: **BUCKLEY SCHOOL**

BORING LOG B-1 SHEET 2 OF 2

DATE EXCAVATED 2-23-94

SAMPLE METHOD: 8-inch ϕ H.S.
140 lbs., 30-inch Drop

⊠ Standard Penetration Test
∿ Water Seepage into Hole
▨ Ring Sample

Depth (ft.)	Sample: Bulk	Sample: Undisturbed	Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)		Description of Material
40		▨	31 36 50/3"	BR	100.6	18.6		@ 40', Bedrock, yellowish-brown, silty SANDSTONE bedrock, very oxidized, moist, hard to very hard.
			50/3"		NR			
45		▨		BR				@ 45', Dark brown SILT/fine sandstone bedrock, slightly moist, hard to very hard.
								Total Depth 45' No Water
50								
55								
60								
65								
70								
75								

BORING LOG

GeoSoils, Inc.

W.O. 4213-VN

PROJECT: BUCKLEY SCHOOL

BORING LOG B-2 SHEET 1 OF 1

DATE EXCAVATED 2-23-94

SAMPLE METHOD: 8-inch Ø H.S.
140 lbs 30-inch Drop

Standard Penetration Test — Water Seepage into Hole

Ring Sample

Depth (ft.)	Sample: Bulk	Sample: Undis-turbed	Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)	Description of Material
							COMPACTED FILL: (Caf) 0 - 15' 0 - 2', Dark brown, silty fine SAND with organic roots, loose, wet. @ 2 - 3', Light brown, silty fine to medium SAND, occasional with small rocks, loose, moist.
		Ring	18 15 15	CL/SM	103.1	18.6	@ 3', Dark brown, sandy CLAY with silty fine sand in layers, moist, stiff, medium dense, occasional with small rocks and some organic roots. Medium plastic.
5							
		Ring	10 16 23	SC/CL	104.4	18.2	@ 8', Brown, clayey, silty fine SAND with sandy clay lenses, moist, loose to medium dense. One organic root tip of sampler.
10							
		Ring	10 22 34	SC/CL	101.9	21.1	@ 13', Dark brown, clayey silty, fine SAND with clay lenses, moist, medium dense to dense, slight caliche.
15							**ALLUVIUM: (Qal) 15 - 20'**
		Ring	14 25 38	ML	93.0	24.1	@ 18', Yellowish-brown, clayey fine, sandy SILT, caliche, moist (near optimum), medium dense to dense, porous, increased moisture and wet @ approximately 21'.
20							**BEDROCK: (Tm) 20 - 35'**
25		Ring	17 34 49	BR	91.6	26.1	@ 25', White brown, yellowish-brown, tan clayey SILTSTONE, oxidized, moist, firm.
30		Ring	21 45 50/4"	BR	93.7	25.2	@ 30', Tan, SILTSTONE BEDROCK, oxidized, moist, hard to very hard.
35		Ring	36 50/4"	BR	89.6	29.4	@ 35', Brown, light gray SILTSTONE bedrock, oxidized, moist, hard to very hard. Total Depth 35' No Water No Caving

BORING LOG

GeoSoils, Inc.

W.O. 4213-VN

PROJECT: BUCKLEY SCHOOL

BORING LOG B-3 SHEET 1 OF 1

DATE EXCAVATED 2-24-94

SAMPLE METHOD: 8-inch ϕ H.S.
140 lbs., 30-inch Drop

Standard Penetration Test — Water Seepage into Hole

Ring Sample

Depth (ft.)	Sample: Bulk	Sample: Undisturbed	Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)	Description of Material
0–4	X						**COMPACTED FILL: (Caf) 0 - 21'** 0 - 0.5', Asphalt concrete. 0.5 - 4', Light brown to dark brown clayey SILT/SAND with small rocks.
5		X	9 17 17	CL/SM	101.7	21.8	@ 4', Dark brown, silty, sandy CLAY with SILT/SAND lenses, shale fragments, moist, medium stiff, medium dense.
10		X	11 12 13	ML	104.2	19.8	@ 9', Dark brown, silty fine SAND with (Approximately 2 1/2" black asphalt concrete @ 10.5'), moist, loose. Change to dark brown, sandy, silty clay @ 13', moist, medium stiff, plastic.
15		X	12 18 22	CL	103.1	20.6	@ 14', Dark brown, gray, sandy CLAY, occasional with silty fine silty fine sand lenses, moist, stiff to very stiff, plastic.
20		X	18 42 44	CL	86.2	33.7	
21							**ALLUVIUM: (Qal) 21 - 25'** @ 21', Dark brown, silty sandy CLAY, moist, stiff to very stiff, plastic.
25		X	20 43 50/3"	BR	84.8	37.6	**BEDROCK (Tm)** @ 25', Tan, light brown SILTSTONE with fine sandstone bedrock, oxidized, caliche, moist, hard. Total Depth 25' No Water
30							
35							

GeoSoils, Inc.

PLATE A-4

GeoSoils, Inc.

BORING LOG

W.O. 4213-VN

PROJECT: BUCKLEY SCHOOL

BORING LOG B-4 SHEET 1 OF 1

DATE EXCAVATED 2-25-94

SAMPLE METHOD: 8-inch ϕ H.S.
140 lbs., 30-inch Drop

Standard Penetration Test — Water Seepage into Hole — Ring Sample

Depth (ft.)	Sample: Bulk	Sample: Undis-turbed	Sample: Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)	Description of Material
							COMPACTED FILL: (Caf) 0 - 20' 0 - 5', Brown, sandy, silty CLAY, scattered with small rocks and shale fragments, moist to over optimum, soft to medium stiff, medium plastic to plastic.
5		Ring	9 12 13	CL	89.2	28.9	@ 5', Brown, sandy silty CLAY with scattered small rocks and shale fragments, moist to over optimum, soft to medium stiff, plastic.
10		Ring	19 22 32	CL	97.0	24.1	@ 10', Brown, silty CLAY/sandy clay with lenses, scattered with rocks and shale fragments, some organic roots, moist, soft to medium stiff, plastic.
15		Ring	7 8 17	CL	100.7	23.6	@ 15', Dark brown, gray, sandy silty CLAY with scattered rocks and shale fragments, rotten organic and sewer smell, moist, soft to medium stiff.
20		Ring	12 21 24	SC	95.9	22.5	**ALLUVIUM: (Qal) 20-25'** @ 20', Dark brown, clayey silty SAND with shale fragments, moist, loose to medium dense, low plastic.
25		Ring	23 50/3"	BR	78.7	31.1	**BEDROCK: (Tm) 25' - 31'** @ 25', Tan, brown, SILTSTONE BEDROCK, moist, medium hard, diatomaceous, oxidized.
30		Ring	27 50/5"	BR	82.4	39.9	@ 30', Tan, brown, SILTSTONE with thin layer, fine to medium sandstone bedrock, moist, medium hard to hard, oxidized, diatomaceous. Total Depth 30' No Water
35							

BORING LOG

GeoSoils, Inc.

W.O. 4213-VN

PROJECT: BUCKLEY SCHOOL

BORING LOG B-5 SHEET 1 OF 2

DATE EXCAVATED 2-24-94

SAMPLE METHOD: 8-inch ϕ H.S
140 lbs., 30-inch Drop

☒ Standard Penetration Test
Water Seepage into Hole
▨ Ring Sample

Depth (ft.)	Bulk	Undis-turbed	Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)	Description of Material
							COMPACTED FILL: (Caf) 0 - 30' 0 - 4" Concrete slab. 4" - 12", Dark brown, silty fine SAND, loose, moist. 12" - 3', Dark brown, sandy, silty CLAY with shale fragments, roots, scattered with small rocks, moist, medium stiff to stiff, plastic.
		▨	9 12 18	CL	94.7	24.2	@ 3', Dark brown, sandy, silty CLAY with shale fragments, roots scattered with small rocks, one piece of electrical wire, moist, medium stiff to stiff, plastic.
5							
		▨	5 9 12	CL	88.1	26.7	@ 8', Dark brown, sandy, silty CLAY with scattered small rocks and shale fragments, moist, soft to medium stiff, plastic.
10							
		▨	9 18 23	CL	96.8	23.2	@ 13', Dark brown, sandy, silty CLAY with scattered rocks (approximately 1 1/2" diameter), shale fragments, moist, medium stiff to stiff, plastic.
15							
		▨	15 20 32	CL	105.0	16.3	@ 18', Dark brown, sandy, silty CLAY with scattered rocks (approximately 2" diameter), red brick and shale fragments, stiff to very stiff, plastic.
20							
25		▨	12 25 36	CL	102.5	15.5	
30		▨	13 22 38	CL/SM	108.2	16.1	ALLUVIUM: (Qal) 30 - 40' @ 30', Dark brown, silty CLAY with silty fine SAND lenses, rock (approximately 2" diameter), small shale fragments, stiff to very stiff, plastic.
35		▨	13 24 44	CL	101.0	21.2	@ 35', Dark brown, silty CLAY with silty fine sand lense, rock (approximately 2" diameter) small shale fragments, stiff to very stiff, plastic.
							@ 38', Light brown, silty CLAY, moist (over optimum) stiff,

BORING LOG

GeoSoils, Inc.

W.O. 4213-VN

PROJECT: BUCKLEY SCHOOL

BORING LOG B-5 SHEET 2 OF 2

DATE EXCAVATED 2-24-94

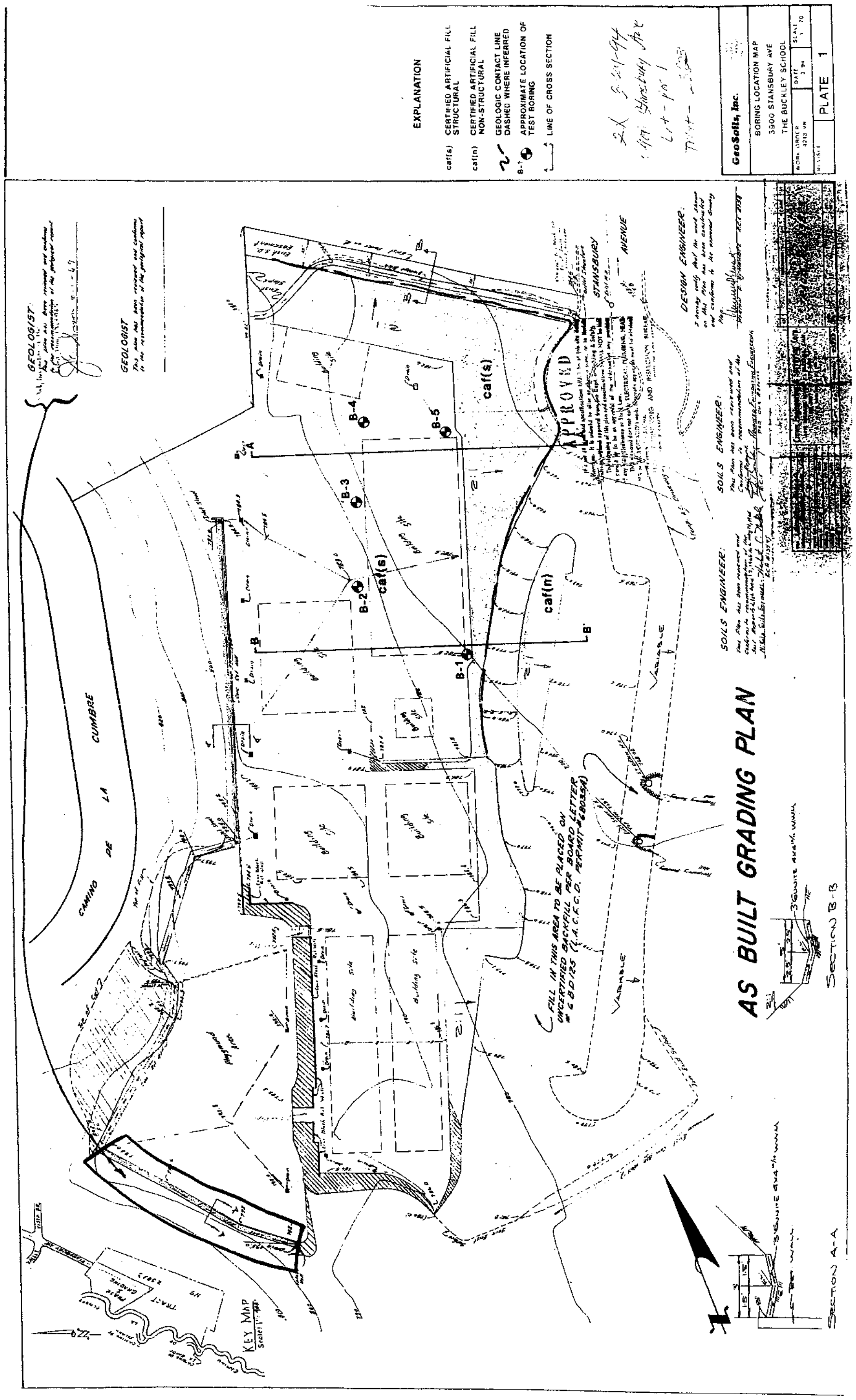
SAMPLE METHOD: 8-inch ϕ H.S.
140 lbs., 30-inch Drop

Standard Penetration Test

Water Seepage into Hole

Ring Sample

Depth (ft.)	Sample: Bulk	Sample: Undis-turbed	Sample: Blows 6"	USCS SYMBOL	Dry Unit Wt. (pcf)	Moisture (%)	Description of Material
							plastic.
40		Ring	19 50/5"	BR	68.7	51.3	**BEDROCK: (Tm) 40.5 - 45'** Yellowish-brown, SILTSTONE BEDROCK, moist, hard, oxidized caliche.
45		Ring	29 50/4"	BR	76.1	43.9	@ 45', Tan SILTSTONE BEDROCK, moist, hard to very hard, oxidized, caliche. Total Depth 45' No Water
50							
55							
60							
65							
70							
75							


EXPLANATION
caf(s) CERTIFIED ARTIFICIAL FILL STRUCTURAL
caf(n) CERTIFIED ARTIFICIAL FILL NON-STRUCTURAL
GEOLOGIC CONTACT LINE DASHED WHERE INFERRED
B-1 APPROXIMATE LOCATION OF TEST BORING
LINE OF CROSS SECTION
GeoSoils, Inc.
BORING LOCATION MAP
3900 STANSBURY AVE
THE BUCKLEY SCHOOL
PLATE 1
GEOLOGIST
CAMINO DE LA CUMBRE
STANSBURY AVENUE
APPROVED
DESIGN ENGINEER
SOILS ENGINEER
B-1
B-2
B-3
B-4
B-5
caf(s)
caf(n)
AS BUILT GRADING PLAN
FILL IN THIS AREA TO BE PLACED ON UNCERTIFIED BACKFILL PER BOARD LETTER
SECTION A-A
SECTION B-B
KEY MAP

11x17

RICHARD J. RIORDAN
MAYOR

DEPARTMENT OF
BUILDING AND SAFETY
400, CITY HALL
LOS ANGELES, CA 90012-4869
WARREN V. O'BRIEN
GENERAL MANAGER
ARTHUR J. JOHNSON, JR
EXECUTIVE OFFICER

June 20, 1994

Log # 36054
(SOILS/GEOLOGY FILE-2)

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

TRACT: 23823
LOT: Por 1
LOCATION: 3900 STANSBURY AVENUE

CURRENT REFERENCE REPORT/LETTER(S)	REPORT NO.	DATE(S) OF DOCUMENT	PREPARED BY
Soils/Geo Report	4213-VN	03/24/94	GeoSoils, Inc
Grading Ovrszd Doc	4213-VN	03/24/94	--

The subject report concerning settlement within the classroom building resulting from the Northridge earthquake has been reviewed by the Grading Division of the Department of Building and Safety. The report recommends underpinning of the building below the underlying fill and alluvium. The existing concrete slabs could then be structurally tied to the new underpinning. For reasons that are unclear, the report does not recommend compaction grouting.

It shall be understood that the proposed method of repair is not in full conformance with current Code regulations and must, therefore, be classified as remedial and intended to improve site conditions over that which presently exists.

The report is acceptable as remedial repair to improve the existing building on the site. The following conditions shall be incorporated into the plans:

1. Cast in place piles and caissons are an acceptable method of repair. The other referenced method, chance anchors, will require a special design plus product approval from Research Division prior to acceptance by the Department.

2. The soils engineer shall review and approve the detailed plans prior to issuance of any permit. This approval shall be by signature on the plans which clearly indicates that the soils engineer has reviewed the plans prepared by the design engineer and that the plans included the recommendations contained in his report.

3. The soil engineer shall inspect the excavations for the footings to determine that they are founded in the recommended strata before calling the Department for footing inspection.

4. All friction pile or caisson drilling and installation shall be performed under the continuous inspection and approval of the Foundation Engineer.

5. Pile and/or caisson foundation ties are required by Code Section 91.2908(b). Exceptions and modification to this requirement are provided in Rule of General Application 662.

6. Pile and/or caisson shafts shall be designed for a lateral load of 1000 pounds per linear foot of shaft exposed to fill, soil and weathered bedrock.

7. Footings shall be located from the face of the slope a minimum horizontal distance of H/3.

8. It shall be understood that the existing building slabs will be subject to settlement within the underpinned building if not tied to the new foundation.

9. A grading permit shall be obtained.

10. All recommendations of the report which are in addition to or more restrictive than the conditions contained herein shall be incorporated into the plans.

11. The applicant is advised that the approval of this report does not waive the requirements for excavations contained in the State Construction Safety Orders enforced by the State Division of Industrial Safety.

12. A copy of the subject and appropriate referenced reports and this approval letter shall be attached to the District Office and field set of plans. Submit one copy of the above reports to the Building Department Plan Checker prior to issuance of the permit.

13. All roof and pad drainage shall be conducted to the street in an acceptable manner.

14. Prior to the placing of compacted fill, a representative of the consulting Soils Engineer shall inspect and approve the bottom excavations. He shall post a notice on the job site for the City Grading Inspector and the Contractor stating that the soil inspected meets the conditions of the report, but that no fill shall be placed until the City Grading Inspector has also inspected and approved the bottom excavations. A written certification to this effect shall be filed with the Department upon completion of the work. The fill shall be placed under the inspection and approval of the Foundation Engineer. A compaction report shall be submitted to the Department upon completion of the compaction.

15. Prior to the pouring of concrete, a representative of the consulting Soil Engineer shall

inspect and approve the footing excavations. He shall post a notice on the job site for the City Building Inspector and the Contractor stating that the work so inspected meets the conditions of the report, but that no concrete shall be poured until the City Building Inspector has also inspected and approved the footing excavations. A written certification to this effect shall be filed with the Department upon completion of the work.

16. A registered grading deputy inspector approved by and responsible to the project geotechnical engineer shall be required to provide continuous inspection for the proposed slot cutting, underpinning, shoring, tie-back, buttress, and the drilling and installation of all deep foundations.

17. Existing uncertified fill shall not be used for lateral support of deep foundation.

LARRY WESTPHAL
Chief of Grading Division

J. W. COBARRUBIAS
Engineering Geologist III

RICARDO TRES
Structural Engineer Asst. II

JWC/RT:rlm
A:\JUN36054
(213) 485-2160

cc: GeoSoils, Inc
RTK & Assoc
VN District Office

Consulting Engineers and Geologists

CONVERSE, DAVIS AND ASSOCIATES

126 West Del Mar Boulevard, Post Office Box 1449, Pasadena, California 91105 Telephone (213) 681-1111

August 7, 1972

RECEIVED
AUG 10 1972
DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

F and A Construction Co., Inc.
1200 West 220th Street
Torrance, California 90502

Attention: Mr. William N. Weeger

Subject: Project No. 72-143-DG, Report on Compacted Fill Administration Building, High School Facilities The Buckley School, 3900 Stansbury Avenue Sherman Oaks, California TRACT 23993 LOT - 1

Gentlemen:

This is to report the results of tests and observations made during the placement of compacted fill on the subject site.

Periodic tests and inspections were provided by a representative of Converse, Davis and Associates to check the grading contractor on compliance with the drawings and job specifications. The presence of our field representative at the site was to provide to the owner a continuing source of professional advice, opinions and recommendations based upon the field representative's observations of the contractor's work and did not include any superintending, supervision or direction of the actual work of the contractor or the contractor's workmen. The opinions and recommendations presented hereafter are based on our tests and observations of the grading procedures used, and represent our engineering judgment as to the contractor's compliance with the drawings and job specifications.

The grading operation was observed to be performed in the following general manner:

1. Vegetation, surface trash and miscellaneous debris were cleared from the areas to be graded and were hauled off the property.

2. Unsatisfactory soils were excavated to expose competent materials on which to start the fill.

3. Approved soils were placed in layers on the prepared surface, and each layer was compacted to the specified density before the next layer was added.

4. Placement of the compacted fill was continued to the final grades indicated on Drawing No. 1.

5. The minimum acceptable degree of compaction was 90 percent of the maximum density.

6. Maximum density and optimum moisture content were determined by the A.S.T.M. D1557-70 method.

7. The soils used in the compacted fill consisted of clay, silt and sandy silt and were classified as moderately expansive with respect to volume-change characteristics. A list of soil types encountered during testing is presented in the "Table of Test Results."

Field density tests were made during the placement of fill to determine the degree of compaction and moisture content. Where tests or field observations indicated insufficient density, additional compaction with adjustment of the moisture content where necessary was performed before the next layer was added. All field density tests are listed in the "Table of Test Results," and their approximate locations are shown on Drawing No. 1. Also shown are the limits and depths of the controlled fill placed during this grading operation.

Undisturbed samples were obtained from the compacted fill. The samples were obtained by hand driving a thin-walled steel sampler. One sample was tested at varying normal loads in a direct shear machine to determine the Coulomb shear strength parameter. The sample was saturated and drained prior to testing. The result of the shear test is listed in the "Table of Test Results."

CONCLUSIONS AND RECOMMENDATIONS

Based on the final results of the tests, on observation of the construction procedures used in the field and on our experience, it is our opinion that the controlled compacted fill shown on Drawing No. 1 has been placed in accordance with the applicable portions of the job specifications and with the recommendations of Converse, Davis and Associates. The compacted fill discussed in this report will support spread footings, slabs-on-grade, and pavement. Any fill added beyond the limits or above the grades shown should be placed under engineering control and in accordance with the specifications, if it is to be covered by the recommendations of this report.

Footings should be at least 18 inches in width and bottomed 12 inches and 18 inches below lowest adjacent final surface on controlled compacted fill for interior and exterior footings, respectively. The permissible bearing value is 2000 pounds per square foot on the proper bearing soils, as discussed in the report of the Foundation Investigation.

Footings adjacent to the storm drain at the northwest corner of the Administration Building must be founded below a line rising at 45 degrees from the nearest point of the storm drain pipe.

It is recommended that all footing excavations be inspected by Converse, Davis and Associates prior to pouring concrete to see that they are into satisfactory soils and are free of loose and disturbed materials. If conditions are encountered during building construction that appear to be different from those presented in this report, this office should be notified.

Our findings have been obtained in accordance with accepted professional engineering practice in the fields of engineering and soil mechanics. This warranty is in lieu of all other warranties, either express or implied.

F and R Construction Co., Inc.
Project No. 73-143-DG
August 7, 1973
Page Four

The undersigned licensed Civil Engineer certifies that he has personally inspected the placement of and tested the compacted earth fill being reported, and that in his opinion the same was placed in conformity with the applicable portions of the City of Los Angeles Building Code.*

Respectfully submitted,

CONVERSE, DAVIS AND ASSOCIATES

By ______________________
Ellis J. Jones, Project Engineer

____
Reviewed and approved:
C. R. MacFadyen, Principal Engineer

EJJ/CRM:eg
Encl: Table of Test Results, Sheets 1 and 2
Drawing No. 1
Dist: (2) Addressee
(2) City of Los Angles, Department of Building and Safety, Grading Division
(2) Ragnar C. Ovale and Associates

*For the purpose of this certificate, to "have personally inspected and tested" shall include inspection and testing performed by any person or persons employed by, and responsible to the licensed Civil Engineer signing this report. Where the inspection and testing of all or part of the work above is delegated, full responsibility shall be assumed by the licensed Civil Engineer whose signature is affixed hereon.

TABLE OF TEST RESULTS

TABLE I
FIELD DENSITY TESTS

Test No.	Test Date	Test Location	Approx. Test Eleva- tion Feet	Approx. Depth of Fill Below Test-Ft.	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Com- paction
16	7/12/72	Northwest	759	2.0	101	19.5	1	92
17	7/12/72	Southeast	763	2.0	96	18.8	2	94
20	7/12/72	Center	765	4.0	101	16.7	1	92
21	7/12/72	Southwest	766	2.0	95	22.2	2	93
22	7/13/72	Northeast	768	8.0	99	19.4	1	91
23	7/13/72	Southeast	767	6.0	92	18.8	2	90
24	7/13/72	Southwest	769	8.0	96	16.8	2	94
26	7/13/72	Center	771	10.0	91	22.9	3	84
28A	7/14/72	Center	771	10.0	98	20.9	3	90

(1) Density of the compacted fill was determined in the field by the A.S.T.M. D1556-64 sand cone test. Soil samples obtained from the sand cone tests were oven-dried to obtain the field moisture content.

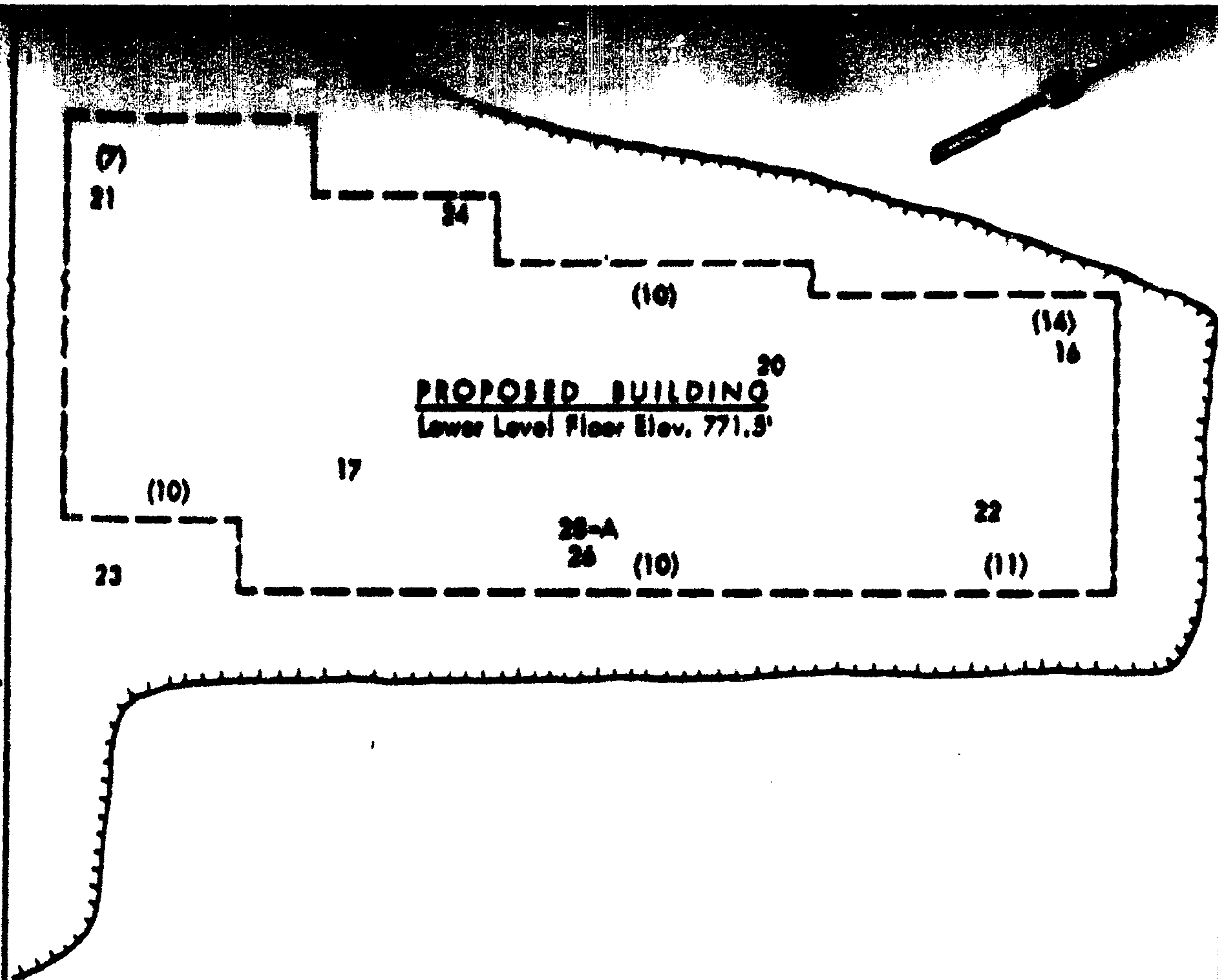
(2) Soil Type is given on Table II, Laboratory Maximum Density Tests.

A - Tests taken to recheck areas of substandard compaction.

TABLE II
LABORATORY MAXIMUM DENSITY TESTS*

Soil Type	Soil Description	Maximum Dry Density, p.c.f.	Optimum Moisture Content-Percent
1	Black CLAY	110	14.3
2	Dark Brown SILT	102	18.0
3	Brown SANDY SILT	109	16.7

*A.S.T.M. D1557-70 test method.



(10) Indicates approximate area and depth in feet of controlled compacted fill.

26 Indicates number and approximate location of field density test.

REFERENCE:
Grading plan furnished by client.

LOCATION OF CONTROLLED COMPACTED FILL

PREPARED BY: R.B.	NEW ADMINISTRATION BUILDING The Buckley School, Sherman Oaks, California for P. & A. Construction Company		DRAWING NUMBER 1
CHECKED BY HRB			
APPROVED BY	DATE Aug. 8, 1972	SCALE 1" = 20'	PROJECT NUMBER 72 - 143 - DG

CONVERSE, DAVIS AND ASSOCIATES — PASADENA · SANTA ANA, CALIFORNIA

WILLIAMS
[illegible] MANAGER

CITY OF LOS ANGELES

CALIFORNIA

DEPARTMENT OF
BUILDING AND SAFETY
[illegible]

F. & A. Construction Co., Inc.
1820 West [illegible] Street
Torrance, California 90502
Attn: Mr. William B. [illegible]

TRACT: [illegible]
LOT: 1
LOCATION: [illegible] Avenue

DATE: August 16, 1972
PERMIT: [illegible]
DM# 7357

Fill soil classification, per Table [illegible] See report

Lots having compacted fill: None

Approval is granted for compacted fill constructed on the above lots as described in the compaction report dated August 7, 1972, prepared by [illegible] Report No. 72-147-[illegible].

Approval is limited to the [illegible] and by the following requirements:

A. Footings for [illegible] are [illegible] dimensioned from Table [illegible] without use of [illegible] value.
B. Footing bearing pressure for [illegible] structures shall not exceed a value of 2000 lbs. per sq. ft. at 18 inches minimum, below approved compacted surface.
C. Continuous footings per [illegible] are required.
D. All footings supported partly or wholly on compacted fill shall be reinforced continuously with at least one number 4 bar at the top and bottom of the footing.
E. Slope erosion control, planting, and [illegible] of fill slopes, and runoff control are required as per Code Section 91.3007.
F. Building or structure footings shall be set back 5 feet from the face of slopes [illegible] feet or less in vertical height where the slope angle is between [illegible] horizontal to 1 vertical and [illegible] horizontal to 1 vertical. Where the vertical height of slope exceeds [illegible] feet and the slope angle is as described above, the setback shall be increased 1 foot for each additional 5 feet in vertical height over [illegible] feet to a maximum setback of [illegible] feet. [illegible] slopes exceeding [illegible] feet in vertical height, the setback shall be [illegible] feet except as permitted in Code Section 91.3009 [illegible].

G. Footings adjacent to the storm drain at the Northwest corner of the [illegible] Bldg. may be founded below [illegible] a line rising at [illegible] from the nearest point of the storm drain pipe. Footings to be 18" wide. [illegible] for exterior footings. Interior footings may use 12".

[illegible] WILLIAMS
[illegible] Manager

F.K. BAUER, Grading Engineer

Consulting Engineers and Geologists

CONVERSE, DAVIS AND ASSOCIATES

[illegible] West Del Mar Boulevard, Post Office Box [illegible], Pasadena, California 91109 Telephone (213) 681-[illegible]

August 14, 1972

RECEIVED
AUG 1 8 1972
DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

F and A Construction Co., Inc.
1800 West [illegible] Street
Torrance, California 90502

Attention: Mr. William N. Weager

Subject: Project No. 72-143-DH, Report on Compacted Fill Classroom Buildings, High School Facilities, The Buckley School, [illegible] Avenue, Sherman Oaks, California [illegible]-[illegible] GP-1

Gentlemen:

This is to report the results of tests and observations made during the placement of compacted fill on the subject site.

Periodic tests and inspections were provided by a representative of Converse, Davis and Associates to check the grading contractor on compliance with the drawings and job specifications. The presence of our field representative at the site was to provide to the owner a continuing source of professional advice, opinions and recommendations based upon the field representative's observations of the contractor's work and did not include any superintending, supervision or direction of the actual work of the contractor or the contractor's workmen. The opinions and recommendations presented hereafter are based on our tests and observations of the grading procedures used, and represent our engineering judgment as to the contractor's compliance with the drawings and job specifications.

The grading operation was observed to be performed in the following general manner:

1. Vegetation, surface trash and miscellaneous debris were cleared from the areas to be graded and were hauled off the property.

2. Unsatisfactory soils were excavated to expose competent materials on which to start the fill.

3. Approved soils were placed in layers on the prepared surface, and each layer was compacted to the specified density before the next layer was added.

4. Placement of the compacted fill was continued to the final grades indicated on Drawing No. 2.

5. The minimum acceptable degree of compaction was 90 percent of the maximum density.

6. Maximum density and optimum moisture content were determined by the A.S.T.M. D1557-70 method.

7. The soils used in the compacted fill consisted of clay, silt and sandy silt and were classified as moderately expansive with respect to volume-change characteristics. A list of soil types encountered during testing is presented in the "Table of Test Results."

Field density tests were made during the placement of fill to determine the degree of compaction and the moisture content. Where tests or field observations indicated insufficient density, additional compaction with adjustment of the moisture content where necessary was performed before the next layer was added. All field density tests are listed in the "Table of Test Results," and their approximate locations are shown on Drawing No. 2. Also shown are the limits and depths of the controlled fill placed during this grading operation.

Undisturbed samples were obtained from the compacted fill. The samples were obtained by hand driving a thin-walled steel sampler. The samples were tested at varying normal loads in a direct shear machine to determine the Coulomb shear strength parameter. The samples were saturated and drained prior to testing. The results of the shear tests are listed in the "Table of Test Results."

CONCLUSIONS AND RECOMMENDATIONS

Based on the final results of the tests, on observations of the construction procedures used in the field and on our experience, it is our opinion that the controlled compacted fill shown on Drawing No. 2 has been placed in accordance with the applicable portions of the job specifications and with the recommendations of Converse, Davis and Associates. The compacted fill discussed in this report will support spread footings, slabs-on-grade, and pavement. Any fill added beyond the limits or above the grades shown should be placed under engineering control and in accordance with the specifications, if it is to be covered by the recommendations of this report. Loose fill on the surface of the north slope of the Pavilion excavation is to be removed during construction of the Pavilion.

Footings should be at least 18 inches in width and bottomed 12 inches and 18 inches below lowest adjacent final surface on controlled compacted fill for interior and exterior footings, respectively. The permissible bearing value is 2,000 pounds per square foot on the proper bearing soils, as discussed in the report on the Foundation Investigation.

Footings of the west classroom building adjacent to the storm drain must be founded below a line rising at 45 degrees from the nearest point of the pipe.

It is recommended that all footing excavations be inspected by Converse, Davis and Associates prior to pouring concrete to see that they are into satisfactory soils and are free of loose and disturbed materials. If conditions are encountered during building construction that appear to be different from those presented in this report, this office should be notified.

Our findings have been obtained in accordance with accepted professional engineering practice in the fields of engineering and soil mechanics. This warranty is in lieu of all other warranties, either express or implied.

The undersigned licensed Civil Engineer certifies that he has personally inspected the placement of and tested the compacted earth fill being reported, and that in his opinion the same was placed in conformity with the applicable portions of the City of Los Angeles Building Code.*

Respectfully submitted,

CONVERSE, DAVIS AND ASSOCIATES

By [illegible]
Ellis J. Jo[illegible], Project Engineer

Reviewed and Approved:
C. R. MacFadyen, Principal Engineer

EJJ/CRM:bh
Encl: Table of Test Results, I, II and III
Drawing No. 2
Dist: (2) Addressee
(2) City of Los Angeles, Department of Building and Safety, Grading Division
(2) Ragnar C. Qvale and Associates

*For the purpose of this certificate, to "have personally inspected and tested" shall include inspection and testing performed by any person employed by, and responsible to the licensed Civil Engineer signing this report. Where the inspection and testing of all or part of the work above is delegated, full responsibility shall be assumed by the licensed Civil Engineer whose signature is affixed hereon.

TABLE OF TEST RESULTS

TABLE 1
FIELD DENSITY TESTS

Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Tests Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Compaction
1	7/6/72	East Classroom Bldg.	763	2.0	88	23.4	2	86
2A	7/6/72	East Classroom Bldg.	763	2.0	92	26.6	2	90
3	7/7/72	East Classroom Bldg.	765	4.0	92	28.6	2	90
4	7/7/72	East Classroom Bldg.	767	1.0	82	33.8	2	80
5A	7/7/72	East Classroom Bldg.	767	1.0	98	21.4	3	90
6	7/7/72	East Classroom Bldg.	769	5.0	96	21.0	2	94
7	7/7/72	East Classroom Bldg.	772	6.0	98	18.4	2	90
8	7/7/72	East Classroom Bldg.	769	3.0	93	24.8	2	91
9	7/10/72	East Classroom Bldg.	771	5.0	98	18.8	3	90
10	7/10/72	East Classroom Bldg.	775	1.0	102	16.4	1	93
11	7/10/72	East Classroom Bldg.	774	13.0	98	18.4	3	90
12	7/11/72	East Classroom Bldg.	775	9.0	92	23.9	2	90
13	7/11/72	East Classroom Bldg.	775	14.0	96	23.1	2	94
14	7/11/72	East Classroom Bldg.	776	2.0	92	19.9	2	90
15	7/11/72	East Classroom Bldg.	776	10.0	100	21.4	3	92
18	7/12/72	East Classroom Bldg.	779	13.0	93	22.4	2	91
19	7/12/72	East Classroom Bldg.	777	16.0	97	21.0	2	95
3	7/13/72	East Classroom Bldg.	780	6.0	107	17.2	1	97
27	7/14/72	East Classroom Bldg.	781	18.0	99	12.3	1	90
29	7/14/72	East Classroom Bldg.	782	16.0	96	22.6	2	94
30	7/18/72	West Classroom Bldg.	766	1.0	99	23.0	3	91
31	7/18/72	West Classroom Bldg.	764	2.0	90	21.6	3	83
32A	7/18/72	West Classroom Bldg.	764	2.0	98	20.2	3	90
33	7/18/72	West Classroom Bldg.	765	4.0	84	24.3	2	82
34A	7/18/72	West Classroom Bldg.	768	4.0	94	25.0	2	92
35	7/19/72	West Classroom Bldg.	770	5.0	90	24.0	2	88
37A	7/19/72	West Classroom Bldg.	770	5.0	97	24.0	2	95
36	7/19/72	West Classroom Bldg.	769	7.0	92	23.2	2	90
38	7/19/72	West Classroom Bldg.	773	7.0	100	21.1	3	92
39	7/19/72	West Classroom Bldg.	773	10.0	99	20.9	3	90
40	7/19/72	West Classroom Bldg.	775	8.0	102	19.8	1	93
41	7/20/72	West Classroom Bldg.	774	10.0	105	19.7	1	95
42	7/20/72	West Classroom Bldg.	777	10.0	103	23.6	1	94
43	7/21/72	West Classroom Bldg.	776	14.0	107	17.2	1	97
44	7/21/72	West Classroom Bldg.	778	11.0	92	18.8	2	90
45A	7/21/72	West Classroom Bldg.	778	11.0	96	21.8	2	94
46	7/21/72	West Classroom Bldg.	774	2.0	99	17.7	3	91

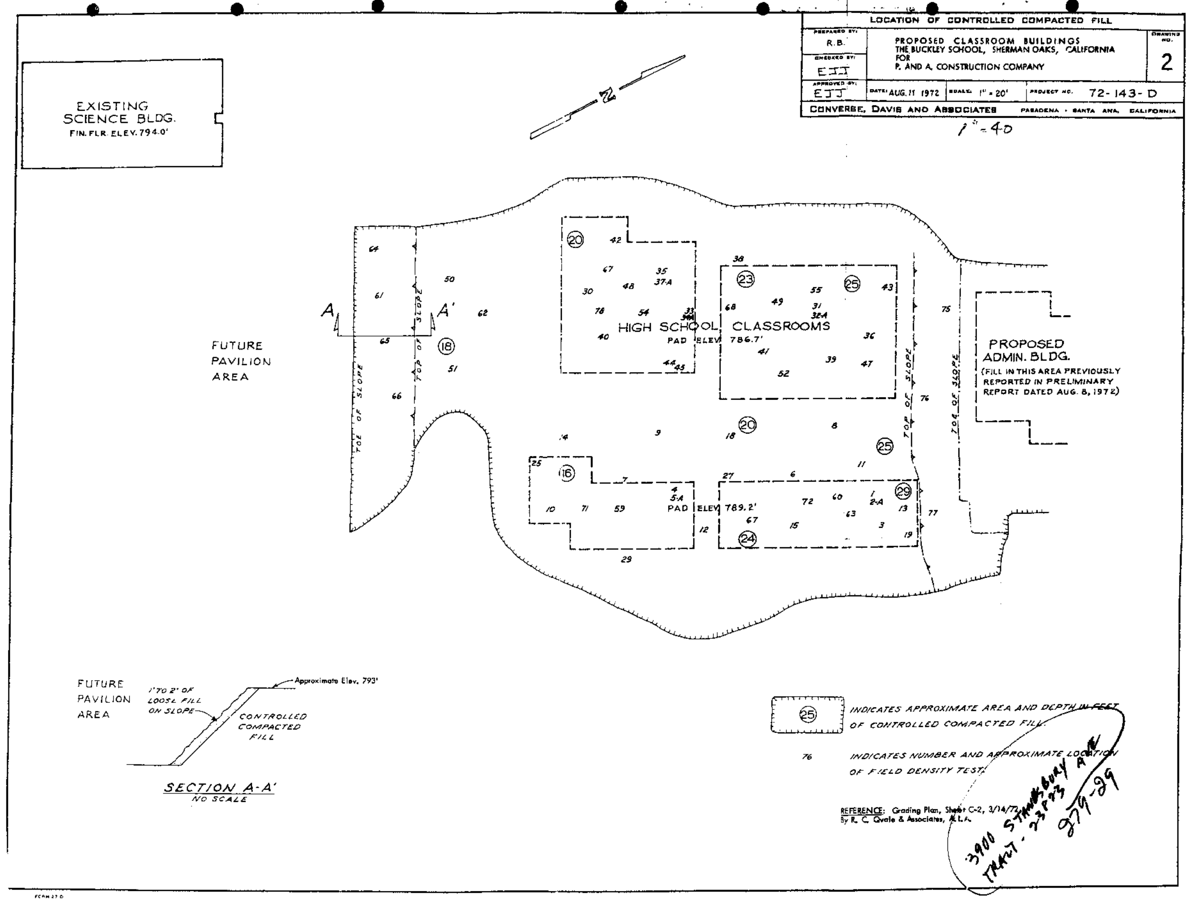
TABLE II
LABORATORY MAXIMUM DENSITY TESTS*

Soil Type	Soil Description	Maximum Dry Density, p.c.f.	Optimum Moisture Content, Percent
1	Black CLAY	110	14.3
2	Dark Brown SILT	102	18.0
3	Brown SANDY SILT	109	16.7
4	Brown SANDY SILT (Import)	121	10.2

*A.S.T.M. D1557-70 test method.

TABLE III
DIRECT SHEAR TESTS

Sample No.	Location	Depth Below Finish Grade (Feet)	c (Pounds Per Square Foot)	ϕ Degrees
1	West Classroom Bldg.	1.5	670	31
2	East Classroom Bldg.	1.5	520	28


LOCATION OF CONTROLLED COMPACTED FILL
PROPOSED CLASSROOM BUILDINGS
THE BUCKLEY SCHOOL, SHERMAN OAKS, CALIFORNIA
FOR
P. AND A. CONSTRUCTION COMPANY
PREPARED BY: R.B.
CHECKED BY: EJJ
APPROVED BY: EJJ
DATE: AUG. 11 1972
SCALE: 1" = 20'
PROJECT NO. 72-143-D
DRAWING NO. 2
CONVERSE, DAVIS AND ASSOCIATES
PASADENA · SANTA ANA, CALIFORNIA
1" = 40
EXISTING SCIENCE BLDG.
FIN. FLR. ELEV. 794.0'
FUTURE PAVILION AREA
HIGH SCHOOL CLASSROOMS
PAD ELEV. 786.7'
PAD ELEV. 789.2'
PROPOSED ADMIN. BLDG.
(FILL IN THIS AREA PREVIOUSLY REPORTED IN PRELIMINARY REPORT DATED AUG. 8, 1972)
TOP OF SLOPE
TOE OF SLOPE
A
A'
FUTURE PAVILION AREA
1' TO 2' OF LOOSE FILL ON SLOPE
Approximate Elev. 793'
CONTROLLED COMPACTED FILL
SECTION A-A'
NO SCALE
INDICATES APPROXIMATE AREA AND DEPTH IN FEET OF CONTROLLED COMPACTED FILL
76 INDICATES NUMBER AND APPROXIMATE LOCATION OF FIELD DENSITY TEST
REFERENCE: Grading Plan, Sheet C-2, 3/14/72, By R. C. Quale & Associates, A.I.A.
3900 STANSBURY AVE
TRACT - 23893
279-99

11x17

R. J. WILLIAMS
GENERAL MANAGER

DEPARTMENT OF
BUILDING AND SAFETY
800 CITY HALL
LOS ANGELES CALIF 90012

SAM YORTY
MAYOR

P. & A. Construction Co., Inc.
[redacted]
Attn: [redacted]

TRACT: [redacted]
LOT: [redacted]
LOCATION: [redacted]

DATE: [redacted]
PERMIT: [redacted]
DM# [redacted]

Fill soil classification, per Table 28-A: See report

Lots having compacted fill: [redacted]

Approval is granted for compacted fill constructed on the above lots as described in the compaction report dated [redacted], prepared by [redacted] Report No. [redacted].

Approval is limited to the area shown in the report and by the following requirements:

A: Footings for one-story wood-frame structures may be dimensioned from Table 17-B without use of the soil bearing value.
B. Footing bearing pressure for all other structures shall not exceed a value of [redacted] lbs. per sq. ft. at [redacted] inches minimum, below approved compacted surface.
C. Continuous footings per Code Section 91.3012 are required.
D. All footings supported partly or wholly on compacted fill shall be reinforced continuously with at least one number 4 bar at the top and bottom of the footing.
E. Slope erosion control, planting, and irrigating of fill slopes, and runoff control are required as per Code Section 91.3007.
F. Building or structure footings shall be set back 5 feet from the face of slopes 20 feet or less in vertical height where the slope angle is between 1½ horizontal to 1 vertical and 2 horizontal to 1 vertical. Where the vertical height of slope exceeds 20 feet and the slope angle is as described above, the set back shall be increased 1 foot for each additional 5 feet in vertical height over 20 feet to a maximum set back of 10 feet. For slopes exceeding 100 feet in vertical height, the set back shall be 40 feet except as permitted in Code Section 91.3009 (c).
G. [illegible] Interior footings [illegible]

R. J. WILLIAMS
General Manager

By ______________________

F.R. [illegible], Grading Engineer

B&S B-142 R10.71

Consulting Engineers [illegible]

CONVERSE, DAVIS AND ASSOCIATES

[illegible] West Del Mar Boulevard, Post Office Box [illegible], Pasadena, California [illegible] Telephone [illegible]

May 24, 1971

RECEIVED
MAY 28 1971
DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

The Buckley School
3900 Standsbury Avenue
Sherman Oaks, California 91403

Attention: Mr. Charles McAdam

Subject: Project No. 71-125-D, Report on Field Density Tests, Blanket Fill Slope, Proposed Athletic Field, 3900 Standsbury Avenue Sherman Oaks, California

TRACT - 23893
LOT - 1

Gentlemen:

This is to report the results of 26 field density tests made during construction of the subject blanket fill slope located along the northernmost perimeter of the proposed athletic field on the subject campus.

Specifications for the proposed grading were prepared by personnel of The Buckley School. Mr. Charles McAdam authorized Converse, Davis and Associates to perform periodic tests at random locations in the recently compacted fill slope.

Representative samples of the soils encountered at the test locations were tested in the laboratory to determine the maximum dry density and optimum moisture content. The on-site soils encountered during testing were classified as clayey silt and sandy silt. Density of the compacted fill was checked in the field by the sand cone method. A list of all field and laboratory tests made to date is presented in the "Table of Test Results."

The Buckley School
Project No. 71-125-D
May 24, 1971
Page two

Unless we are notified otherwise, we shall consider our work on this project complete.

Respectfully submitted,

William F. J. Chang

William F. J. Chang, Project Engineer

Thomas D. Lake

Reviewed and approved:
Thomas D. Lake, Principal Engineer

WFJC/TDL:eg
Encl: Table of Test Results I and II, Sheets 1 and 2
Dist: (4) Addressee
(1) Ragnar C. Qvale and Associates Architects
(2) City of Los Angeles, Department of Building and Safety, Grading Division
Van Nuys District Office
Attention: Mr. John S. Westphal

0530130173

The Buckley School
Project No. 71-125-D
May 24, 1971

TABLE OF TEST RESULTS

TABLE I
FIELD DENSITY TESTS

Test No.	Test Date	Test Location	Approx. Test Eleva-tion Feet	Approx. Depth of Fill Below Test-Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Com-paction
1	3/18/71	Blanket Fill	802	1	93	19.8	1	85
2	3/18/71	Blanket Fill	805	7	104	17.4	1	95
3	3/19/71	Blanket Fill	807	9	105	15.3	1	97
4	3/19/71	Blanket Fill	810	12	100	15.7	1	92
5	3/22/71	Blanket Fill	804	2	102	15.0	1	94
6	3/22/71	Blanket Fill	813	4	105	21.2	1	97
7	3/23/71	Blanket Fill	816	4	105	21.6	1	97
8	3/24/71	Blanket Fill	818	4	106	15.6	1	97
9	3/24/71	Blanket Fill	820	4	100	20.5	1	92
[illegible]	3/25/71	Blanket Fill	822	4	106	19.0	1	97
[illegible]	3/26/71	Blanket Fill	825	4	117	9.1	2	99
12	3/29/71	Blanket Fill	827	4	106	16.5	1	97
13	3/30/71	Blanket Fill	827	4	112	8.6	2	95
14	3/31/71	Blanket Fill	829	4	115	11.4	2	97
15	4/1/71	Blanket Fill	830	4	110	14.1	2	93
16	4/2/71	Blanket Fill	832	4	107	17.9	1	98
17	4/5/71	Blanket Fill	835	4	112	16.7	2	95
18	4/6/71	Blanket Fill	837	4	104	10.2	1	95
19	4/7/71	Blanket Fill	840	4	109	7.5	2	92
20	4/8/71	Blanket Fill	844	4	106	4.6	2	90
21	4/9/71	Blanket Fill	844	4	112	8.6	2	95
22	4/13/71	Blanket Fill	849	4	100	14.5	1	92
23	5/4/71	Blanket Fill	834	4	106	12.5	1	97
24S	5/7/71	West Slope	840	4	97	20.2	1	90
25S	5/7/71	West Slope	840	4	101	14.0	1	93
26	5/10/71	West Slope	843	4	98	15.0	1	90

(1) Density of the compacted fill was determined in the field by the A.S.T.M. D1556-64 sand cone test. Soil samples obtained from the sand cone tests were oven-dried to obtain the field moisture content.

(2) Soil Type is given on Table II, Laboratory Maximum Density Tests.

S - Tests made in the exposed face of a compacted fill slope.

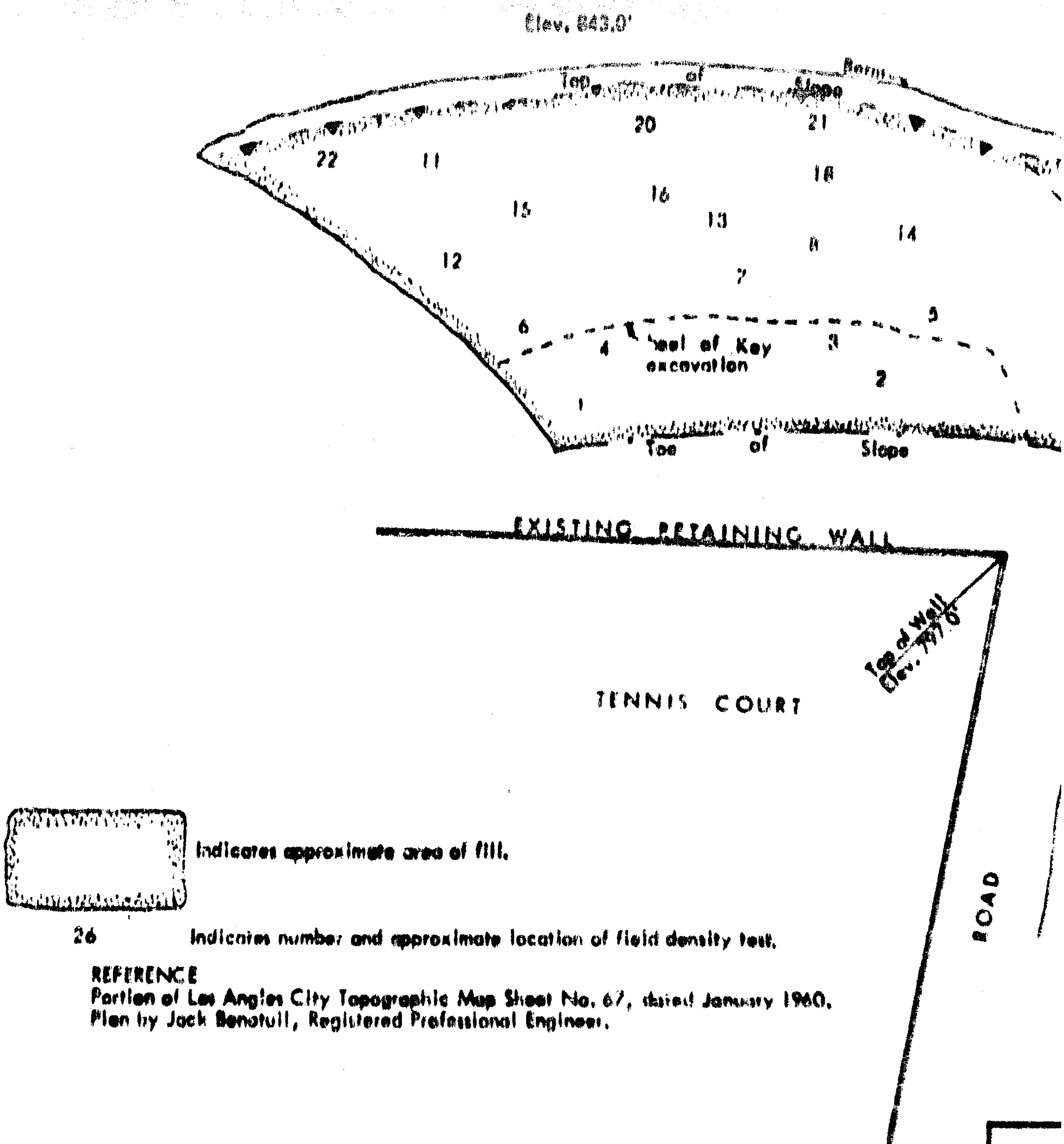
The Buckley School
Project No. 71-125-D
May 24, 1971

TABLE OF TEST RESULTS (Cont'd.)

TABLE II
LABORATORY MAXIMUM DENSITY TESTS*

Soil Type	Soil Description	Maximum Dry Density, p.c.f.	Optimum Moisture Content-Percent
1	Gray-Brown CLAYEY SILT	109	15.0
2	Brown SANDY SILT	118	12.8

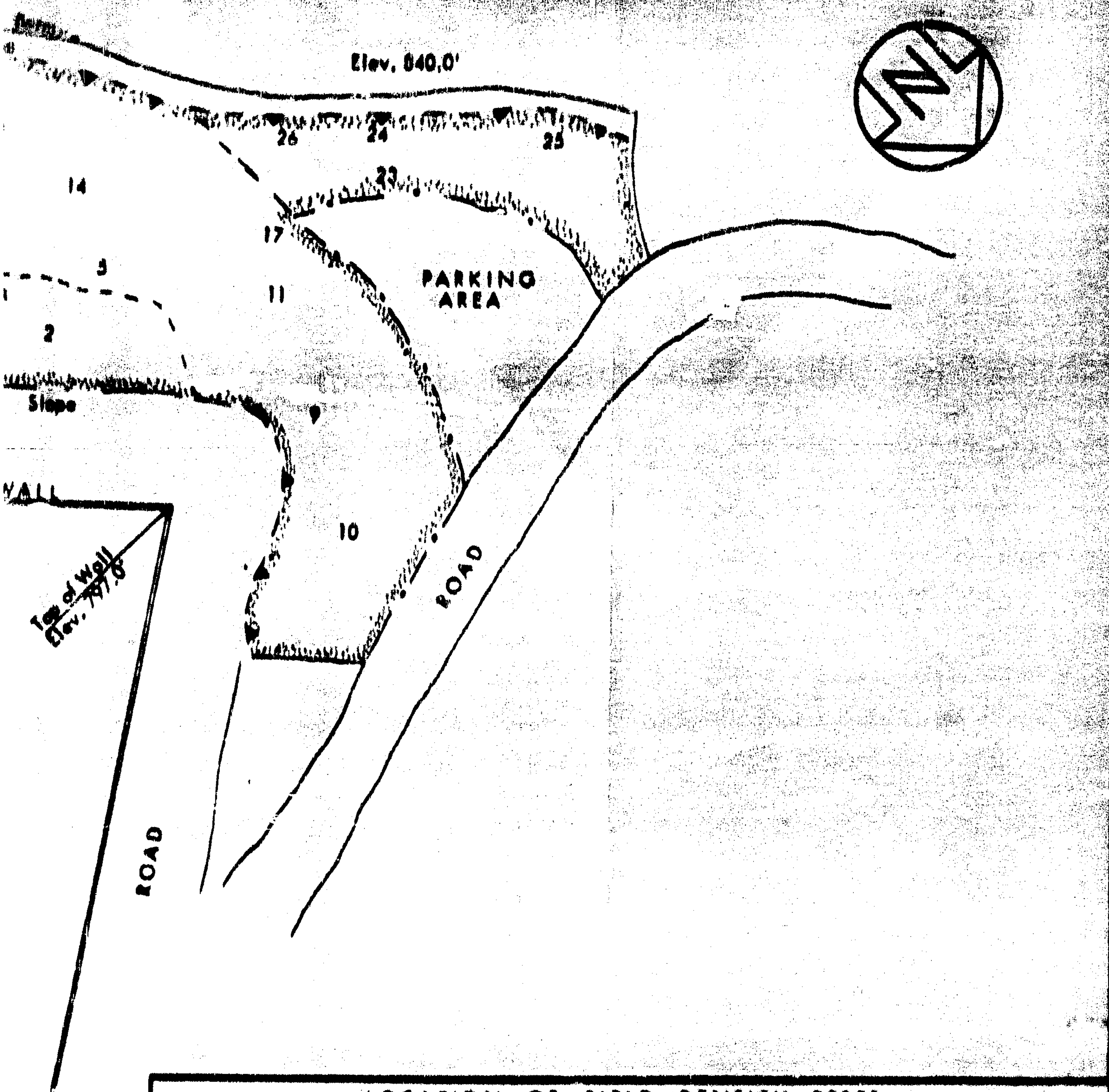
*A.S.T.M. D1557-70 test method.



Indicates approximate area of fill.

26 Indicates number and approximate location of field density test.

REFERENCE
Portion of Los Angles City Topographic Map Sheet No. 67, dated January 1960.
Plan by Jack Benatull, Registered Professional Engineer.



LOCATION OF FIELD DENSITY TESTS

PREPARED BY: J. B. B.	NORTH OF PROPOSED ATHLETIC FIELD Sherman Oaks, California for Buckley School	2
CHECKED BY: [signature]		
APPROVED BY: WCSC	DATE: June 9, 1971	SCALE: 1" = 40'

71-124-D

CONVERSE, DAVIS AND ASSOCIATES — PASADENA • SANTA ANA, CALIFORNIA

CITY OF LOS ANGELES

CALIFORNIA

[illegible] WILLIAMS
[illegible] MANAGER

DEPARTMENT OF
BUILDING AND SAFETY
[illegible] CITY HALL
LOS ANGELES, CALIF. 90012

SAM YORTY
MAYOR

The Buckley School
3900 Stansbury Avenue
Sherman Oaks, California 91403

Attention: Mr. Charles McAdam

TRACT: [illegible] DATE: [illegible], 1971
LOT: [illegible]
LOCATION: 3900 Stansbury Avenue ([illegible])

Lots having compacted fill: Same as above.

[redacted] approval is granted for compacted fill constructed on above lot(s) of subject property as described in report dated [illegible], 1971 (No. 71-[illegible]), prepared by [illegible].

The approval is limited exclusively to the area shown in the report and subject to the following requirements:

1. The compacted fill is approved only as a non-structural fill. This fill is not to be used for support of structural footings.
2. Slope erosion control, planting and irrigating of fill slopes and run-off control are required for those areas outside the building per Section 91.3007.

F.R. BAUER, Grading Engineer

[illegible]

B&S B-143 R3.70

GRADING OCT 4 1972

Consulting Engineers and Geologists

[CON]VERSE, DAVIS AND ASSOCIATES

126 West Del Mar Boulevard, Post Office Box 2268D, Pasadena, California 91105 Telephone (213) 681-1121

September 25, 1972

RECEIVED
OCT 11 1972
DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

P and A Construction Co., Inc.
1200 West 220th Street
Torrance, California 90502

Attention: Mr. William N. Weeger

Subject: Project No. 72-143-DH, Report on Compacted Fill, Proposed Library, High School Facilities The Buckley School, 3900 Stansbury Avenue Sherman Oaks, California

TRACT 23823 LOT 1

Gentlemen:

This is to report the results of tests and observations made during the placement of compacted fill on the subject site.

Periodic tests and inspections were provided by a representative of Converse, Davis and Associates to check the grading contractor on compliance with the drawings and job specifications. The presence of our field representative at the site was to provide to the owner a continuing source of professional advice, opinions and recommendations based upon the field representative's observations of the contractor's work and did not include any superintending, supervision or direction of the actual work of the contractor or the contractor's workmen. The opinions and recommendations presented hereafter are based on our tests and observations of the grading procedures used, and represent our engineering judgment as to the contractor's compliance with the drawings and job specifications.

The grading operations was observed to be performed in the following general manner:

1. Vegetation, surface trash and miscellaneous debris were cleared from the areas to be graded and were hauled off the property.

2. Unsatisfactory soils were excavated to expose competent materials on which to start the fill.

3. Approved soils were placed in layers on the prepared surface, and each layer was compacted to the specified density before the next layer was added.

4. Placement of the compacted fill was continued to the final grades indicated on Drawing No. 3.

5. The minimum acceptable degree of compaction was 90 percent of the maximum density.

6. Maximum density and optimum moisture content were determined by the A.S.T.M. D1557-70 method.

7. The soils used in the compacted fill consisted of silt and sandy silt and were classified as moderately expansive with respect to volume-change characteristics. A list of soil types encountered during testing is presented in the "Table of Test Results."

Field density tests were made during the placement of fill to determine the degree of compaction and the moisture content. Where tests or field observations indicated insufficient density, additional compaction with adjustment of the moisture content where necessary was performed before the next layer was added. All field density tests are listed in the "Table of Test Results," and their approximate locations are shown on Drawing No. 3. Also shown are the limits and depths of the controlled fill placed during this grading operation. Controlled compacted fill placed in the Administration Building and high school classrooms was reported August 7 and August 14, 1972, respectively.

Undisturbed samples were obtained from the compacted fill. The samples were obtained by hand driving a thin-walled steel sampler. One sample was tested at varying normal loads in a direct shear machine to determine the Coulomb shear strength parameter. The sample was saturated and drained prior to testing. The result of the shear test is listed in the "Table of Test Results."

CONCLUSIONS AND RECOMMENDATIONS

Based on the final results of the tests, on observations of the construction procedures used in the field and on our experience, it is our opinion that the controlled compacted fill shown on Drawing No. 3 has been placed in accordance with the applicable portions of the job specifications and with the recommendations of Converse, Davis and Associates. The compacted fill discussed in this report will support spread footings, slabs-on-grade, and pavement. Any fill added beyond the limits or above the grades shown should be placed under engineering control and in accordance with the specifications, if it is to be covered by the recommendations of this report. Loose fill as indicated on Drawing No. 3 is to be removed during backfilling of the Administration Building. The two to three feet of fill placed above Elevation 771 within the future library are to be removed during construction of the future library.

Footings should be at least 18 inches in width and bottomed 12 inches and 18 inches below lowest adjacent final surface on controlled compacted fill for interior and exterior footings, respectively. The permissible bearing value is 2,000 pounds per square foot on the proper bearing soils, as discussed in the report on the Foundation Investigation.

It is recommended that all footing excavations be inspected by Converse, Davis and Associates prior to pouring concrete to see that they are into satisfactory soils and are free of loose and disturbed materials. If conditions are encountered during building construction that appear to be different from those presented in this report, this office should be notified.

Our findings have been obtained in accordance with accepted professional engineering practice in the fields of engineering and soil mechanics. This warranty is in lieu of all other warranties, either express or implied.

The undersigned licensed Civil Engineer certifies that he has personally inspected the placement of and tested the compacted earth fill being reported, and that in his opinion the same was placed in conformity with the applicable portions of the City of Los Angeles Building Code.*

Respectfully submitted,

CONVERSE, DAVIS AND ASSOCIATES

By Ellis J. Jones
Ellis J. Jones, Project Engineer

C. R. MacFadyen
Reviewed and approved;
C. R. MacFadyen, Principal Engineer

EJJ/CRM:bh
Encl: Table of Test Results, I, II and III
Drawing No. 3
Dist: (2) Addressee
(2) City of Los Angeles, Department of Building and Safety, Grading Division
(2) Ragnar C. Qvale and Associates

*For the purpose of this certificate, to "have personally inspected and tested" shall include inspection and testing performed by any person employed by, and responsible to the licensed Civil Engineer signing this report. Where the inspection and testing of all or part of the work above is delegated, full responsibility shall be assumed by the licensed Civil Engineer whose signature is affixed hereon.

TABLE OF TEST RESULTS

TABLE I
FIELD DENSITY TESTS

[illegible]	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test-Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Compaction
[illegible]	8/1/72	Library	757	2	93	22.6	2	91
[illegible]	8/2/72	Library	759	4	93	21.6	2	91
[illegible]	8/3/72	Library	761	3	97	17.6	2	95
[illegible]	8/8/72	Library	764	3	119	7.2	4	98
[illegible]	8/8/72	Library	763	8	113	10.5	4	93
[illegible]	8/9/72	Library	767	7	115	9.7	4	95
[illegible]	8/9/72	Library	769	8	116	10.8	4	96
[illegible]	8/9/72	Berm	775	15	112	18.3	4	93
[illegible]	8/10/72	Berm	779	19	110	8.1	4	91
[illegible]	8/11/72	Library	771	11	109	11.8	4	90

(1) Density of the compacted fill was determined in the field by the A.S.T.M. D1556-64 sand cone test. Soil samples obtained from the sand cone tests were oven-dried to obtain the field moisture content.

(2) Soil Type is given on Table II, Laboratory Maximum Density Tests.

TABLE II
LABORATORY MAXIMUM DENSITY TESTS*

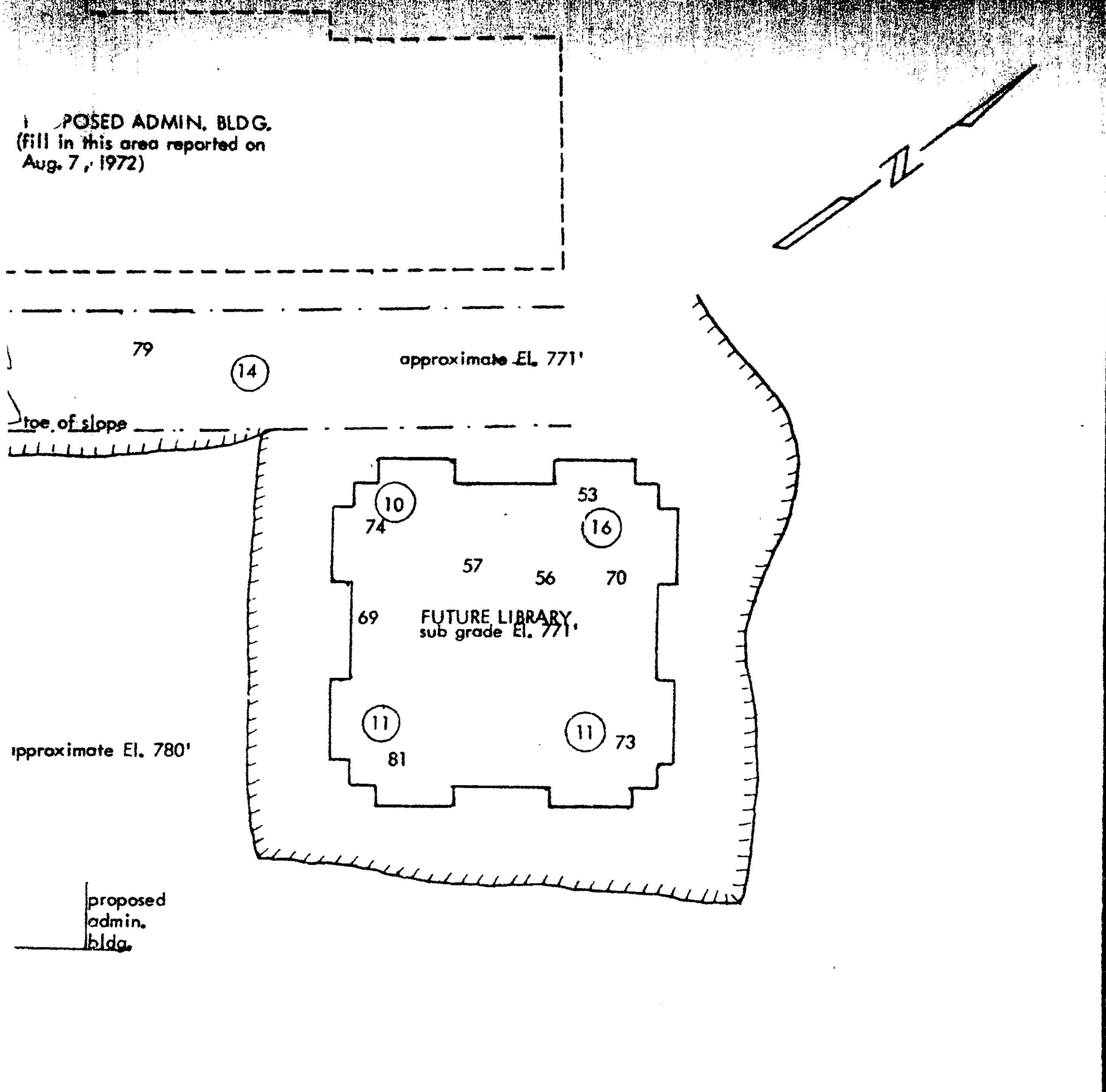
Soil Type	Soil Description	Maximum Dry Density, p.c.f.	Optimum Moisture Content-Percent
1	Black CLAY	110	14.3
2	Dark Brown SILT	102	18.0
3	Brown SANDY SILT	109	16.7
4	Brown SANDY SILT (Import)	121	10.2

*A.S.T.M. D1557-70 test method.

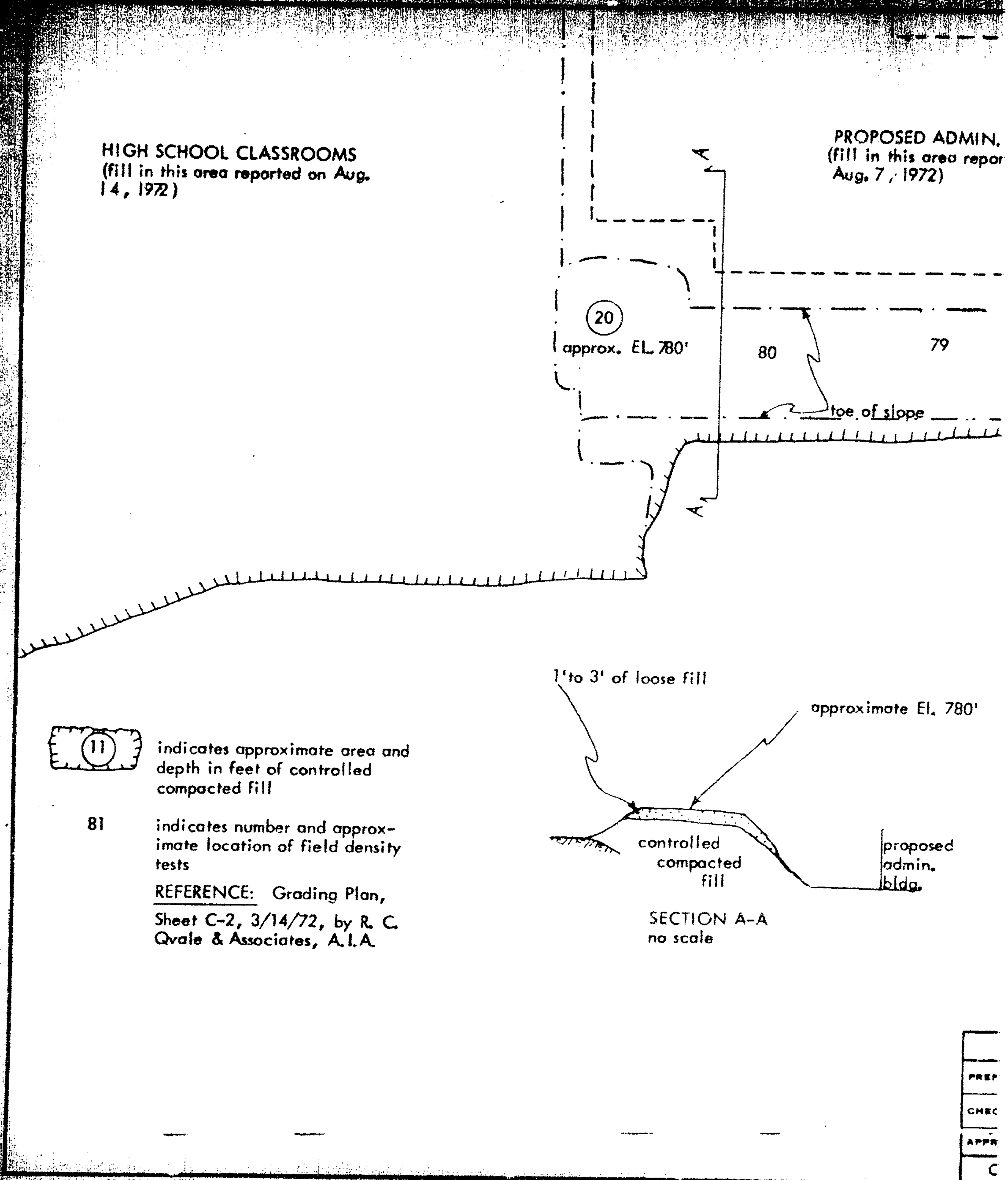
TABLE OF TEST RESULTS (Continued)

TABLE III
DIRECT SHEAR TESTS

Sample No.	Location	Depth Below Finish Grade (Feet)	c (Pounds Per Square Foot)	ϕ Degrees
1	Proposed Library	1.5	970	33



LOCATION OF CONTROLLED COMPACTED FILL			
PREPARED BY: B. F.	PROPOSED LIBRARY BUILDING BUCKLEY SCHOOL, SHERMAN OAKS, CAL. for P. and A. CONSTRUCTION COMPANY		DRAWING NUMBER 3
CHECKED BY: EJJ.			
APPROVED BY:	DATE: Sep. 21, 1972	SCALE: 1"=20'	PROJECT NUMBER: 72-143-DG
CONVERSE, DAVIS AND ASSOCIATES		PASADENA • SANTA ANA, CALIFORNIA	



HIGH SCHOOL CLASSROOMS
(fill in this area reported on Aug. 14, 1972)
PROPOSED ADMIN.
(fill in this area repor
Aug. 7, 1972)
A
A
20
approx. EL. 780'
80
79
toe of slope
1'to 3' of loose fill
approximate El. 780'
controlled compacted fill
proposed admin. bldg.
SECTION A-A
no scale
11
indicates approximate area and depth in feet of controlled compacted fill
81
indicates number and approximate location of field density tests
REFERENCE: Grading Plan, Sheet C-2, 3/14/72, by R. C. Qvale & Associates, A.I.A.
PREP
CHEC
APPR
C

CITY OF LOS ANGELES
CALIFORNIA

R. J. WILLIAMS
GENERAL MANAGER

DEPARTMENT OF
BUILDING AND SAFETY
402, CITY HALL
LOS ANGELES, CALIF. 90012

SAM YORTY
MAYOR

F and A Constr. Co.
1200 West 220th Street
Torrance, California 90502
Attn: Mr. W. N. Weeger

TRACT: [illegible]
LOT: 1
LOCATION: 3900 Stansbury Avenue

DATE: October 13, 1972
PERMIT: LA53311
DM# 7327

Fill soil classification, per Table 28-A: See report

Lots having compacted fill: same

Approval is granted for compacted fill constructed on the above lots as described in the compaction report dated September 25, 1972, prepared by Converse, Davis and Associates Report No. 72-143-DH.

Approval is limited to the area shown in the report and by the following requirements:

A. Footings for one-story wood-frame structures may be dimensioned from Table 17-B without use of the soil bearing value.
B. Footing bearing pressure for all other structures shall not exceed a value of 2000* lbs. per sq. ft. at 18** inches minimum, below approved compacted surface.
C. Continuous footings per Code Section 91.3012 are required.
D. All footings supported partly or wholly on compacted fill shall be reinforced continuously with at least one number 4 bar at the top and bottom of the footing.
E. Slope erosion control, planting, and irrigating of fill slopes, and runoff control are required as per Code Section 91.3007.
F. Building or structure footings shall be set back 5 feet from the face of slopes 20 feet or less in vertical height where the slope angle is between 1½ horizontal to 1 vertical and 2 horizontal to 1 vertical. Where the vertical height of slope exceeds 20 feet and the slope angle is as described above, the set back shall be increased 1 foot for each additional 5 feet in vertical height over 20 feet to a maximum set back of 10 feet. For slopes exceeding 100 feet in vertical height, the set back shall be 40 feet except as permitted in Code Section 91.3009 (c).

* footings to be minimum 18" wide.
** For exterior footings. Interior footings may use 12"

R. J. WILLIAMS
General Manager

By____________________

F.R. BAUER, Grading Engineer

B&S B-142 R10.71

Geotechnical Consultants

CONVERSE DAVIS DIXON ASSOCIATES

126 West Del Mar Boulevard, Box 2268D, Pasadena, California 91105 • (213) 681-1121

JUN 29 1977
DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

June 8, 1977

Paul W. Speer, Inc.
15450 Cabrito Road
Van Nuys, California 91406

Attention: Mr. Paul W. Speer

Subject: Final Report on Backfill, Pavilion Building and Passage Structure, The Buckley School, Sherman Oaks, California
Our Project No. 75-149-DG

Gentlemen:

This is to report the results of tests and observations made during the placement of compacted backfill on the subject site.

Periodic tests and observations were provided by a representative of Converse Davis Dixon Associates to check the grading contractor on compliance with the drawings and job specifications. The opinions and recommendations presented hereafter are based on our tests and observations of the backfilling procedures used, and represent our engineering judgment as to the contractor's compliance with the drawings and job specifications.

1. Excavations were found to be clean of loose or disturbed materials.

2. Approved soils were placed in layers on the prepared surface, and each layer was compacted to the specified density before the next layer was added.

3. Placement of the compacted backfill was continued to the final grades indicated on Drawing Nos. 1 and 2.

4. The minimum acceptable degree of compaction was 90 percent of the maximum density.

5. Maximum density and optimum moisture content were determined by the A.S.T.M. D1557-70 method.

6. A list of soil types encountered during testing is presented in Table II.

Field density test were made during backfilling to determine the degree of compaction and moisture content. Where tests or field observations indicated insufficient density, additional compaction with adjustment of the moisture content where necessary was performed before the next layer was added. It is not to be construed that Converse Davis Dixon Associates supervised, directed or superintended the contractor's work, since these functions were the sole responsibility of the contractor.

All field density tests are listed in the "Table of Test Results," and their approximate locations are shown on Drawing Nos. 1 and 2. Also shown are the limits and depths of the compacted backfill.

CONCLUSIONS AND RECOMMENDATIONS

Based on the final results of the tests, on observations of the construction procedures used in the field and on our experience, it is our opinion that the compacted fill shown on Drawing Nos. 1 and 2 have been placed in accordance with the applicable portions of the job specifications and with the recommendations of Converse Davis Dixon Associates. Any fill added beyond the limits or above the grades shown should be placed under engineering control and in accordance with the specifications, if it is to be covered by the recommendations of this report.

The compacted backfill discussed in this report is intended to support outside slabs-on-grade, pavements and passage canopy footings. General recommendations presented in the report on the Foundation Investigation, dated January 27, 1972 (our Project No. 71-486-A), are applicable on the compacted fill.

Services rendered on this project complied with generally accepted soil and foundation engineering practice. No other warranty, either express or implied, is made.

Respectfully submitted,

CONVERSE DAVIS DIXON ASSOCIATES

By Al Leskys

Algirdas G. Leskys, Senior Engineer

AGL:eh

Encl: Table of Test Results
Drawing Nos. 1 and 2

Dist: (2) Addressee
(1) Ragnar C. Qvale & Associates, Architects
(1) Hillman, Biddison and Loevenguth, Structural Engineers
(2) City of Los Angeles, Department of Building and Safety, Van Nuys Office

TABLE OF TEST RESULTS

TABLE I
FIELD DENSITY TESTS

Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Perce[illegible] Com[illegible] pacti[illegible]
1	12/15/75	Northside	771.0	1.0	96	22.3	6	94
2	12/15/75	Northside	771.4	1.5	99	21.1	1	90
3	12/16/75	Northside	773.5	3.5	92	19.8	6	90
4	12/16/75	Northside	772.5	2.5	95	23.5	6	93
5	12/17/75	Northside	774.5	4.5	94	25.7	6	92
6	12/17/75	Westside	772.0	2.0	92	23.0	6	90
7	12/18/75	Westside	772.0	2.0	82	23.0	6	80
9A	12/19/75	Westside	772.0	2.0	92	14.8	6	90
8	12/18/75	Southside	771.0	1.0	99	18.0	6	97
10	12/22/75	Southside	772.5	2.0	111	11.8	7	90
11	12/23/75	Southside	774.0	4.0	113	11.7	7	91
12	12/31/75	Southside	776.0	6.0	98	16.6	3	90
13	1/6/76	Eastside	774.0	4.0	93	15.5	6	91
14	1/8/76	Eastside	776.5	6.5	90	12.4	6	87
17A	1/12/76	Eastside	776.5	6.5	73	34.2	5	90
15	1/8/76	Southside	77.0	7.0	96	16.0	6	94
[illegible]	1/9/76	Southside	778.0	8.0	100	18.7	6	98
18	1/12/76	Southside	781.0	11.0	77	29.4	5	95
19	1/14/76	Southside	780.5	10.5	104	19.0	1	95
20	1/14/76	Southside	782.0	12.0	94	12.1	1	85
21A	1/15/76	Southside	782.0	12.0	93	13.3	1	86
22A	1/16/76	Southside	782.0	23.0	81	25.8	12	88
23A	1/16/76	Southside	782.0	12.0	63	31.6	12	69
24A	1/16/76	Southside	782.0	12.0	75	23.8	12	82
25A	1/19/76	Southside	782.0	12.0	86	26.0	12	93
26	1/20/76	Northside	783.0	13.0	101	23.2	1	92
27	1/21/76	Southside	784.0	14.0	102	19.1	1	93
28	1/22/76	Eastside	776.0	6.0	98	19.8	6	95
29	2/19/76	Westside	776.0	6.0	125	5.3	8	94
30	2/20/76	Westside	778.0	8.0	126	7.8	8	95
31	2/20/76	Westside	780.0	10.0	125	7.8	8	94
32	2/20/76	Westside	782.0	12.0	128	6.1	8	96
33	2/21/76	Eastside	778.0	8.0	122	8.5	8	92
34	2/21/76	Eastside	780.0	10.0	126	8.5	8	94
35	2/21/76	Eastside	782.0	12.0	127	8.2	8	95
36	2/23/76	Eastside	784.0	14.0	129	8.7	8	97

TABLE I, Continued

Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Com-paction
4/19/76	Westside	784.0	14.0	126	12.1	8	95
4/19/76	Westside	785.0	15.0	126	10.5	8	95
4/20/76	Northside	776.0	6.0	99	22.0	6	97
4/20/76	Northside	778.0	8.0	120	10.2	8	90
4/20/76	Northside	780.0	10.0	127	11.0	8	95
4/21/76	Northside	781.5	11.5	125	12.2	8	94
4/21/76	Northside	783.0	13.0	123	8.3	8	92
4/21/76	Northside	784.5	14.5	130	9.4	8	97
4/22/76	Northside	784.5	14.5	122	13.4	8	92
5/3/76	Sewer - West	784.0	2.0	125	9.4	8	94
5/3/76	Sewer - West	784.0	2.0	111	9.0	8	84
5/4/76	Sewer - West	784.0	2.0	125	10.0	8	94
5/3/76	Storm Drain - Southwest	786.0	3.0	122	12.8	8	92
5/3/76	Storm Drain - Southwest	788.0	5.0	128	11.2	8	96
5/4/76	Storm Drain - Southwest	790.0	7.0	101	16.0	1	92
5/4/76	Westside	786.0	16.0	122	12.0	2	93
5/4/76	Southside	786.0	16.0	121	9.0	2	93
5/5/76	Southside	786.0	3.0	97	23.4	6	95
5/576	Westside	786.0	16.0	94	17.6	6	92
5/5/76	Southside	787.0	17.0	95	23..4	6	94
5/5/76	Southside	787.0	17.0	94	28.9	6	92
5/576	Westside	787.0	17.0	95	23.4	6	93
5/6/76	Westside	788.0	18.0	96	21.3	6	94
5/6/76	Westside	788.0	18.0	92	17.8	6	91
5/6/76	Southside	788.0	18.0	96	22.4	6	94
5/6/76	Southside	792.0	12.0	91	22.0	6	90
5/7/76	Westside	789.0	19.0	94	22.0	6	92
5/7/76	Southside	789.0	19.0	94	16.6	6	92
5/7/76	Westside	789.0	19.0	97	22.7	6	95
5/7/76	Southside	789.0	19.0	97	20.0	6	95
5/10/76	Eastside	786.0	16.0	94	18.6	6	92
5/10/76	Eastside	786.0	3.0	97	20.1	6	95
5/10/76	Eastside	787.0	17.0	96	15.8	6	94
5/10/76	Eastside	787.0	17.0	96	13.6	6	94
5/11/76	Eastside	788.0	18.0	94	15.6	6	92
5/11/76	Eastside	788.0	5.0	98	20.9	6	96
5/11/76	Eastside	789.0	19.0	97	16.0	6	95
5/12/76	Sewer - North	780.0	1.0	98	20.1	6	96
5/12/76	Sewer - North	782.0	3.0	95	21.7	6	93

TABLE I, Continued

Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Compaction
[illegible]	5/12/76	Sewer - North	784.0	5.0	93	17.2	6	91
[illegible]	5/13/76	Sewer - North	785.0	6.0	96	20.5	6	93
[illegible]	5/13/76	Southside	784.0	1.0	94	16.8	6	91
[illegible]	5/13/76	Southside	785.0	2.0	102	15.1	3	93
[illegible]	5/14/76	Southside	786.0	3.0	87	16.5	3	80
[illegible]A	5/20/76	Southside	786.0	3.0	104	19.4	3	95
[illegible]	5/18/76	Southside	791.0	21.0	119	12.3	9	93
[illegible]	5/18/76	Westside	790.0	20.0	117	12.1	9	92
[illegible]	5/19/76	Eastside	787.5	15.0	122	9.8	9	95
[illegible]	5/19/76	Eastside	790.0	7.0	108	12.8	9	85
[illegible]	5/20/76	Eastside	790.0	7.0	115	11.1	9	90
[illegible]	5/19/76	Eastside	789.0	19.0	116	12.2	9	91
[illegible]	5/20/76	Eastside	791.5	21.5	118	8.2	9	92
[illegible]	5/20/76	Eastside	792.5	22.5	114	8.4	9	90
[illegible]	5/21/76	Westside	788.0	18.0	117	15.9	9	91
[illegible]	5/21/76	Westside	791.0	21.0	118	13.1	9	92
[illegible]	5/24/76	Eastside	791.0	21.0	121	10.9	9	95
[illegible]	5/24/76	Westside	789.5	19.5	118	16.1	9	92
[illegible]	5/24/76	Westside	790.5	20.5	120	13.9	9	94
[illegible]	5/25/76	Westside	790.5	2.0	125	9.8	9	97
[illegible]	5/25/76	Westside	792.5	22.5	125	9.3	9	97
[illegible]	5/25/76	Westside	792.0	3.0	119	10.4	9	93
[illegible]	6/15/76	Northside	784.0	10.0	111	11.6	7	90
[illegible]	6/15/76	Northside	783.0	5.0	113	11.1	7	91
[illegible]	7/13/76	Southside	787.5	2.0	99	17.0	6	97
[illegible]	7/13/76	Northside	772.5	2.5	115	15.0	7	93
[illegible]	7/13/76	Southside	790.0	5.0	96	19.5	6	94
[illegible]	7/13/76	Southside	792.0	7.0	95	19.7	6	93
[illegible]	7/14/76	Northside	774.0	4.0	113	15.0	7	91
105	7/14/76	Southside	789.5	4.5	103	14.5	1	93
106	7/14/76	Southside	790.5	5.5	100	24.0	1	91
107	7/14/76	Northside	773.0	2.0	94	11.0	6	92
108	7/14/76	Southside	792.5	7.5	99	6.0	1	90
109	8/10/76	Northside	774.0	6.0	116	14.1	9	91
110	8/11/76	Northside	776.0	7.0	100	19.4	1	90
111	8/11/76	Northside	777.0	9.0	102	16.7	1	93
112	8/12/76	Northside	779.0	9.0	107	17.2	1	98
113	8/12/76	Northside	780.0	10.0	102	18.1	1	93
114	8/13/76	Northside	782.0	12.0	116	10.4	9	91
115	8/13/76	Northside	784.0	14.0	102	19.3	1	93

TABLE I, Continued

Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Compaction
[illegible]6	8/13/76	Northside	786.0	16.0	118	9.7	9	92
[illegible]7	8/16/76	Northside	787.0	17.0	110	10.9	1	91
[illegible]8	8/16/76	Northside	787.0	17.0	109	4.8	3	90
119	8/24/76	Northside	789.5	19.5	112	11.7	11	96
120	8/24/76	Northside	788.5	18.5	106	7.9	11	91
[illegible]21	8/24/76	Northside	786.0	2.0	107	8.2	11	92
[illegible]2	8/25/76	Northside	787.5	17.5	105	6.0	11	91
[illegible]	8/25/76	Northside	790.0	20.0	102	8.0	11	88
[illegible]A	8/25/76	Northside	790.0	20.0	109	12.2	11	94
[illegible]	8/25/76	Northside	790.0	17.0	110	13.0	11	95
[illegible]	8/26/76	Northside	787.5	0.5	112	11.1	11	96
[illegible]	8/26/76	Northside	790.0	0.5	108	15.4	11	93
[illegible]	8/26/76	Northside	790.0	15.0	106	9.0	11	91
[illegible]	8/27/76	Northside	790.0	18.0	105	17.4	1	95
[illegible]0	8/27/76	Northside	791.0	2.0	106	17.0	11	91
[illegible]1	8/27/76	Northside	791.0	21.0	99	17.7	11	91
[illegible]2	8/31/76	Northside	793.0	23.0	123	10.5	10	92
[illegible]3	8/31/76	Northside	792.5	19.0	128	11.5	10	96
[illegible]4	9/1/76	Northside	791.0	1.5	120	10.0	8	90
[illegible]	9/1/76	Northside	792.0	2.5	125	13.0	8	94
[illegible]	9/20/76	Elec. Trench - North	786.0	2.0	119	12.8	8	90
[illegible]7	9/21/76	Stairwell - North	784.5	2.5	119	11.7	8	90
[illegible]38	9/21/76	Elec. Trench - North	792.0	2.0	104	14.6	11	90
[illegible]39	9/21/76	Stairwell - North	784.0	2.0	109	10.8	8	82
[illegible]1A	9/21/76	Stairwell - North	784.0	2.0	121	10.2	8	91
[illegible]0	9/21/76	Stairwell - North	788.5	6.5	125	12.9	8	94
[illegible]42	9/21/76	Elec. Trench -	793.0	3.0	121	12.8	8	91
[illegible]43	9/21/76	Stairwell - North	788.0	6.0	122	10.4	8	92
[illegible]44	9/28/76	Pipe - North	791.5	21.5	108	6.8	11	92
[illegible]45	9/28/76	Pipe - North	793.0	23.0	123	10.2	8	92
146	12/9/76	Canopy Footing Line	790.0	1.0	111	17.0	13	94
147	12/9/76	Canopy Footing Line	790.0	1.0	106	18.6	13	90
148	12/9/76	Canopy Footing Line	791.5	2.5	113	16.5	13	96
149	12/9/76	Canopy Footing Line	791.5	2.5	113	15.5	13	96
150	12/9/76	Canopy Footing Line	792.0	3.0	108	10.8	13	92

TABLE I, Continued

Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Compaction
[illegible]	12/9/76	Canopy Footing Line	791.5	2.5	111	11.1	13	94
[illegible]	12/9/76	Canopy Footing Line	793.0	4.0	116	12.1	13	98
153	12/10/76	Canopy Footing Line	790.5	1.0	111	13.8	13	94
154	12/10/76	Canopy Footing Line	791.0	1.5	119	12.5	13	100
[illegible]	12/10/76	Canopy Footing Line	792.0	2.5	113	11.7	13	96
[illegible]	12/10/76	Canopy Footing Line	793.0	3.5	111	13.2	13	94
[illegible]	12/15/76	Canopy Footing Line	789.5	1.0	113	12.4	13	96
[illegible]	12/15/76	Canopy Footing Line	790.5	2.0	119	12.6	13	100
159	12/15/76	Canopy Footing Line	790.0	1.5	116	13.0	13	98
160	12/15/76	Canopy Footing Line	791.5	3.0	113	13.2	13	96
161	12/15/76	Canopy Footing Line	791.0	2.5	111	13.4	13	94
[illegible]	12/15/76	Canopy Footing Line	792.0	3.5	107	13.1	13	91
163	12/15/76	Canopy Footing Line	792.5	4.0	114	13.9	13	97
164	12/15/76	Canopy Footing Line	789.0	0.5	109	16.9	13	92
165	12/16/76	Canopy Footing Line	789.0	0.5	113	13.9	13	96
166	12/16/76	Canopy Footing Line	789.5	1.0	111	16.0	13	94
167	12/16/76	Canopy Footing Line	790.0	1.5	109	13.4	13	93
168	12/16/76	Canopy Footing Line	790.5	2.0	114	14.7	13	97
169	12/16/76	Canopy Footing Line	791.0	2.5	112	14.0	13	95
170	12/16/76	Canopy Footing Line	791.5	3.0	110	16.7	13	93
171	12/16/76	Canopy Footing Line	792.0	3.5	104	12.8	13	88
173A	12/16/76	Canopy Footing Line	792.0	3.5	104	13.8	13	88
174A	12/16/76	Canopy Footing Line	792.0	3.5	114	12.8	13	96
172	12/16/76	Canopy Footing	791.0	3.0	118	12.9	13	100

TABLE I, Continued

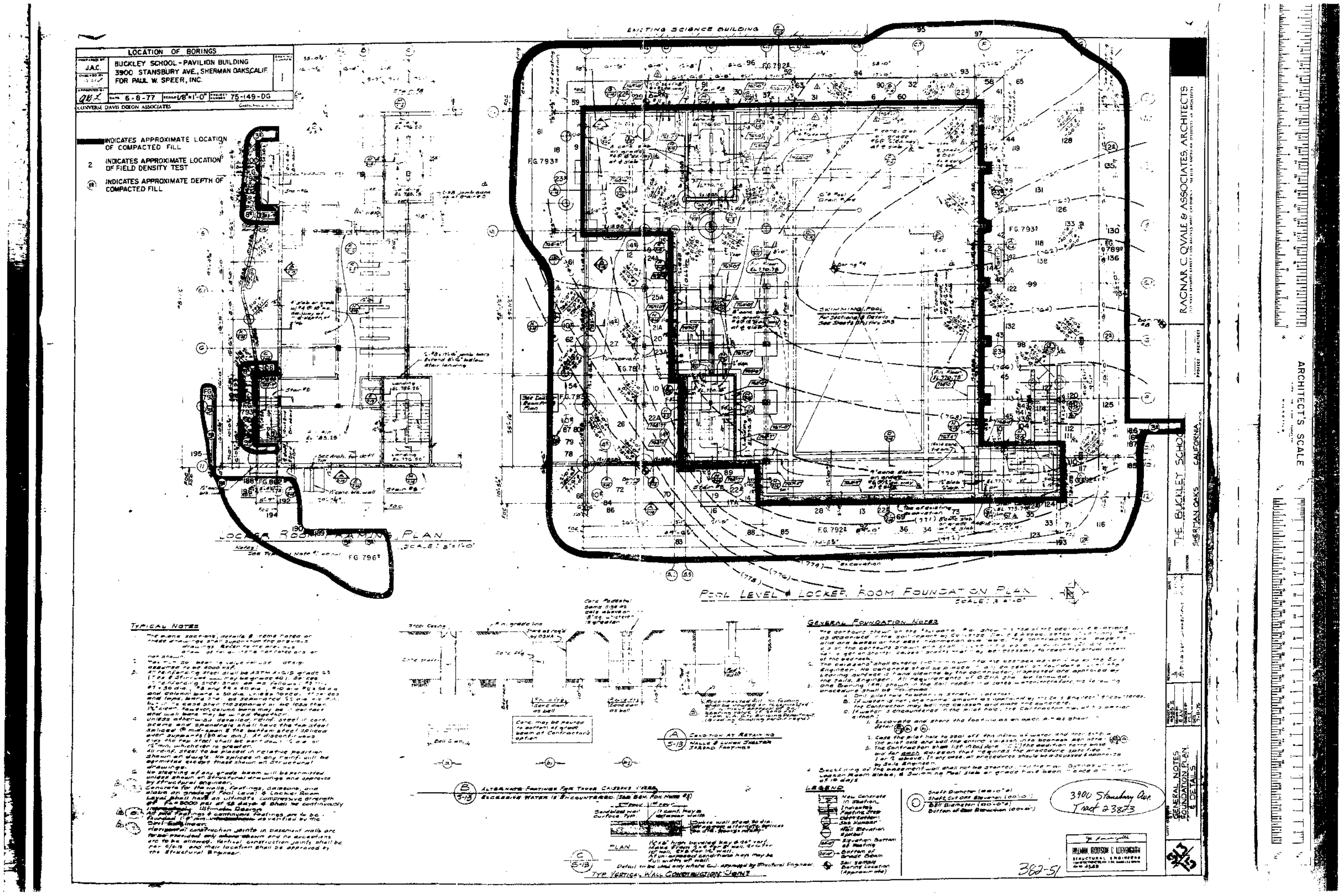
Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p.c.f.	Field Moisture Content Percent of Dry Wt.	(2) Soil Type	Percent Compaction
[illegible]	12/16/76	Canopy Footing Line	793.0	4.5	112	14.2	13	95
[illegible]	12/17/76	Canopy Footing Line	788.0	0.0	111	15.0	13	94
[illegible]	12/17/76	Canopy Footing Line	788.0	0.0	115	14.2	13	97
[illegible]	12/17/76	Canopy Footing Line	789.0	1.0	112	14.6	13	95
179	12/17/76	Canopy Footing Line	788.5	0.5	116	15.2	13	98
[illegible]	12/17/76	Canopy Footing Line	789.5	1.5	117	13.5	13	99
[illegible]	12/17/76	Canopy Footing Line	790.0	2.0	113	14.6	13	96
[illegible]	12/17/76	Canopy Footing Line	790.5	2.5	113	14.2	13	96
[illegible]	12/17/76	Canopy Footing Line	791.0	3.0	118	12.9	13	10[illegible]
[illegible]	12/17/76	Canopy Footing Line	791.5	3.5	110	16.3	13	93
185	1/16/77	Retaining Wall Line	788.0	1.5	125	9.3	10	93
186	1/28/77	Retaining Wall Line	790.0	3.5	122	13.3	10	91
187	1/31/77	Retaining Wall Line	791.5	5.0	115	13.3	9	90
[illegible]8	2/2/77	Retaining Wall Line	795.5	2.0	102	19.0	3	94
189	2/2/77	Retaining Wall Line	797.5	4.0	100	14.7	3	93
190	2/4/77	Retaining Wall Line	798.0	4.5	109	17.5	3	10[illegible]
191	3/2/77	Retaining Wall Line	799.5	6.0	105	16.9	3	96
192	4/27/77	Retaining Wall Line	800.0	6.5	119	12.8	2	92
193	4/27/77	Retaining Wall Line	794.0	1.5	121	11.2	2	93
194	5/17/77	Retaining Wall Line	802.0	7.0	113	14.8	4	93
195	5/17/77	Retaining Wall Line	796.0	3.0	113	12.7	4	93
196	6/6/77	Retaining Wall Line	802.0	8.0	113	8.7	4	93

(1) Density of the compacted fill was determined in the field by the A.S.T.M. D1556-64 sand cone test.
(2) Soil type is given on Table II, Laboratory Maximum Density Tests.
A - Tests taken to recheck areas of substandard compaction.

TABLE II
LABORATORY MAXIMUM DENSITY TESTS*

Soil Type	Soil Description	Maximum Dry Density, p.c.f.	Optimum Moisture Content-Percent
1	Black CLAY with Diatomaceous SHALE	110	14.3
2	Brown SILTY SAND and GRAVEL	130	8.3
3	Light Brown SANDY SILT	109	16.7
4	Brown SANDY SILT (Import)	121	10.2
5	Light Brown SILTSTONE and Dark Brown SILTY CLAY	81	34.0
6	Dark Brown SILT with Diatomaceous SHALE	102	18.0
7	Dark Red-Brown CLAYEY SAND (Import)	124	12.5
8	Brown SILTY SAND D.G. (Import)	133	9.6
9	Brown Fine SANDY SILT with GRAVEL (Import)	128	9.8
10	Red-Brown SILTY SAND (Import)	134	7.5
11	Light Brown SILTY SAND with CLAY	116	11.2
**12	Mixed Brown SILTY CLAY, SILTSTONE, Dark Brown SILT with Diatomaceous SHALE	92	29.0
**13	Black SANDY CLAY	118	15.0

*A.S.T.M. D1557-70 test method.
**Field Checkpoint.


LOCATION OF BORINGS
BUCKLEY SCHOOL - PAVILION BUILDING
3900 STANSBURY AVE., SHERMAN OAKS, CALIF
FOR PAUL W. SPEER, INC.
J.A.C.
6-6-77
1/8"=1'-0"
75-149-DG
INDICATES APPROXIMATE LOCATION OF COMPACTED FILL
INDICATES APPROXIMATE LOCATION OF FIELD DENSITY TEST
INDICATES APPROXIMATE DEPTH OF COMPACTED FILL
EXISTING SCIENCE BUILDING
POOL LEVEL & LOCKER ROOM FOUNDATION PLAN
LOCKER ROOM FRAMING PLAN
TYPICAL NOTES
GENERAL FOUNDATION NOTES
LEGEND
TYP. VERTICAL WALL CONSTRUCTION JOINT
RAGNAR C. QVALE & ASSOCIATES, ARCHITECTS
THE BUCKLEY SCHOOL
SHERMAN OAKS, CALIFORNIA
GENERAL NOTES FOUNDATION PLAN & DETAILS
3900 Stansbury Ave
Tract 23873
382-51
ARCHITECT'S SCALE

11x17

RECEIVED

JUN 29 1977

DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

CITY OF LOS ANGELES

DEPARTMENT OF BUILDING AND SAFETY

ENGINEER'S CERTIFICATE OF COMPLIANCE FOR COMPACTION

LOCATION OF FILL: TRACT NO. 23823 LOT NOS. 1
Buckley School Pavilion Building and Passage Structures as shown on Drawing Nos. 1 and 2 of report listed below.

JOB ADDRESS: 3900 Stansbury Avenue, Sherman Oaks, California

SOIL TESTING AGENCY: Converse Davis Dixon Associates

PROPERTY OWNER'S NAME Buckley School

OWNER'S ADDRESS: 3900 Stansbury Avenue, Sherman Oaks, California

PER REPORTS ON OUR PROJECT NO. 75-149-DG dated June 8, 1977

DATE WORK STARTED ON PROJECT: December 15, 1975

DATE FILL WAS COMPLETED: June 6, 1977

DATE OF THIS CERTIFICATE: June 8, 1977

TO THE SUPERINTENDENT OF BUILDING:

*I hereby certify that I have personally inspected and tested the placing of compacted earth fill on the above described property, and on the basis of these inspections and tests it is my opinion that the same was placed in conformity with the requirements of the Los Angeles City Building Code.

Civil Engineer Algirdas G. Leskys
California Certificate No. 21783

*For the purpose of this Certificate, to "have personally inspected and tested" shall include inspection and testing performed by any person responsible to the licensed engineer signing this certificate. Where the inspection and test of all or part of the work above is delegated, full responsibility shall be assumed by the licensed engineer whose signature is affixed thereon.

X B&S G-22 4.67

C A Fair

CITY OF LOS ANGELES
CALIFORNIA

R.J. WILLIAMS
GENERAL MANAGER

DEPARTMENT OF
BUILDING AND SAFETY
402, CITY HALL
LOS ANGELES, CALIF. 90012

TOM BRADLEY
MAYOR

Buckley School
3900 Stansbury Ave.
Sherman Oaks, Ca. 91403

TRACT: 23823
LOT: 11
LOCATION: 3900 Stansbury Ave.

DATE: 30 June 1977
PERMIT: LA 53311
DM# 7327

Fill soil classification, per Table 28-A: See report

Lots having compacted fill: 1

Approval is granted for compacted fill constructed on the above lots as described in the compaction report dated June 8, 1977, prepared by Converse-Davis-Dixon Assoc. Report No. 75-149-DD.

Approval is limited to the area shown in the report and by the following requirements:

A. Footings for one-story wood-frame structures may be dimensioned from Table 17-B without use of the soil bearing value.
B. Footing bearing pressure for all other structures shall not exceed a value of * lbs. per sq. ft. at * inches minimum, below approved compacted surface.
C. Continuous footings per Code Section 91.3012 are required.
D. Dwelling foundations located partially or wholly upon compacted fill ground shall meet the requirements of Section 91.3012.
E. Slope erosion control, planting, and irrigating of fill slopes, and runoff control are required as per Code Section 91.3007.
F. Building or structure footings shall be set back 5 feet from the face of slopes 20 feet or less in vertical height where the slope angle is between 1½ horizontal to 1 vertical and 2 horizontal to 1 vertical. Where the vertical height of slope exceeds 20 feet and the slope angle is as described above, the set back shall be increased 1 foot for each additional 5 feet in vertical height over 20 feet to a maximum set back of 10 feet. For slopes exceeding 100 feet in vertical height, the set back shall be 40 feet except as permitted in Code Section 91.3009(c).

* See report dated January 27, 1972.

G. The soil engineer shall inspect the footing excavations to determine that they are founded in the recommended strata before calling the Department for footing inspection.

R.J. WILLIAMS
General Manager

By ______________

F.R. Bauer, Grading Engineer

B&S B-142 R11.74

Consulting Engineers and Geologists

...ERSE, DAVIS AND ASSOCIATES

126 West Del Mar Boulevard, Post Office Box 2268D, Pasadena, California 91105 Telephone (213) 681-1121

December 13, 1972

RECEIVED
DEC 1 9 1972
DEPARTMENT OF BUILDING & SAFETY
VAN NUYS DISTRICT OFFICE
GRADING DIVISION

P and A Construction Co., Inc.
1200 West 220th Street
Torrance, California 90502

Attention: Mr. William N. Weeger

Subject: Project No. 72-245-DG, Report on Compacted Fill Maintenance Building, The Buckley School 3900 Stansbury Avenue, Sherman Oaks, California

Gentlemen: TRACT 23823 LOT 1

This is to report the results of tests and observations made during the placement of compacted fill on the subject site.

Periodic tests and inspections were provided by a representative of Converse, Davis and Associates to check the grading contractor on compliance with the drawings and job specifications. The presence of our field representative at the site was to provide to the owner a continuing source of professional advice, opinions and recommendations based upon the field representative's observations of the contractor's work and did not include any superintending, supervision or direction of the actual work of the contractor or the contractor's workmen. The opinions and recommendations presented hereafter are based on our tests and observations of the grading procedures used, and represent our engineering judgment as to the contractor's compliance with the drawings and job specifications.

The grading operation was observed to be performed in the following general manner:

1. Vegetation, surface trash and miscellaneous debris were cleared from the areas to be graded and were hauled off the property.

2. Unsatisfactory soils were excavated to expose competent materials on which to start the fill. Portions of an existing fill placed in 1965 under engineering inspection by Advanced Foundation Engineering, Incorporated, Consulting Foundation Engineers, were encountered during this excavation. This previously placed fill was inspected and found to be suitable to receive the new fill.

3. Approved soils were placed in layers on the prepared surface, and each layer was compacted to the specified density before the next layer was added.

4. Placement of the compacted fill was continued to the final grades indicated on Drawing No. 1.

5. The minimum acceptable degree of compaction was 90 percent of the maximum density.

6. Maximum density and optimum moisture content were determined by the A.S.T.M. D1557-70 method.

7. The soils used in the compacted fill consisted of sandy silt and silty sand with gravel and were classified as nonexpansive with respect to volume-change characteristics. A list of soil types encountered during testing is presented in the "Table of Test Results."

Field density tests were made during the placement of fill to determine the degree of compaction and moisture content. Where tests or field observations indicated insufficient density, additional compaction with adjustment of the moisture content where necessary was performed before the next layer was added. All field density tests are listed in the "Table of Test Results," and their approximate locations are shown on Drawing No. 1. Also shown are the limits and depths of the controlled fill placed during this grading operation.

Undisturbed samples were obtained from the compacted fill. The samples were obtained by hand driving a thin-walled steel sampler. One sample was tested at varying normal loads in a direct shear machine to determine the Coulomb shear strength parameter. The sample was saturated and drained prior to testing. The result of the shear test is listed in the "Table of Test Results."

CONCLUSIONS AND RECOMMENDATIONS

Based on the final results of the tests, on observation of the construction procedures used in the field and on our experience, it is our opinion that the controlled compacted fill shown on Drawing No. 1 has been placed in accordance with the applicable portions of the job specifications and with the recommendations of Converse, Davis and Associates. The compacted fill discussed in this report will support spread footings, slabs-on-grade, and pavement. Any fill added beyond the limits or above the grades shown should be placed under engineering control and in accordance with the specifications, if it is to be covered by the recommendations of this report.

No warranty concerning the performance of the preexisting fill mentioned above, either express or implied, is made by Converse, Davis and Associates by virtue of this compacted fill report.

Footings should be at least 18 inches in width and bottomed 18 inches below lowest adjacent final surface on controlled compacted fill. The permissible bearing value is 2000 pounds per square foot on the proper bearing soils.

It is recommended that all footing excavations be inspected by Converse, Davis and Associates prior to pouring concrete to see that they are into satisfactory soils and are free of loose and disturbed materials. If conditions are encountered during building construction that appear to be different from those presented in this report, this office should be notified.

Our findings have been obtained in accordance with accepted professional engineering practice in the fields of engineering and soil mechanics. This warranty is in lieu of all other warranties, either express or implied.

The undersigned licensed Civil Engineer certifies that he has personally inspected the placement of and tested the compacted earth fill being reported, and that in his opinion the same was placed in conformity with the applicable portions of the City of Los Angeles Building Code.*

Respectfully submitted,

CONVERSE, DAVIS AND ASSOCIATES

By Ellis J. Jones
Ellis J. Jones, Project Engineer

C. R. MacFadyen
Reviewed and approved;
C. R. MacFadyen, Principal Engineer

EJJ/CRM:eg
Encl: Table of Test Results I, II and III, Sheets 1 and 2
Drawing No. 1
Dist: (2) Addressee
(2) City of Los Angeles
Department of Building and Safety
Grading Division
(2) Ragnar C. Qvale and Associates

*For the purpose of this certificate, to "have personally inspected and tested" shall include inspection and testing performed by any person or persons employed by, and responsible to the licensed Civil Engineer signing this report. Where the inspection and testing of all or part of the work above is delegated, full responsibility shall be assumed by the licensed Civil Engineer whose signature is affixed hereon.

A Construction [illegible], Inc. Sheet 1 of 2
[illegible]ct No. 72-245-DG
[illegible]ember 13, 1972

TABLE OF TEST RESULTS

TABLE I
FIELD DENSITY TESTS

Test No.	Test Date	Test Location	Approx. Test Elevation Feet	Approx. Depth of Fill Below Test Feet	(1) Dry Density p. c. f.	Field Moisture Content Percent of Dry Weight	(2) Soil Type	Percent Compaction
1	10/25/72	East of Concrete Apron	821	2	86	20.3	1	71
2-A	10/25/72	East of Concrete Apron	821	2	112	16.7	1	90
3	10/26/72	East of Concrete Apron	824	2	104	12.0	2	95
4	10/27/72	East of Concrete Apron	827	4	113	12.2	1	91
5	10/27/72	East of Concrete Apron	829	4	112	12.6	1	90
6	10/27/72	East of Concrete Apron	832	7	112	11.2	1	90
7	10/30/72	East of Concrete Apron	835	8	113	12.8	1	91
8	10/30/72	East of Concrete Apron	838	12	115	11.7	1	92
9	10/30/72	Concrete Apron	834	3	112	10.0	1	90
10	10/31/72	Concrete Apron	836	8	113	10.6	1	91
11	10/31/72	Concrete Apron	838	6	113	16.4	1	90
12	10/31/72	Concrete Apron	840	10	105	15.9	2	96
13	11/2/72	Concrete Apron	842	6	105	17.9	2	96
14	11/2/72	Concrete Apron	844	8	104	19.1	2	95
15	11/3/72	Building Area	846	6	116	10.5	1	93
16	11/7/72	Building Area	846	2	91	9.0	2	84
17-A	11/7/72	Building Area	846	2	113	9.8	1	90
18	11/7/72	Building Area	848	4	107	13.4	2	98
19	11/8/72	Building Area	848	8	113	9.5	1	90

(1) Density of the compacted fill was determined in the field by the A.S.T.M. D1556-64 sand cone test. Soil samples obtained from the sand cone tests were oven-dried to obtain the field moisture content.

(2) Soil Type is given on Table II, Laboratory Maximum Density Tests.

A - Tests taken to recheck areas of substandard compaction.

TABLE OF TEST RESULTS (Cont'd.)

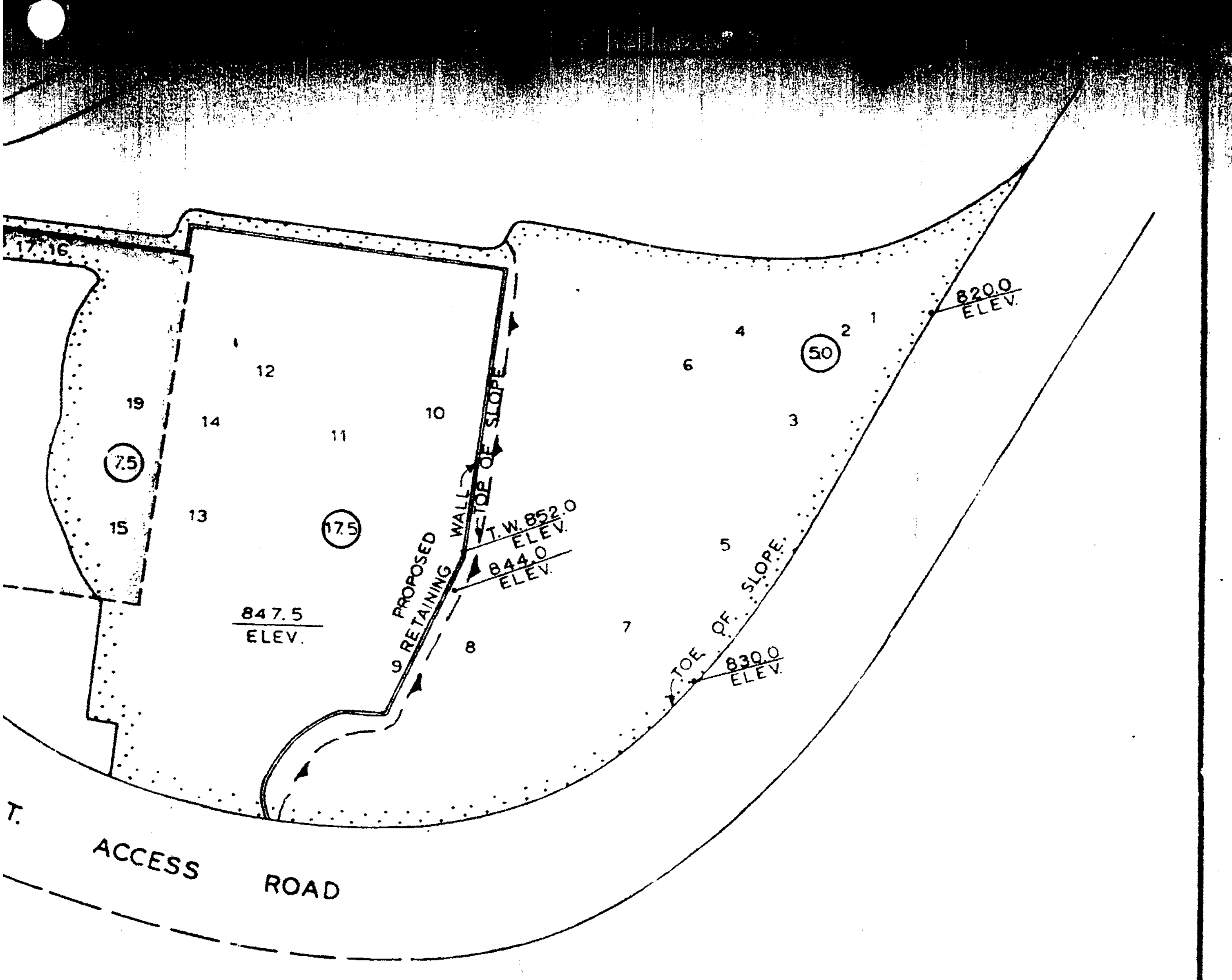
TABLE II
LABORATORY MAXIMUM DENSITY TESTS*

Soil Type	Soil Description	Maximum Dry Density, p.c.f.	Optimum Moisture Content-Percent
1	Brown SILTY SAND and GRAVEL	125	9.3
2	Light Brown SANDY SILT	109	16.7

*A.S.T.M. D1557-70 test method.

TABLE III

Sample No.	Location	Depth Below Finish Grade (Feet)	c (Pounds Per Square Foot)	ø Degrees
1	Maintenance Building	1.5	350	27

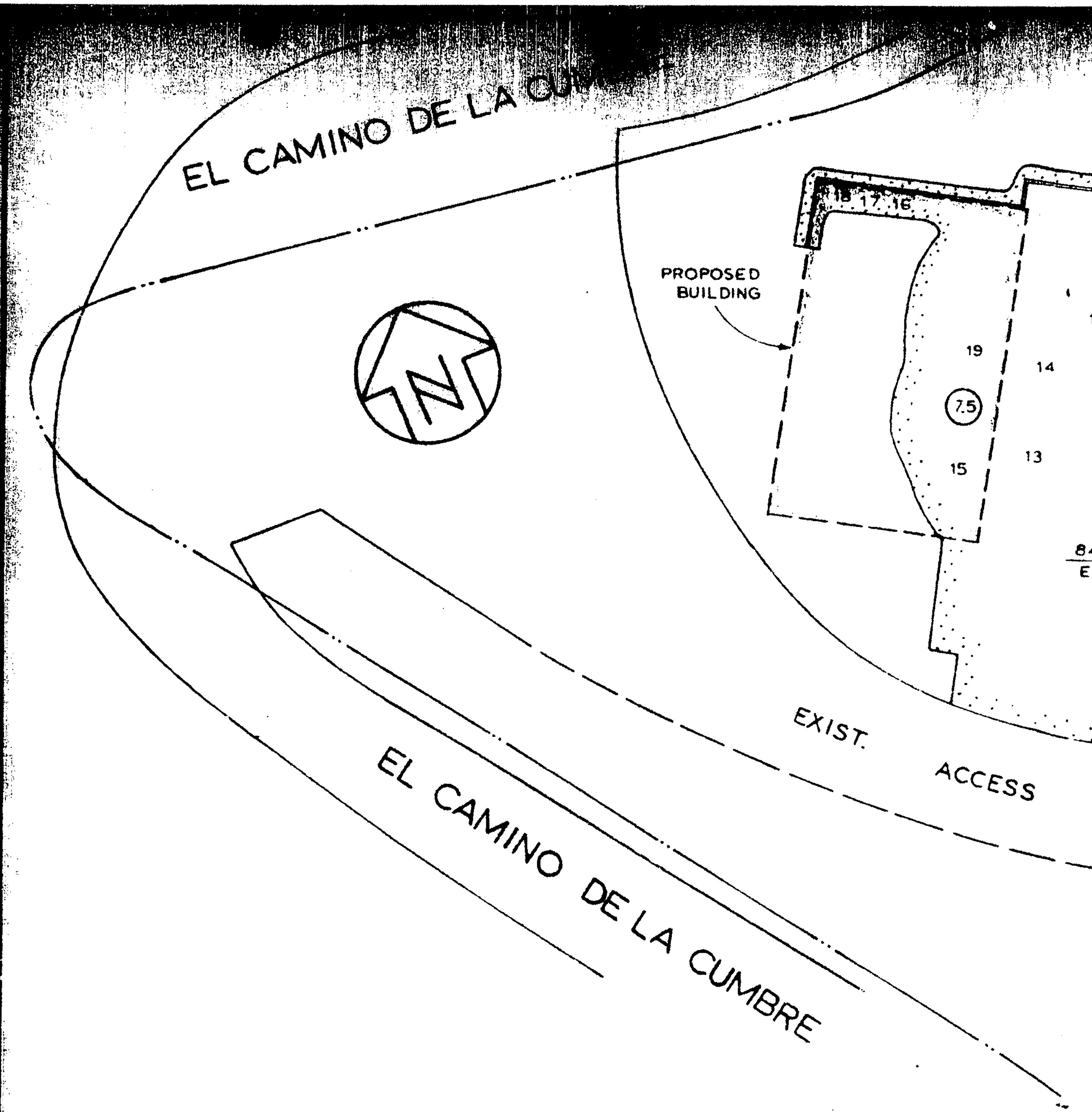


(5.0) INDICATES APPROXIMATE AREA AND DEPTH IN FEET OF CONTROLLED COMPACTED FILL

12 INDICATES NUMBER AND APPROXIMATE LOCATION OF FIELD DENSITY TEST

I,

LOCATION OF CONTROLLED COMPACTED FILL			
PREPARED BY: WTS	PROPOSED MAINTENANCE BUILDING The Buckley School, Sherman Oaks, California for P & A Construction Company, Inc.		DRAWING NUMBER 1
CHECKED BY: HRB			
APPROVED BY: EJJ	DATE Dec. 12, 1972	SCALE 1" = 20'	PROJECT NUMBER: 72-245-D
CONVERSE, DAVIS AND ASSOCIATES	PASADENA • SANTA ANA CALIFORNIA		



REFERENCE:

Site Plan - Unit "E", Sheet A-10/17, Project No. 9585-11, dated 9-10-71, Ragnar C. Qvale & Assoc., Architects.

GRADING APR 18 1968

ADVANCED FOUNDATION ENGINEERING INCORPORATED

CONSULTING FOUNDATION ENGINEERS

3310 AIRPORT WAY
LONG BEACH CALIF 90806
426 3355 426 7386 278 6433
LONG BEACH LOS ANGELES [illegible]

February 16, 1968
Project 67-2746

The Buckley Schools
3900 Stansbury Avenue
Sherman Oaks, California

PROJECT: BUCKLEY SCHOOL
3190 Stansbury Avenue
Sherman Oaks, California

Legal Description. Portion of Lot 1 Tract 23823

SUBJECT: Soil Compaction Tests - Progress Report

This report contains the results of Density Tests Nos. 1 thru 36 taken on the subject project on January 15 thru 30, 1968. Refer to the attached plot plan, Plate "A", for the location of tests.

PREPARATION OF AREAS TO RECEIVE FILL

Prior to the placing of any fill, the area is being cleared of all organic or deleterious material, scarified to a depth of 6 inches and inspected by this [illegible]atory. The area was then recompacted to provide a bonding between natural soils and the fill material.

The natural ground is considered adequate to safely support the imposed fill.

In areas of natural slopes, benches are being cut into firm natural material every 5 feet in vertical height of fill placed to provide an interlocking effect between the fill and natural soil.

PREPARATION OF AREAS TO RECEIVE FILL - continued

The structural area is being excavated to natural soil and recompacted to required relative density of 90%.

The non-structural area is being scarified at existing surface and compacting additional fill placed to 90% of relative density.

PLACING OF THE FILL

The fill material was cut from the site, placed in 6 inch layers, watered to approximate Optimum Moisture, and compacted to the specified relative compaction of 90%.

The contractors attention is being called to areas falling below the required relative compaction. These areas are being reworked, recompacted and retested until they meet the specified relative compaction.

Tests are being taken every 1.5 feet in vertical height of fill placed to insure complete control of grading operations.

EQUIPMENT ON JOB

1 - Cat. D-8 Dozer
1 - John Deere TD-24 Dozer
1 - Dual 5 x 5 Sheepsfoot Roller
1 - Water Truck
1 - Scraper

PROGRESS OF JOB

Structural area tested and approved to Elev. 775± to date.

COMPACTION STANDARD - ASTM D1557-64T

10 pound hammer, 18 inch drop, 25 blows per layer on each of 5 equal layers of soil in a 1/30 cubic foot mold.

February 16, 1968
Project 67-2746

COMPACTION STANDARD - continued

Material Classification	Maximum Density Lbs./Cubic Foot	Optimum Moisture Per Cent
Brown sandy silty clay w/shale fragments	113.0	16.5
Dark brown fine to coarse sandy clay	114.5	16.0
Light brown clay w/diatomaceous and shale fragments	100.0	21.0
Brown silty clay w/shale	110.0	17.0

FIELD DENSITY TESTS

Test No.	Wet Density Lbs./Cu.Ft.	% Field Moisture	Dry Density Lbs./Cu.Ft.	% Maximum Density	Depth of Test	Depth of Fill
1-15-68						
1	125.6	17.0	107.2	94.8	-0.3'	2.0'
2	117.2	16.0	101.0	92.7	-0.5'	3.0'
3	112.6	25.5	89.6	82.4	-1.0'	4.0'
4	122.8	22.6	100.2	92.0	-0.5'	5.0'
1-16-68						
5	124.0	18.3	104.7	92.3	-0.5'	5.0'
6	122.2	16.5	105.0	93.0	-0.5'	6.5'
7	123.2	17.0	105.3	93.3	Retest #3	
8	123.8	18.3	104.5	92.5	-0.5'	2.0'
9	122.0	17.1	104.2	92.3	-1.0'	8.0'
10	124.8	18.3	105.3	93.3	-0.5'	5.0'
11	125.4	19.1	105.3	93.3	-0.5'	5.0'
1-18-68						
12	124.0	18.0	105.0	92.0	-0.5'	4.0'
13	123.8	17.0	105.8	92.4	-0.5'	7.5'
14	121.1	16.0	104.4	91.3	-0.5'	10.0'
15	122.6	18.0	103.8	90.3	-0.5'	2.0'
1-19-68						
16	124.0	17.0	105.9	92.4	-0.5'	13.0'
17	121.4	16.5	104.2	91.0	-0.5'	8.5'
18	107.6	16.5	107.5	94.0	-0.5'	5.0'
1-22-68						
19	128.0	18.0	108.5	94.5	-0.5'	15.0'
20	119.0	15.0	103.5	90.3	-0.5'	13.0'
21	120.7	15.0	104.4	91.4	-0.5'	3.0'
22	126.4	17.0	108.0	94.3	-0.5'	3.0'
1-26-68						
23	111.2	20.5	91.5	91.5	-1.0'	15.0'
24	119.2	20.0	99.4	90.3	-1.0'	17.0'
25	115.8	16.0	99.7	90.7	-0.5'	19.0'
26	120.2	18.0	103.0	92.5	-1.0'	17.0'
27	121.4	22.0	101.2	92.0	-1.0'	8.0'

February 16, 1968
Project 67-276

FIELD DENSITY TESTS - continued

Test No.	Wet Density Lbs./Cu.Ft.	% Field Moisture	Dry Density Lbs./Cu.Ft.	% Maximum Density	Depth of Test	Depth of Fill
1-29-68						
28	106.8	20.5	83.5	83.5	-1.0'	7.0'
29	117.4	25.5	93.5	93.5	-1.0'	20.0'
30	110.0	21.5	90.5	90.9	-1.0'	18.0'
31	116.6	25.5	92.7	92.0	Retest #28	
1-30-68						
32	116.4	27.4	91.3	91.3	-1.0'	20.0'
33	112.6	23.4	91.0	91.0	-1.0'	23.0'
34	117.6	25.0	94.0	94.0	-1.0'	6.0'
35	116.4	24.0	93.8	93.8	-1.0'	12.0'
36	115.4	33.0	87.0	87.0	-1.0'	19.0'

ADVANCED FOUNDATION ENGINEERING, INC.

Stanley C. Davidson

P. L. Bailey
Civil Engineer

SCD:PLB:lr

cc: The Buckley Schools/3
R. C. Uvalo & Assoc.
Otis Moore

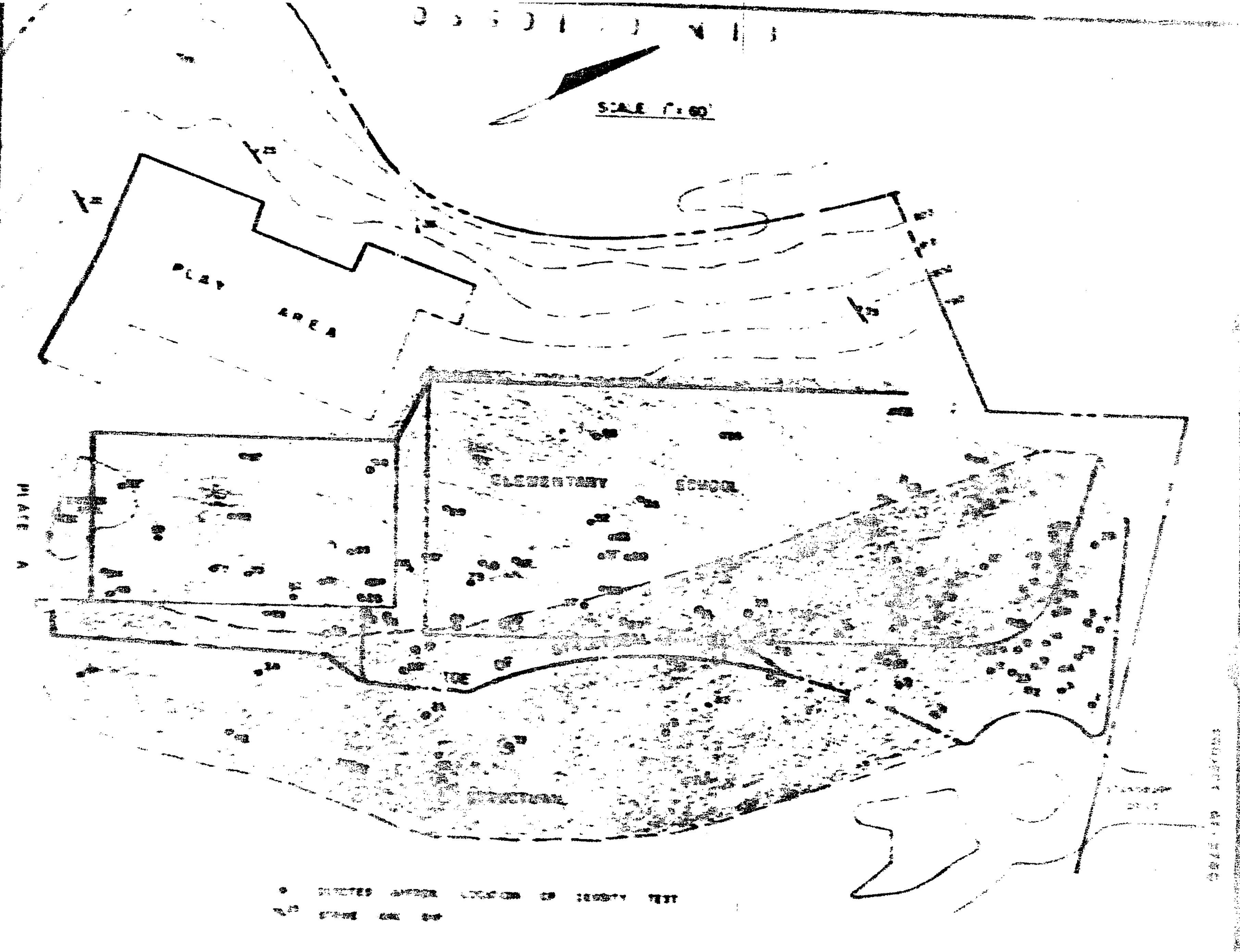


PLATE A

CONSULTING FOUNDATION ENGINEERS

April 4, 1968
Project 68-2746

The Buckley Schools
3900 Stansbury Avenue
Sherman Oaks, California

PROJECT: BUCKLEY SCHOOL
3190 Stansbury Avenue
She[illegible]n Oaks, California

Legal Description: Portion of Lot 1 Tract 23883

SUBJECT: Soil Compaction Tests - Progress Report No. 2

This report contains the results of Density Tests Nos. 37 thru 83 taken on the subject project on February 2 thru March 30, 1968. Refer to the attached plot plan, Plate "A", for the location of tests.

PREPARATION OF AREAS TO RECEIVE FILL

Prior to the placing of any fill, the area is being cleared of all organic or deleterious material, scarified to a depth of 6 inches and inspected by this laboratory. The area was then recompacted to provide a bonding between natural soils and the fill material.

The natural ground is considered adequate to safely support the imposed fill.

In areas of natural slopes, benches are being cut into firm natural material every 5 feet in vertical height of fill placed to provide an interlocking effect between the fill and natural soil.

STRUCTURAL AREA

The structural area is being excavated to natural soils and recompacted to required relative density of 90%.

NON-STRUCTURAL AREA

The non-structural area is being scarified at existing surface and compacting additional fill placed to 90% of relative density.

PLACING OF THE FILL

The fill material was cut from the site and imported, placed in 8 inch layers, watered to approximate Optimum Moisture, and compacted to the specified relative compaction of 90%.

The contractor's attention is being called to areas falling below the required relative compaction. These areas are being reworked, recompacted and retested until they meet the specified relative compaction.

Tests are being taken every 1.5 feet in vertical height of fill placed to insure complete control of grading operations.

EQUIPMENT ON JOB

1 - Cat. D-8 Dozer
1 - John Deere TD-24 Dozer
1 - Dual 5 x 5 Sheepsfoot Roller
1 - Water Truck
1 - Scraper

PROGRESS OF JOB

Fill tested to finish grade at north end and to 5' below finish grade at south end on structural area.

Tested to 3' above existing grade on non-structural area shown on plot plan.

COMPACTION STANDARD - ASTM D1557-64T

10 pound hammer, 18 inch drop, 25 blows per layer on each of 5 equal layers of soil in a 1/30 cubic foot mold.

Material Classification	Maximum Density Lbs./Cubic Foot	Optimum Moisture Per Cent
Dark brown fine to coarse sandy clay	114.5	16.0
Light brown fine clay w/diatomaceous and shale fragments	100.0	21.0
Brown silty clay w/shale (import)	110.0	17.0
Light brown clayey medium to coarse sand (import)	119.5	13.0
Yellow brown clay w/diatomaceous (import)	99.5	23.5
Red[illegible] brown clayey fine to coarse sand (import)	125.0	13.5
Light brown clay w/sandstone (import)	116.0	17.0

FIELD DENSITY TESTS

Test No.	Wet Density Lbs./Cu.Ft.	% Field Moisture	Dry Density Lbs./Cu.Ft.	% Maximum Density	Depth of Test	Depth of Fill
2-2-68						
37	122.4	30.0	94.5	94.5	-1.0'	25.0'
38	118.0	29.0	91.3	91.3	-1.0'	16.0'
39	113.2	25.0	90.7	90.7	Retest #36	
40	121.8	32.7	92.5	92.5	-1.0'	5.0'
41	116.8	28.0	91.2	91.2	-0.2'	1.5'
42	115.4	30.0	89.0	89.0	-0.3'	1.5'
43	120.6	29.0	93.3	93.3	-0.2'	2.0'
2-5-68						
44	116.2	16.0	100.4	91.3	-1.0'	12.0'
45	112.0	22.0	91.7	91.7	-1.0'	26.0'
46	111.4	22.0	91.3	91.3	-1.0'	14.0'
47	120.2	18.0	103.0	92.7	-1.0'	14.0'
2-26-68						
48	125.0	23.5	101.0	92.0	-0.5'	2.5'
49	121.0	22.0	99.2	90.2	-0.5'	2.5'
50	120.2	20.0	100.1	91.2	-0.5'	1.5'
51	122.4	22.0	100.4	91.3	-0.5'	4.5'
52	117.6	13.6	103.7	91.0	-0.5'	5.0'
53	123.4	22.0	101.2	92.2	-0.5'	4.0'
2-27-68						
54	120.4	19.0	101.2	92.2	-1.0'	8.0'
55	121.0	20.0	100.8	91.5	-1.0'	27.0'
56	120.2	18.0	102.0	93.0	-1.0'	22.0'

April 4, 1968
Project 68-2746

FIELD DENSITY TESTS - continued

Test No.	Wet Density Lbs./Cu.Ft.	% Field Moisture	Dry Density Lbs./Cu.Ft.	% Maximum Density	Depth of Test	Depth of Fill
3-1-68						
57	112.8	13.0	99.9	90.7	-1.0'	26.0'
58	116.8	14.9	101.7	92.4	-1.0'	19.0'
3-20-68						
59	116.4	16.3	100.2	91.0	-1.0'	6.0'
60	124.8	19.1	104.6	91.3	-1.0'	2.0'
61	129.6	13.0	114.3	91.4	-1.0'	29.0'
62	121.4	11.1	109.0	90.[illegible]	-1.0'	27.0'
3-27-68						
63	125.8	13.5	110.7	92.5	-0.5'	3.0'
64	125.0	13.0	110.8	92.6	-0.5'	6.5'
65	130.0	15.0	113.0	94.5	-0.3'	2.5'
3-28-[illegible]						
66	115.6	10.0	104.9	83.7	-0.5'	5.0'
67	135.6	13.0	119.8	95.7	Retest #66	
68	127.0	14.9	110.0	88.2	-0.5'	22.0'
3-29-68						
69	131.1	14.9	118.0	94.7	-0.5'	8.0'
70	113.0	14.3	98.8	79.2	-0.5'	11.0'
71	131.0	14.9	114.0	91.3	Retest #68	
72	116.3	14.9	101.2	81.2	-0.5'	8.0'
73	127.0	13.0	112.3	90.0	Retest #70	
3-30-68						
74	136.2	15.0	118.0	93.4	Retest #72	
75	129.1	14.9	112.3	90.3	-1.0'	28.0'
76	127.6	11.0	115.0	92.0	-1.0'	21.0'
77	120.2	11.0	108.4	87.0	-1.0'	24.0'
78	119.0	10.0	108.3	86.5	-0.5'	18.0'
79	108.4	19.1	90.7	90.7	Retest #78	
80	136.2	19.0	116.5	91.7	Retest #77	
81	134.6	18.0	113.9	91.2	-1.0'	10.0'
82	122.5	12.0	109.2	91.5	-1.0'	19.0'
83	128.8	13.5	113.3	90.7	-0.5'	22.0'

ADVANCED FOUNDATION ENGINEERING, INC.

Stanley C. Davidson

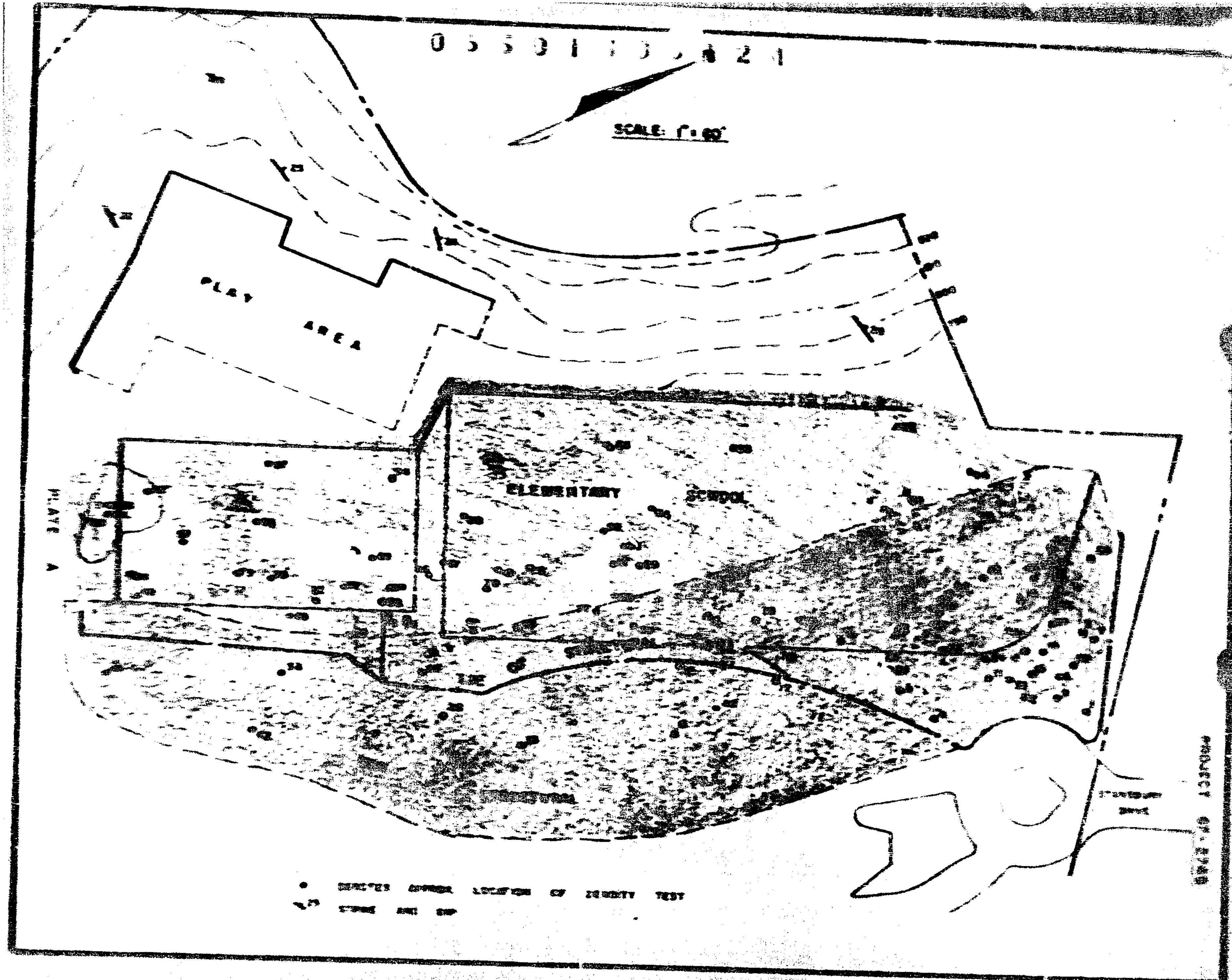
Syed Z. Ahmad
R.C.E. 16621

SCD,SZA:lr

cc Buckley Schools/3
R. C. Qvale & Assoc.
Otis Moore

ADVANCED FOUNDATION ENGINEERING, INC

ADVANCED FOUNDATION ENGINEERING INCORPORATED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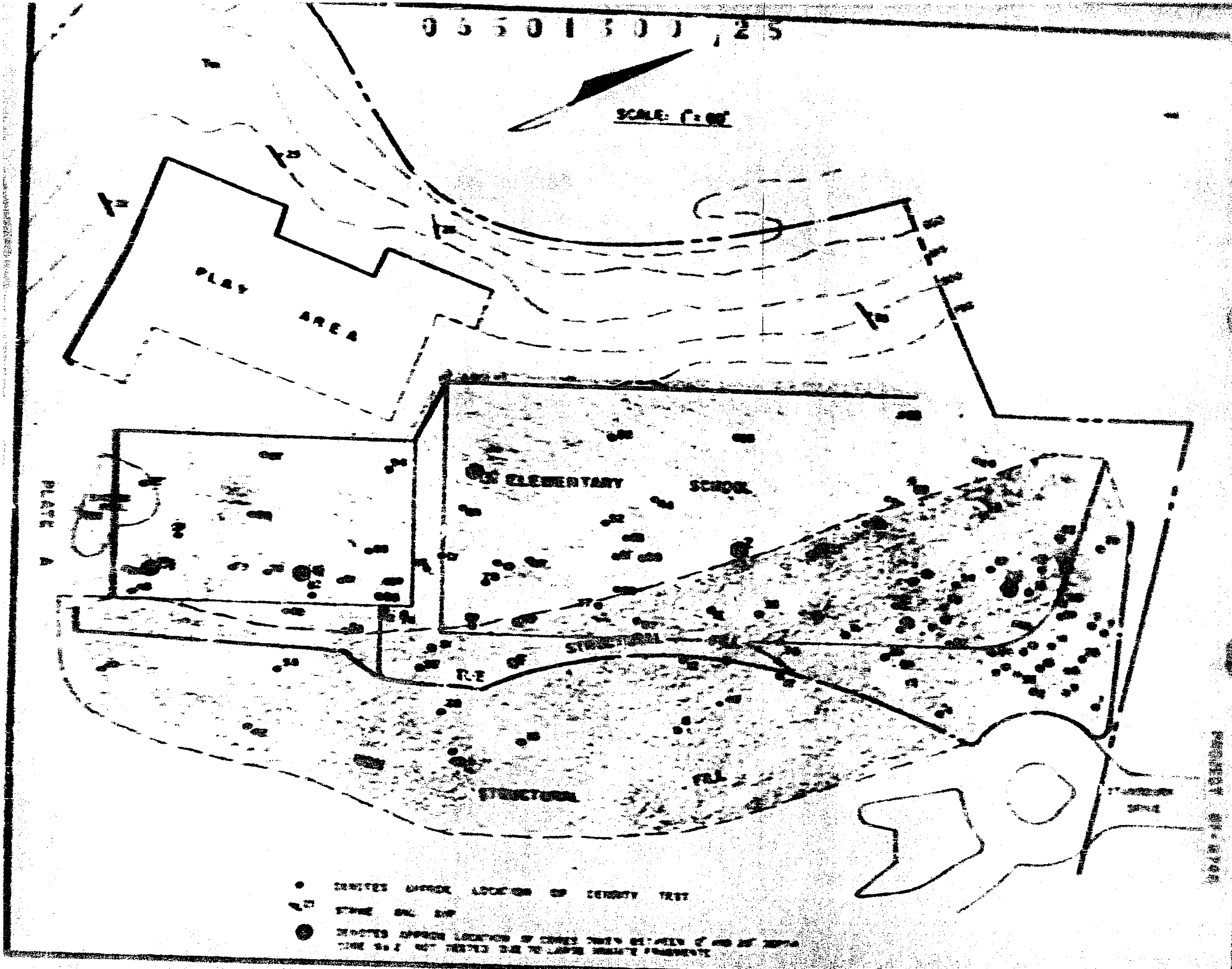
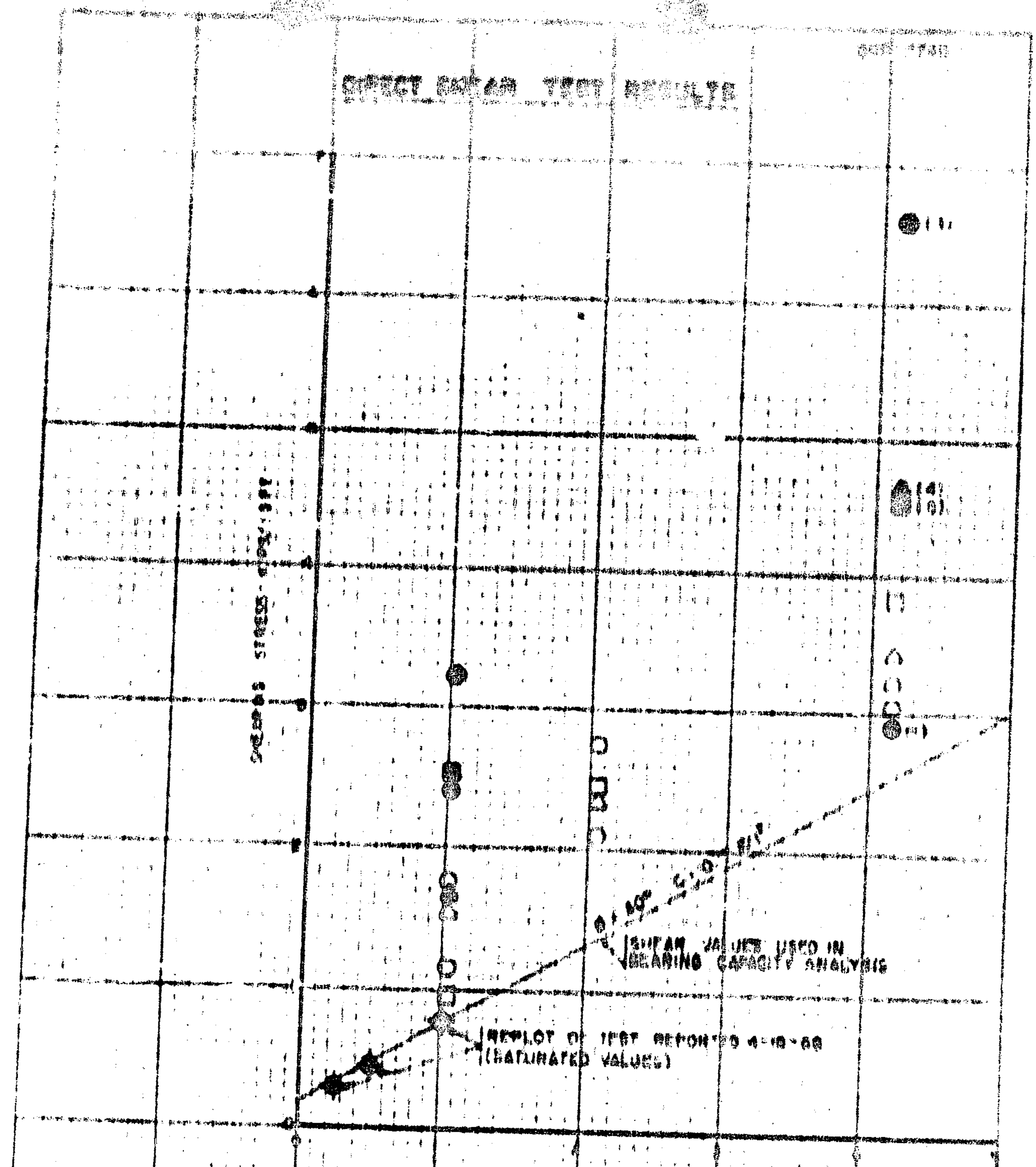
PLAY AREA
ELEMENTARY SCHOOL
PROJECT 67-2748
DENOTES APPROX. LOCATION OF DENSITY TEST
STRIKE AND DIP
PLATE A



0550150025
SCALE: 1"=80'
PLAY AREA
ELEMENTARY SCHOOL
STRUCTURAL
STRUCTURAL FILL
DENOTES APPROX. LOCATION OF DENSITY TEST
STRIKE AND DIP
PLATE A



( ) DENOTES SAMPLE NUMBER - REFER TO PLATE A FOR LOCATION AND DEPTH
● TESTED AT FIELD MOISTURE CONTENTS
○ TESTED AT INCREASED MOISTURE CONTENTS

PLATE 6

P. L. DAILEY

CITY OF LOS ANGELES

DEPARTMENT OF BUILDING AND SAFETY

ENGINEER'S CERTIFICATE OF COMPLIANCE FOR CONSOLIDATED EARTH FILLS

LEGAL DESCRIPTION: Portion of Lot 1, Tract 23023

SOIL TESTING AGENCY: ADVANCED FOUNDATION ENGINEERING, INC.

PROPERTY OWNER'S NAME: Buckley School

OWNER'S ADDRESS: [redacted], Sherman Oaks, California

AREA TESTED: Structural Areas

PER REPORTS ON OUR PROJECT NO.: 68-2766

DATE WORK STARTED ON PROJECT: December 26, 1967

DATE FILL WAS COMPLETED: April 8, 1968

DATE OF THIS CERTIFICATE: April 12, 1968

TO THE SUPERINTENDENT OF BUILDING:

*I hereby certify that I have personally supervised the placing of consolidated earth fill on the above described property, and that the same was placed in conformity with requirements of the Los Angeles Building Code of the City of Los Angeles.

Civil Engineer
California Certificate No. 6128

RECEIVED
APR 1 3 1968

My address is: 3310 Airport Way - Long Beach, California 90806

*For the purpose of this Certificate, to "have personally supervised" shall include supervision performed by any person or persons employed by, and responsible to, the licensed engineer signing this certificate. Where the supervision of all or part of the work above is delegated, full responsibility shall be assumed by the licensed engineer whose signature is affixed hereon.

ADVANCED FOUNDATION ENGINEERING INCORPORATED

CONSULTING FOUNDATION ENGINEERS

3310 AIRPORT WAY
LONG BEACH, CALIF. 90806
426-3355 636-7386 870-6432
LONG BEACH LOS ANGELES [illegible]

OFFICERS
[illegible] BAILEY - President
[illegible] AHMAD - Asst. Vice Pres.
STANLEY C. DAVIDSON - Vice Pres.
MARTIN C. CALAWAY - Secretary
[illegible] HARRINGTON - Treasurer

April 12, 1968
Project 68-2746

The Buckley Schools
3900 Stansbury Avenue
Sherman Oaks, California

PROJECT: BUCKLEY SCHOOL
3900 Stansbury Avenue
Sherman Oaks, California

Legal Description: Portion of Lot 1 Tract 23823

SUBJECT: Soil Compaction Tests - Final Report on Structural Areas

This report contains the results of Density Tests Nos. 84 thru 95 taken on the subject project on April 1 thru 8, 1968. Refer to the attached plot plan, Plate "A", for the location of tests. This report should be used in conjunction with progress reports 1 and 2.

PREPARATION OF AREAS TO RECEIVE FILL

Prior to the placing of any fill, the area is being cleared of all organic or deleterious material, scarified to a depth of 6 inches and inspected by this laboratory. The area was then recompacted to provide a bonding between natural soils and the fill material.

The natural ground is considered adequate to safely support the imposed fill. In areas of natural slopes, benches are being cut into firm natural material

PREPARATION OF AREAS TO RECEIVE FILL - continued

every 5 feet in vertical height of fill placed to provide an interlocking effect between the fill and natural soil.

NON-STRUCTURAL AREA

The non-structural area is being scarified at existing surface and compacting additional fill placed to 90% of relative density.

PLACING OF THE FILL

The fill material was cut from the site and imported, placed in 8 inch layers, watered to approximate Optimum Moisture, and compacted to the specified relative compaction of 90%.

The contractor's attention was being called to areas falling below the required relative compaction. These areas were reworked, recompacted and retested until they meet the specified relative compaction.

Tests were taken every 1.5 feet in vertical height of fill placed to insure complete control of grading operations.

EQUIPMENT ON JOB

- 1 - Cat. D-8 Dozer
- 1 - John Deere TD-24 Dozer
- 1 - Dual 5 X 5 Sheepsfoot Rooler
- 1 - Water Truck
- 1 - Scraper

PROGRESS OF JOB

Fill tested to finish grade on structural area, additional fill is being placed in non-structural areas.

RECOMMENDATION

All recommendations contained in our Preliminary Foundation Investigation dated October 30, 1967 Project #M67-515 has been complied with and Bearing Values and recommendation contained therein should be used.

COMPACTION STANDARD - ASTM D1557-64T

10 pound hammer, 18 inch drop, 25 blows per layer on each of 5 equal layers of soil in a 1/30 cubic foot mold.

Material Classification	Maximum Density Lbs./Cubic Foot	Optimum Moisture Per Cent
Dark brown fine to coarse sandy clay	114.5	16.0
Light brown fine clay w/diatomaceous and shale fragments	100.0	21.0
Brown silty clay w/shale (Import)	110.0	17.0
Light brown clayey medium to coarse sand (Import)	119.5	13.0
Yellow brown clay w/diatomaceous (Import)	99.5	23.5
Reddish brown clayey fine to coarse sand (Import)	125.0	13.5
Light brown clay w/sandstone (Import)	116.0	17.0
Light brown very fine to medium sandy clay	109.5	18.5

FIELD DENSITY TESTS

Test No.	Wet Density Lbs./Cu.Ft.	% Field Moisture	Dry Density Lbs./Cu.Ft.	% Maximum Density	Depth of Test	Depth of Fill
4-1-68						
84	114.2	12.4	101.3	92.4	-0.5'	14.0'
85	120.6	14.9	104.9	95.6	-0.5'	7.0'
86	116.0	14.3	101.3	92.4	-1.0'	3.0'
87	116.0	14.9	101.0	92.2	-1.0'	3.0'
4-4-68						
88	115.0	14.0	101.6	92.0	-0.5'	21.0'
89	118.0	15.0	102.4	93.6	-1.0'	14.0'
90	119.2	18.5	100.5	91.8	-0.5'	18.0'
91	122.8	20.5	101.7	92.7	-0.5'	20.0'

April 12, 1968
Project 68-2746

FIELD DENSITY TESTS - continued

Test No.	Wet Density Lbs./Cu.Ft.	% Field Moisture	Dry Density Lbs./Cu.Ft.	% Maximum Density	Depth of Test	Depth of Fill
4-8-68						
92	117.6	12.0	105.0	95.6	-0.3'	5.0'
93	119.0	15.0	103.3	94.5	-0.4'	5.0'
94	115.8	14.0	101.6	92.6	-0.2'	4.0'
95	118.2	14.0	103.7	94.7	-0.3'	4.0'

ADVANCED FOUNDATION ENGINEERING, INC.

Stanley C. Davidson

P. L. Bailey
Civil Engineer

SCD:PLB:am

cc: Buckley Schools - 3
R. C. Qvale & Assoc.
Oris Moore

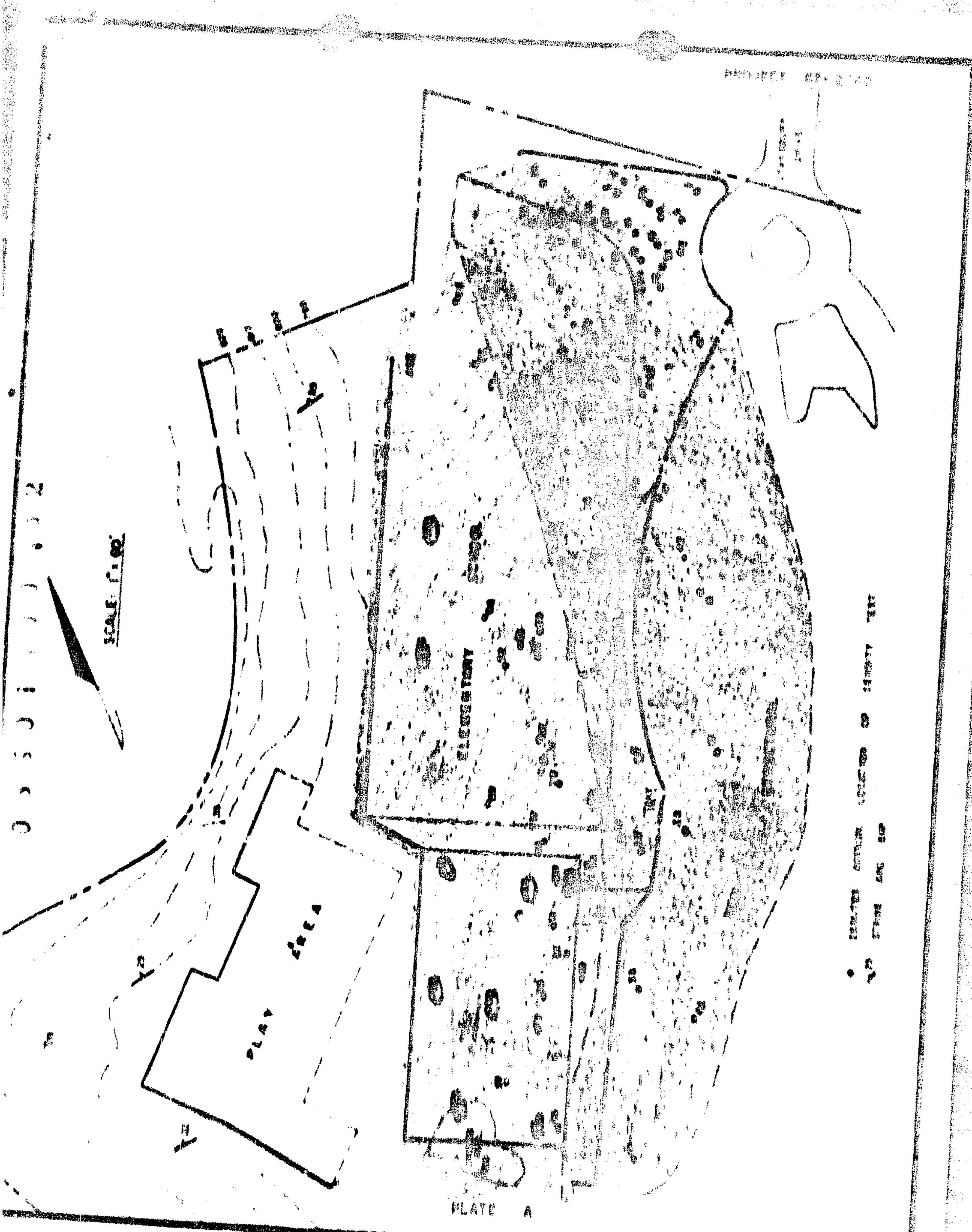


PLATE A

CITY OF LOS ANGELES
CALIFORNIA

DEPARTMENT OF
BUILDING AND SAFETY

Isabelle Buckley Schools
3190 Stansbury Avenue
Sherman Oaks, California

TRACT: 23823
LOT: 1
LOCATION: 3900 Stansbury Avenue

DATE: April 25, 1968
PERMIT: LA 58345

Fill soil classification, per Table 28-A: Sandy Clay

Lots having compacted fill:

Approval is granted for compacted fill constructed on the above lots as described in the compaction report dated [illegible], [illegible], [illegible], [illegible] prepared by Advanced Foundation Engineering, Inc., Report No. 68-2746.

Approval is limited to the area shown in the report and by the following requirements:

A. Footings for one-story wood frame structures may be dimensioned from Table 17-R without use of the soil bearing value.
B. Footing bearing pressure for all other structures shall not exceed a value of 2200 lbs. per sq. ft. at 1800 inches minimum, below approved compacted surface.
C. Continuous footings per Code Section 91.3012 are required.
D. All footings supported partly or wholly on compacted fill shall be reinforced continuously with at least one number 4 bar at the top and bottom of the footing.
E. Slope erosion control, planting, and irrigating of fill slopes, and runoff control are required as per Code Section 91.3007.
F. Building or structure footings shall be set back 5 feet from the face of slopes 20 feet or less in vertical height where the angle of slope is between 1½ horizontal to 1 vertical and two horizontal to 1 vertical. Where the vertical height of slope exceeds 20 feet and the angle of slope is as described above the set back shall be increased 1 foot for each additional 5 feet in vertical height over 20 feet to a maximum set back of 10 feet. For slopes exceeding 100 feet in vertical height, the set back shall be 40 feet except as permitted in Code Section 91.3009 (c).
G. Refer to above reports for location of non-structural fill areas.
H. Refer to above report, dated April 18, 1968, for additional requirements pertaining to minimum footing depths.

Superintendent of Building

By____________________
R. W. HARRINGTON
Grading Engineer

DM# 7907

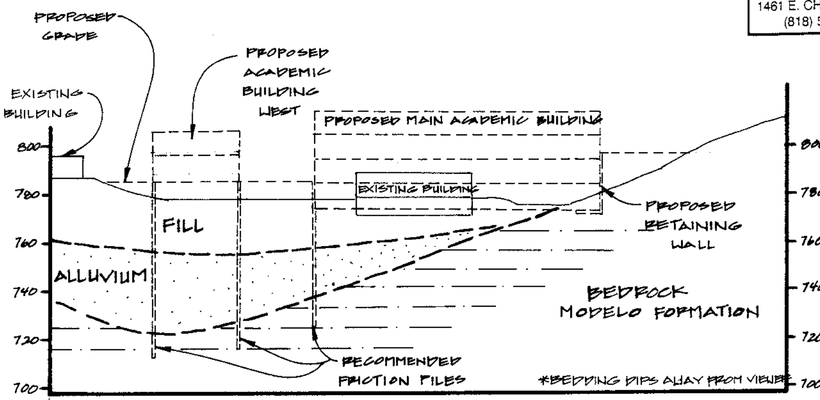
B&S B-142 R1.68

RWH:em
cc: Advanced Foundation Engineering, Inc.

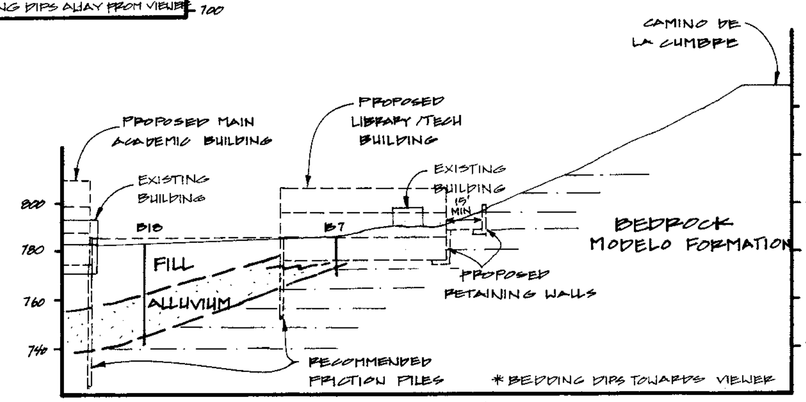
THE J. BYER GROUP, INC.
[redacted]
1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

SECTION A & B	
JB: 19376-B THE BUCKLEY SCHOOL	
CONSULTANT: JET	SCALE: 1"=40'

JUNE 6, 2006



SECTION A



SECTION B

11x17

THE J. BYER GROUP, INC.

1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

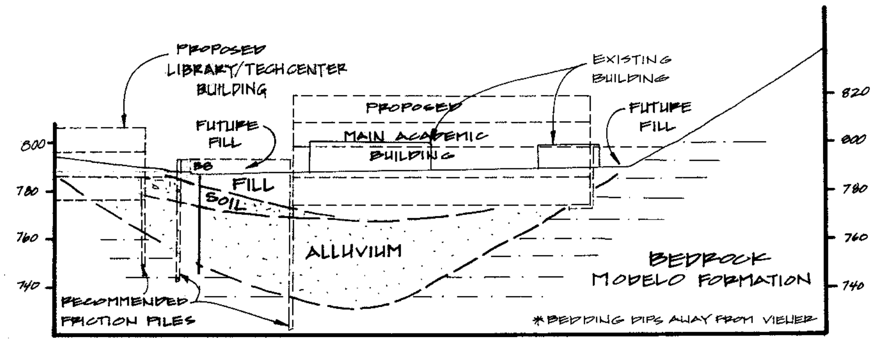
SECTION C & D

JB: 19376-B THE BUCKLEY SCHOOL

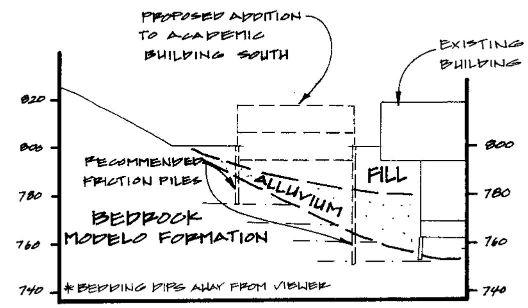
CONSULTANT: JET

SCALE: 1"=40'

JUNE 6, 2006



SECTION C



SECTION D

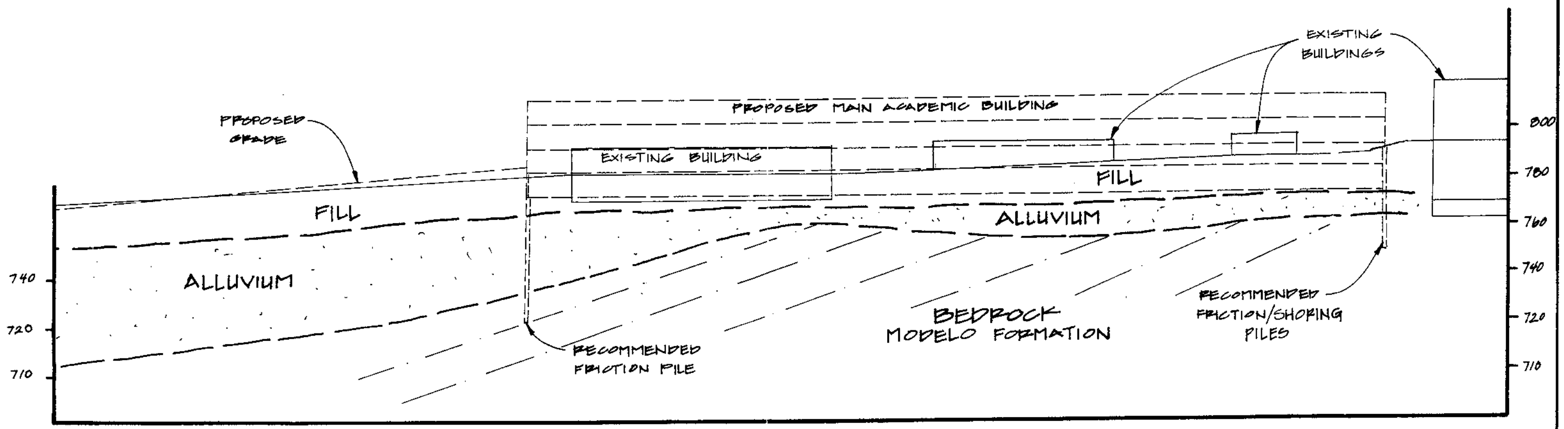
11x17

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

SECTION E

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JET | SCALE: 1"=40'



SECTION E

11x17

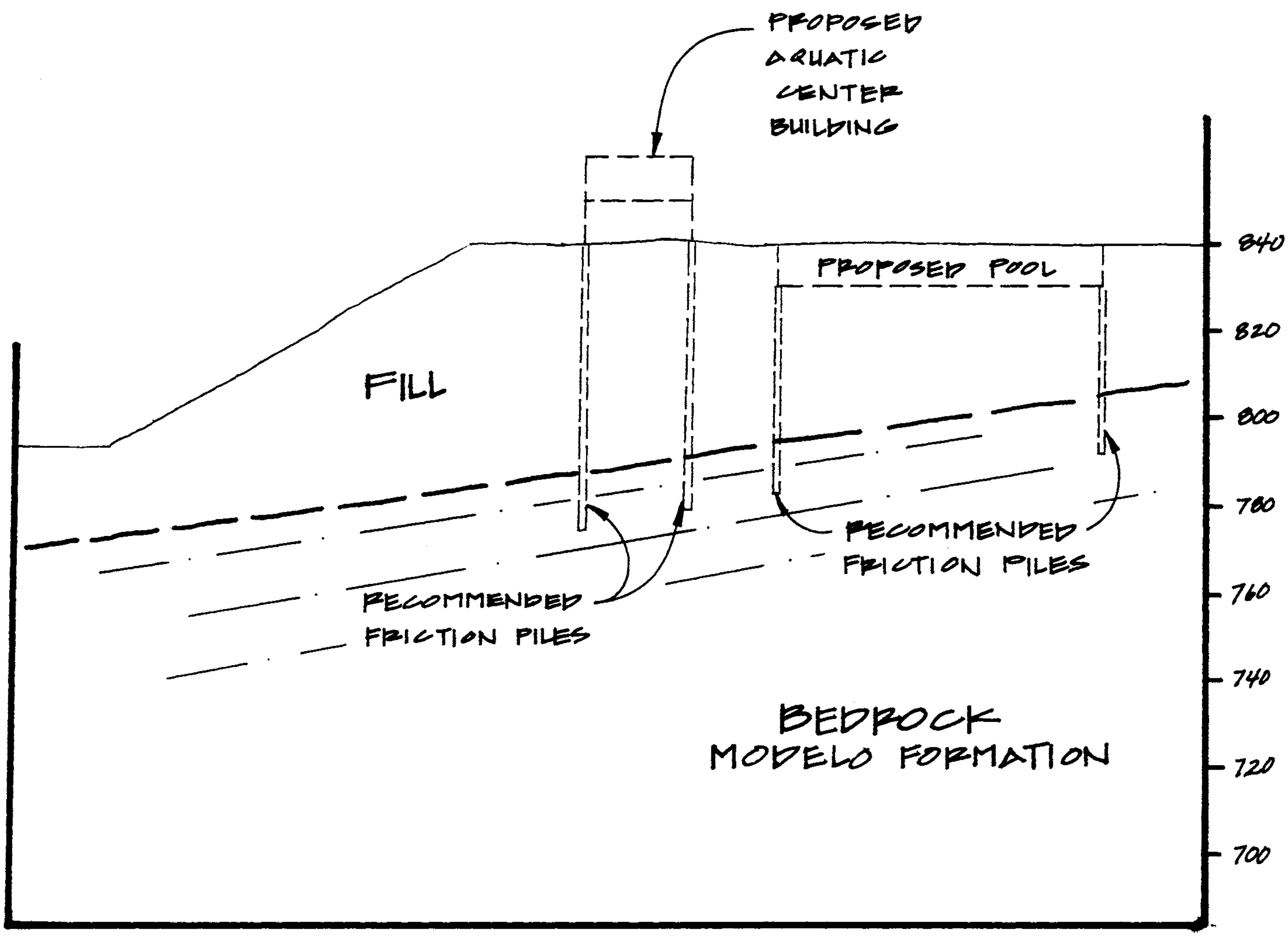
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

SECTION F

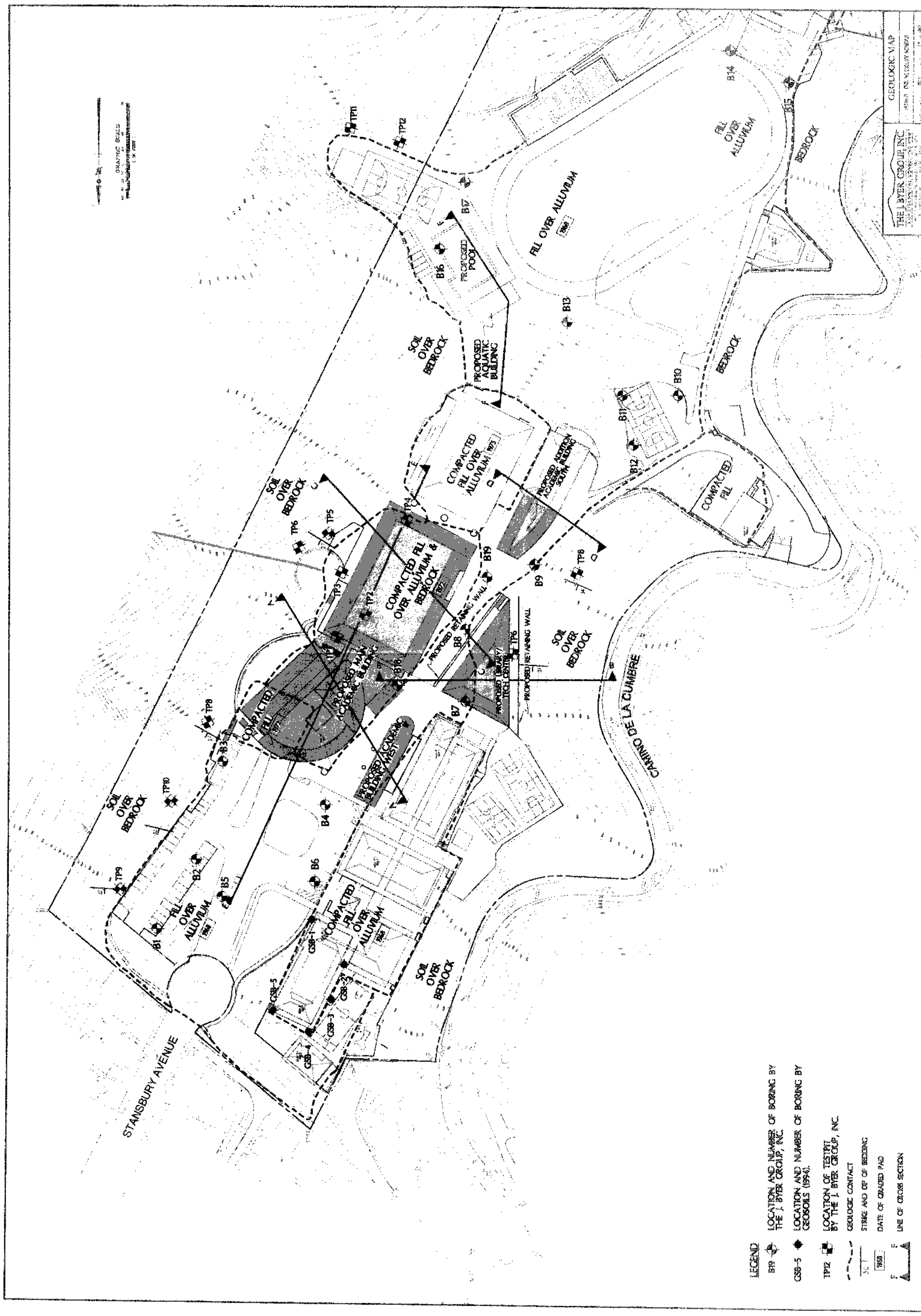
JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JET

SCALE: 1"=40'



SECTION F


GEOLOGIC MAP
THE J. BYER GROUP, INC.
STANSBURY AVENUE
CAMINO DE LA CUMBRE
SOIL OVER BEDROCK
FILL OVER ALLUVIUM
COMPACTED FILL OVER ALLUVIUM & BEDROCK
COMPACTED FILL OVER ALLUVIUM
COMPACTED FILL
BEDROCK
PROPOSED AQUATIC BUILDING
PROPOSED POOL
PROPOSED RETAINING WALL
LEGEND
LOCATION AND NUMBER OF BORING BY THE J. BYER GROUP, INC.
LOCATION AND NUMBER OF BORING BY GEOSOILS (1994)
LOCATION OF TESTPIT BY THE J. BYER GROUP, INC.
GEOLOGIC CONTACT
STRIKE AND DIP OF BEDDING
DATE OF GRADED PAD
LINE OF CROSS SECTION

11x17

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. CHEVY CHASE DR. #200, GLENDALE, CA 91206
818•549•9959 TEL 818•543•3747 FAX
"Trust the Name You Know"

October 20, 2006
JB 19376-B

The Buckley School
% Jeffrey M. Kalban & Associates
10780 Santa Monica Boulevard, Suite 120
Los Angeles, California 90025-4749

Attention: Susan Oakley

Subject

Addendum Geologic and Soils Engineering Exploration
Proposed Addition, Four New Buildings, Retaining Walls, and Swimming Pool
The Buckley School
Lot 1, Tract 23823
3900 Stansbury Avenue
Sherman Oaks, California

References: Report by The J. Byer Group, Inc.:

Geologic and Soils Engineering Exploration, Proposed Addition, Four New Buildings, Retaining Walls, and Swimming Pool, The Buckley School, Lot 1, Tract 23823, 3900 Stansbury Avenue, Sherman Oaks, California, dated June 6, 2006.

Response Letter by City of Los Angeles (LADBS):

Geology and Soils Report Correction Letter, Log # 54269, dated September 1, 2006.

Gentlepersons:

The J. Byer Group, Inc., has completed our addendum report which provides the additional information requested by the City of Los Angeles, Department of Building and Safety.

RESPONSE

1. *Identify the access road from the school entrance to the athletic field and the existing storm drains, on the map and on the appropriate cross-sections. Provide an evaluation of the settlement characteristics of the existing fill and a detailed justification demonstrating that potential future settlement of the fill, will not result in future damage or excessive settlement to the access road surface. Alternatively, revise recommendations for new fill, to be placed in compliance with section 7011.3 of the LA City Building Code and identify details on the map and cross-sections.*

Response: The existing access road and the easement for storm drain and sewer purposes have been plotted on the enclosed Geologic Map and cross Sections A, B, C, and D. Cross Section A was used to evaluate future settlement from the proposed fill to be placed over the existing fill. Our calculations indicate that up to five inches of settlement could occur as a result of placing fill over the existing fill. This settlement could affect the existing sewer and storm drain pipes which are shown on Section A. As an alternative to using fill to raise the grades, the proposed access road could be supported on a structural deck which can derive support from the piles for the proposed main academic building and the piles for the academic building to the west. The proposed project as shown on the enclosed Geologic Map is a conceptual master plan drawing which may be revised. The purpose of the report is to submit the master plan to the various agencies for their review and comment. The department will be provided with plan review and update reports as the project is prepared for submittal to the building department.

2. *The report indicates (see pages 4 and 12) that the "natural drainages" which enter from the east can be sources of eroded soil material and will carry natural runoff, on to the site. Provide recommendations for mud/debris flow control systems within and at the base of concentrated drainage areas using the minimum design parameters specified in section 7014.3 of the LA City Building Code. The entire contributing watershed area on the slopes above the property shall be identified on the topographic map. If such evaluation is to be performed by a licensed civil engineer, include a wet-signed original and two copies with the addendum.*

Response: The secondary drainages will be captured through the use of debris basins and storm drains. These features will be designed by the project civil engineer. The current report is a planning document with respect to obtaining approval for a master plan. Details of the grading and drainage will be furnished at a later date.

3. *Explain what the approximately 220-feet long (and about 2-feet-wide) line on the map shown on the slope within the existing natural drainage course (above location TP-3 and the curvilinear structure), represents. Note: A similar line on the map is also shown within the natural drainage area in the southern portion of the site (canyon to the east of locations TP-11 and TP-12). If the line represents an existing pipe or other device that conveys slope drainage, provide recommendations and show on the map how drainage will be conveyed around the buildings in a non-erosive device to a location that is acceptable to the Department.*

Response: The two-foot wide line shown on the map is drafting error. The original survey shows that the bottom of the drainage course in its natural condition. The line shown on the map above the athletic field bleachers is a dirt path. Details of the site drainage plan are not available, but will be provided at a later date. The current map shows the proposed master plan which will require approval at the various agencies. Once approved, detailed plans will be provided the department.

4. *Provide the test pit logs for exploration conducted at locations TP-11 and TP-12.*

Response: Test Pits 11 and 12 were not excavated and were deleted from the exploration program. Therefore, no logs exist. The Geologic Map has been revised.

5. *Explain what the two curvilinear structures shown east of the proposed Main Academic Building represent. Indicate if these structures are existing , or proposed. If they are existing, clarify if they will be removed or if they will remain. If they are proposed, explain if they will part of the proposed building or, will be detached from the building.*

Response: The curved structure is a seat wall for the lunch area. The larger structure to the north is also a concrete seat wall.

6. *It appears from the recommendations provided on page 20 of the report, that removal of the porous, unsuitable upper portion of the alluvium will be required if the floor slab of the Main Academic Building is to be supported on newly-placed certified compacted fill. Shoring is planned to facilitate removal along the west and south sides. Clarify how any removals for building construction and setback wall/slope protection wall construction, will be achieved along the southeastern portion of the building and along the entire length of the building, on the east side.*

Provide additional geologic cross-sections drawn through the proposed building, any setback wall and/or slope protection walls proposed and, the immediate slope located above the walls to illustrate the proposed construction.

Response: The final design of the Academic Building and the finished floor elevations are not determined. This report is a planning document for approval of the Master Plan. The Department will be furnished with a plan review and update report for each of the structures and developments shown on the Master Plan during the building permit process. All removals, temporary slopes, grading, and structures will conform to the requirements of LADBS. The proposed structure will conform to the Building Setback code as required by LADBS. Additional cross sections are not necessary at this time, but will be provided for the plan review and update report once the formal plans are available.

7. *Verify using the sections requested, that the entire face of the new Main Academic Building will be provided the required level clearance building setback and, identify the required setback on all cross-sections drawn through the Main Academic Building.*

Response: The proposed academic building is shown on Sections A and C, which indicate adequate setback from the ascending natural slope. Formal plans for the project have not been prepared and await approval of the master plan by the various agencies. The proposed academic building will conform to all applicable codes of the LADBS.

8. *It appears from the documented geologic orientation (N88W; 31N) plotted on the map, that the correct location for test pit TP-6 is between the proposed toe of slope wall and the Library Building. A location TP-6 is also shown on the east side of the proposed Main Academic building (east of TP-5). Please explain, verify and correct, as necessary. Provide an exploration log, if applicable.*

Response: Test Pit 6 is on the west side of the project located at the point where the excavation was performed. The bedding plane attitude is shown west of the test pit because of the crowded nature of the lettering on the map. Test Pit 6, shown east of the Academic Building, was deleted and moved to the west side as plotted on the Geologic Map. The bedding plane orientations shown on the Geologic Map are consistent on both the east and west sides of the main canyon and are consistent with trends from north to south. These bedding plane attitudes were obtained from the test pits and are considered more reliable than the regional attitudes shown on the City Map.

9. *The geologic data on the slope above the proposed Main Academic Building is limited to the one orientation from location TP-5. The mapped strike and dip on the City map page 67, shown on the slope in this area, indicates a near east-west strike and a north dip of 16 degrees. Provide additional data with regard to the bedrock orientation on the slope using additional mapping and/or exploration.*

Response: The geologic data at the site is consistent on both the east and west sides of the central canyon. Bedding plane attitudes measured by The J. Byer Group are consistent with those shown on the Regional Geologic Map prepared by the Dibblee Foundation in 1991.

10. *It appears that geologic cross-section I-I was not drawn through the slope directly above the proposed Main Academic Building. Provide two additional geologic cross-sections drawn through location TP-5. The sections shall be extended up to show the <u>entire slope</u> both in the north-south direction (general true dip direction) and, along the steepest portion of the slope (perpendicular to contours). Provide stability evaluation along these sections using appropriate strengths and demonstrate that the slope above the proposed building will have the required minimum factor of safety of 1.5 for long-term stability (gross and seismic).*

Note: The subject property on Plate A of the DMG Open-File Report 95-02 is shown as being in an area of "weak bedrock" which consists of thin-bedded, densely jointed siltstone, platy shale, and fine-grained sandstone units" of the Modelo Formation which was "severely affected" by the Northridge Earthquake.

Response: Cross Section J has been drawn through the location of Test Pit 5 and includes the top of the ridge. This new section is shown on the enclosed Vicinity Map #2 and was used for the additional slope stability analysis. A north-south cross section was not prepared as the bedding planes within the diatomaceous siltstone bedrock dip to the north and the strike is perpendicular to the slope. The bedding planes are not unsupported in the down dip direction. The calculation indicates that the slope above the proposed academic building is grossly and seismically stable with a factor of safety in excess of the LADBS standard. The geologic and geotechnical conditions are based upon site specific exploration and borings. Exploration and testing was not performed as part of the DMG Open File Report 95-02.

11. *Revise recommendations as necessary and provide an itemized response to this letter.*

Response: This report contains an itemized response to the correction letter dated September 1, 2006.

Should you have any questions, please feel free to contact the undersigned.

Respectfully submitted,
THE J. BYER GROUP, INC.

ENGINEERING GEOLOGIST JOHN W. BYER E. G. 883 Exp. 4/30/08 STATE OF CALIFORNIA

REGISTERED PROFESSIONAL ENGINEER ROBERT I. ZWEIGLER No. 2120 Exp. 06-30-08 GEOTECHNICAL STATE OF CALIFORNIA

John W. Byer
E. G. 883

Robert I. Zweigler
G. E. 2120

JWB:RIZ:flh
S:\FINAL\ADDENDUM\19376_Buckley_School_Addendum_Geologic_Report.wpd

Enc: City of Los Angeles Geology and Soils Report Correction Letter, dated September 1, 2006 (3 Pages)
Revised Sections A, B, C, and D (2 Sheets)
Section J
Vicinity Map #2
Slope Stability Analysis (24 Pages)

In Pocket: Revised Geologic Map

xc:
(4) Addressee
(4) Bruce A. Miller & Associates
(1) Englekirk & Sabol, Attention: Bill Wallace
(1) Project Development Group, Attention: James J. Shelton, Jr.
(2) Latham & Watkins, LLP, Attention: David F. Thompson (Include two copies of June 6, 2006)

THE J. BYER GROUP, INC.

1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

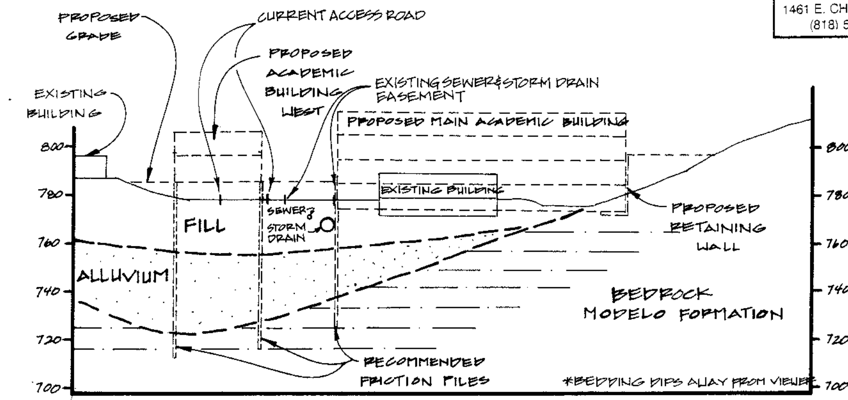
SECTION A & B

JB: 19376-B THE BUCKLEY SCHOOL

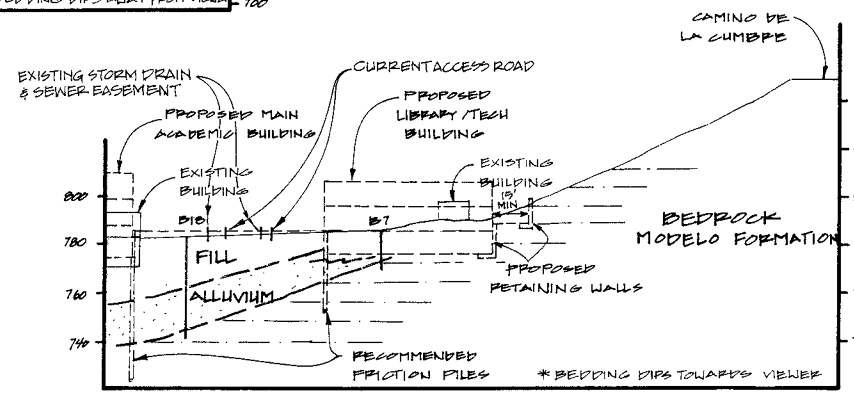
CONSULTANT: JET

SCALE: 1" = 40'

JUNE 6, 2006
OCTOBER 20, 2006



SECTION A

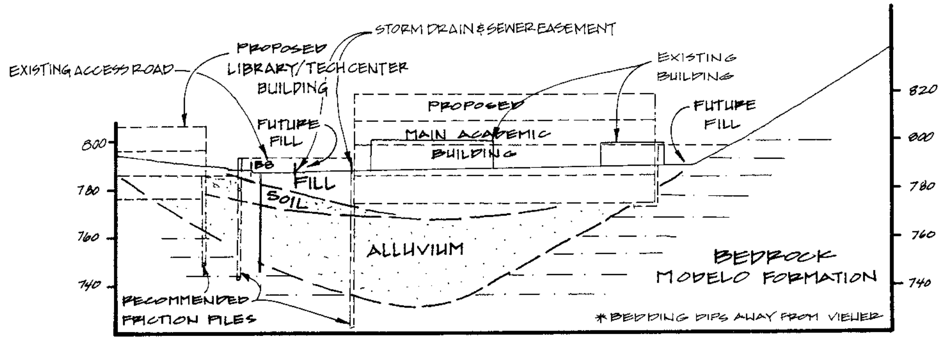


SECTION B

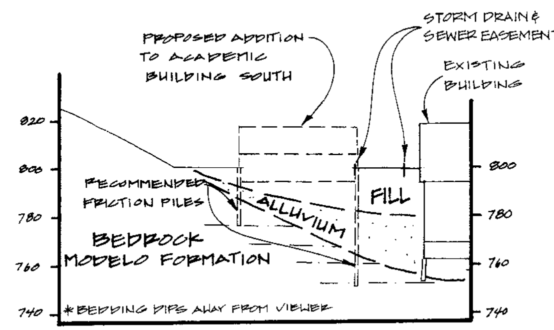
11x17

THE J. BYER GROUP, INC. A GEOTECHNICAL CONSULTING FIRM 1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206 (818) 549-9959 Tel • (818) 543-3747 Fax	SECTION C & D	
	JB: 19376-B THE BUCKLEY SCHOOL	
	CONSULTANT: JET	SCALE: 1"=40'

JUNE 6, 2006
OCTOBER 20, 2006

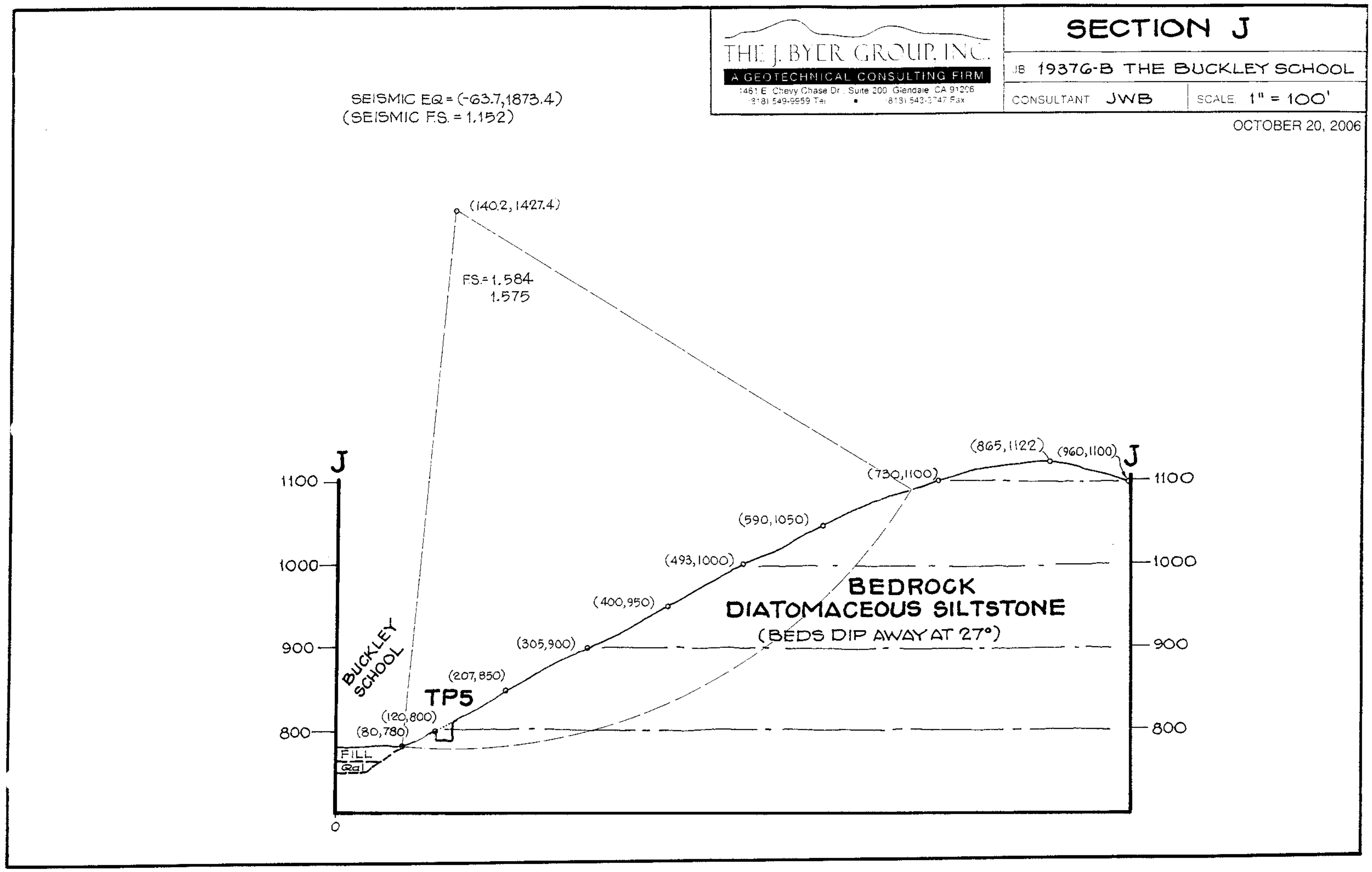


SECTION C

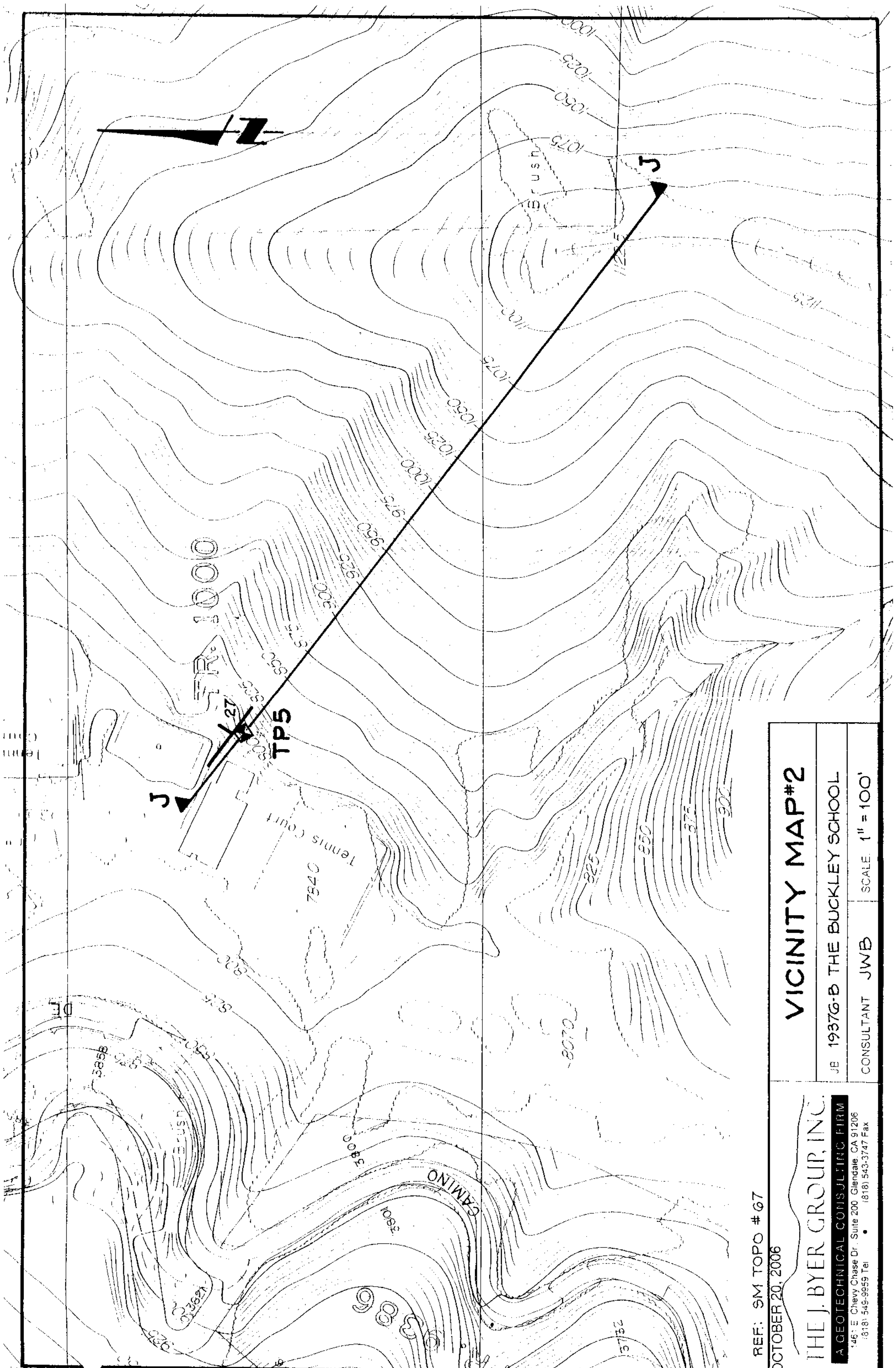


SECTION D

11x17


SECTION J
JB 19376-B THE BUCKLEY SCHOOL
CONSULTANT JWB
SCALE 1" = 100'
OCTOBER 20, 2006
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200 Glendale CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax
SEISMIC EQ = (-63.7,1873.4)
(SEISMIC F.S. = 1.152)
(140.2, 1427.4)
F.S.= 1.584
1.575
J
J
1100
1000
900
800
0
BUCKLEY SCHOOL
TP5
FILL
Qal
(80,780)
(120,800)
(207,850)
(305,900)
(400,950)
(493,1000)
(590,1050)
(730,1100)
(865,1122)
(960,1100)
BEDROCK
DIATOMACEOUS SILTSTONE
(BEDS DIP AWAY AT 27°)

11x17


VICINITY MAP#2
JB 1937G-B THE BUCKLEY SCHOOL
CONSULTANT JWB
SCALE 1" = 100'
REF: SM TOPO #67
OCTOBER 20, 2006
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr. Suite 200 Glendale CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax
TP5
J
J
Tennis Court
Brush
CAMINO

11x17

S

CITY OF LOS ANGELES
CALIFORNIA

ANTONIO R. VILLARAIGOSA
MAYOR

DEPARTMENT OF
BUILDING AND SAFETY

201 NORTH FIGUEROA STREET
LOS ANGELES, CA 90012

ANDREW A. ADELMAN, P.E.
GENERAL MANAGER
RAYMOND CHAN
EXECUTIVE OFFICER

GEOLOGY AND SOILS REPORT CORRECTION LETTER

September 1, 2006

Log # 54269
SOILS/GEOLOGY FILE - 2

The Buckley School
3900 N. Stansbury Avenue
Sherman Oaks, CA 91423

TRACT: 23823
LOT: Lot 1
LOCATION: 3900 N. Stansbury Avenue

CURRENT REFERENCE REPORT/LETTER(S)	REPORT NO.	DATE(S) OF DOCUMENT	PREPARED BY
Geology/Soils Report	JB 19376-B	06/06/2006	The J. Byer Group
Oversized Document	"	"	"

The referenced report concerning the proposed new construction on the subject 2-acre school property has been reviewed by the Grading Division of the Department of Building and Safety.

The following are proposed: (i) a new 4-level Main Academic Building (two stories of classrooms and offices over two levels of partial subterranean parking; (ii) a new 2-story Academic Building West; (iii) a new 2-story Library/Tech. Center Building, with basement; (iii) A 2-story addition to the north side of the existing Academic Building South; (iv) a new Aquatic Center Building and, (v) a new swimming pool.

Re-grading of the access road from the school entrance to the athletic field, is planned. The consultants have indicated that the removal and replacement of the existing uncertified fill is not practical, due to its thickness and the presence of an existing storm drain. The placement of new fill over existing uncertified fill, does not comply with the Code as indicated on page 14 of the report, and is not approved at this time.

The consultants are referred to the following maps, which were also reviewed: (i) map page 67 of the 1960 City Geologic Maps of the Santa Monica Mountains, and (ii) Plate A of DMG Open-File Report 95-02 (Landslide Hazards & Effects of the Northridge Earthquake of January 17, 1994).

The review of the subject report cannot be completed at this time and will be continued upon submittal of an addendum to the report which shall include, but need not be limited to, the following:

1. Identify the access road from the school entrance to the athletic field and the existing storm drains, on the map and on the appropriate cross-sections. Provide an evaluation of the settlement characteristics of the existing fill and a detailed justification demonstrating that potential future settlement of the fill, will not result in future damage or excessive settlement to the access road surface. Alternatively, revise recommendations for new fill, to be placed in compliance with section 7011.3 of the LA City Building Code and identify details on the map and cross-sections.

2. The report indicates (see pages 4 and 12) that the "natural drainages" which enter from the east can be sources of eroded soil material and will carry natural runoff, on to the site. Provide recommendations for mud/debris flow control systems within and at the base of concentrated drainage areas using the minimum design parameters specified in section 7014.3 of the LA City Building Code. The entire contributing watershed area on the slopes above the property shall be identified on the topographic map. If such evaluation is to be performed by a licensed civil engineer, include a wet-signed original and two copies with the addendum.

3. Explain what the approximately 220-feet-long (and about 2-feet-wide) line on the map shown on the slope within the existing natural drainage course (above location TP-3 and the curvilinear structure), represents. Note: A similar line on the map is also shown within the natural drainage area in the southern portion of the site (canyon to the east of locations TP-11 and TP-12). If the line represents an existing pipe or other device that conveys slope drainage, provide recommendations and show on the map how drainage will be conveyed around the buildings in a non-erosive device to a location that is acceptable to the Department.

4. Provide the test pit logs for exploration conducted at locations TP-11 and TP-12.

5. Explain what the two curvilinear structures shown east of the proposed Main Academic Building represent. Indicate if these structures are existing, or proposed. If they are existing, clarify if they will be removed or if they will remain. It they are proposed, explain if they will part of the proposed building or, will be detached from the building.

6. It appears from the recommendations provided on page 20 of the report, that removal of the porous, unsuitable upper portion of the alluvium will be required if the floor slab of the Main Academic Building is to be supported on newly-placed certified compacted fill. Shoring is planned to facilitate removal along the west and south sides. Clarify how any removals for building construction and setback wall/slope protection wall construction, will be achieved along the southeastern portion of the building and along the entire length of the building, on the east side.

   Provide additional geologic cross-sections drawn through the proposed building, any setback wall and/or slope protection walls proposed and, the immediate slope located above the walls to illustrate the proposed construction.

7. Verify using the sections requested, that the entire face of the new Main Academic Building will be provided the required level clearance building setback and, identify the required setback on all cross-sections drawn through the Main Academic Building.

8. It appears from the documented geologic orientation (N88W; 31N) plotted on the map, that the correct location for test pit TP-6 is between the proposed toe of slope wall and the Library Building. A location TP-6 is also shown on the east side of the proposed Main Academic Building (east of TP-5). Please explain, verify and correct, as necessary. Provide an exploration log, if applicable.

9. The geologic data on the slope above the proposed Main Academic Building is limited to the one orientation from location TP-5. The mapped strike and dip on the City map page 67, shown on the slope in this area, indicates a near east-west strike and a north dip of 16 degrees. Provide additional data with regard to the bedrock orientation on the slope using additional mapping and/or exploration.

10. It appears that geologic cross-section I-I was not drawn through the slope directly above the proposed Main Academic Building. Provide two additional geologic cross-sections drawn through location TP-5. The sections shall be extended up to show the entire slope both in the north-south direction (general true dip direction) and, along the steepest portion of the slope (perpendicular to contours). Provide stability evaluation along these sections using appropriate strengths and demonstrate that the slope above the proposed building will have the required minimum factor of safety of 1.5 for long-term stability (gross and seismic).

    Note: The subject property on Plate A of the DMG Open-File Report 95-02 is shown as being in an area of "weak bedrock" which consists of thin-bedded, densely jointed siltstone, platy shale, and fine-grained sandstone units" of the Modelo Formation which was "severely affected" by the Northridge Earthquake.

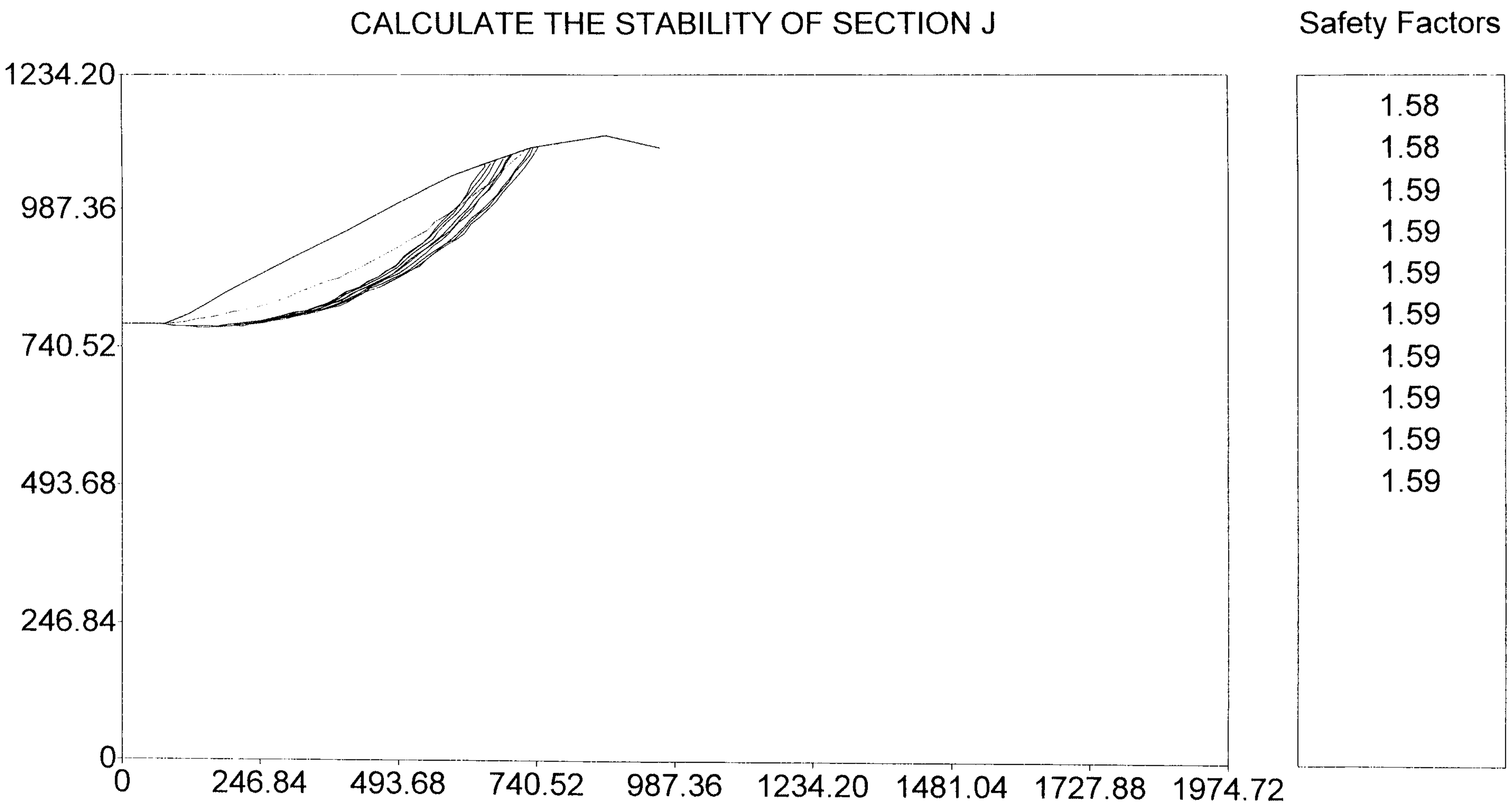
11. Revise recommendations as necessary and provide an itemized response to this letter.

STEPHEN DAWSON
Engineering Geologist I

PASCAL CHALLITA
Geotechnical Engineer II

SD/PC:sd/pc
54269
(213) 482-0480

cc: Bruce A. Miller & Associates (Applicant)
The J. Byer Group
VN District Office


CALCULATE THE STABILITY OF SECTION J
Safety Factors
1234.20
987.36
740.52
493.68
246.84
0
0
246.84
493.68
740.52
987.36
1234.20
1481.04
1727.88
1974.72
1.58
1.58
1.59
1.59
1.59
1.59
1.59
1.59
1.59
1.59

JB 19876-B BUCKLEY SCHOOL-SECTION J
** PCSTABL6 **

by
Purdue University

modified by
Peter J. Bosscher
University of Wisconsin-Madison

--Slope Stability Analysis--
Simplified Janbu, Simplified Bishop
or Spencer`s Method of Slices

PROBLEM DESCRIPTION   CALCULATE THE STABILITY OF SECTION J

BOUNDARY COORDINATES

10 Top   Boundaries
10 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	780.00	80.00	780.00	1
2	80.00	780.00	120.00	800.00	1
3	120.00	800.00	207.00	850.00	1
4	207.00	850.00	305.00	900.00	1
5	305.00	900.00	400.00	950.00	1
6	400.00	950.00	493.00	1000.00	1
7	493.00	1000.00	590.00	1050.00	1
8	590.00	1050.00	730.00	1100.00	1
9	730.00	1100.00	865.00	1122.00	1
10	865.00	1122.00	960.00	1100.00	1

ISOTROPIC SOIL PARAMETERS

1 Type(s) of Soil

Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
1	125.0	125.0	951.0	30.0	0.00	0.0	0

A Critical Failure Surface Searching Method, Using A Random Technique For Generating Circular Surfaces, Has Been Specified.

25000 Trial Surfaces Have Been Generated.

500 Surfaces Initiate From Each Of 50 Points Equally Spaced
Along The Ground Surface Between X = 70.00 ft.
and X = 80.00 ft.

Each Surface Terminates Between   X = 100.00 ft.
and   X = 900.00 ft.

Unless Further Limitations Were Imposed, The Minimum Elevation At Which A Surface Extends Is Y = 0.00 ft.

20.00 ft. Line Segments Define Each Trial Failure Surface.

Following Are Displayed The Ten Most Critical Of The Trial

Failure Surfaces Examined. They Are Ordered - Most Critical First.

* * Safety Factors Are Calculated By The Modified Bishop Method * *

Failure Surface Specified By 38 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	80.00	780.00
2	99.81	782.79
3	119.56	785.93
4	139.25	789.43
5	158.87	793.29
6	178.42	797.51
7	197.89	802.08
8	217.28	807.00
9	236.57	812.27
10	255.77	817.89
11	274.85	823.86
12	293.83	830.17
13	312.69	836.83
14	331.43	843.82
15	350.03	851.16
16	368.50	858.83
17	386.83	866.84
18	405.01	875.17
19	423.04	883.84
20	440.90	892.83
21	458.60	902.14
22	476.13	911.78
23	493.48	921.72
24	510.65	931.99
25	527.62	942.56
26	544.41	953.44
27	560.99	964.62
28	577.37	976.09
29	593.53	987.87
30	609.49	999.93
31	625.21	1012.29
32	640.72	1024.92
33	655.99	1037.84
34	671.02	1051.03
35	685.82	1064.49
36	700.36	1078.21
37	714.66	1092.20
38	718.18	1095.78

Circle Center At X = -63.7 ; Y = 1873.4 and Radius, 1102.8

*** 1.575 ***

Failure Surface Specified By 38 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.65	780.00

2	92.58	778.23
3	112.54	777.07
4	132.53	776.53
5	152.53	776.60
6	172.52	777.29
7	192.48	778.59
8	212.39	780.50
9	232.23	783.02
10	251.98	786.15
11	271.63	789.89
12	291.15	794.23
13	310.53	799.16
14	329.76	804.69
15	348.80	810.81
16	367.64	817.51
17	386.27	824.79
18	404.67	832.63
19	422.82	841.04
20	440.70	850.00
21	458.29	859.50
22	475.59	869.54
23	492.57	880.11
24	509.22	891.19
25	525.52	902.78
26	541.45	914.87
27	557.01	927.44
28	572.17	940.48
29	586.93	953.98
30	601.26	967.93
31	615.16	982.31
32	628.61	997.11
33	641.60	1012.32
34	654.11	1027.92
35	666.14	1043.90
36	677.68	1060.24
37	688.70	1076.92
38	695.30	1087.61

Circle Center At X = 140.2 ; Y = 1427.4 and Radius, 650.9

*** 1.584 ***

Failure Surface Specified By 36 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.86	780.00
2	92.78	778.24
3	112.75	777.14
4	132.75	776.70
5	152.74	776.92
6	172.72	777.80
7	192.67	779.33
8	212.55	781.52
9	232.34	784.37
10	252.03	787.86
11	271.60	792.00
12	291.02	796.79

13	310.27	802.21
14	329.33	808.26
15	348.19	814.94
16	366.81	822.24
17	385.18	830.14
18	403.28	838.65
19	421.09	847.74
20	438.59	857.42
21	455.77	867.67
22	472.59	878.48
23	489.05	889.84
24	505.13	901.74
25	520.81	914.16
26	536.07	927.09
27	550.89	940.51
28	565.27	954.42
29	579.18	968.79
30	592.61	983.61
31	605.54	998.87
32	617.96	1014.54
33	629.86	1030.62
34	641.22	1047.07
35	652.04	1063.90
36	658.31	1074.40

Circle Center At X = 136.1 ; Y = 1383.6 and Radius, 607.0

*** 1.585 ***

Failure Surface Specified By 37 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	74.90	780.00
2	94.82	778.18
3	114.78	777.01
4	134.77	776.49
5	154.77	776.63
6	174.76	777.41
7	194.71	778.85
8	214.60	780.94
9	234.41	783.68
10	254.12	787.07
11	273.71	791.09
12	293.16	795.76
13	312.44	801.05
14	331.55	806.98
15	350.45	813.52
16	369.12	820.68
17	387.55	828.44
18	405.72	836.80
19	423.61	845.75
20	441.19	855.28
21	458.46	865.38
22	475.38	876.04
23	491.95	887.24
24	508.14	898.98
25	523.94	911.24

26	539.33	924.01
27	554.30	937.28
28	568.83	951.02
29	582.90	965.24
30	596.49	979.91
31	609.60	995.01
32	622.22	1010.53
33	634.31	1026.46
34	645.89	1042.77
35	656.92	1059.45
36	667.40	1076.48
37	668.23	1077.94

Circle Center At X = 140.6 ; Y = 1388.9 and Radius, 612.4

*** 1.586 ***

Failure Surface Specified By 40 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	78.57	780.00
2	98.50	778.26
3	118.46	777.09
4	138.45	776.52
5	158.45	776.52
6	178.44	777.11
7	198.41	778.29
8	218.33	780.05
9	238.20	782.39
10	257.98	785.30
11	277.67	788.80
12	297.26	792.87
13	316.71	797.51
14	336.02	802.71
15	355.17	808.48
16	374.14	814.81
17	392.92	821.68
18	411.50	829.11
19	429.84	837.07
20	447.95	845.56
21	465.80	854.58
22	483.38	864.12
23	500.67	874.17
24	517.67	884.71
25	534.34	895.75
26	550.69	907.28
27	566.69	919.27
28	582.34	931.73
29	597.61	944.64
30	612.51	957.99
31	627.00	971.77
32	641.09	985.97
33	654.75	1000.57
34	667.99	1015.57
35	680.78	1030.94
36	693.11	1046.69
37	704.98	1062.78

38	716.38	1079.22
39	727.29	1095.98
40	729.66	1099.88

Circle Center At X = 148.2 ; Y = 1460.9 and Radius, 684.4

*** 1.588 ***

Failure Surface Specified By 37 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	78.78	780.00
2	98.69	778.11
3	118.65	776.87
4	138.64	776.27
5	158.64	776.31
6	178.63	777.00
7	198.58	778.33
8	218.49	780.30
9	238.31	782.91
10	258.05	786.16
11	277.67	790.04
12	297.15	794.55
13	316.48	799.69
14	335.64	805.45
15	354.59	811.82
16	373.34	818.79
17	391.85	826.37
18	410.10	834.54
19	428.09	843.29
20	445.78	852.62
21	463.16	862.51
22	480.22	872.95
23	496.93	883.94
24	513.28	895.46
25	529.24	907.51
26	544.82	920.06
27	559.98	933.10
28	574.71	946.63
29	589.00	960.62
30	602.83	975.07
31	616.19	989.95
32	629.06	1005.26
33	641.44	1020.97
34	653.30	1037.07
35	664.64	1053.55
36	675.44	1070.38
37	683.13	1083.26

Circle Center At X = 147.3 ; Y = 1397.4 and Radius, 621.2

*** 1.588 ***

Failure Surface Specified By 41 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.65	780.00
2	92.58	778.25
3	112.54	777.06
4	132.53	776.43
5	152.53	776.36
6	172.53	776.85
7	192.50	777.90
8	212.43	779.51
9	232.32	781.67
10	252.13	784.39
11	271.86	787.66
12	291.49	791.48
13	311.01	795.86
14	330.40	800.77
15	349.64	806.23
16	368.72	812.22
17	387.63	818.74
18	406.34	825.79
19	424.85	833.36
20	443.15	841.44
21	461.21	850.04
22	479.02	859.13
23	496.57	868.72
24	513.85	878.80
25	530.83	889.36
26	547.52	900.38
27	563.89	911.87
28	579.93	923.82
29	595.63	936.21
30	610.98	949.03
31	625.96	962.27
32	640.57	975.93
33	654.79	990.00
34	668.61	1004.45
35	682.03	1019.29
36	695.02	1034.50
37	707.58	1050.06
38	719.70	1065.97
39	731.37	1082.21
40	742.58	1098.77
41	744.91	1102.43

Circle Center At X = 145.0 ; Y = 1491.2 and Radius, 714.9

*** 1.588 ***

Failure Surface Specified By 38 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	73.67	780.00
2	93.56	777.91
3	113.51	776.45

4	133.49	775.62
5	153.49	775.41
6	173.49	775.83
7	193.46	776.87
8	213.39	778.54
9	233.26	780.84
10	253.04	783.76
11	272.73	787.30
12	292.29	791.45
13	311.72	796.22
14	330.98	801.59
15	350.07	807.56
16	368.96	814.13
17	387.63	821.29
18	406.08	829.03
19	424.26	837.35
20	442.18	846.23
21	459.82	855.67
22	477.14	865.66
23	494.15	876.18
24	510.82	887.24
25	527.13	898.81
26	543.07	910.89
27	558.62	923.46
28	573.77	936.52
29	588.51	950.04
30	602.81	964.02
31	616.67	978.44
32	630.07	993.29
33	643.00	1008.55
34	655.44	1024.21
35	667.38	1040.25
36	678.82	1056.66
37	689.73	1073.42
38	699.20	1089.00

Circle Center At X = 150.1 ; Y = 1412.9 and Radius, 637.5

*** 1.591 ***

Failure Surface Specified By 40 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	74.69	780.00
2	94.60	778.05
3	114.55	776.68
4	134.54	775.90
5	154.54	775.69
6	174.53	776.07
7	194.51	777.03
8	214.45	778.57
9	234.34	780.69
10	254.15	783.39
11	273.88	786.67
12	293.51	790.51
13	313.02	794.93
14	332.38	799.92

15	351.60	805.46
16	370.65	811.57
17	389.51	818.22
18	408.17	825.42
19	426.61	833.16
20	444.81	841.44
21	462.77	850.24
22	480.47	859.56
23	497.88	869.40
24	515.01	879.73
25	531.82	890.56
26	548.31	901.88
27	564.47	913.67
28	580.27	925.92
29	595.71	938.63
30	610.78	951.79
31	625.45	965.38
32	639.73	979.39
33	653.59	993.81
34	667.02	1008.62
35	680.02	1023.82
36	692.57	1039.40
37	704.65	1055.33
38	716.28	1071.61
39	727.42	1088.22
40	735.39	1100.88

Circle Center At X = 151.6 ; Y = 1462.4 and Radius, 686.8

*** 1.592 ***

Failure Surface Specified By 36 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	75.71	780.00
2	95.62	778.02
3	115.58	776.73
4	135.57	776.13
5	155.57	776.21
6	175.55	776.98
7	195.50	778.44
8	215.38	780.58
9	235.18	783.40
10	254.87	786.90
11	274.43	791.07
12	293.84	795.91
13	313.07	801.42
14	332.09	807.58
15	350.90	814.40
16	369.46	821.85
17	387.75	829.94
18	405.75	838.65
19	423.44	847.97
20	440.81	857.90
21	457.82	868.42
22	474.46	879.51
23	490.71	891.17

JB 19876-B BUCKLEY SCHOOL-SECTION J

24	506.55	903.38
25	521.96	916.13
26	536.92	929.40
27	551.42	943.18
28	565.44	957.44
29	578.96	972.18
30	591.96	987.37
31	604.44	1003.01
32	616.37	1019.06
33	627.74	1035.51
34	638.55	1052.34
35	648.76	1069.53
36	649.76	1071.34

Circle Center At X = 143.2 ; Y = 1358.3 and Radius, 582.3

*** 1.592 ***

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            Y            A     X     I     S            F     T

              0.00    246.84    493.68    740.52    987.36   1234.20

X       0.00 +---------+---------+---------+-*-------+---------+
             -
             -                              .*
             -                             .2*.
             -                           ...21..
             -                          ....811*.
      246.84 +                          .....21...
             -                         ......211.*.
             -                         ......221...
             -                         .......211...
             -                         .......5211.*.
             -                         ........2211...
A     493.68 +                         .........2211..*
             -                         ..........5211...
             -                          ..........5211..*
             -                          ...........52213.
             -                           ............52113
             -                            ............7511
X     740.52 +                             ..............5*
             -                               ...............
             -                                 .............
             -                                   .........*
             -                                        .....
             -                                            *
I     987.36 +
             -
             -
             -
             -
             -
S    1234.20 +
             -
             -
             -
             -
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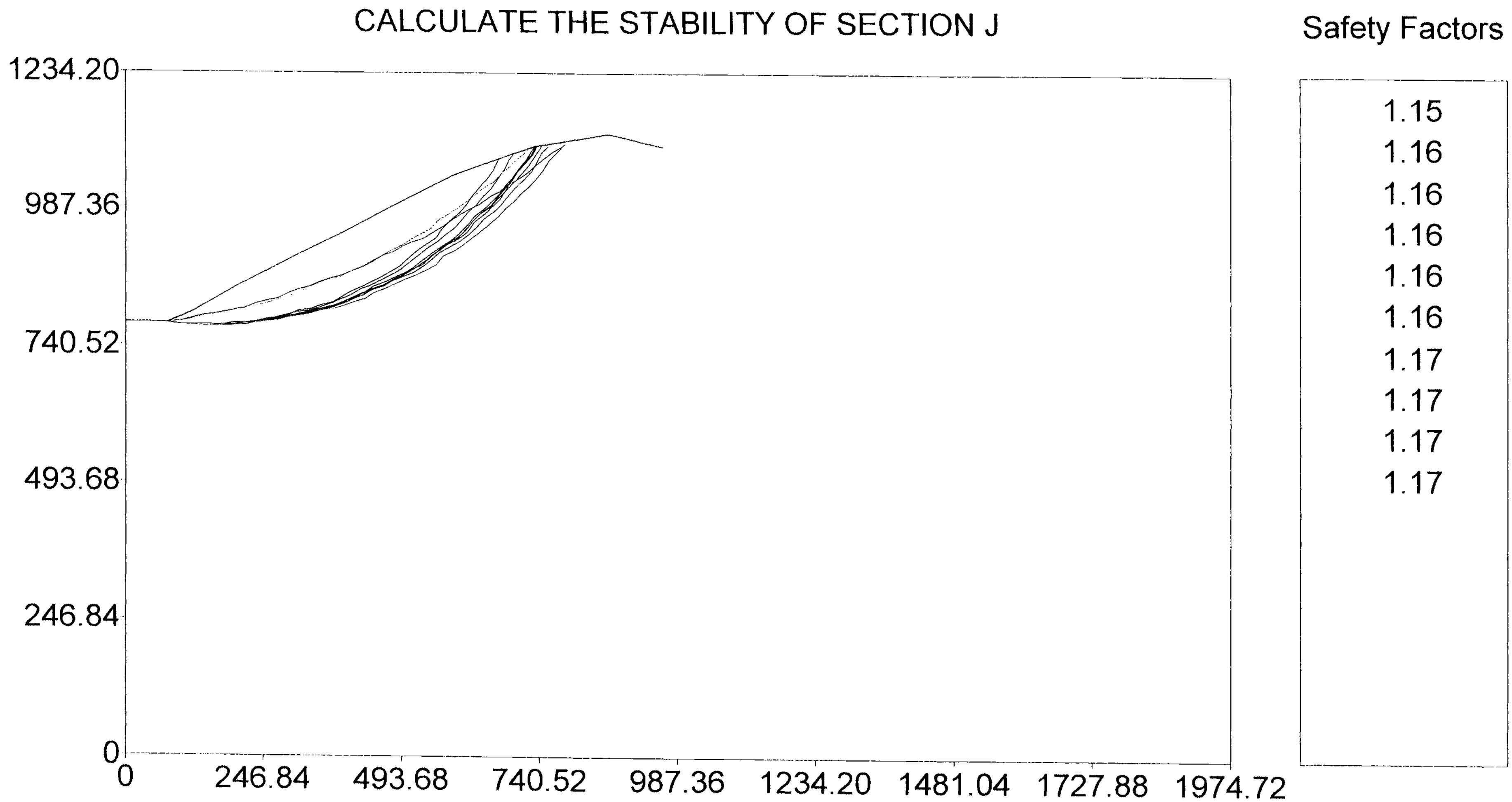
         -
 1481.04 +
         -
         -
         -
         -
         -
F 1727.88 +
         -
         -
         -
         -
         -
T 1974.72 +
```


CALCULATE THE STABILITY OF SECTION J
1234.20
987.36
740.52
493.68
246.84
0
0
246.84
493.68
740.52
987.36
1234.20
1481.04
1727.88
1974.72
Safety Factors
1.15
1.16
1.16
1.16
1.16
1.16
1.17
1.17
1.17
1.17

JB 19876-B BUCKLEY SCHOOL-SECTION J-EQ
** PCSTABL6 **

by
Purdue University

modified by
Peter J. Bosscher
University of Wisconsin-Madison

--Slope Stability Analysis--
Simplified Janbu, Simplified Bishop
or Spencer`s Method of Slices

PROBLEM DESCRIPTION   CALCULATE THE SEISMIC STABILITY OF SECTION J

BOUNDARY COORDINATES

10 Top   Boundaries
10 Total Boundaries

Boundary No.	X-Left (ft)	Y-Left (ft)	X-Right (ft)	Y-Right (ft)	Soil Type Below Bnd
1	0.00	780.00	80.00	780.00	1
2	80.00	780.00	120.00	800.00	1
3	120.00	800.00	207.00	850.00	1
4	207.00	850.00	305.00	900.00	1
5	305.00	900.00	400.00	950.00	1
6	400.00	950.00	493.00	1000.00	1
7	493.00	1000.00	590.00	1050.00	1
8	590.00	1050.00	730.00	1100.00	1
9	730.00	1100.00	865.00	1122.00	1
10	865.00	1122.00	960.00	1100.00	1

ISOTROPIC SOIL PARAMETERS

1 Type(s) of Soil

Soil Type No.	Total Unit Wt. (pcf)	Saturated Unit Wt. (pcf)	Cohesion Intercept (psf)	Friction Angle (deg)	Pore Pressure Param.	Pressure Constant (psf)	Piez. Surface No.
1	125.0	125.0	951.0	30.0	0.00	0.0	0

A Horizontal Earthquake Loading Coefficient
Of0.150 Has Been Assigned

A Vertical Earthquake Loading Coefficient
Of0.000 Has Been Assigned

Cavitation Pressure =   0.0 psf

A Critical Failure Surface Searching Method, Using A Random
Technique For Generating Circular Surfaces, Has Been Specified.

25000 Trial Surfaces Have Been Generated.

500 Surfaces Initiate From Each Of 50 Points Equally Spaced
Along The Ground Surface Between X = 70.00 ft.
and X = 80.00 ft.

Each Surface Terminates Between   X = 100.00 ft.

JB 19876-B BUCKLEY SCHOOL-SECTION J-EQ
and X = 900.00 ft.

Unless Further Limitations Were Imposed, The Minimum Elevation At Which A Surface Extends Is Y = 0.00 ft.

20.00 ft. Line Segments Define Each Trial Failure Surface.

Following Are Displayed The Ten Most Critical Of The Trial Failure Surfaces Examined. They Are Ordered - Most Critical First.

* * Safety Factors Are Calculated By The Modified Bishop Method * *

Failure Surface Specified By 38 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	80.00	780.00
2	99.81	782.79
3	119.56	785.93
4	139.25	789.43
5	158.87	793.29
6	178.42	797.51
7	197.89	802.08
8	217.28	807.00
9	236.57	812.27
10	255.77	817.89
11	274.85	823.86
12	293.83	830.17
13	312.69	836.83
14	331.43	843.82
15	350.03	851.16
16	368.50	858.83
17	386.83	866.84
18	405.01	875.17
19	423.04	883.84
20	440.90	892.83
21	458.60	902.14
22	476.13	911.78
23	493.48	921.72
24	510.65	931.99
25	527.62	942.56
26	544.41	953.44
27	560.99	964.62
28	577.37	976.09
29	593.53	987.87
30	609.49	999.93
31	625.21	1012.29
32	640.72	1024.92
33	655.99	1037.84
34	671.02	1051.03
35	685.82	1064.49
36	700.36	1078.21
37	714.66	1092.20
38	718.18	1095.78

Circle Center At X = -63.7 ; Y = 1873.4 and Radius, 1102.8

*** 1.152 ***

JB 19876-B BUCKLEY SCHOOL-SECTION J-EQ

Failure Surface Specified By 41 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	80.00	780.00
2	99.68	783.58
3	119.31	787.42
4	138.88	791.52
5	158.40	795.88
6	177.86	800.51
7	197.25	805.39
8	216.58	810.54
9	235.84	815.94
10	255.02	821.60
11	274.12	827.51
12	293.15	833.68
13	312.09	840.10
14	330.94	846.78
15	349.70	853.71
16	368.37	860.89
17	386.94	868.32
18	405.41	875.99
19	423.77	883.91
20	442.03	892.08
21	460.17	900.49
22	478.20	909.15
23	496.12	918.04
24	513.91	927.17
25	531.58	936.54
26	549.12	946.15
27	566.54	955.98
28	583.82	966.06
29	600.96	976.36
30	617.96	986.89
31	634.82	997.64
32	651.54	1008.62
33	668.11	1019.83
34	684.52	1031.25
35	700.78	1042.89
36	716.89	1054.75
37	732.83	1066.83
38	748.61	1079.11
39	764.23	1091.61
40	779.68	1104.31
41	785.22	1109.00

Circle Center At X = -177.5 ; Y = 2252.5 and Radius, 1494.9

*** 1.158 ***

Failure Surface Specified By 41 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.65	780.00

2	92.58	778.25
3	112.54	777.06
4	132.53	776.43
5	152.53	776.36
6	172.53	776.85
7	192.50	777.90
8	212.43	779.51
9	232.32	781.67
10	252.13	784.39
11	271.86	787.66
12	291.49	791.48
13	311.01	795.86
14	330.40	800.77
15	349.64	806.23
16	368.72	812.22
17	387.63	818.74
18	406.34	825.79
19	424.85	833.36
20	443.15	841.44
21	461.21	850.04
22	479.02	859.13
23	496.57	868.72
24	513.85	878.80
25	530.83	889.36
26	547.52	900.38
27	563.89	911.87
28	579.93	923.82
29	595.63	936.21
30	610.98	949.03
31	625.96	962.27
32	640.57	975.93
33	654.79	990.00
34	668.61	1004.45
35	682.03	1019.29
36	695.02	1034.50
37	707.58	1050.06
38	719.70	1065.97
39	731.37	1082.21
40	742.58	1098.77
41	744.91	1102.43

Circle Center At X = 145.0 ; Y = 1491.2 and Radius, 714.9

*** 1.163 ***

Failure Surface Specified By 40 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	78.57	780.00
2	98.50	778.26
3	118.46	777.09
4	138.45	776.52
5	158.45	776.52
6	178.44	777.11
7	198.41	778.29
8	218.33	780.05
9	238.20	782.39

10	257.98	785.30
11	277.67	788.80
12	297.26	792.87
13	316.71	797.51
14	336.02	802.71
15	355.17	808.48
16	374.14	814.81
17	392.92	821.68
18	411.50	829.11
19	429.84	837.07
20	447.95	845.56
21	465.80	854.58
22	483.38	864.12
23	500.67	874.17
24	517.67	884.71
25	534.34	895.75
26	550.69	907.28
27	566.69	919.27
28	582.34	931.73
29	597.61	944.64
30	612.51	957.99
31	627.00	971.77
32	641.09	985.97
33	654.75	1000.57
34	667.99	1015.57
35	680.78	1030.94
36	693.11	1046.69
37	704.98	1062.78
38	716.38	1079.22
39	727.29	1095.98
40	729.66	1099.88

Circle Center At X = 148.2 ; Y = 1460.9 and Radius, 684.4

*** 1.164 ***

Failure Surface Specified By 41 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.86	780.00
2	92.78	778.19
3	112.73	776.92
4	132.72	776.20
5	152.72	776.03
6	172.72	776.41
7	192.70	777.34
8	212.64	778.82
9	232.54	780.84
10	252.37	783.41
11	272.13	786.53
12	291.79	790.18
13	311.35	794.38
14	330.78	799.11
15	350.08	804.37
16	369.22	810.16
17	388.20	816.47
18	406.99	823.31

19	425.59	830.65
20	443.99	838.51
21	462.16	846.86
22	480.09	855.71
23	497.78	865.06
24	515.20	874.88
25	532.34	885.18
26	549.20	895.94
27	565.75	907.17
28	581.99	918.84
29	597.90	930.96
30	613.48	943.51
31	628.70	956.48
32	643.56	969.87
33	658.05	983.65
34	672.15	997.83
35	685.86	1012.40
36	699.16	1027.33
37	712.05	1042.62
38	724.51	1058.27
39	736.54	1074.24
40	748.13	1090.55
41	757.46	1104.48

Circle Center At X = 148.9 ; Y = 1504.1 and Radius, 728.1

*** 1.165 ***

Failure Surface Specified By 38 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.65	780.00
2	92.58	778.23
3	112.54	777.07
4	132.53	776.53
5	152.53	776.60
6	172.52	777.29
7	192.48	778.59
8	212.39	780.50
9	232.23	783.02
10	251.98	786.15
11	271.63	789.89
12	291.15	794.23
13	310.53	799.16
14	329.76	804.69
15	348.80	810.81
16	367.64	817.51
17	386.27	824.79
18	404.67	832.63
19	422.82	841.04
20	440.70	850.00
21	458.29	859.50
22	475.59	869.54
23	492.57	880.11
24	509.22	891.19
25	525.52	902.78
26	541.45	914.87

27	557.01	927.44
28	572.17	940.48
29	586.93	953.98
30	601.26	967.93
31	615.16	982.31
32	628.61	997.11
33	641.60	1012.32
34	654.11	1027.92
35	666.14	1043.90
36	677.68	1060.24
37	688.70	1076.92
38	695.30	1087.61

Circle Center At X = 140.2 ; Y = 1427.4 and Radius, 650.9

*** 1.165 ***

Failure Surface Specified By 40 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	74.69	780.00
2	94.60	778.05
3	114.55	776.68
4	134.54	775.90
5	154.54	775.69
6	174.53	776.07
7	194.51	777.03
8	214.45	778.57
9	234.34	780.69
10	254.15	783.39
11	273.88	786.67
12	293.51	790.51
13	313.02	794.93
14	332.38	799.92
15	351.60	805.46
16	370.65	811.57
17	389.51	818.22
18	408.17	825.42
19	426.61	833.16
20	444.81	841.44
21	462.77	850.24
22	480.47	859.56
23	497.88	869.40
24	515.01	879.73
25	531.82	890.56
26	548.31	901.88
27	564.47	913.67
28	580.27	925.92
29	595.71	938.63
30	610.78	951.79
31	625.45	965.38
32	639.73	979.39
33	653.59	993.81
34	667.02	1008.62
35	680.02	1023.82
36	692.57	1039.40
37	704.65	1055.33

38	716.28	1071.61
39	727.42	1088.22
40	735.39	1100.88

Circle Center At X = 151.6 ; Y = 1462.4 and Radius, 686.8

*** 1.167 ***

Failure Surface Specified By 43 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	75.51	780.00
2	95.43	778.22
3	115.39	776.96
4	135.38	776.22
5	155.38	776.00
6	175.37	776.30
7	195.36	777.13
8	215.31	778.47
9	235.22	780.34
10	255.08	782.73
11	274.87	785.63
12	294.58	789.05
13	314.18	792.98
14	333.69	797.42
15	353.06	802.37
16	372.30	807.83
17	391.40	813.78
18	410.33	820.23
19	429.09	827.18
20	447.65	834.60
21	466.02	842.52
22	484.18	850.91
23	502.11	859.76
24	519.80	869.09
25	537.25	878.87
26	554.43	889.11
27	571.34	899.79
28	587.96	910.91
29	604.29	922.45
30	620.32	934.42
31	636.02	946.81
32	651.40	959.60
33	666.43	972.78
34	681.12	986.36
35	695.45	1000.31
36	709.41	1014.64
37	722.99	1029.32
38	736.18	1044.35
39	748.98	1059.72
40	761.37	1075.42
41	773.34	1091.44
42	784.90	1107.76
43	785.79	1109.09

Circle Center At X = 153.7 ; Y = 1542.2 and Radius, 766.3

*** 1.169 ***

Failure Surface Specified By 40 Coordinate Points

Point No.	X-Surf (ft)	Y-Surf (ft)
1	72.45	780.00
2	92.34	777.89
3	112.28	776.37
4	132.26	775.44
5	152.26	775.10
6	172.25	775.35
7	192.24	776.19
8	212.19	777.62
9	232.08	779.63
10	251.91	782.23
11	271.66	785.41
12	291.30	789.18
13	310.83	793.52
14	330.21	798.43
15	349.45	803.92
16	368.51	809.96
17	387.39	816.57
18	406.06	823.73
19	424.51	831.44
20	442.73	839.69
21	460.70	848.47
22	478.40	857.78
23	495.82	867.61
24	512.95	877.95
25	529.76	888.78
26	546.24	900.11
27	562.38	911.92
28	578.17	924.20
29	593.59	936.93
30	608.62	950.12
31	623.26	963.75
32	637.50	977.80
33	651.31	992.26
34	664.69	1007.13
35	677.63	1022.38
36	690.11	1038.01
37	702.12	1054.00
38	713.66	1070.33
39	724.71	1087.00
40	733.10	1100.51

Circle Center At X = 153.8 ; Y = 1453.5 and Radius, 678.4

*** 1.169 ***

Failure Surface Specified By 37 Coordinate Points

Point X-Surf Y-Surf

JB 19876-B BUCKLEY SCHOOL-SECTION J-EQ

No.	(ft)	(ft)
1	74.90	780.00
2	94.82	778.18
3	114.78	777.01
4	134.77	776.49
5	154.77	776.63
6	174.76	777.41
7	194.71	778.85
8	214.60	780.94
9	234.41	783.68
10	254.12	787.07
11	273.71	791.09
12	293.16	795.76
13	312.44	801.05
14	331.55	806.98
15	350.45	813.52
16	369.12	820.68
17	387.55	828.44
18	405.72	836.80
19	423.61	845.75
20	441.19	855.28
21	458.46	865.38
22	475.38	876.04
23	491.95	887.24
24	508.14	898.98
25	523.94	911.24
26	539.33	924.01
27	554.30	937.28
28	568.83	951.02
29	582.90	965.24
30	596.49	979.91
31	609.60	995.01
32	622.22	1010.53
33	634.31	1026.46
34	645.89	1042.77
35	656.92	1059.45
36	667.40	1076.48
37	668.23	1077.94

Circle Center At X = 140.6 ; Y = 1388.9 and Radius, 612.4

*** 1.170 ***

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          Y            A      X      I      S            F      T

          0.00    246.84    493.68    740.52    987.36   1234.20

X      0.00 +---------+---------+---------+-*-------+---------+
            -
            -                               .*
            -                              .3*.
            -                            ...31..
            -                           ....511*.
    246.84  +                           .....31...
            -                          ......311.*.
            -                          ......331...
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                JB 19876-B BUCKLEY SCHOOL-SECTION J-EQ
              -                          .......311...
              -                          .......3311.*.
              -                          ........3411...
A     493.68  +                          ........83311..*
              -                          .........53411...
              -                           .........83311..*
              -                           ..........833210.
              -                            ...........532110
              -                             ...........83211
X     740.52  +                              ............822*
              -                                ............22
              -                                  ............
              -                                    .........*
              -                                         .....
              -                                             *
I     987.36  +
              -
              -
              -
              -
              -
S    1234.20  +
              -
              -
              -
              -
              -
     1481.04  +
              -
              -
              -
              -
              -
F    1727.88  +
              -
              -
              -
              -
              -
T    1974.72  +
```
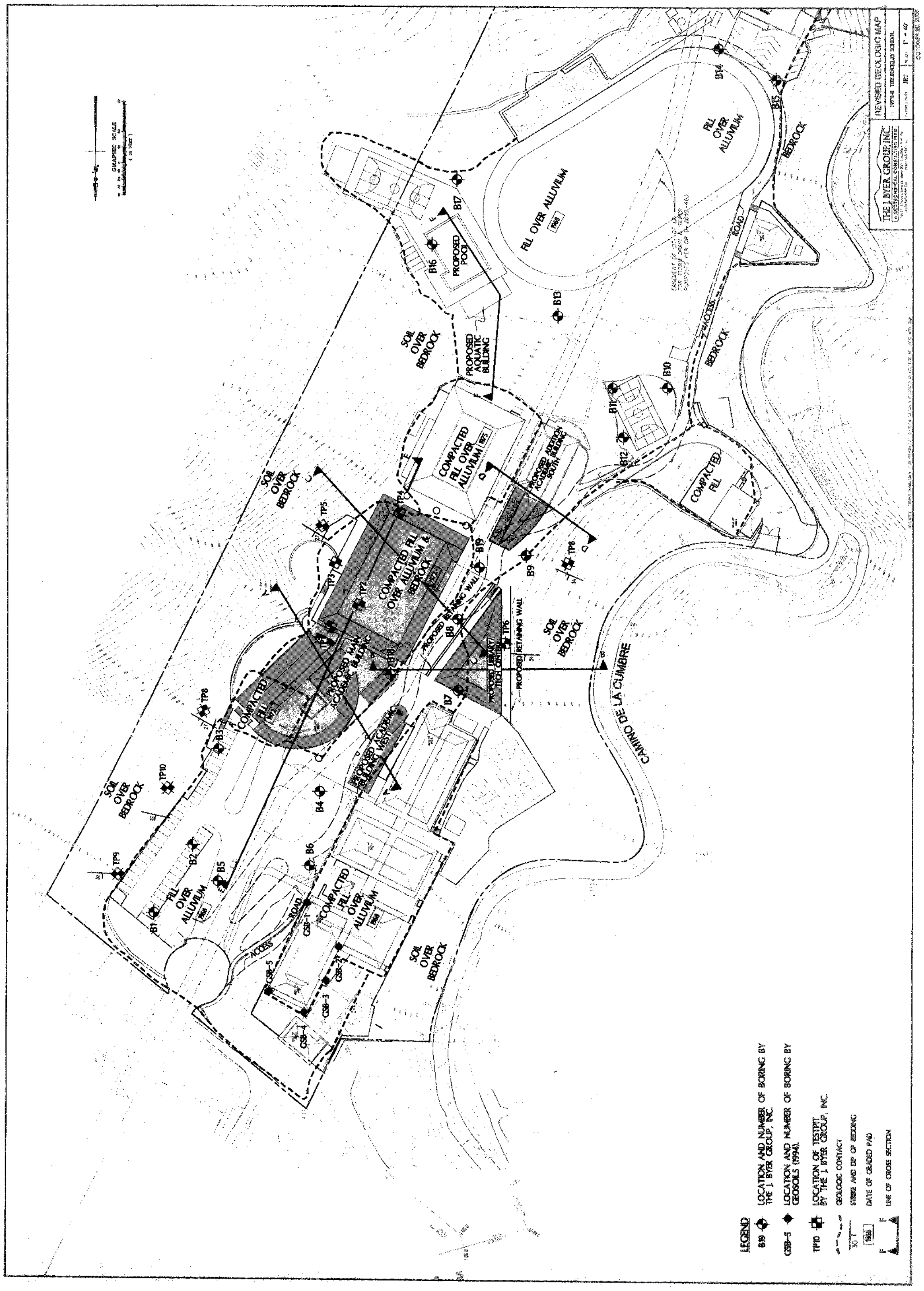
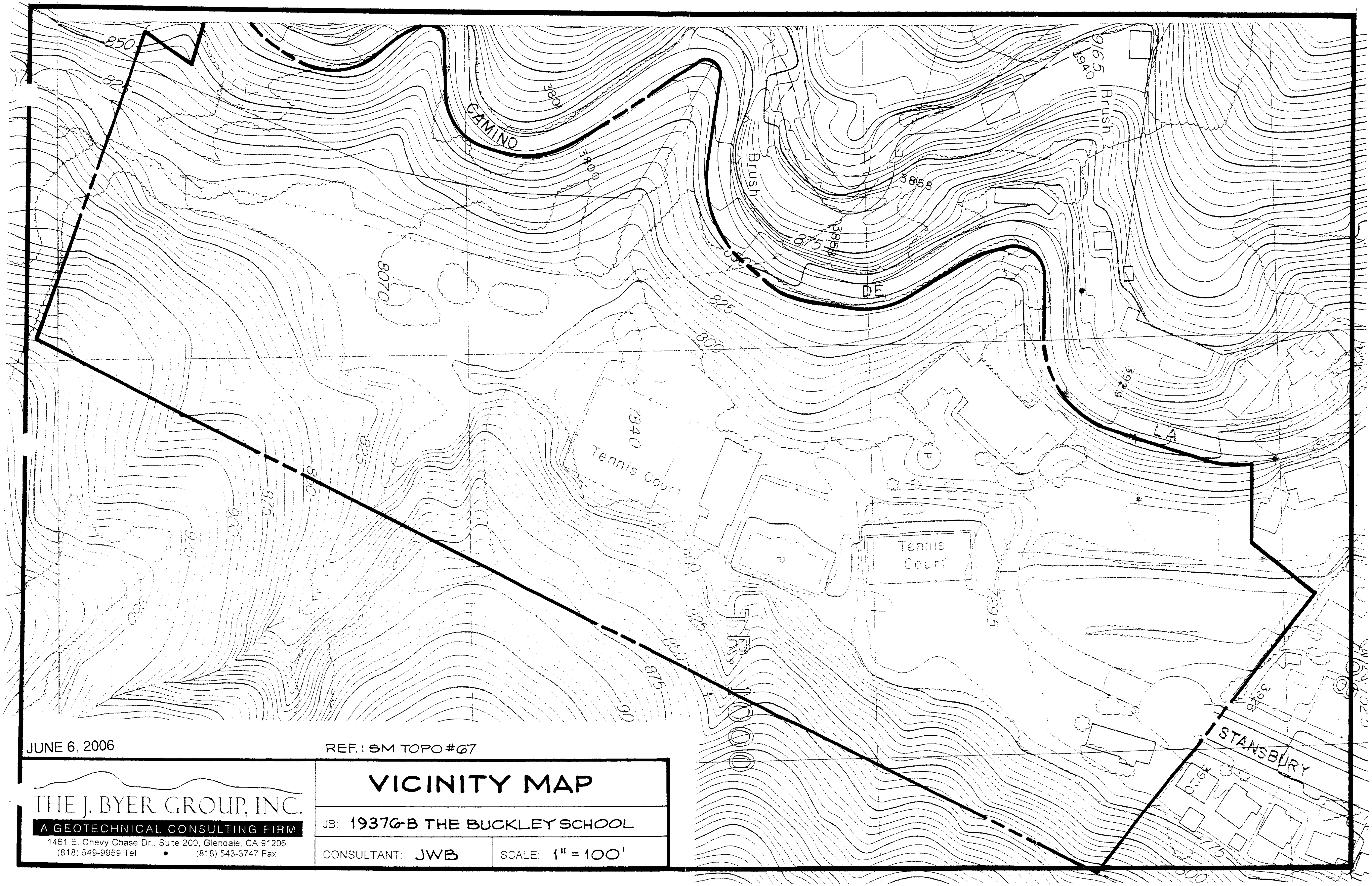


REVISED GEOLOGIC MAP
THE J. BYER GROUP, INC.
LEGEND
B19 LOCATION AND NUMBER OF BORING BY THE J. BYER GROUP, INC.
GSB-5 LOCATION AND NUMBER OF BORING BY GEOSOILS (1994).
TP10 LOCATION OF TESTPIT BY THE J. BYER GROUP, INC.
GEOLOGIC CONTACT
STRIKE AND DIP OF BEDDING
DATE OF GRADED PAD
LINE OF CROSS SECTION
FILL OVER ALLUVIUM
COMPACTED FILL OVER ALLUVIUM
COMPACTED FILL OVER ALLUVIUM & BEDROCK
SOIL OVER BEDROCK
COMPACTED FILL
BEDROCK
PROPOSED POOL
PROPOSED AQUATIC BUILDING
PROPOSED MAIN SCHOOL BUILDING
PROPOSED RETAINING WALL
CAMINO DE LA CUMBRE
ACCESS ROAD

11x17



JUNE 6, 2006

REF.: SM TOPO #67

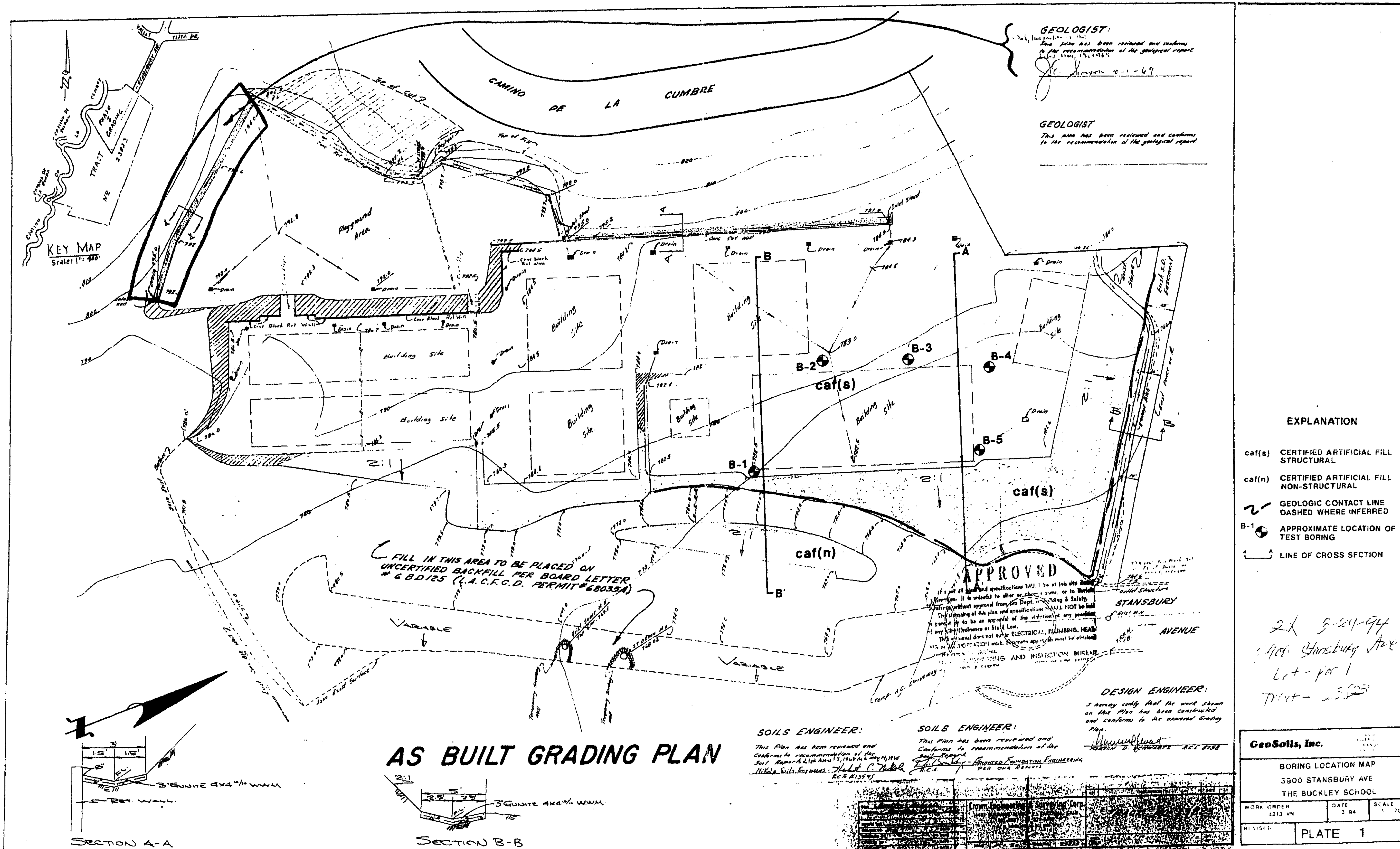
VICINITY MAP

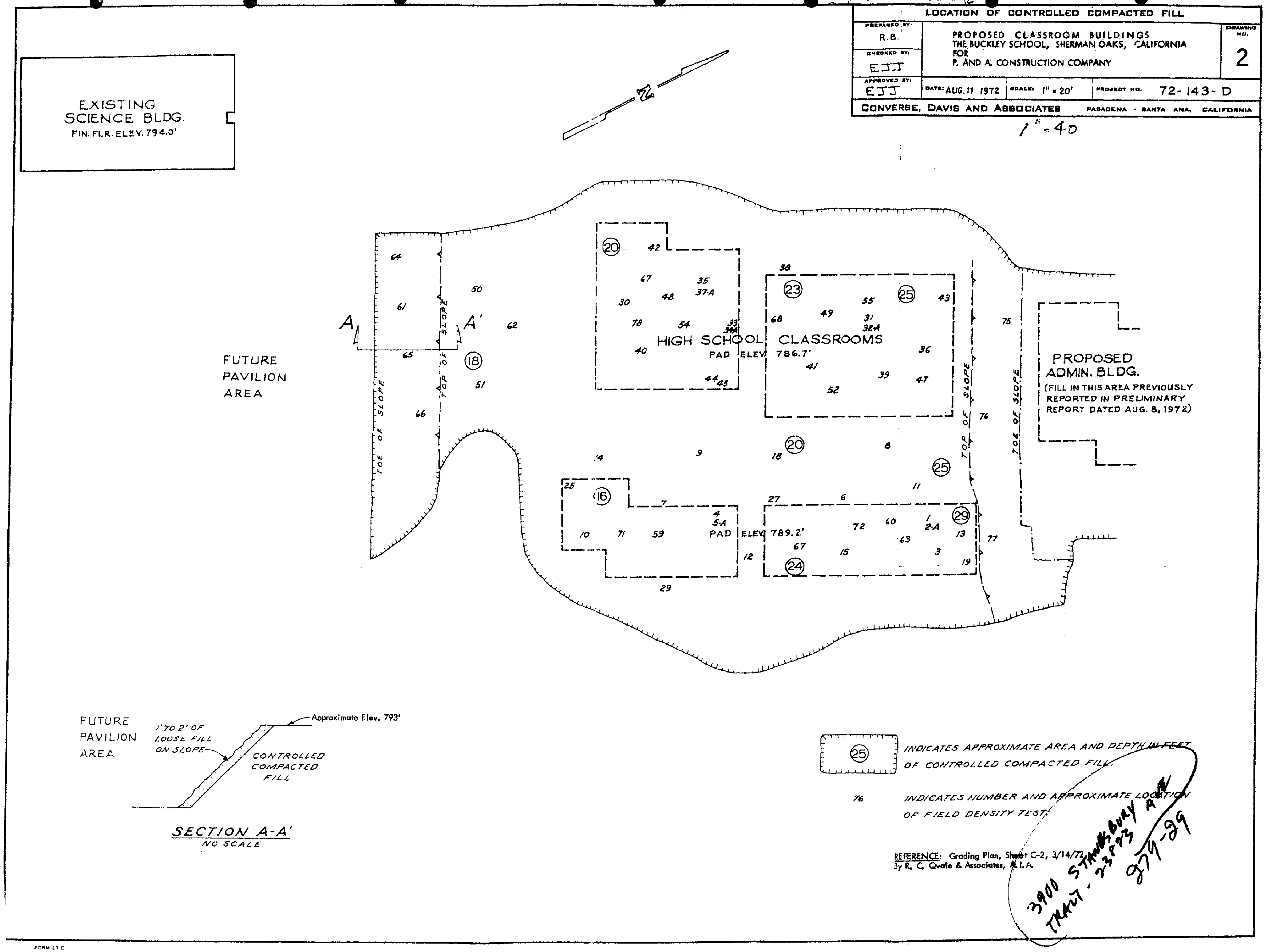
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JWB

SCALE: 1" = 100'


AS BUILT GRADING PLAN
CAMINO DE LA CUMBRE
STANSBURY AVENUE
KEY MAP
Scale: 1" = 400'
Playground Area
Building Site
caf(s)
caf(n)
B-1
B-2
B-3
B-4
B-5
FILL IN THIS AREA TO BE PLACED ON UNCERTIFIED BACKFILL PER BOARD LETTER # 6BD125 (L.A.C.F.C.D. PERMIT # 68035A)
VARIABLE
APPROVED
GEOLOGIST:
This plan has been reviewed and conforms to the recommendation of the geological report.
SOILS ENGINEER:
This Plan has been reviewed and conforms to recommendation of the Soil Report.
DESIGN ENGINEER:
I hereby certify that the work shown on this Plan has been constructed and conforms to the approved Grading Plan.
SECTION A-A
SECTION B-B
3" GUNITE 4x4 10/10 WWM
EXPLANATION
caf(s) CERTIFIED ARTIFICIAL FILL STRUCTURAL
caf(n) CERTIFIED ARTIFICIAL FILL NON-STRUCTURAL
GEOLOGIC CONTACT LINE DASHED WHERE INFERRED
APPROXIMATE LOCATION OF TEST BORING
LINE OF CROSS SECTION
GeoSoils, Inc.
BORING LOCATION MAP
3900 STANSBURY AVE
THE BUCKLEY SCHOOL
WORK ORDER 4213 VN
DATE 3 94
SCALE 1" 20'
REVISED
PLATE 1



LOCATION OF CONTROLLED COMPACTED FILL
PREPARED BY: R.B.
CHECKED BY: EJJ
APPROVED BY: EJJ
PROPOSED CLASSROOM BUILDINGS
THE BUCKLEY SCHOOL, SHERMAN OAKS, CALIFORNIA
FOR
P. AND A. CONSTRUCTION COMPANY
DRAWING NO. 2
DATE: AUG. 11 1972
SCALE: 1" = 20'
PROJECT NO. 72-143-D
CONVERSE, DAVIS AND ASSOCIATES
PASADENA - SANTA ANA, CALIFORNIA
1" = 40
EXISTING SCIENCE BLDG.
FIN. FLR. ELEV. 794.0'
N
FUTURE PAVILION AREA
A
A'
TOE OF SLOPE
TOP OF SLOPE
HIGH SCHOOL CLASSROOMS
PAD ELEV 786.7'
PAD ELEV 789.2'
PROPOSED ADMIN. BLDG.
(FILL IN THIS AREA PREVIOUSLY REPORTED IN PRELIMINARY REPORT DATED AUG. 8, 1972)
FUTURE PAVILION AREA
1' TO 2' OF LOOSE FILL ON SLOPE
Approximate Elev. 793'
CONTROLLED COMPACTED FILL
SECTION A-A'
NO SCALE
25 INDICATES APPROXIMATE AREA AND DEPTH IN FEET OF CONTROLLED COMPACTED FILL.
76 INDICATES NUMBER AND APPROXIMATE LOCATION OF FIELD DENSITY TEST.
REFERENCE: Grading Plan, Sheet C-2, 3/14/72, By R. C. Qvale & Associates, A.I.A.
3900 STANSBURY AVE
TRACT - 23893
279-29
FORM 27 D

LOCATION OF BORINGS

BUCKLEY SCHOOL - PAVILION BUILDING
3900 STANSBURY AVE., SHERMAN OAKS, CALIF.
FOR PAUL W. SPEER, INC.

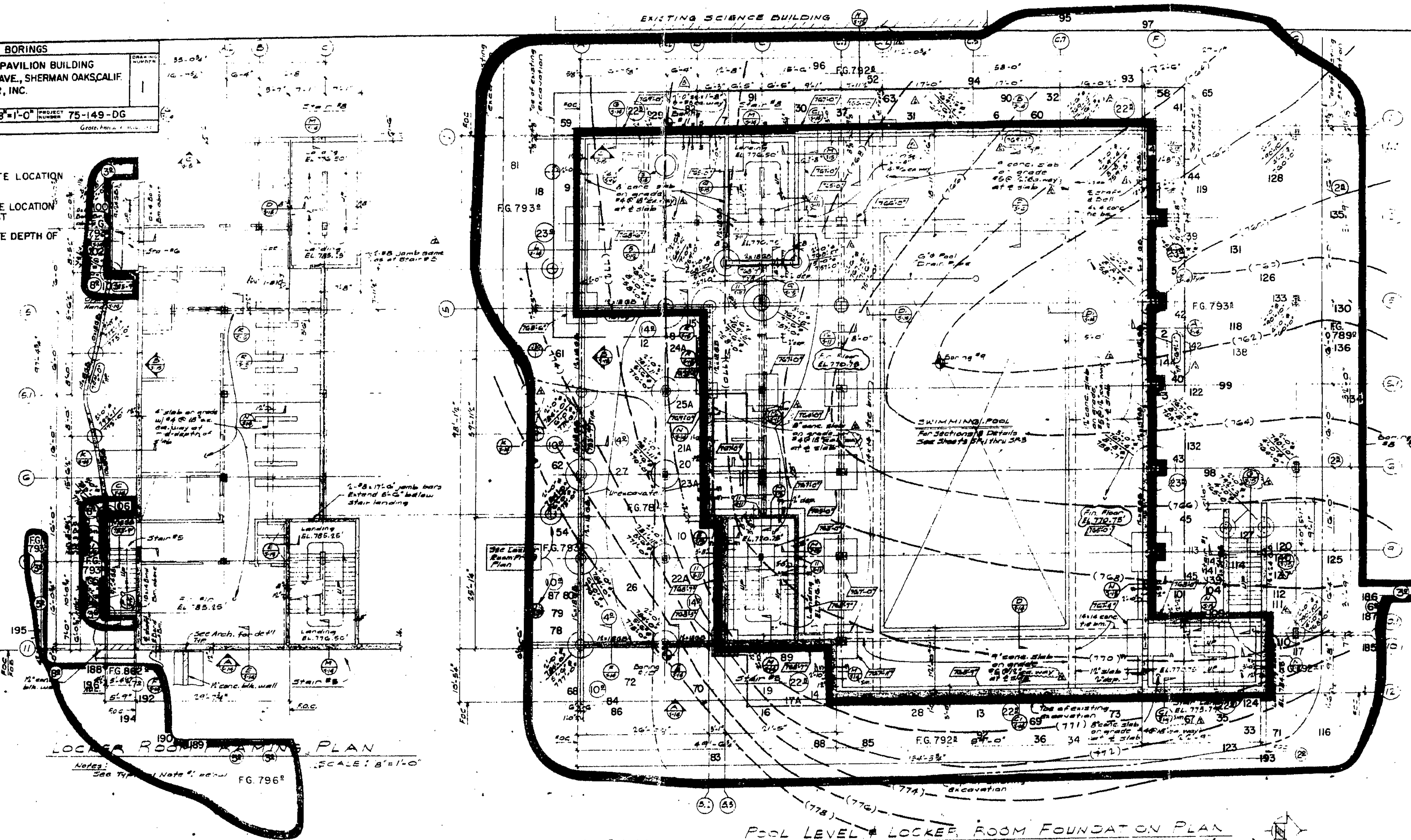
PREPARED BY: J.A.C.	CHECKED BY	APPROVED BY	DRAWING NUMBER: 1
DATE: 6-8-77	SCALE: 1/8" = 1'-0"	PROJECT NUMBER: 75-149-DG	

CONVERSE DAVIS DIXON ASSOCIATES

INDICATES APPROXIMATE LOCATION OF COMPACTED FILL

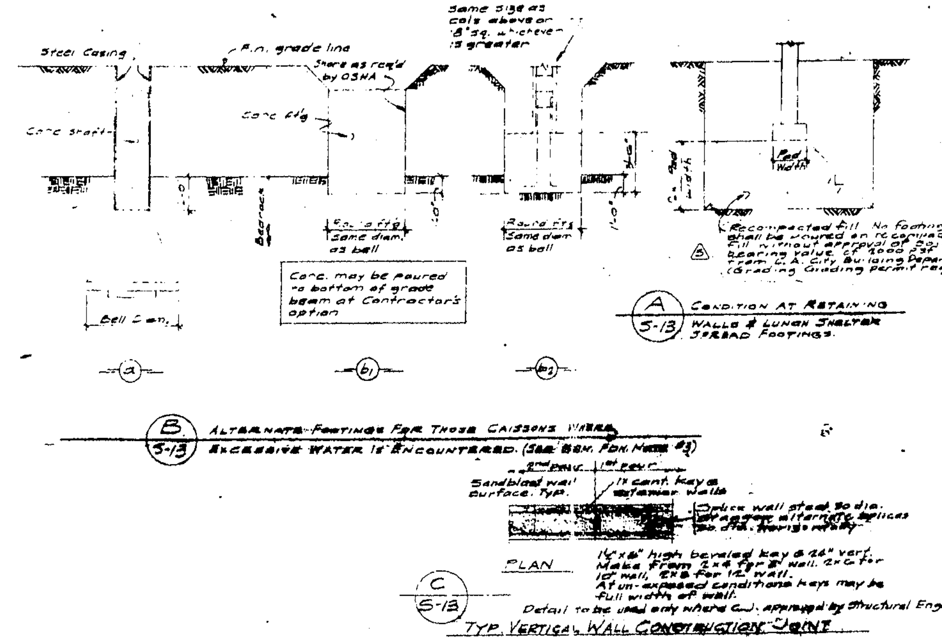
2 INDICATES APPROXIMATE LOCATION OF FIELD DENSITY TEST

(12) INDICATES APPROXIMATE DEPTH OF COMPACTED FILL



TYPICAL NOTES

1. The plans, sections, details & items noted on these drawings shall supersede the previous drawings. Refer to the previous drawings for all items not noted and/or not shown.
2. Maximum soil bearing value for use in design assumed to be 4000 psf.
3. All reinforcing steel shall be ASTM A-615 grade 60 (Ties & Stirrups may be grade 40). Splices of reinforcing steel shall be as follows: #5 thru #7 = 30 dia., #8 and #9 = 40 dia., #10 and #11 = 54 dia. and column bars = 30 dia. unless noted. At splices and laps, bars shall be separated 1½ dia. o.c. min., but in no case shall the separation be less than 1½" clear. However, column bars may be in contact and wall bars may be wired together.
4. Unless otherwise detailed, reinf. steel in cont. beams and spandrels shall have the top steel spliced @ mid-span & the bottom steel spliced over supports (30 dia. min.). At discontinuous ends the top steel shall be bent down ½ dia. or 12" min. whichever is greater.
5. All reinf. steel to be placed in relative position shown on dwg's. No splices in any reinf. will be permitted except those shown on Structural drawings.
6. No sleeving of any grade beam will be permitted unless shown on structural drawings and approved by structural engineer.
7. Concrete for the walls, footings, caissons, and slabs on grade at Pool Level & Locker Room Level shall have an ultimate compressive strength of f'c = 3000 psi at 28 days & shall be continuously inspected. Ultimate Design.
8. All pad footings & continuous footings are to be founded 1'-0" min. as verified by the Soil Engineer.
9. Horizontal construction joints in basement walls are to be provided only where shown and no exceptions are to be allowed. Vertical construction joints shall be per C/5-13 and their location shall be approved by the Structural Engineer.



GENERAL FOUNDATION NOTES

1. The contours shown on the foundation plan show the top of the bedrock elevations as described in the soil report by Converse Davis & Assoc. dated January 1976 and are based on the best information available. The contractor shall base his bid on the contours shown and shall include in his bid a unit price for longer or shorter caisson shafts that may be necessary to reach the actual depth of the bedrock.
2. The caissons shall extend 1'-0" minimum into the bedrock as verified by the Soils Engineer. No concrete shall be placed in any caisson or foundation until the bearing surface is hand cleaned by the contractor, inspected and approved by the Soils Engineer. All requirements of OSHA shall be followed.
3. One Boring (#9) shown in the soil report indicates water, therefore, the following procedure shall be followed:
   - A. Drill pilot hole to bearing stratum (bedrock).
   - B. If water is not (or a normal amount as approved by the Soils Engineer) encountered, the Contractor may bell the caisson and place the concrete.
   - C. If water is encountered in the pilot hole, the Contractor may at his option either:
     1. Excavate and shore the footing as an open pit as shown in detail B/5-13 (b1) & (b2).
     2. Case the pilot hole to seal off the inflow of water and then extend the pilot hole and bell the entire caisson into bedrock per detail B/5-13 (a).
     3. The Contractor shall list in bid form the addition to the base bid for each caisson that requires the procedure specified in 1 or 2 above. In any case, all procedures should be discussed & approved by Soils Engineer.
4. Backfilling of the basement wall shall not be started until the main Gymnasium floor, Locker Room slabs, & Swimming Pool slab on grade have been in place a minimum of 10 days.

LEGEND

- New Concrete in Section
- Indicates Footing Step
- Wall Elevation Symbol
- Elevation Bottom of Footing
- (00-0") Bottom of Grade Beam
- Soil Sample Boring Location (Approximate)

Shaft Diameter (00-0"φ)
Shaft Cut Off Elevation (00-0")
Bell Diameter (00-0"φ)
Bottom of Bell Elevation (00-0")

3900 Stansbury Ave.
Tract 23823

BRUMAN, DOBSON & LOEVENGUTH STRUCTURAL ENGINEERS

382-51

RAGNAR C. QVALE & ASSOCIATES, ARCHITECTS

THE BUCKLEY SCHOOL
SHERMAN OAKS CALIFORNIA

GENERAL NOTES FOUNDATION PLAN & DETAILS

S13

ARCHITECT'S SCALE

THE J. BYER GROUP, INC.

1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

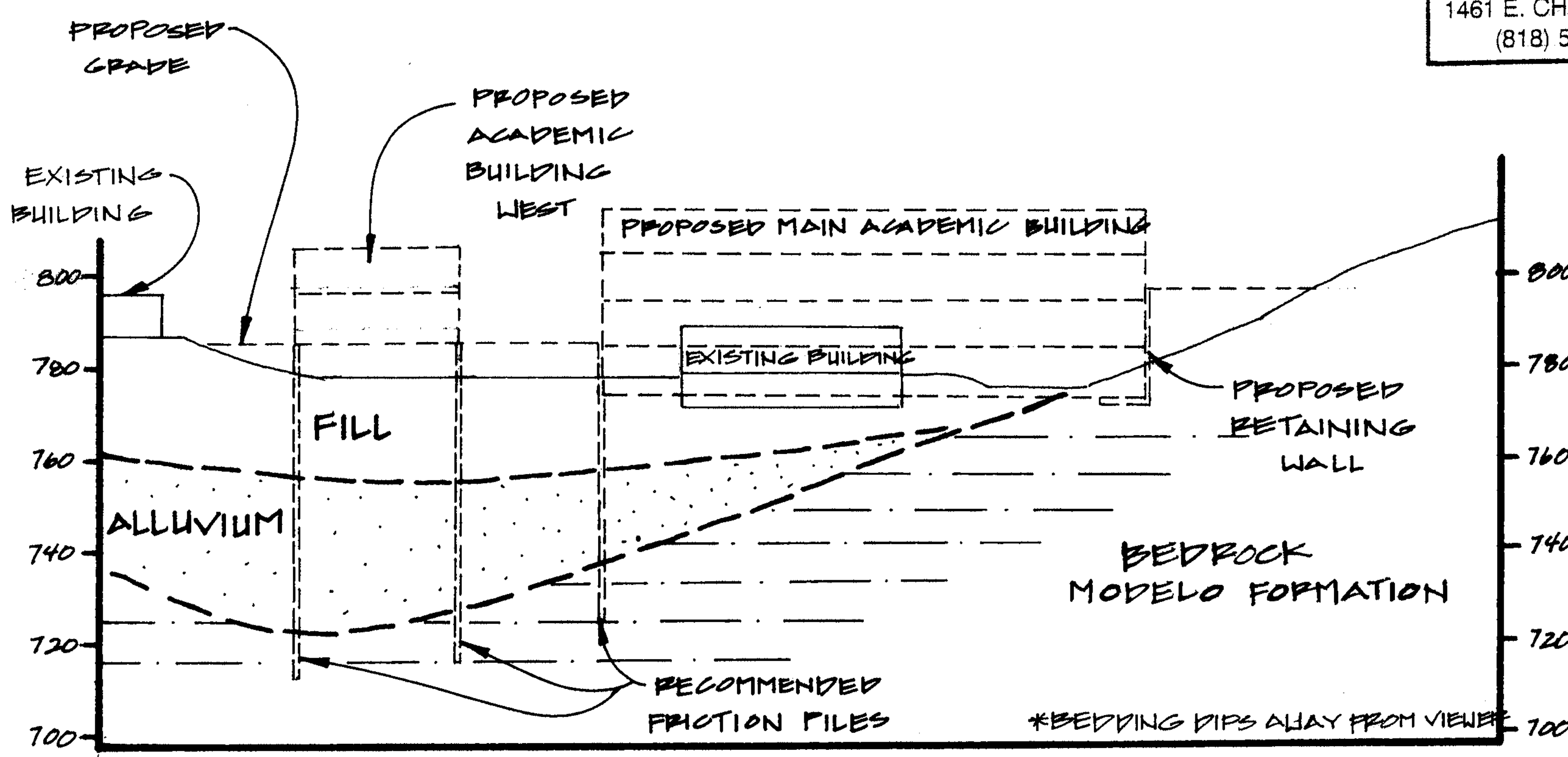
SECTION A & B

JB: 19376-B THE BUCKLEY SCHOOL

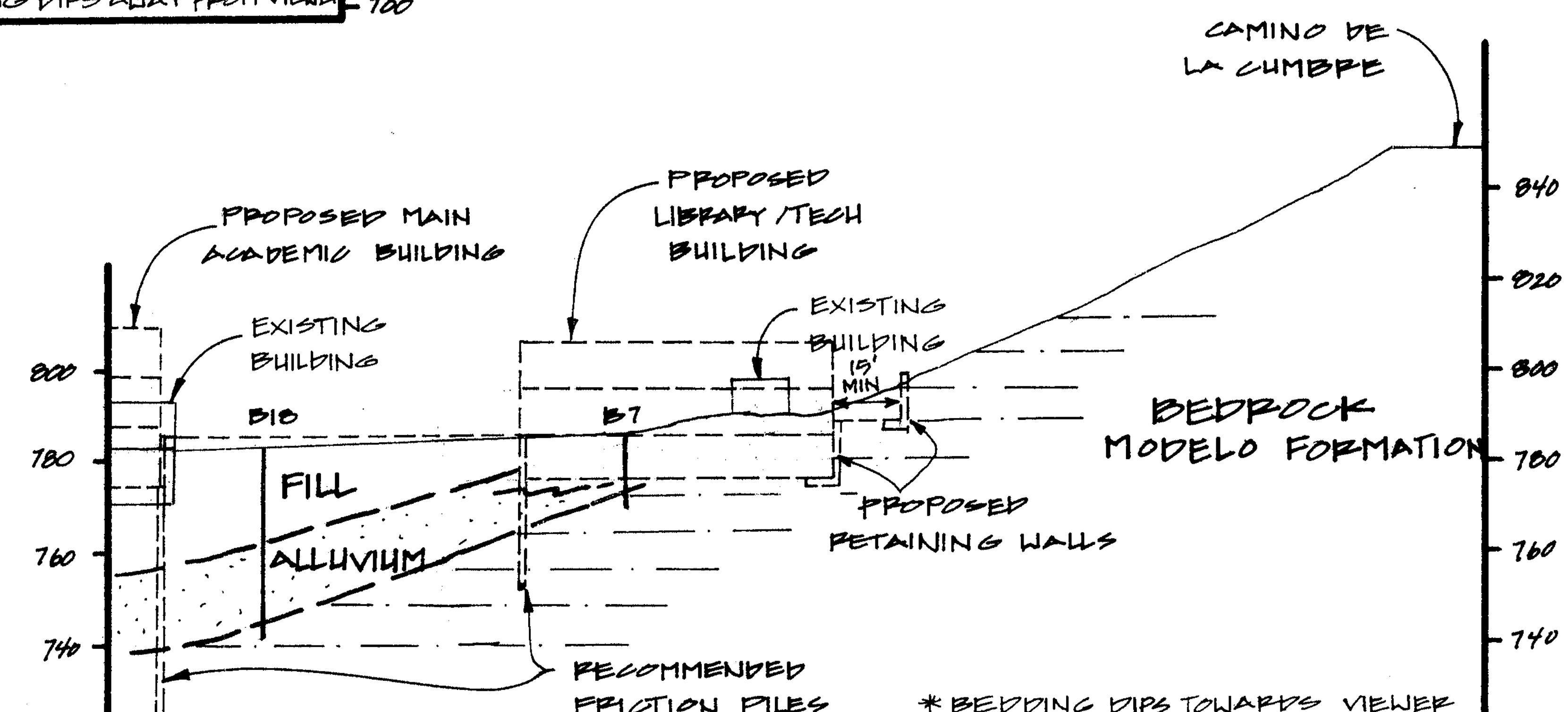
CONSULTANT: JET

SCALE: 1"=40'

JUNE 6, 2006



SECTION A



SECTION B

THE J. BYER GROUP, INC.
1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

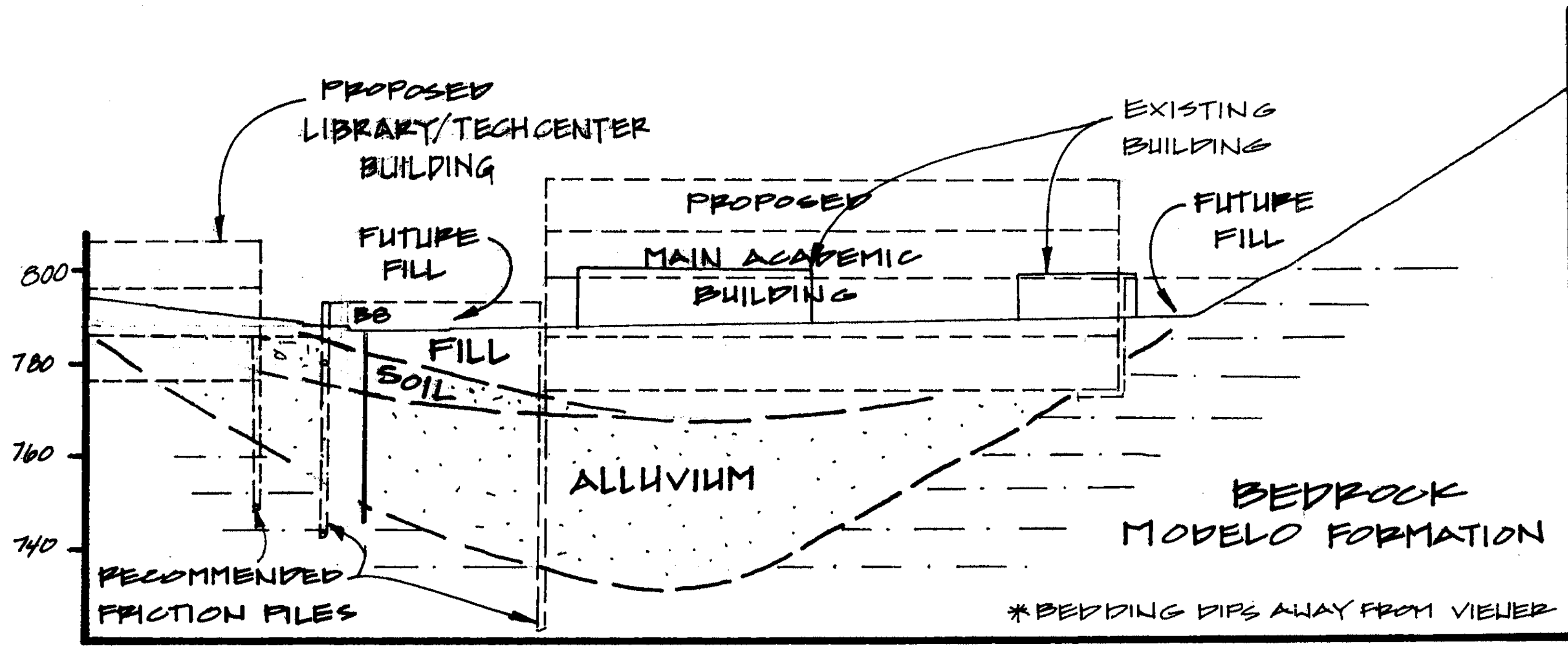
SECTION C & D

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JET

SCALE: 1"=40'

JUNE 6, 2006



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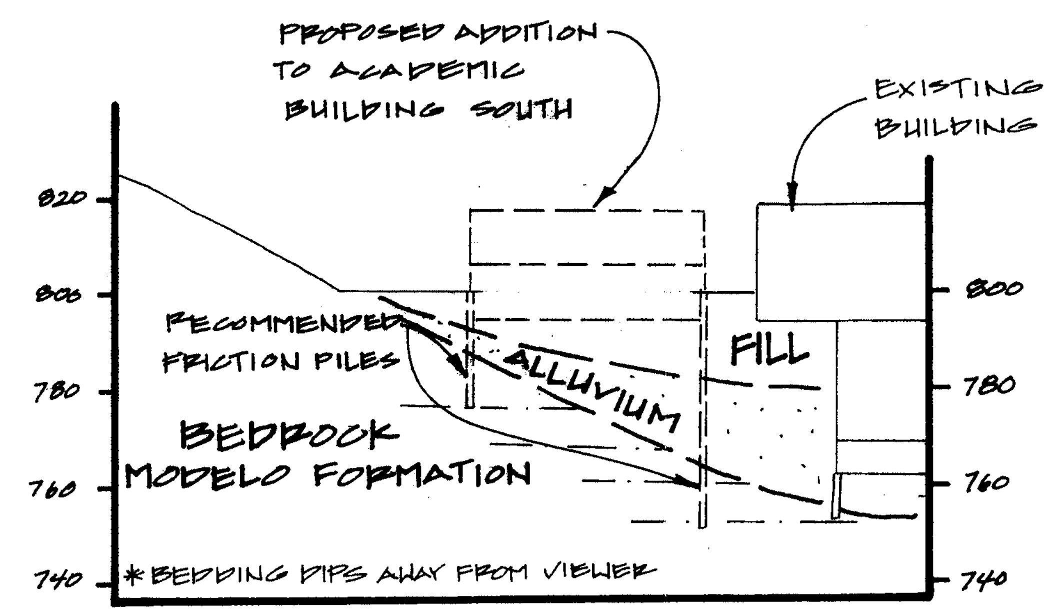


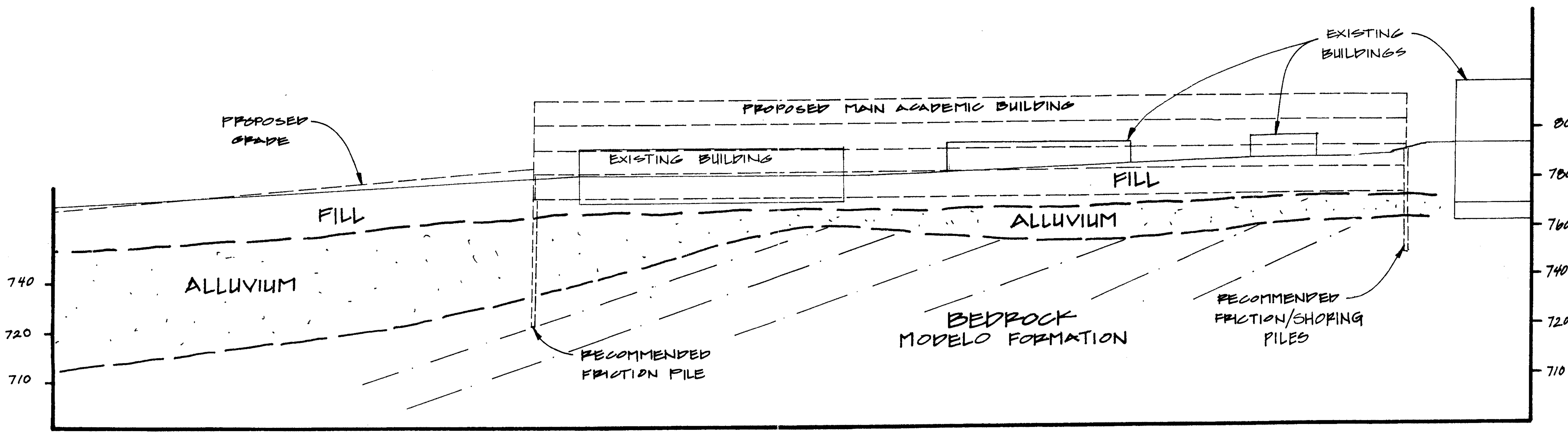
SECTION D

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

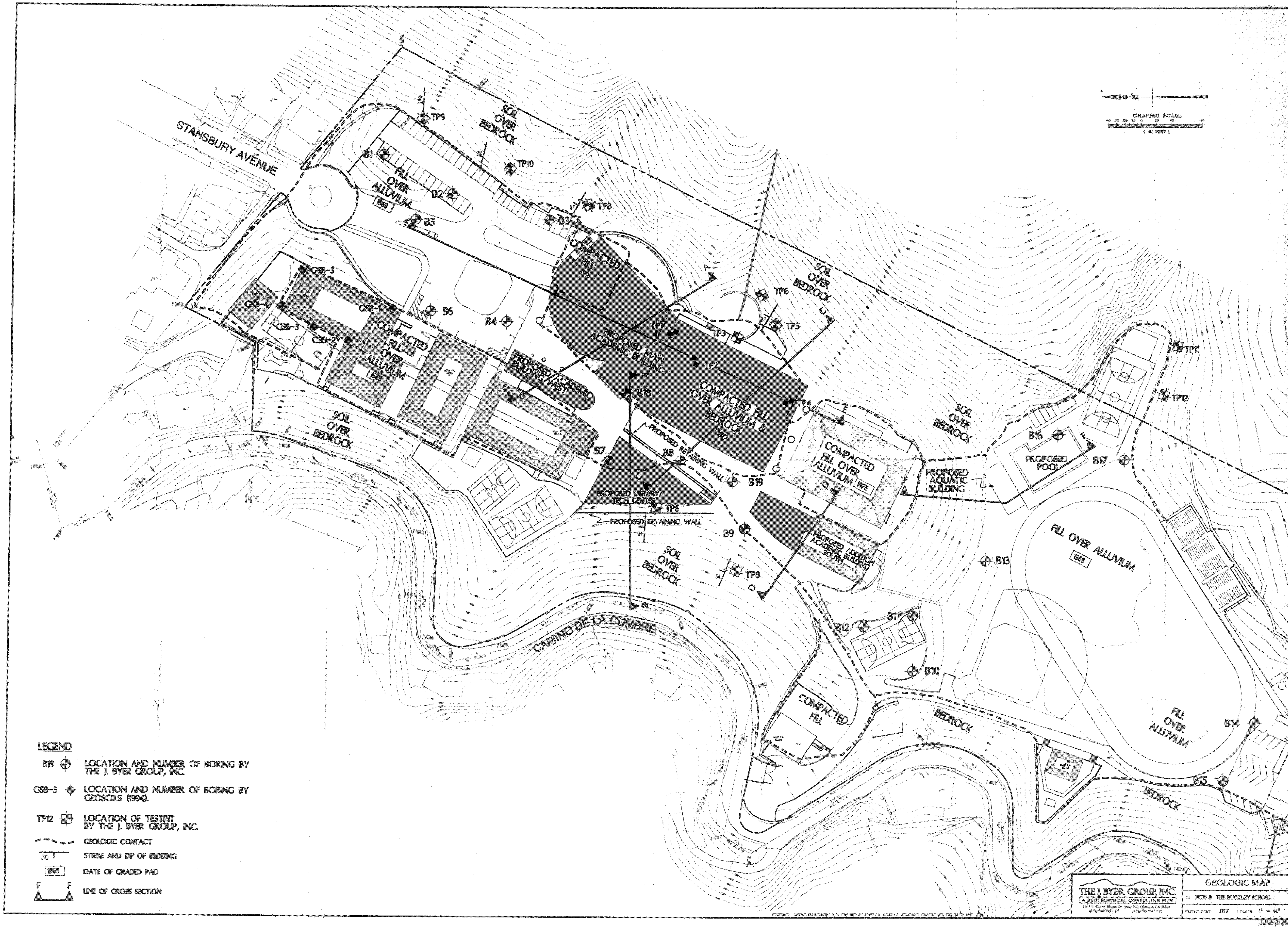
SECTION E

JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JET | SCALE: 1"=40'



SECTION E

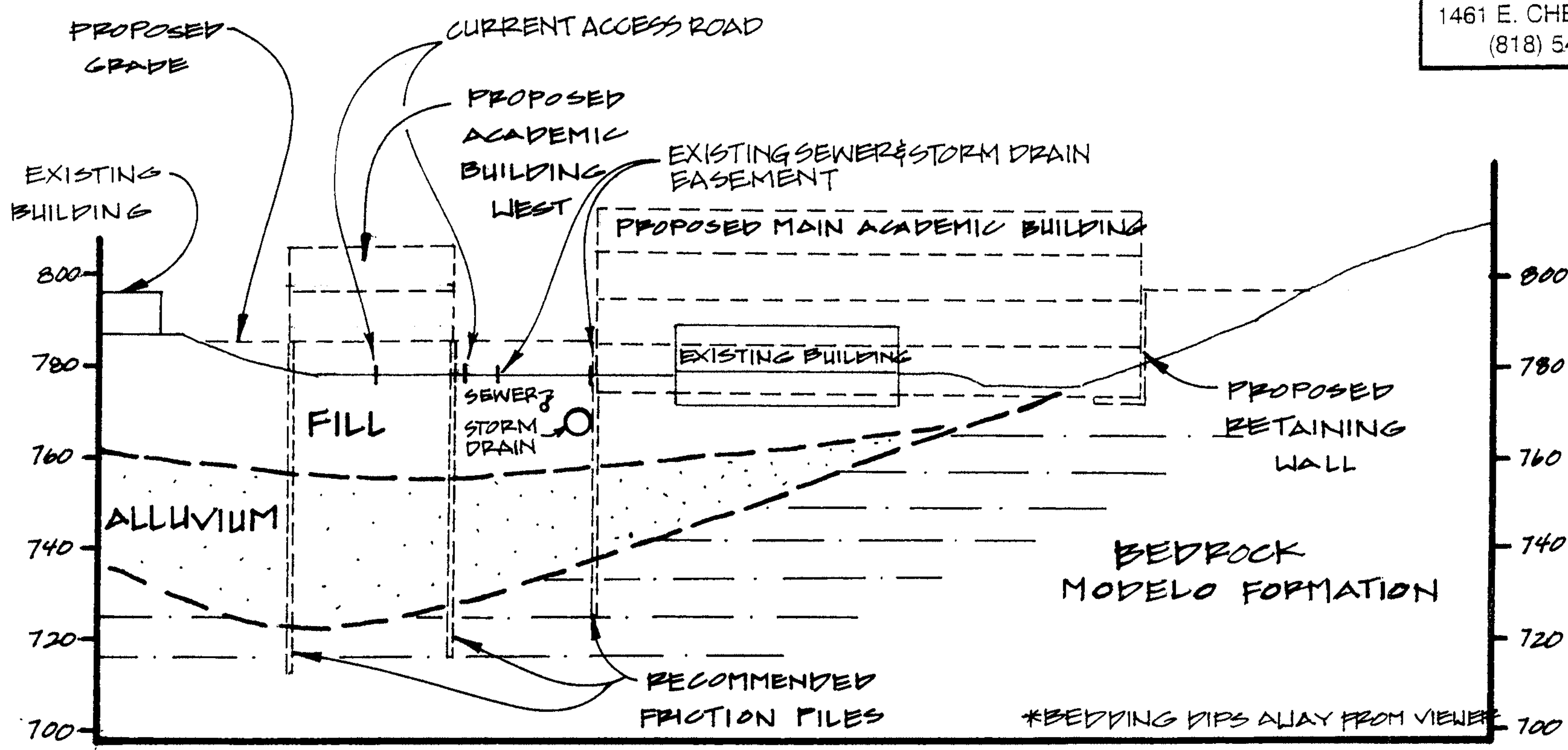


STANSBURY AVENUE
CAMINO DE LA CUMBRE
SOIL OVER BEDROCK
FILL OVER ALLUVIUM
COMPACTED FILL
COMPACTED FILL OVER ALLUVIUM
COMPACTED FILL OVER ALLUVIUM & BEDROCK
PROPOSED MAIN ACADEMIC BUILDING
PROPOSED ACADEMIC BUILDING WEST
PROPOSED LIBRARY/ TECH CENTER
PROPOSED RETAINING WALL
PROPOSED AQUATIC BUILDING
PROPOSED POOL
PROPOSED ADDITION ACADEMIC BUILDING SOUTH
BEDROCK
GRAPHIC SCALE
LEGEND
B19 LOCATION AND NUMBER OF BORING BY THE J. BYER GROUP, INC.
GSB-5 LOCATION AND NUMBER OF BORING BY GEOSOILS (1994).
TP12 LOCATION OF TESTPIT BY THE J. BYER GROUP, INC.
GEOLOGIC CONTACT
STRIKE AND DIP OF BEDDING
DATE OF GRADED PAD
LINE OF CROSS SECTION
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
GEOLOGIC MAP
THE BUCKLEY SCHOOL
JET
SCALE 1" = 40'

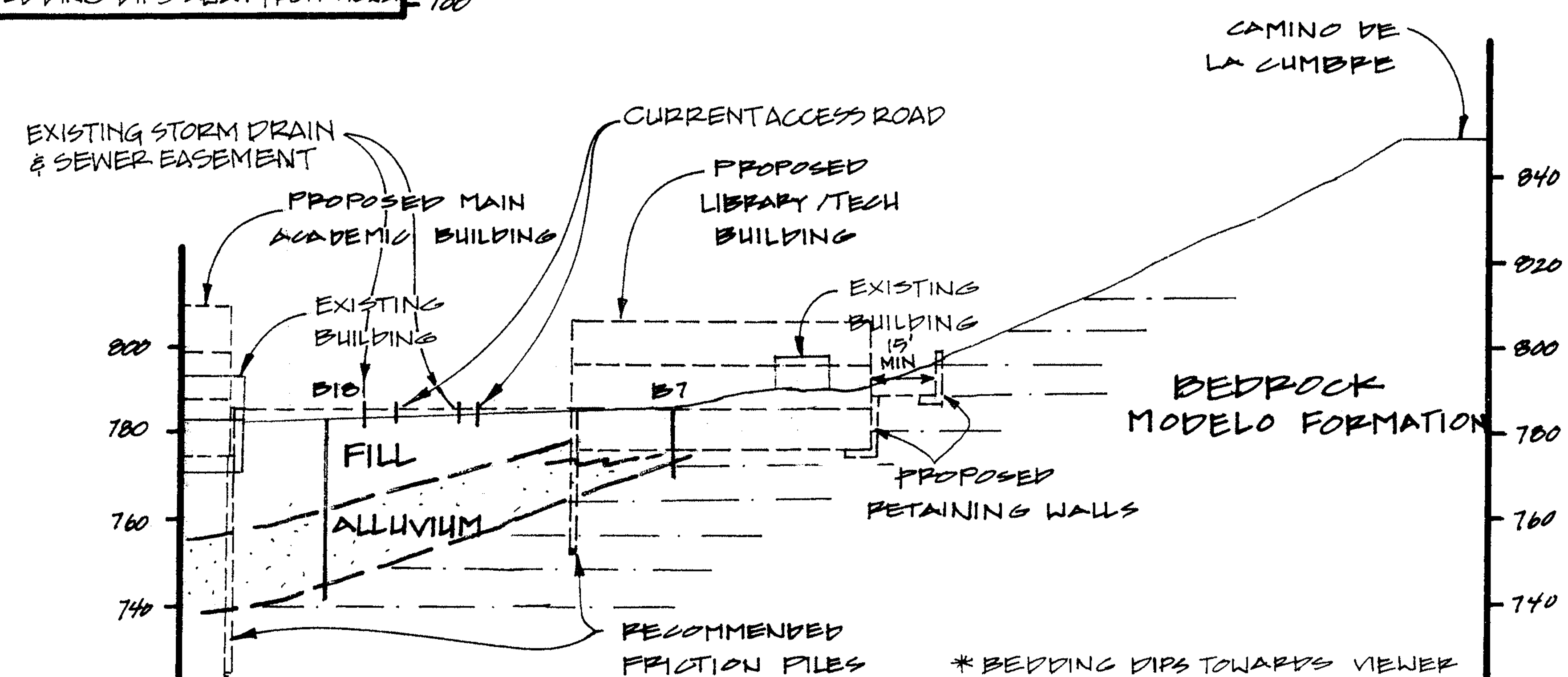
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

SECTION A & B		
JB: 19376-B THE BUCKLEY SCHOOL		
CONSULTANT: JET	SCALE: 1"= 40'	

JUNE 6, 2006
OCTOBER 20, 2006



SECTION A



SECTION B

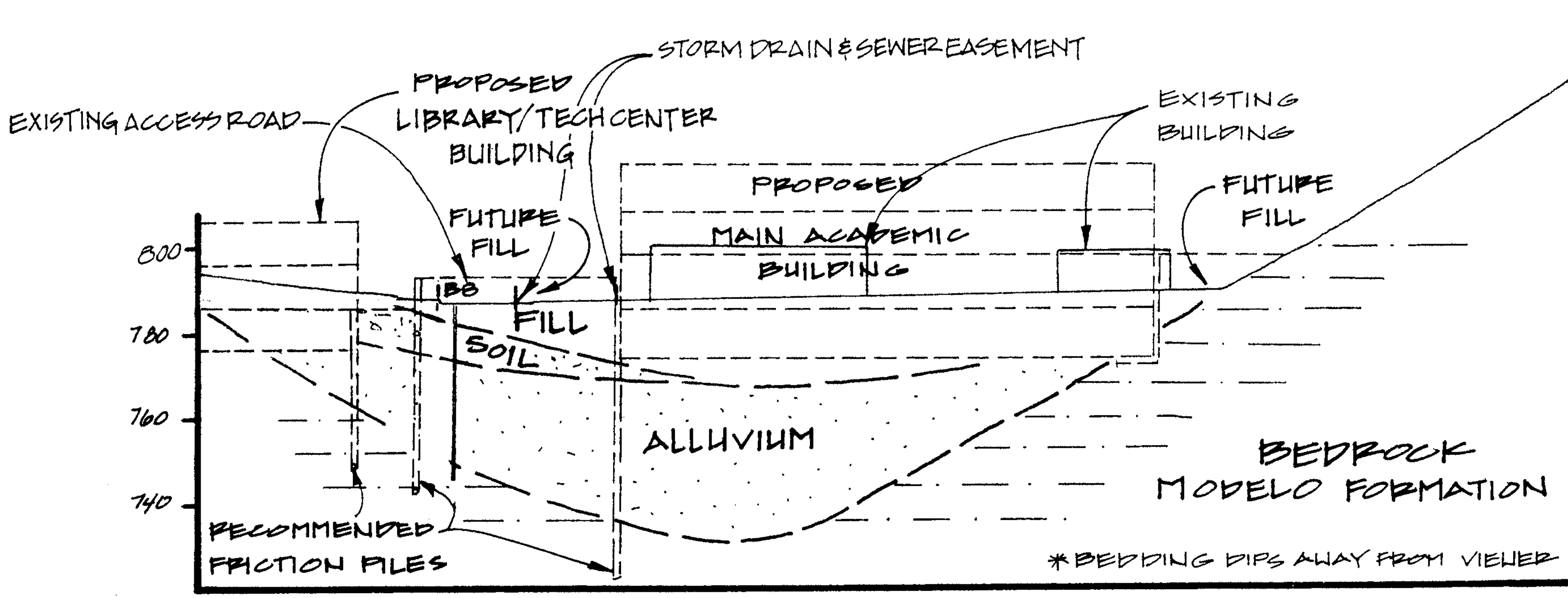
THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. CHEVY CHASE DRIVE, GLENDALE, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

SECTION C & D

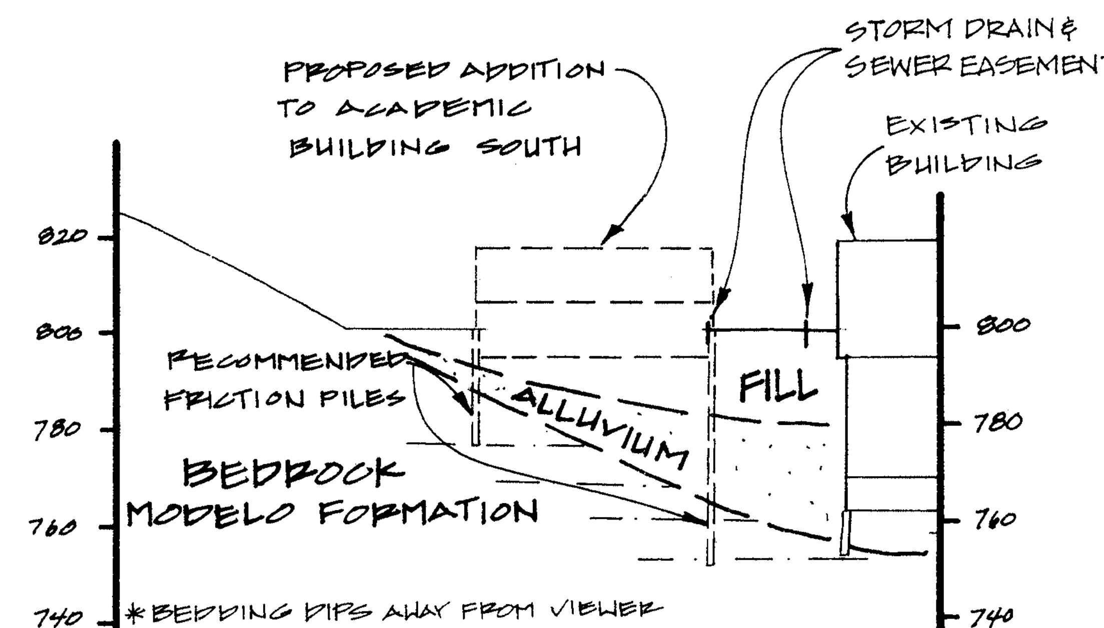
JB: 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JET	SCALE: 1" = 40'

JUNE 6, 2006
OCTOBER 20, 2006



SECTION C



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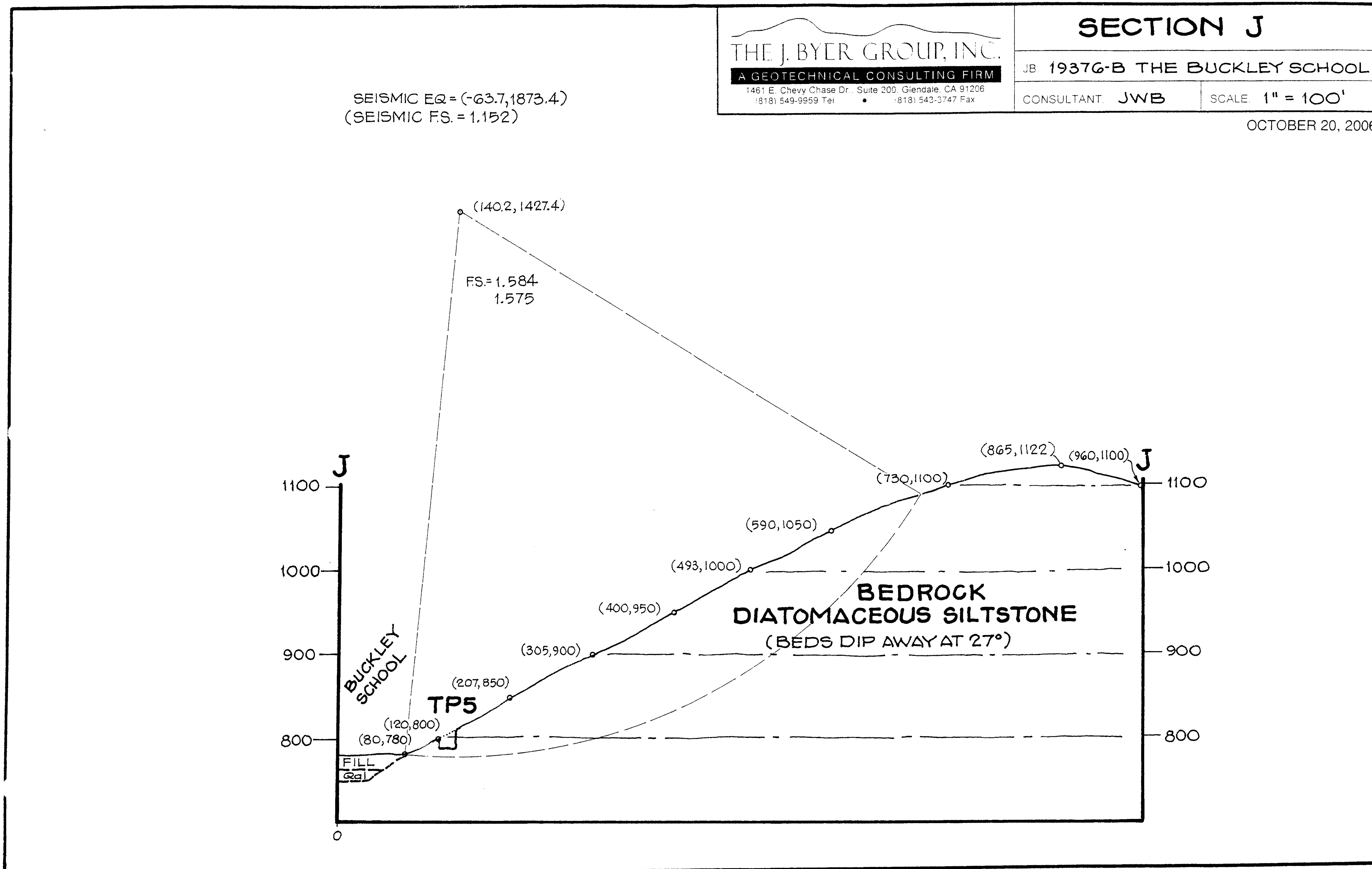
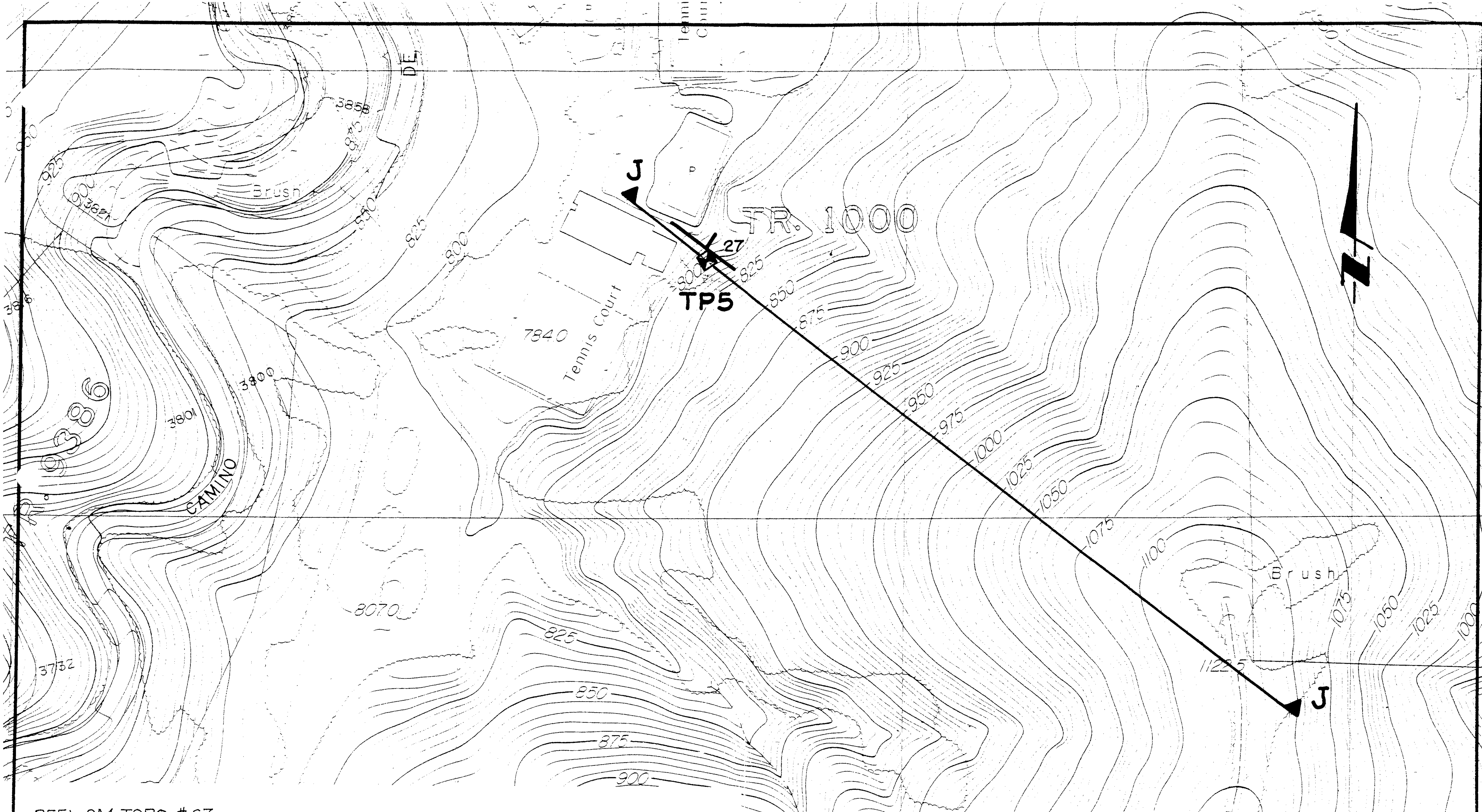

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax
SECTION J
JB 19376-B THE BUCKLEY SCHOOL
CONSULTANT JWB
SCALE 1" = 100'
OCTOBER 20, 2006
SEISMIC EQ = (-63.7,1873.4)
(SEISMIC F.S. = 1.152)
(140.2, 1427.4)
F.S.= 1.584
1.575
J
1100
1000
900
800
0
BUCKLEY SCHOOL
TP5
FILL
Qal
(80,780)
(120,800)
(207,850)
(305,900)
(400,950)
(493,1000)
(590,1050)
(730,1100)
(865,1122)
(960,1100)
BEDROCK
DIATOMACEOUS SILTSTONE
(BEDS DIP AWAY AT 27°)



REF: SM TOPO #67

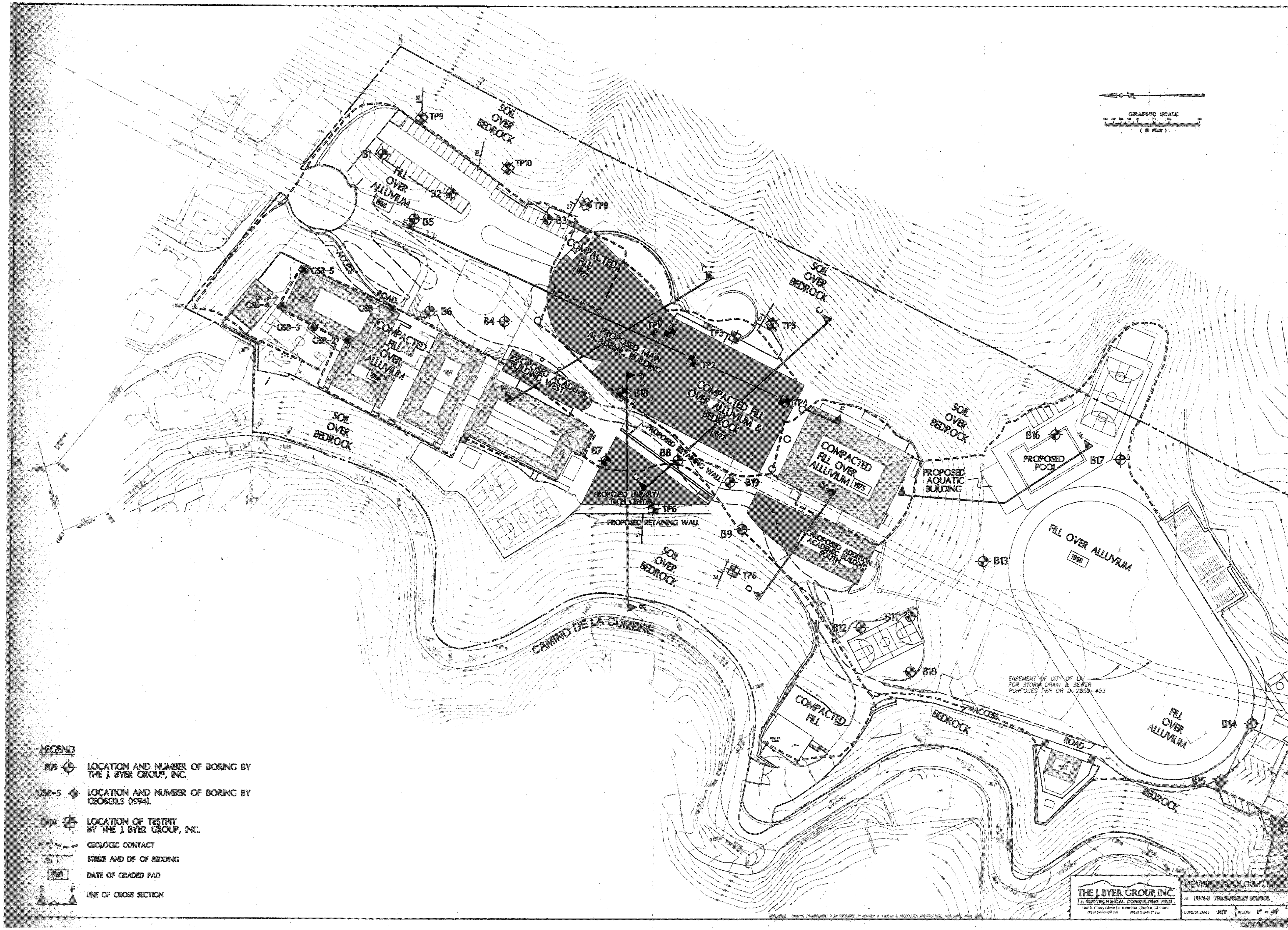
OCTOBER 20, 2006

THE J. BYER GROUP, INC.
A GEOTECHNICAL CONSULTING FIRM
1461 E. Chevy Chase Dr., Suite 200, Glendale, CA 91206
(818) 549-9959 Tel • (818) 543-3747 Fax

VICINITY MAP #2

JB. 19376-B THE BUCKLEY SCHOOL

CONSULTANT: JWB | SCALE: 1" = 100'


GRAPHIC SCALE
(IN FEET)
SOIL OVER BEDROCK
TP9
TP10
B1
FILL OVER ALLUVIUM
B2
TP8
B3
B5
ACCESS ROAD
COMPACTED FILL
GSB-5
GSB-4
GSB-1
GSB-3
GSB-2
B6
B4
COMPACTED FILL OVER ALLUVIUM
PROPOSED MAIN ACADEMIC BUILDING
PROPOSED ACADEMIC BUILDING WEST
TP1
TP3
TP5
TP2
TP4
B18
COMPACTED FILL OVER ALLUVIUM & BEDROCK
SOIL OVER BEDROCK
B7
B8
PROPOSED RETAINING WALL
B19
PROPOSED LIBRARY/TECH CENTER
TP6
PROPOSED RETAINING WALL
COMPACTED FILL OVER ALLUVIUM
PROPOSED AQUATIC BUILDING
B16
PROPOSED POOL
B17
B9
PROPOSED ADDITION ACADEMIC BUILDING SOUTH
FILL OVER ALLUVIUM
B13
SOIL OVER BEDROCK
TP8
CAMINO DE LA CUMBRE
B12
B11
B10
EASEMENT OF CITY OF LA FOR STORM DRAIN & SEWER PURPOSES PER OR D-2659-463
COMPACTED FILL
BEDROCK
ACCESS ROAD
FILL OVER ALLUVIUM
B14
B15
BEDROCK
LEGEND
B19 LOCATION AND NUMBER OF BORING BY THE J. BYER GROUP, INC.
GSB-5 LOCATION AND NUMBER OF BORING BY GEOSOILS (1994).
TP10 LOCATION OF TESTPIT BY THE J. BYER GROUP, INC.
GEOLOGIC CONTACT
STRIKE AND DIP OF BEDDING
DATE OF GRADED PAD
LINE OF CROSS SECTION
THE J. BYER GROUP, INC
A GEOTECHNICAL CONSULTING FIRM
THE BUCKLEY SCHOOL
SCALE: 1" = 40'

Appendix G:

Lead Based Paint Report and Asbestos Report

Lead Based Paint Report

LEAD-BASED PAINT

INSPECTION

REPORT
Report ID #LBP-01

Prepared for:

The Buckley School
3900 Stansbury Road
Sherman Oaks, CALIFORNIA 91423

Curtis Covington, Director of Physical Plant
(818).783-1610 Office
(818).461-6712 Fax

Prepared by:

4/28/06

Kenneth Medici
Certified Asbestos Consultant
California DOSH #92-0007
Lead Inspector/Assessor CA-DHS ID#1629

Site: **The Buckley School, Sherman Oaks Campus - Phase One and Phase Two Structures**

Dates: April 26, 2006 (On-Site XRF Testing)
April 26, 2006 (On-site Assessment)
April 28, 2006 (Issue Inspection Report)

Table of Contents

LIST OF APPENDICES

Lead-Based Paint Inspection & Assessment

The Buckley School
3900 Stansbury Ave
Sherman Oaks, CA 91423

EXECUTIVE SUMMARY

The Buckley School conducted XRF Lead-Based Paint Inspection and Assessment on April 26, 2006 at 3900 Stansbury Ave Sherman Oaks, CA 91423. Structures engaged within this investigation include The Robert Young Library, The Main Campus Administration Building, the Upper School North and South Buildings, the Milkhouse, The College Counselors Trailor, and the Merchandise Trailor. Lead-based paint was discovered at a set of restrooms under the breezeway of the upper school, specifically upon the doorframes of these restrooms. Lead in ceramic tiles was also discovered. See Appendix 1 and details of floor plan of the XRF report. Lead-Dust Wipes, Lead-Air Samples, Lead-in soil samples were not collected for analysis because intact paint containing lead was found and the vast majority of painted surfaces were found not to contain lead. The Buckley School campus was deemed in compliance with all laws regarding lead-based paint.

Section 1.0 Introduction

On April 26, 2006 Applied Toxicology conducted an Lead-paint inspection at the above address. The primary objective of the work was to identify the existence and extent of major lead-containing materials paints utilizing non-destructive investigations. The site construction is believed to have occurred prior to 1970 . An XRF machine was used to accomplish non-destructive testings. AllState Services Environmental Company was employed by Applied Toxicology to conduct the XRF testings.

The accessible areas were visually inspected for suspect lead-containing materials. All accessible suspected lead-containing painted materials were tested using and XRF machine. Areas such as behind/within walls, under existing ACM's, linoleum, under the building, within the structure (hidden by known ACM), under concrete, within layered components, attic interstitial spaces, sub-structure areas, etc. were inaccessible within the scope of this investigation.

Section 2.0 Summary of all Field and Observation Methods Used

XRF Tests - Collection
The survey of April 26, 2006 processed approximately 694 tests of individual surfaces resulting in 16 positive findings of lead in material. The survey of homogeneous building material areas was conducted in a manner that minimized damage to the structure and minimized the health hazard to occupants or inspectors. The number of tests conducted from each suspect homogeneous building material area did follow HUD guidelines for Lead-Paint Inspection

See attached XRF Report prepared by AllState Services Environmental for protocols, testing methodology, detailed XRF findings, recommendations.

Analytical Laboratory Analysis

No Atomic Absorption Spectroscopy (AAS) analysis was performed.
(No samples collected)

Laboratory Analysis Results

N/A

Conclusions and Recommendations

We conclude that ceramic tile, a water fountain, two door frames as stated in the attached XRF report contain lead above the legal limits and caution must be taken by the owner when disturbing these materials.

Because The Buckley School is planning Demolition of these Buildings which contain the above lead materials, the conclusions and recommendations may be tailored as such. We recommend that the owner not utilize this survey report as a stand alone document for bidding purposes by abatement contractors. We recommend the owner employ a CA Certified Asbestos/Lead Consultant and Lead-Related Construction Inspector Assessor - Project Designer to develop and implement an abatement plan along with air monitoring for community/School safety purposes.

Estimated Costs for Abatement (Removal) of Lead Materials

The costs of the above lead-containing materials will not affect the total budget for abatement of asbestos within the Phase one or Phase Two Structures under the current Modernization Project.

The information presented in this Asbestos Survey is based upon the agreed upon scope of work outlined in the above Report text. This environmental assessment is based mainly upon a limited collection and analysis of a limited number of samples from accessible suspected homogeneous material sampling areas. This report is not a legal opinion. The services performed by Applied Toxicology have been conducted in manner consistent with the level of care ordinarily exercised by members of our profession currently practicing under similar conditions. No warranty, expressed or implied is made. Applied Toxicology is not responsible for any claims or damages associated with interpretation of available information. This assessment should not be regarded as a guarantee that no further lead materials beyond that which was suspected to be present at the property, is present at this property. In the event site changes occur, or additional relevant information about the property is brought to our attention, the recommendations contained in this assessment may not be valid unless these changes and additional relevant information are reviewed and recommendations of this assessment are modified or verified in writing. Draft reports are not to be considered final reports.

Ken Medici 4/28/06

==================

Ken Medici
Certified Asbestos Consultant
Cal-OSHA ID # 92-0007
Certified Lead-related Construction Inspector/Assessor
Calif. Dept of Health Services ID#1629

APPENDIX

1.0

XRF REPORT

Professional Environmental Consulting
and Training

Allstate Services
Environmental, Inc.

Working for a clean environment
1826 Pomona Road
Corona, California 92880
(951) 340-1717 (800) 320-LEAD
Fax (951) 340-1448

LEAD-BASED PAINT TESTING

@

THE BUCKLEY SCHOOL
3900 STANSBURY AVENUE
SHERMAN OAKS, CALIFORNIA 917423

PREPARED FOR:
KEN MEDICI
APPLIED TOXICOLOGY
1450 NORTH SANTA FE, SUITE C, PMB #144
VISTA, CALIFORNIA 92083

PREPARED BY:
JAMES HANTGIN & GEORGE MUNOZ
INSPECTOR/ASSESSOR
CERTIFICATION #I-6259 & I-11268

APRIL 28, 2006

Professional Environmental Consulting
and Training

Allstate Services
Environmental, Inc.

Working for a clean environment
1826 Pomona Road
Corona, California 92880
(951) 340-1717 (800) 320-LEAD
Fax (951) 340-1448

April 28, 2006

Ken Medici
Applied Toxicology
1450 Santa Fe, Suite C, PMB #144
Vista, California 92083

RE: Lead-based paint testing at The Buckley School, 3900 Stansbury Avenue, Sherman Oaks, CA

Dear Mr. Medici:

In accordance with your request and authorization, Allstate Services Environmental, Inc. conducted lead-based paint testing at The Buckley School, 3900 Stansbury Avenue in Sherman Oaks, California on April 26, 2006. The on-site work was conducted by James Hantgin and George Munoz, both California Certified Lead Inspector/Assessors.

If you need any further assistance after reviewing your report, please do not hesitate to contact me. Allstate Services Environmental, Inc. remains available to assist you in anyway possible.

Sincerely,

Stacey J. Phelps

Stacey J. Phelps
President

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Appendices

1.0 TESTING METHODOLOGY

Lead-based paint testing was conducted using portable x-ray fluorescence (XRF) spectrum analyzer, Model MAP-4, Manufactured Keymaster Products Division of Kennewick, Washington. The MAP-4 is calibrated to measure the K-shell and the L-shell x-ray emission lines of lead. During testing, only the K-shell readings were recorded per the recommendation of the HUD Guidelines and the XRF Performance Characteristic Sheet (PCS) for the instrument. The K-shell is normally used for paint analysis because it measures lead in all layers of paint films, including the lower layers where higher concentrations of lead are usually found.

Lead-based paint testing was conducted in accordance with *Title 17, California Code of Regulations, Division 1, Chapter 8, Accreditation, Certification, and Work Practice in Lead Related Construction Section 36000* and the United States Department of Housing and Urban Development's *Guidelines for the Evaluation and Control of Lead-Based Paint Hazards in Housing, Chapter 7 Lead-Based Paint Inspection,* as published in June 1995 and revised in 1997.

The purpose of this inspection is to identify surfaces that contain lead-based paint as per *California regulations, the HUD Guidelines and section 403 of the Toxic Substances Control Act.*

The state of California, HUD and the EPA currently define lead-based paint as a paint or other surface coating which contains lead equal to or greater than 1.0 milligrams of lead per square centimeter of surface area (mg/cm^2).

The Los Angeles County Department of Health Services has established a more stringent threshold level of 0.7 mg/cm^2 for lead in paint for lead poisoning cases (LACC Title 11, Chapter 11.28.010, Section C). Due to fact that the subject property is in the Los Angeles County and for the purpose of this report the more stringent standard of 0.7 mg/cm^2 would be used as the threshold level for this survey.

XRF readings were taken using the "Unlimited" mode of the MAP-4. "Unlimited" mode measurements have no predetermined testing length, and automatically adjust to account for various types of substrates and material's densities. The precision of the XRF readings is proportional to the square root of the number of x-rays counted by the scanner. The longer the test, the higher the level of precision as compared against the set threshold level of 0.7 mg/cm^2.

In the "Unlimited" mode, the MAP-4 tests until a K-shell result is indicated as either positive or negative, compared to the threshold level based on the current precision of the test. Correction for paint matrix and substrate effects is performed automatically. The correction function is based on measurements performed by the manufacturer with NIST paint film standards laid over a variety of substrates typically encountered in construction.

Based on the XRF Performance Characteristic Sheet (PCS) jointly released by HUD and EPA (effective June 26, 1996), the inconclusive range of the MAP-4 in the "Unlimited" mode is 0.61 mg/cm^2 to 0.89 mg/cm^2. Results are classified as positive if they are greater than the upper limit of the inconclusive range. Results are classified as negative if they are less than the lower limit of the inconclusive range. No substrate correction is required for testing using the "Unlimited" mode.

XRF readings were made on testing combinations in all room equivalents in an effort to test typical materials, which are representative of the room equivalent. Testing combinations were tested non-destructively by holding the MAP-4 against the surface being tested. At each XRF sample location the MAP-4 shutter is opened, and one reading was made using the "Unlimited"-testing testing mode. Results of each test were read from the digital display of the instrument console and recorded on the XRF Detailed Testing Data Sheet attached in Appendix B.

To ensure that the XRF equipment was working properly, various quality control tests were performed before, during and after the on-site work. At the beginning of the workday, three start up validation measurements were made in the "Test" mode, using the calibration check standard associated with the particular MAP-4 that was used. This painted standard contains a known quantity of lead and allows the XRF operator to determine whether the instrument is functioning within acceptable tolerance ranges for accuracy and precision, as determined by the manufacturer.

In addition to the three starts up tests, calibration readings were taken on the red 1.02 mg/cm^2 Standard Reference Material (SRM) paint film, developed by the National Institute of Standards and Technology (NIST). Results of each reading, along with computed readings averages were recorded on the XRF Calibration Form, and compared against the calibration tolerance range defined the MAP-4 PCS. This calibration check was also performed after four hours and at the end of the day. The quality control tests taken during testing at the subject property were within the acceptable performance range prescribed by the PCS and by the XRF equipment manufacturer. Documentation of the quality control calibration check is included in Appendix A, following the detailed testing data.

2.0 BUILDING DESCRIPTION

The property tested is a school campus with several buildings. The exteriors consist of brick and concrete walls, plaster canopies, brick columns and metal door and window systems. The interiors contain drywall and concrete walls, wood doors with metal frames and metal window systems.

3.0 LEAD-BASED PAINT FINDINGS

Lead-based paint was found at or above the Los Angeles County threshold level of 0.7 mg/cm^2 on the following components:

- ***Interior metal door frames***

Please see Appendix A - XRF Positive Summary Report for a complete list of positive components and specific locations.

4.0 FEDERAL REQUIREMENTS

A copy of this summary must be provided to new lessees (tenants) and purchaser of this property under federal law (24 CFR part 35 and 40 CFR part 745) before they become obligated under a lease or sales contract. The complete report must also be provided to new purchasers and it must be made available to tenants. Landlord (lessors) and sellers are also required to distribute an educational pamphlet approved by the U. S. Environmental Protection Agency and include standard warning language in their lease or sales contracts to ensure that parents have the information they need to protect their children from lead-based paint hazards.

5.0 CALIFORNIA STATE REQUIREMENTS

Allstate Services Environmental, Inc. is required under California regulations (Title 17, CCR, Division 1, Chapter 8) to notify the California Department of Health Services that a lead hazard evaluation survey was conducted at the subject property.

Please see Appendix E for DHS Form 8552, Lead Hazard Evaluation Report.

6.0 LOS ANGELES COUNTY REQUIREMENTS

Allstate Services Environmental, Inc. hereby calls attention to Los Angeles County Code Title 11, Chapter 11.28 "Lead Hazards." As specified by the above, lead-based paint is defined as at or above the level of 0.7mg/cm^2. Thus for this report, all paint tested at or above the Los Angeles County level is considered "Positive."

7.0 RECOMMENDATIONS

If this building undergoes renovation in the future, personnel performing the construction work should be properly trained in lead-related construction. California regulations define lead-related construction work as, "Construction, alteration, painting, demolition, salvage, renovation, repair, or maintenance of any residential, public or commercial building, including preparation and cleanup, that, by using or disturbing lead containing material or soil, may result in significant exposure of individuals to lead."

California has a certification process for lead related construction workers. To receive a list of certified individuals, you may contact the Lead Accreditation and Certification Unit Hotline at (800) 597-5323.

There are different methods of addressing lead hazards. These methods include:

Abatement: A measure or set of measures designed to permanently eliminate lead-based paint hazards or lead-based paint. There are different methods of abatement.

Replacement: Removing the old component and installing a new non-lead containing component. Replacement is best suited for components that are easily removed. This includes doors, windows, trim, etc.

Enclosure: Covering a surface with a durable mechanically affixed, dust tight material, such as drywall, paneling, aluminum siding, etc. Enclosure is best used on walls, ceilings, floors, and some exterior components.

Removal: Removing the paint from the substrate. This is accomplished by wet scraping, using power tools with special HEPA vacuum attachments, heat guns, and chemical stripping either on or off site. Paint removal is best suited when a component is to be preserved or when a component cannot be easily replaced or enclosed. Lead-based paint encapsulant products must have a minimum of twenty years warranty.

Encapsulation: The process that makes lead-based paint inaccessible by providing a barrier between the lead-based paint and the environment. This barrier is formed using a liquid applied coating or an adhesive bonded covering material. Encapsulation is best used on walls and ceilings. Please note that ordinary lead-free paint is not considered an encapsulation.

Interim Controls A set of measures designed to temporarily reduce human exposure or likely exposure to lead-based paint hazards. Interim controls include specialized cleaning, repairs, maintenance, painting, temporary containment, ongoing monitoring of lead-based paint hazards or potential hazards and the establishment and operation of management and resident education programs.

Interim controls should be used only if full abatement is not feasible. Reducing the hazards can be accomplished by simply keeping the painted surfaces intact and through specialized cleaning methods. If abatement cannot take place soon, interim controls should be implemented and maintained until full abatement can be made.

As previously stated, any activities involving lead hazard control and/or lead abatement must be performed by certified individuals.

8.0 OSHA COMPLIANCE

OSHA Regulations (Title 8 CCR Section 1532.1 and 29 CFR 1926.62) apply to all construction work where an employee may be occupationally exposed to lead, and therefore may be applicable to renovation or demolition projects involving paints with any concentration of lead.

It should be noted that "Lead-Based Paint Inspection" is a survey to discover the existence of lead-based paint only, which is defined as paint or other coating with lead levels of 1.0 mg/cm^2 or 0.5%. There are many other building materials, which may contain lead in the average building. When conducting construction activities, which disturb lead in any amount or create an exposure to workers, the employer is required to provide worker protection and conduct exposure assessments. All employers should consult Federal OSHA Regulations at 29 CFR 1926.62 and Cal-OSHA Regulations at Title 8, 1532.1, "Lead in Construction" standards for complete requirements.

APPENDIX A
SUMMARY INSPECTION NOTICE

Professional Environmental Consulting
and Training

Allstate Services
Environmental, Inc.

Working for a clean environment
1826 Pomona Road
Corona, California 92880
(951) 340-1717 (800) 320-LEAD
Fax (951) 340-1448

Summary Notice of Lead-Based Paint Inspection

Address/location of property or structures(s) this summary notice applies to:
The Buckley School
3900 Stansbury Avenue
Sherman Oaks, California 91423

Lead-based paint inspection description:
Dates(s) of inspection: ***April 26, 2006***

Summary of inspection results (check all that apply):
A. ______ No lead-based paint was found.
B. __X__ Lead-based paint was found.
C. __X__ A brief summary of the findings of the inspection is provided below (required if lead-based paint is found)

See positive summary table.

Prepared by: ***James Hantgin*** Certification Number: ***#I-6259***

Signature: James Hantgin Date: ***April 28, 2006***

Prepared by: ***George Munoz*** Certification Number: ***#I-11268***

Signature: George Mu Date: ***April 28, 2006***

POSITIVE XRF SUMMARY REPORT

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
347	Interior	MEN'S RESTROOM	A	Door Frame	Metal	White	Intact	1.32	Positive	1 Ea.	
359	Interior	WOMAN'S RESTROOM	C	Door Frame	Metal	White	Intact	2.01	Positive	1 Ea.	

*** Quantity estimations of leaded materials are provided for budget considerations only.

APPENDIX B
DETAILED XRF TESTING RESULTS

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
1	Exterior	COLLEGE COUNSELOR I	A	Wall	Metal	Tan	Intact	-0.15	Negative		
2	Exterior	COLLEGE COUNSELOR I	B	Wall	Metal	Tan	Intact	0.03	Negative		
3	Exterior	COLLEGE COUNSELOR I	C	Wall	Metal	Tan	Intact	0.09	Negative		
4	Exterior	COLLEGE COUNSELOR I	D	Wall	Metal	Tan	Intact	0.14	Negative		
5	Exterior	COLLEGE COUNSELOR I	A	Fascia	Metal	Tan	Intact	0.16	Negative		
6	Exterior	COLLEGE COUNSELOR I	A	Door	Metal	Tan	Intact	0.33	Negative		
7	Exterior	COLLEGE COUNSELOR I	A	Door Frame	Metal	Tan	Intact	0.22	Negative		
8	Exterior	COLLEGE COUNSELOR II	A	Wall	Metal	Tan	Fair	-0.13	Negative		
9	Exterior	COLLEGE COUNSELOR II	B	Wall	Metal	Tan	Fair	-0.12	Negative		
10	Exterior	COLLEGE COUNSELOR II	C	Wall	Metal	Tan	Fair	0.07	Negative		
11	Exterior	COLLEGE COUNSELOR II	D	Wall	Metal	Tan	Fair	0.10	Negative		
12	Exterior	COLLEGE COUNSELOR II	A	Fascia	Metal	Tan	Fair	0.03	Negative		
13	Exterior	COLLEGE COUNSELOR II	A	Door	Metal	Tan	Fair	0.18	Negative		
14	Exterior	COLLEGE COUNSELOR II	A	Door Frame	Metal	Tan	Fair	0.06	Negative		
15	Exterior	MILK HOUSE	A	Wall	Brick	Tan	Fair	0.30	Negative		
16	Exterior	MILK HOUSE	B	Wall	Brick	Tan	Fair	0.20	Negative		
17	Exterior	MILK HOUSE	C	Wall	Brick	Tan	Fair	0.04	Negative		
18	Exterior	MILK HOUSE	D	Wall	Brick	Tan	Fair	0.18	Negative		
19	Exterior	MILK HOUSE	B	Fascia	Wood	Green	Fair	0.10	Negative		
20	Exterior	MILK HOUSE	B	Overhang	Wood	Tan	Fair	0.30	Negative		
21	Exterior	MILK HOUSE	C	Door	Metal	White	Fair	-0.07	Negative		
22	Exterior	MILK HOUSE	C	Door Frame	Metal	White	Fair	-0.14	Negative		
23	Exterior	LIBRARY	A	Wall	Concrete	Tan	Intact	-0.37	Negative		
24	Exterior	LIBRARY	B	Wall	Concrete	Tan	Intact	-0.26	Negative		
25	Exterior	LIBRARY	C	Wall	Concrete	Tan	Intact	-0.04	Negative		
26	Exterior	LIBRARY	D	Wall	Concrete	Tan	Intact	-0.39	Negative		
27	Exterior	LIBRARY	A	Column	Concrete	Tan	Intact	-0.18	Negative		
28	Exterior	LIBRARY	A	Fascia	Wood	Brown	Intact	-0.13	Negative		
29	Exterior	LIBRARY	A	Overhang	Plaster	Tan	Intact	0.22	Negative		
30	Exterior	LIBRARY	A	Gutter	Metal	White	Intact	0.27	Negative		
31	Exterior	LIBRARY	B	Railing	Metal	Green	Intact	0.44	Negative		
32	Exterior	LIBRARY	C	Boiler Door	Metal	Tan	Fair	0.01	Negative		
33	Exterior	LIBRARY	C	Boiler Door Frame	Metal	Tan	Fair	0.23	Negative		
34	Exterior	SOUTH CAMPUS BLDG.	A	Wall	Plaster	White	Intact	-0.29	Negative		
35	Exterior	SOUTH CAMPUS BLDG.	B	Wall	Plaster	White	Intact	0.23	Negative		
36	Exterior	SOUTH CAMPUS BLDG.	C	Wall	Plaster	White	Intact	-0.45	Negative		
37	Exterior	SOUTH CAMPUS BLDG.	D	Wall	Plaster	White	Intact	0.04	Negative		
38	Exterior	SOUTH CAMPUS BLDG.	C	Window Frame	Wood	Brown	Intact	-0.50	Negative		
39	Exterior	SOUTH CAMPUS BLDG.	A	Door Frame	Wood	Tan	Intact	0.17	Negative		
40	Exterior	SOUTH CAMPUS BLDG.	A	Door	Metal	Tan	Intact	0.04	Negative		
41	Exterior	SOUTH CAMPUS BLDG.	A	Lower Fascia	Wood	Brown	Intact	0.03	Negative		
42	Exterior	SOUTH CAMPUS BLDG.	A	Overhang	Plaster	White	Intact	0.26	Negative		
43	Exterior	SOUTH CAMPUS BLDG.	A	Tile	Ceramic Tile	Red	Intact	0.18	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/cm²)	Results	Quantities For Entire Area	Comments
44	Exterior	SOUTH CAMPUS BLDG.	A	Fountain	Ceramic Tile	Yellow	Intact	31.97	Positive	1 Ea.	Not a paint
45	Exterior	SOUTH CAMPUS BLDG.	A	Locker Counter	Wood	White	Intact	0.06	Negative		
46	Exterior	SOUTH CAMPUS BLDG.	A	Locker	Metal	Gray	Intact	-0.24	Negative		
47	Exterior	SOUTH CAMPUS BLDG.	A	Gutter	Metal	White	Intact	-0.03	Negative		
48	Exterior	NORTH CAMPUS BLDG.	A	Wall	Plaster	Tan	Intact	0.01	Negative		
49	Exterior	NORTH CAMPUS BLDG.	B	Wall	Plaster	Tan	Intact	0.04	Negative		
50	Exterior	NORTH CAMPUS BLDG.	C	Wall	Plaster	Tan	Intact	0.05	Negative		
51	Exterior	NORTH CAMPUS BLDG.	D	Wall	Plaster	Tan	Intact	-0.43	Negative		
52	Exterior	NORTH CAMPUS BLDG.	C	Fascia	Wood	Brown	Intact	0.03	Negative		
53	Exterior	NORTH CAMPUS BLDG.	C	Overhang	Plaster	Tan	Intact	0.06	Negative		
54	Exterior	NORTH CAMPUS BLDG.	C	Tile	Ceramic Tile	Red	Intact	0.11	Negative		
55	Exterior	NORTH CAMPUS BLDG.	C	Fountain	Ceramic Tile	White	Intact	0.08	Negative		
56	Exterior	NORTH CAMPUS BLDG.	C	Door	Wood	White	Intact	-0.76	Negative		
57	Exterior	NORTH CAMPUS BLDG.	C	Door Frame	Metal	White	Intact	0.03	Negative		
58	Exterior	NORTH CAMPUS BLDG.	C	Window Frame	Wood	Brown	Intact	0.24	Negative		
59	Exterior	NORTH CAMPUS BLDG.	B	Lockers	Metal	White	Fair	0.17	Negative		
60	Exterior	NORTH CAMPUS BLDG.	C	Gutter	Metal	White	Intact	0.09	Negative		
61	Exterior	NORTH CAMPUS BLDG.	C	Lubbers	Metal	White	Fair	0.07	Negative		
62	Exterior	NORTH CAMPUS BLDG.	D	Mech. Door	Metal	Tan	Intact	-0.31	Negative		
63	Exterior	ADMINISTRATIVE BLDG.	A	Wall	Plaster	White	Intact	-0.05	Negative		
64	Exterior	ADMINISTRATIVE BLDG.	B	Wall	Plaster	White	Intact	-0.50	Negative		
65	Exterior	ADMINISTRATIVE BLDG.	C	Wall	Plaster	White	Intact	0.07	Negative		
66	Exterior	ADMINISTRATIVE BLDG.	D	Wall	Plaster	White	Intact	-0.33	Negative		
67	Exterior	ADMINISTRATIVE BLDG.	C	Handrail	Metal	Green	Intact	-0.26	Negative		
68	Exterior	ADMINISTRATIVE BLDG.	C	Gutter	Metal	White	Intact	-0.19	Negative		
69	Exterior	ADMINISTRATIVE BLDG.	C	Fascia	Wood	Brown	Intact	-0.24	Negative		
70	Exterior	ADMINISTRATIVE BLDG.	---	Overhang	Plaster	White	Intact	0.16	Negative		
71	Exterior	ADMINISTRATIVE BLDG.	C	Column	Brick	Brown	Intact	0.03	Negative		
72	Exterior	ADMINISTRATIVE BLDG.	C	Window Frame	Wood	Brown	Intact	0.13	Negative		
73	Exterior	ADMINISTRATIVE BLDG.	C	Window Sill	Wood	Brown	Intact	-0.28	Negative		
74	Exterior	ADMINISTRATIVE BLDG.	C	Door	Metal	Black	Intact	-0.11	Negative		
75	Exterior	ADMINISTRATIVE BLDG.	A	Lockers	Metal	Tan	Intact	-0.13	Negative		
76	Exterior	ADMINISTRATIVE BLDG.	---	Vent Caps	Metal	Tan	Intact	0.06	Negative		On the Roof
77	Exterior	ADMINISTRATIVE BLDG.	---	Vent	Metal	Tan	Intact	0.09	Negative		On the Roof

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/cm²)	Results	Quantities For Entire Area	Comments
78	Interior	COLLEGE COUNSELOR I	A	Wall	Drywall	White	Intact	-0.11	Negative		
79	Interior	COLLEGE COUNSELOR I	B	Wall	Drywall	White	Intact	-0.08	Negative		
80	Interior	COLLEGE COUNSELOR I	C	Wall	Drywall	White	Intact	-0.02	Negative		
81	Interior	COLLEGE COUNSELOR I	D	Wall	Drywall	White	Intact	-0.14	Negative		
82	Interior	COLLEGE COUNSELOR I	A	Door	Metal	White	Intact	0.03	Negative		
83	Interior	COLLEGE COUNSELOR I	A	Door Frame	Metal	White	Intact	0.04	Negative		
84	Interior	COLLEGE COUNSELOR I	---	Ceiling	Drywall	White	Intact	-0.08	Negative		
85	Interior	MILK HOUSE	A	Wall	Concrete	White	Intact	-0.07	Negative		
86	Interior	MILK HOUSE	B	Wall	Concrete	White	Intact	0.08	Negative		
87	Interior	MILK HOUSE	C	Wall	Concrete	White	Intact	-0.19	Negative		
88	Interior	MILK HOUSE	D	Wall	Concrete	White	Intact	0.03	Negative		
89	Interior	MILK HOUSE	C	Door	Metal	Tan	Poor	-0.02	Negative		
90	Interior	MILK HOUSE	C	Door Frame	Metal	Tan	Poor	-0.06	Negative		
91	Interior	MILK HOUSE	C	Window Service	Wood	White	Intact	0.03	Negative		
92	Interior	MILK HOUSE	C	Window Frame	Wood	White	Intact	0.14	Negative		
93	Interior	MILK HOUSE	---	Ceiling	Drywall	White	Intact	0.08	Negative		
94	Interior	MILK HOUSE	D	Closet Shelf	Wood	White	Fair	-0.13	Negative		
95	Interior	UPPER LIBRARY	A	Wall	Drywall	White	Intact	-0.03	Negative		
96	Interior	UPPER LIBRARY	B	Wall	Drywall	White	Intact	-0.14	Negative		
97	Interior	UPPER LIBRARY	C	Wall	Drywall	White	Intact	-0.06	Negative		
98	Interior	UPPER LIBRARY	D	Wall	Drywall	White	Intact	-0.11	Negative		
99	Interior	UPPER LIBRARY	---	Ceiling	Wood	Brown	Intact	-0.12	Negative		
100	Interior	UPPER LIBRARY	C	Trim	Wood	Brown	Intact	-0.30	Negative		
101	Interior	UPPER LIBRARY	---	Column	Plaster	White	Intact	0.12	Negative		
102	Interior	LOWER LIBRARY	A	Wall	Drywall	White	Intact	-0.08	Negative		
103	Interior	LOWER LIBRARY	B	Wall	Drywall	White	Intact	-0.14	Negative		
104	Interior	LOWER LIBRARY	C	Wall	Drywall	White	Intact	-0.09	Negative		
105	Interior	LOWER LIBRARY	D	Wall	Drywall	White	Intact	-0.25	Negative		
106	Interior	LOWER LIBRARY	A	Door	Metal	White	Intact	-0.03	Negative		
107	Interior	LOWER LIBRARY	A	Door Frame	Metal	White	Intact	0.21	Negative		
108	Interior	LOWER LIBRARY	---	Ceiling	Drywall	White	Intact	0.06	Negative		
109	Interior	LOWER LIBRARY	---	Stairway Column	Concrete	White	Intact	0.06	Negative		
110	Interior	LOWER LIBRARY	---	Handrail	Wood	Brown	Intact	0.01	Negative		
111	Interior	ROOM 123	A	Wall	Drywall	White	Intact	0.06	Negative		
112	Interior	ROOM 123	B	Wall	Drywall	White	Intact	0.04	Negative		
113	Interior	ROOM 123	C	Wall	Drywall	White	Intact	0.30	Negative		
114	Interior	ROOM 123	D	Wall	Drywall	White	Intact	-0.26	Negative		
115	Interior	ROOM 123	C	Door	Metal	White	Intact	-0.18	Negative		
116	Interior	ROOM 123	C	Door Frame	Metal	White	Intact	-0.10	Negative		
117	Interior	ROOM 123	---	Ceiling	Drywall	White	Intact	-0.04	Negative		
118	Interior	LIBRARY OFFICE	A	Wall	Drywall	Beige	Intact	0.36	Negative		
119	Interior	LIBRARY OFFICE	B	Wall	Drywall	Beige	Intact	0.02	Negative		
120	Interior	LIBRARY OFFICE	C	Wall	Drywall	Beige	Intact	0.11	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
121	Interior	LIBRARY OFFICE	D	Wall	Drywall	Beige	Intact	0.05	Negative		
122	Interior	LIBRARY OFFICE	C	Door	Metal	White	Intact	0.09	Negative		
123	Interior	LIBRARY OFFICE	C	Door Frame	Metal	White	Intact	0.16	Negative		
124	Interior	LIBRARY OFFICE	---	Ceiling	Drywall	White	Intact	0.03	Negative		
125	Interior	LIBRARY OFFICE	A	Upper-Cabinet	Wood	Brown	Intact	0.00	Negative		
126	Interior	LIBRARY OFFICE	A	Lower-Cabinet	Wood	Brown	Intact	-0.16	Negative		
127	Interior	CONFERENCE ROOM	A	Wall	Drywall	White	Intact	0.11	Negative		
128	Interior	CONFERENCE ROOM	B	Wall	Drywall	White	Intact	0.09	Negative		
129	Interior	CONFERENCE ROOM	C	Wall	Drywall	White	Intact	0.22	Negative		
130	Interior	CONFERENCE ROOM	D	Wall	Drywall	White	Intact	0.13	Negative		
131	Interior	CONFERENCE ROOM	A	Door	Wood	White	Intact	0.03	Negative		
132	Interior	CONFERENCE ROOM	A	Door Frame	Metal	White	Intact	0.22	Negative		
133	Interior	CONFERENCE ROOM	---	Ceiling	Drywall	White	Intact	-0.02	Negative		
134	Interior	ADMISSIONS BLDG.	A	Wall	Drywall	White	Intact	0.03	Negative		
135	Interior	ADMISSIONS BLDG.	B	Wall	Drywall	White	Intact	0.08	Negative		
136	Interior	ADMISSIONS BLDG.	C	Wall	Drywall	White	Intact	0.02	Negative		
137	Interior	ADMISSIONS BLDG.	D	Wall	Drywall	White	Intact	0.14	Negative		
138	Interior	ADMISSIONS BLDG.	A	Door	Wood	White	Intact	0.00	Negative		
139	Interior	ADMISSIONS BLDG.	A	Door Frame	Metal	White	Intact	0.01	Negative		
140	Interior	ADMISSIONS BLDG.	---	Ceiling	Drywall	White	Intact	0.08	Negative		
141	Interior	ENGLISH DEPARTMENT	A	Wall	Drywall	Green	Intact	0.08	Negative		
142	Interior	ENGLISH DEPARTMENT	B	Wall	Drywall	Green	Intact	-0.06	Negative		
143	Interior	ENGLISH DEPARTMENT	C	Wall	Drywall	Green	Intact	-0.02	Negative		
144	Interior	ENGLISH DEPARTMENT	D	Wall	Drywall	Green	Intact	0.01	Negative		
145	Interior	ENGLISH DEPARTMENT	A	Door	Wood	Green	Intact	0.08	Negative		
146	Interior	ENGLISH DEPARTMENT	A	Door Frame	Metal	White	Intact	0.16	Negative		
147	Interior	ENGLISH DEPARTMENT	---	Ceiling	Drywall	White	Intact	0.07	Negative		
148	Interior	STORAGE CLOSET	A	Wall	Drywall	White	Intact	-0.01	Negative		
149	Interior	STORAGE CLOSET	B	Wall	Drywall	White	Intact	-0.20	Negative		
150	Interior	STORAGE CLOSET	C	Wall	Concrete	White	Intact	-0.06	Negative		
151	Interior	STORAGE CLOSET	D	Wall	Drywall	White	Intact	-0.04	Negative		
152	Interior	STORAGE CLOSET	D	Door	Wood	Green	Intact	0.06	Negative		
153	Interior	STORAGE CLOSET	D	Door Frame	Metal	White	Intact	0.03	Negative		
154	Interior	STORAGE CLOSET	---	Ceiling	Drywall	White	Intact	0.02	Negative		
155	Interior	WOMAN'S RESTROOM	A	Wall	Ceramic Tile	Yellow	Intact	12.11	Positive		Not a paint
156	Interior	WOMAN'S RESTROOM	B	Wall	Ceramic Tile	Yellow	Intact	13.45	Positive		Not a paint
157	Interior	WOMAN'S RESTROOM	C	Wall	Ceramic Tile	Yellow	Intact	12.22	Positive		Not a paint
158	Interior	WOMAN'S RESTROOM	D	Wall	Ceramic Tile	Yellow	Intact	11.09	Positive		Not a paint
159	Interior	WOMAN'S RESTROOM	C	Door	Wood	White	Intact	0.01	Negative		
160	Interior	WOMAN'S RESTROOM	C	Door Frame	Metal	White	Intact	0.16	Negative		
161	Interior	WOMAN'S RESTROOM	---	Ceiling	Plaster	White	Intact	0.12	Negative		
162	Interior	WOMAN'S RESTROOM	---	Stall	Metal	White	Intact	0.08	Negative		
163	Interior	MEN'S RESTROOM	A	Wall	Ceramic Tile	Yellow	Intact	18.26	Positive		Not a paint

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
164	Interior	MEN'S RESTROOM	B	Wall	Ceramic Tile	Yellow	Intact	12.13	Positive		Not a paint
165	Interior	MEN'S RESTROOM	C	Wall	Ceramic Tile	Yellow	Intact	11.06	Positive		Not a paint
166	Interior	MEN'S RESTROOM	D	Wall	Ceramic Tile	Yellow	Intact	14.31	Positive		Not a paint
167	Interior	MEN'S RESTROOM	C	Door	Wood	White	Intact	0.22	Negative		
168	Interior	MEN'S RESTROOM	C	Door Frame	Metal	White	Intact	0.01	Negative		
169	Interior	MEN'S RESTROOM	---	Ceiling	Plaster	White	Intact	0.08	Negative		
170	Interior	ROOM 101	A	Wall	Drywall	White	Intact	0.11	Negative		
171	Interior	ROOM 101	B	Wall	Drywall	White	Intact	-0.20	Negative		
172	Interior	ROOM 101	C	Wall	Drywall	White	Intact	0.19	Negative		
173	Interior	ROOM 101	D	Wall	Drywall	White	Intact	-0.18	Negative		
174	Interior	ROOM 101	A	Door	Wood	White	Intact	0.07	Negative		
175	Interior	ROOM 101	A	Door Frame	Metal	White	Intact	0.15	Negative		
176	Interior	ROOM 101	A	Window Frame	Wood	White	Intact	0.07	Negative		
177	Interior	ROOM 101	A	Window Sill	Wood	White	Intact	-0.15	Negative		
178	Interior	ROOM 101	C	Window Frame	Metal	White	Intact	0.34	Negative		
179	Interior	ROOM 101	---	Ceiling	Drywall	White	Intact	0.06	Negative		
180	Interior	ROOM 101	B	Upper-Cabinet	Wood	White	Intact	-0.15	Negative		
181	Interior	ROOM 102	A	Wall	Drywall	White	Intact	0.16	Negative		
182	Interior	ROOM 102	B	Wall	Drywall	White	Intact	0.14	Negative		
183	Interior	ROOM 102	C	Wall	Drywall	White	Intact	-0.02	Negative		
184	Interior	ROOM 102	D	Wall	Drywall	White	Intact	-0.15	Negative		
185	Interior	ROOM 102	A	Door	Wood	White	Intact	0.06	Negative		
186	Interior	ROOM 102	A	Door Frame	Metal	White	Intact	0.23	Negative		
187	Interior	ROOM 102	A	Window Frame	Wood	White	Intact	0.13	Negative		
188	Interior	ROOM 102	A	Window Sill	Wood	White	Intact	0.24	Negative		
189	Interior	ROOM 102	---	Ceiling	Drywall	White	Intact	0.03	Negative		
190	Interior	ROOM 102	B	Upper-Cabinet	Wood	White	Intact	0.09	Negative		
191	Interior	ROOM 103	A	Wall	Drywall	White	Intact	0.00	Negative		
192	Interior	ROOM 103	B	Wall	Drywall	White	Intact	-0.04	Negative		
193	Interior	ROOM 103	C	Wall	Drywall	White	Intact	-0.28	Negative		
194	Interior	ROOM 103	D	Wall	Drywall	White	Intact	0.03	Negative		
195	Interior	ROOM 103	A	Door	Wood	White	Intact	0.04	Negative		
196	Interior	ROOM 103	A	Door Frame	Metal	White	Intact	0.18	Negative		
197	Interior	ROOM 103	A	Window Frame	Wood	White	Intact	-0.07	Negative		
198	Interior	ROOM 103	A	Window Sill	Wood	White	Intact	0.09	Negative		
199	Interior	ROOM 103	---	Ceiling	Drywall	White	Intact	0.08	Negative		
200	Interior	ROOM 103	B	Upper-Cabinet	Wood	White	Intact	0.10	Negative		
201	Interior	ROOM 104	A	Wall	Drywall	White	Intact	-0.18	Negative		
202	Interior	ROOM 104	B	Wall	Drywall	White	Intact	0.06	Negative		
203	Interior	ROOM 104	C	Wall	Drywall	White	Intact	0.23	Negative		
204	Interior	ROOM 104	D	Wall	Drywall	White	Intact	0.04	Negative		
205	Interior	ROOM 104	A	Door	Wood	White	Intact	0.08	Negative		
206	Interior	ROOM 104	A	Door Frame	Metal	White	Intact	0.26	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/cm²)	Results	Quantities For Entire Area	Comments
207	Interior	ROOM 104	A	Window Frame	Wood	White	Intact	0.01	Negative		
208	Interior	ROOM 104	A	Window Sill	Wood	White	Intact	0.12	Negative		
209	Interior	ROOM 104	---	Ceiling	Drywall	White	Intact	0.08	Negative		
210	Interior	ROOM 104	B	Upper-Cabinet	Wood	White	Intact	0.30	Negative		
211	Interior	ROOM 105	A	Wall	Drywall	White	Intact	-0.22	Negative		
212	Interior	ROOM 105	B	Wall	Drywall	White	Intact	-0.42	Negative		
213	Interior	ROOM 105	C	Wall	Drywall	White	Intact	0.23	Negative		
214	Interior	ROOM 105	D	Wall	Drywall	White	Intact	0.13	Negative		
215	Interior	ROOM 105	A	Door	Wood	White	Intact	0.06	Negative		
216	Interior	ROOM 105	A	Door Frame	Metal	White	Intact	0.20	Negative		
217	Interior	ROOM 105	A	Window Frame	Wood	White	Intact	0.06	Negative		
218	Interior	ROOM 105	A	Window Sill	Wood	White	Intact	0.09	Negative		
219	Interior	ROOM 105	---	Ceiling	Drywall	White	Intact	0.20	Negative		
220	Interior	ROOM 106	A	Wall	Drywall	White	Intact	0.10	Negative		
221	Interior	ROOM 106	B	Wall	Drywall	White	Intact	0.26	Negative		
222	Interior	ROOM 106	C	Wall	Drywall	White	Intact	0.09	Negative		
223	Interior	ROOM 106	D	Wall	Drywall	White	Intact	0.07	Negative		
224	Interior	ROOM 106	A	Door	Wood	Red	Intact	0.03	Negative		
225	Interior	ROOM 106	A	Door Frame	Metal	Red	Intact	0.43	Negative		
226	Interior	ROOM 106	A	Window Frame	Wood	White	Intact	-0.07	Negative		
227	Interior	ROOM 106	A	Window Sill	Wood	White	Intact	-0.02	Negative		
228	Interior	ROOM 106	---	Ceiling	Drywall	White	Intact	0.08	Negative		
229	Interior	ROOM 106 A	A	Wall	Drywall	White	Intact	-0.31	Negative		
230	Interior	ROOM 106 A	B	Wall	Drywall	White	Intact	0.00	Negative		
231	Interior	ROOM 106 A	C	Wall	Drywall	White	Intact	0.09	Negative		
232	Interior	ROOM 106 A	D	Wall	Drywall	White	Intact	-0.32	Negative		
233	Interior	ROOM 106 A	C	Door	Wood	White	Intact	0.22	Negative		
234	Interior	ROOM 106 A	C	Door Frame	Metal	White	Intact	0.26	Negative		
235	Interior	ROOM 106 A	---	Ceiling	Drywall	White	Intact	-0.27	Negative		
236	Interior	ROOM 106 A	B	Upper-Cabinet	Wood	White	Intact	-0.13	Negative		
237	Interior	ROOM 107	A	Wall	Drywall	White	Intact	0.11	Negative		
238	Interior	ROOM 107	B	Wall	Drywall	White	Intact	-0.62	Negative		
239	Interior	ROOM 107	C	Wall	Drywall	White	Intact	0.31	Negative		
240	Interior	ROOM 107	D	Wall	Drywall	White	Intact	0.20	Negative		
241	Interior	ROOM 107	C	Door	Wood	White	Intact	0.04	Negative		
242	Interior	ROOM 107	C	Door Frame	Metal	White	Intact	0.18	Negative		
243	Interior	ROOM 107	C	Window Frame	Wood	White	Intact	0.31	Negative		
244	Interior	ROOM 107	C	Window Sill	Wood	White	Intact	0.26	Negative		
245	Interior	ROOM 107	---	Ceiling	Drywall	White	Intact	0.03	Negative		
246	Interior	ROOM 107	B	Upper-Cabinet	Wood	White	Intact	0.01	Negative		
247	Interior	ROOM 108	A	Wall	Drywall	White	Intact	0.02	Negative		
248	Interior	ROOM 108	B	Wall	Drywall	White	Intact	0.16	Negative		
249	Interior	ROOM 108	C	Wall	Drywall	White	Intact	0.08	Negative		

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Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
250	Interior	ROOM 108	D	Wall	Drywall	White	Intact	0.19	Negative		
251	Interior	ROOM 108	C	Door	Wood	White	Intact	0.08	Negative		
252	Interior	ROOM 108	C	Door Frame	Metal	White	Intact	-0.13	Negative		
253	Interior	ROOM 108	C	Window Frame	Wood	White	Intact	0.03	Negative		
254	Interior	ROOM 108	C	Window Sill	Wood	White	Intact	0.01	Negative		
255	Interior	ROOM 108	---	Ceiling	Drywall	White	Intact	0.02	Negative		
256	Interior	MATHEMATICS OFFICE	A	Wall	Drywall	White	Intact	0.22	Negative		
257	Interior	MATHEMATICS OFFICE	B	Wall	Drywall	White	Intact	0.03	Negative		
258	Interior	MATHEMATICS OFFICE	C	Wall	Drywall	White	Intact	0.27	Negative		
259	Interior	MATHEMATICS OFFICE	D	Wall	Drywall	White	Intact	0.01	Negative		
260	Interior	MATHEMATICS OFFICE	C	Door	Wood	Red	Intact	0.08	Negative		
261	Interior	MATHEMATICS OFFICE	C	Door Frame	Metal	Red	Intact	-0.22	Negative		
262	Interior	MATHEMATICS OFFICE	C	Window Frame	Wood	White	Intact	-0.30	Negative		
263	Interior	MATHEMATICS OFFICE	C	Window Sill	Wood	White	Intact	-0.18	Negative		
264	Interior	MATHEMATICS OFFICE	---	Ceiling	Drywall	White	Intact	-0.01	Negative		
265	Interior	DEANS OFFICES	A	Wall	Drywall	White	Intact	0.03	Negative		
266	Interior	DEANS OFFICES	B	Wall	Drywall	White	Intact	0.14	Negative		
267	Interior	DEANS OFFICES	C	Wall	Drywall	White	Intact	0.09	Negative		
268	Interior	DEANS OFFICES	D	Wall	Drywall	White	Intact	0.26	Negative		
269	Interior	DEANS OFFICES	C	Door	Wood	White	Intact	-0.22	Negative		
270	Interior	DEANS OFFICES	C	Door Frame	Metal	White	Intact	-0.11	Negative		
271	Interior	DEANS OFFICES	C	Window Frame	Wood	White	Intact	-0.06	Negative		
272	Interior	DEANS OFFICES	C	Window Sill	Wood	White	Intact	-0.12	Negative		
273	Interior	DEANS OFFICES	---	Ceiling	Drywall	White	Intact	0.08	Negative		
274	Interior	ROOM 109	A	Wall	Drywall	White	Intact	0.06	Negative		
275	Interior	ROOM 109	B	Wall	Drywall	White	Intact	-0.31	Negative		
276	Interior	ROOM 109	C	Wall	Drywall	White	Intact	0.20	Negative		
277	Interior	ROOM 109	D	Wall	Drywall	White	Intact	0.08	Negative		
278	Interior	ROOM 109	B	Door	Wood	White	Intact	-0.23	Negative		
279	Interior	ROOM 109	B	Door Frame	Metal	White	Intact	-0.15	Negative		
280	Interior	ROOM 109	---	Ceiling	Drywall	White	Intact	-0.22	Negative		
281	Interior	FACULTY WORK ROOM	A	Wall	Drywall	White	Intact	-0.32	Negative		
282	Interior	FACULTY WORK ROOM	B	Wall	Drywall	White	Intact	0.16	Negative		
283	Interior	FACULTY WORK ROOM	C	Wall	Drywall	White	Intact	-0.40	Negative		
284	Interior	FACULTY WORK ROOM	D	Wall	Drywall	White	Intact	0.12	Negative		
285	Interior	FACULTY WORK ROOM	B	Door	Wood	White	Intact	-0.18	Negative		
286	Interior	FACULTY WORK ROOM	B	Door Frame	Metal	White	Intact	-0.24	Negative		
287	Interior	FACULTY WORK ROOM	---	Ceiling	Drywall	White	Intact	0.03	Negative		
288	Interior	FACULTY WORK ROOM	D	Upper-Cabinet	Wood	Tan	Intact	0.32	Negative		
289	Interior	JANITOR CLOSET	A	Wall	Plaster	Tan	Intact	0.07	Negative		
290	Interior	JANITOR CLOSET	B	Wall	Plaster	Tan	Intact	0.32	Negative		
291	Interior	JANITOR CLOSET	C	Wall	Plaster	Tan	Intact	0.18	Negative		
292	Interior	JANITOR CLOSET	D	Wall	Plaster	Tan	Intact	0.20	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
293	Interior	JANITOR CLOSET	B	Door	Wood	Orange	Fair	0.37	Negative		
294	Interior	JANITOR CLOSET	B	Door Frame	Metal	Orange	Fair	0.14	Negative		
295	Interior	JANITOR CLOSET	---	Ceiling	Plaster	Tan	Intact	0.05	Negative		
296	Interior	JANITOR CLOSET	A	Shelves	Wood	Tan	Fair	0.01	Negative		
297	Interior	ROOM 110	A	Wall	Drywall	White	Intact	0.02	Negative		
298	Interior	ROOM 110	B	Wall	Drywall	White	Intact	0.07	Negative		
299	Interior	ROOM 110	C	Wall	Drywall	White	Intact	-0.30	Negative		
300	Interior	ROOM 110	D	Wall	Drywall	White	Intact	-0.28	Negative		
301	Interior	ROOM 110	A	Door	Wood	White	Intact	0.16	Negative		
302	Interior	ROOM 110	A	Door Frame	Metal	White	Intact	0.04	Negative		
303	Interior	ROOM 110	A	Window Frame	Wood	White	Intact	-0.13	Negative		
304	Interior	ROOM 110	A	Window Sill	Wood	White	Intact	-0.27	Negative		
305	Interior	ROOM 110	---	Ceiling	Drywall	White	Intact	-0.10	Negative		
306	Interior	ROOM 110	B	Upper-Cabinet	Wood	White	Intact	0.13	Negative		
307	Interior	ROOM 111	A	Wall	Drywall	White	Intact	0.11	Negative		
308	Interior	ROOM 111	B	Wall	Drywall	White	Intact	0.10	Negative		
309	Interior	ROOM 111	C	Wall	Drywall	White	Intact	-0.04	Negative		
310	Interior	ROOM 111	D	Wall	Drywall	White	Intact	-0.13	Negative		
311	Interior	ROOM 111	A	Door	Wood	White	Intact	0.09	Negative		
312	Interior	ROOM 111	A	Door Frame	Metal	White	Intact	0.14	Negative		
313	Interior	ROOM 111	A	Window Frame	Wood	White	Intact	-0.10	Negative		
314	Interior	ROOM 111	A	Window Sill	Wood	White	Intact	-0.01	Negative		
315	Interior	ROOM 111	---	Ceiling	Drywall	White	Intact	0.00	Negative		
316	Interior	ROOM 111	D	Upper-Cabinet	Wood	White	Intact	-0.06	Negative		
317	Interior	JANITOR CLOSET	A	Wall	Plaster	Tan	Intact	0.04	Negative		
318	Interior	JANITOR CLOSET	B	Wall	Plaster	Tan	Intact	0.39	Negative		
319	Interior	JANITOR CLOSET	C	Wall	Plaster	Tan	Intact	0.28	Negative		
320	Interior	JANITOR CLOSET	D	Wall	Plaster	Tan	Intact	0.16	Negative		
321	Interior	JANITOR CLOSET	A	Door	Wood	Orange	Fair	0.20	Negative		
322	Interior	JANITOR CLOSET	A	Door Frame	Metal	Orange	Fair	0.06	Negative		
323	Interior	JANITOR CLOSET	---	Ceiling	Plaster	Tan	Intact	0.08	Negative		
324	Interior	ROOM 112	A	Wall	Drywall	White	Intact	0.20	Negative		
325	Interior	ROOM 112	B	Wall	Drywall	White	Intact	0.06	Negative		
326	Interior	ROOM 112	C	Wall	Drywall	White	Intact	0.30	Negative		
327	Interior	ROOM 112	D	Wall	Drywall	White	Intact	0.14	Negative		
328	Interior	ROOM 112	A	Door	Wood	White	Intact	0.26	Negative		
329	Interior	ROOM 112	A	Door Frame	Metal	White	Intact	0.03	Negative		
330	Interior	ROOM 112	A	Window Frame	Wood	White	Intact	0.30	Negative		
331	Interior	ROOM 112	A	Window Sill	Wood	White	Intact	-0.26	Negative		
332	Interior	ROOM 112	---	Ceiling	Drywall	White	Intact	0.01	Negative		
333	Interior	ROOM 113-114	A	Wall	Drywall	White	Intact	0.27	Negative		
334	Interior	ROOM 113-114	B	Wall	Drywall	White	Intact	0.14	Negative		
335	Interior	ROOM 113-114	C	Wall	Drywall	White	Intact	0.38	Negative		

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Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/cm²)	Results	Quantities For Entire Area	Comments
336	Interior	ROOM 113-114	D	Wall	Drywall	White	Intact	0.20	Negative		
337	Interior	ROOM 113-114	D	Door	Wood	White	Intact	-0.03	Negative		
338	Interior	ROOM 113-114	D	Door Frame	Metal	White	Intact	-0.19	Negative		
339	Interior	ROOM 113-114	D	Window Frame	Wood	White	Intact	0.26	Negative		
340	Interior	ROOM 113-114	D	Window Sill	Wood	White	Intact	0.32	Negative		
341	Interior	ROOM 113-114	---	Ceiling	Drywall	White	Intact	0.08	Negative		
342	Interior	MEN'S RESTROOM	A	Wall	Plaster	White	Intact	0.16	Negative		
343	Interior	MEN'S RESTROOM	B	Wall	Plaster	White	Intact	0.03	Negative		
344	Interior	MEN'S RESTROOM	C	Wall	Plaster	White	Intact	0.21	Negative		
345	Interior	MEN'S RESTROOM	D	Wall	Plaster	White	Intact	0.13	Negative		
346	Interior	MEN'S RESTROOM	A	Door	Wood	White	Intact	0.06	Negative		
347	Interior	MEN'S RESTROOM	A	Door Frame	Metal	White	Intact	1.32	Positive	1 Ea.	
348	Interior	MEN'S RESTROOM	---	Ceiling	Plaster	White	Intact	0.03	Negative		
349	Interior	MEN'S RESTROOM	---	Floor	Ceramic Tile	Brown	Intact	-0.03	Negative		
350	Interior	MEN'S RESTROOM	D	Urinal	Ceramic Tile	White	Intact	0.01	Negative		
351	Interior	MEN'S RESTROOM	---	Stall	Metal	White	Intact	0.16	Negative		
352	Interior	MEN'S RESTROOM	---	Tile	Ceramic Tile	Brown	Intact	14.12	Positive	300 SF	Not a paint
353	Interior	MEN'S RESTROOM	---	Sink	Ceramic Tile	White	Intact	-0.17	Negative		
354	Interior	WOMAN'S RESTROOM	A	Wall	Plaster	White	Intact	0.02	Negative		
355	Interior	WOMAN'S RESTROOM	B	Wall	Plaster	White	Intact	0.04	Negative		
356	Interior	WOMAN'S RESTROOM	C	Wall	Plaster	White	Intact	0.18	Negative		
357	Interior	WOMAN'S RESTROOM	D	Wall	Plaster	White	Intact	0.09	Negative		
358	Interior	WOMAN'S RESTROOM	C	Door	Wood	White	Intact	0.28	Negative		
359	Interior	WOMAN'S RESTROOM	C	Door Frame	Metal	White	Intact	2.01	Positive	1 Ea.	
360	Interior	WOMAN'S RESTROOM	---	Ceiling	Plaster	White	Intact	0.06	Negative		
361	Interior	WOMAN'S RESTROOM	---	Stall	Metal	White	Intact	0.04	Negative		
362	Interior	WOMAN'S RESTROOM	---	Floor	Ceramic Tile	Brown	Intact	0.28	Negative		
363	Interior	WOMAN'S RESTROOM	---	Tile	Ceramic Tile	Brown	Intact	10.70	Positive	300 SF	Not a paint
364	Interior	WOMAN'S RESTROOM	A	Sink	Ceramic Tile	White	Intact	0.06	Negative		
365	Interior	PRINCIPLE'S OFFICE	A	Wall	Drywall	White	Intact	0.07	Negative		
366	Interior	PRINCIPLE'S OFFICE	B	Wall	Drywall	White	Intact	0.13	Negative		
367	Interior	PRINCIPLE'S OFFICE	C	Wall	Drywall	White	Intact	0.24	Negative		
368	Interior	PRINCIPLE'S OFFICE	D	Wall	Drywall	White	Intact	0.05	Negative		
369	Interior	PRINCIPLE'S OFFICE	B	Wall	Wood	Brown	Intact	0.12	Negative		
370	Interior	PRINCIPLE'S OFFICE	A	Crown Molding	Wood	Brown	Intact	0.16	Negative		
371	Interior	PRINCIPLE'S OFFICE	B	Door	Wood	Brown	Intact	0.03	Negative		
372	Interior	PRINCIPLE'S OFFICE	B	Door Frame	Wood	Brown	Intact	0.26	Negative		
373	Interior	PRINCIPLE'S OFFICE	D	Window Frame	Wood	Brown	Intact	0.16	Negative		
374	Interior	PRINCIPLE'S OFFICE	D	Window Sill	Wood	Brown	Intact	0.07	Negative		
375	Interior	PRINCIPLE'S OFFICE	---	Ceiling	Drywall	White	Intact	0.05	Negative		
376	Interior	PRINCIPLE'S OFFICE	C	Upper-Cabinet	Wood	Brown	Intact	0.03	Negative		
377	Interior	ASSISTANT PRINCIPLE	A	Wall	Drywall	White	Intact	0.07	Negative		
378	Interior	ASSISTANT PRINCIPLE	B	Wall	Drywall	White	Intact	0.13	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
379	Interior	ASSISTANT PRINCIPLE	C	Wall	Drywall	White	Intact	0.25	Negative		
380	Interior	ASSISTANT PRINCIPLE	D	Wall	Drywall	White	Intact	0.18	Negative		
381	Interior	ASSISTANT PRINCIPLE	B	Wall	Wood	Brown	Intact	0.03	Negative		
382	Interior	ASSISTANT PRINCIPLE	C	Crown Molding	Wood	Brown	Intact	-0.13	Negative		
383	Interior	ASSISTANT PRINCIPLE	B	Door	Wood	Brown	Intact	0.02	Negative		
384	Interior	ASSISTANT PRINCIPLE	B	Door Frame	Wood	Brown	Intact	-0.15	Negative		
385	Interior	ASSISTANT PRINCIPLE	D	Window Frame	Wood	Brown	Intact	-0.30	Negative		
386	Interior	ASSISTANT PRINCIPLE	D	Window Sill	Wood	Brown	Intact	-0.06	Negative		
387	Interior	ASSISTANT PRINCIPLE	---	Ceiling	Drywall	White	Intact	0.04	Negative		
388	Interior	ASSISTANT PRINCIPLE	A	Upper-Cabinet	Wood	Brown	Intact	0.17	Negative		
389	Interior	MID. SCHOOL PRINCIPLE	A	Wall	Drywall	White	Intact	0.04	Negative		
390	Interior	MID. SCHOOL PRINCIPLE	B	Wall	Drywall	White	Intact	-0.37	Negative		
391	Interior	MID. SCHOOL PRINCIPLE	C	Wall	Drywall	White	Intact	0.18	Negative		
392	Interior	MID. SCHOOL PRINCIPLE	D	Wall	Drywall	White	Intact	0.09	Negative		
393	Interior	MID. SCHOOL PRINCIPLE	D	Door	Wood	Brown	Intact	0.01	Negative		
394	Interior	MID. SCHOOL PRINCIPLE	D	Door Frame	Metal	White	Intact	-0.32	Negative		
395	Interior	MID. SCHOOL PRINCIPLE	---	Ceiling	Drywall	White	Intact	0.05	Negative		
396	Interior	MID. SCHOOL PRINCIPLE	A	Door	Wood	White	Intact	-0.12	Negative		
397	Interior	ADMINISTRATIVE OFFICE	A	Wall	Drywall	Tan	Intact	0.01	Negative		
398	Interior	ADMINISTRATIVE OFFICE	B	Wall	Drywall	Tan	Intact	0.03	Negative		
399	Interior	ADMINISTRATIVE OFFICE	C	Wall	Drywall	Tan	Intact	-0.22	Negative		
400	Interior	ADMINISTRATIVE OFFICE	D	Wall	Drywall	Tan	Intact	0.27	Negative		
401	Interior	ADMINISTRATIVE OFFICE	C	Door	Metal	Black	Intact	-0.06	Negative		
402	Interior	ADMINISTRATIVE OFFICE	C	Door Frame	Metal	Black	Intact	-0.38	Negative		
403	Interior	ADMINISTRATIVE OFFICE	C	Window Sill	Wood	Tan	Intact	-0.13	Negative		
404	Interior	ADMINISTRATIVE OFFICE	---	Ceiling	Drywall	White	Intact	0.04	Negative		
405	Interior	COLLEGE COUNSELOR	A	Wall	Drywall	White	Intact	0.07	Negative		
406	Interior	COLLEGE COUNSELOR	B	Wall	Drywall	White	Intact	-0.31	Negative		
407	Interior	COLLEGE COUNSELOR	C	Wall	Drywall	White	Intact	-0.26	Negative		
408	Interior	COLLEGE COUNSELOR	D	Wall	Drywall	White	Intact	0.04	Negative		
409	Interior	COLLEGE COUNSELOR	B	Door	Wood	Brown	Intact	0.16	Negative		
410	Interior	COLLEGE COUNSELOR	B	Door Frame	Metal	White	Intact	0.03	Negative		
411	Interior	COLLEGE COUNSELOR	C	Window Frame	Wood	White	Intact	0.13	Negative		
412	Interior	COLLEGE COUNSELOR	C	Window Sill	Wood	White	Intact	0.09	Negative		
413	Interior	COLLEGE COUNSELOR	---	Ceiling	Drywall	White	Intact	0.01	Negative		
414	Interior	ADMINISTRATIVE SECRETARY	A	Wall	Drywall	Beige	Intact	0.01	Negative		
415	Interior	ADMINISTRATIVE SECRETARY	B	Wall	Drywall	Beige	Intact	0.03	Negative		
416	Interior	ADMINISTRATIVE SECRETARY	C	Wall	Drywall	Beige	Intact	0.14	Negative		
417	Interior	ADMINISTRATIVE SECRETARY	D	Wall	Drywall	Beige	Intact	0.32	Negative		
418	Interior	ADMINISTRATIVE SECRETARY	A	Door	Wood	Brown	Intact	0.14	Negative		
419	Interior	ADMINISTRATIVE SECRETARY	A	Door Frame	Metal	White	Intact	0.05	Negative		
420	Interior	ADMINISTRATIVE SECRETARY	D	Window Frame	Wood	White	Intact	0.04	Negative		
421	Interior	ADMINISTRATIVE SECRETARY	D	Window Sill	Wood	White	Intact	0.11	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/cm²)	Results	Quantities For Entire Area	Comments
422	Interior	ADMINISTRATIVE SECRETARY	---	Ceiling	Drywall	White	Intact	0.07	Negative		
423	Interior	BREAK ROOM	A	Wall	Drywall	Beige	Intact	0.03	Negative		
424	Interior	BREAK ROOM	B	Wall	Drywall	Beige	Intact	0.26	Negative		
425	Interior	BREAK ROOM	C	Wall	Drywall	Beige	Intact	0.17	Negative		
426	Interior	BREAK ROOM	D	Wall	Drywall	Beige	Intact	0.30	Negative		
427	Interior	BREAK ROOM	C	Door	Wood	Brown	Intact	0.17	Negative		
428	Interior	BREAK ROOM	C	Door Frame	Metal	White	Intact	0.39	Negative		
429	Interior	BREAK ROOM	A	Window Frame	Wood	White	Intact	0.70	Negative		
430	Interior	BREAK ROOM	A	Window Sill	Wood	White	Intact	0.08	Negative		
431	Interior	BREAK ROOM	---	Ceiling	Drywall	White	Intact	0.01	Negative		
432	Interior	HEALTH OFFICE	A	Wall	Drywall	Tan	Intact	0.07	Negative		
433	Interior	HEALTH OFFICE	B	Wall	Drywall	Tan	Intact	-0.09	Negative		
434	Interior	HEALTH OFFICE	C	Wall	Drywall	Tan	Intact	-0.22	Negative		
435	Interior	HEALTH OFFICE	D	Wall	Drywall	Tan	Intact	-0.02	Negative		
436	Interior	HEALTH OFFICE	A	Door	Wood	Brown	Intact	-0.10	Negative		
437	Interior	HEALTH OFFICE	A	Door Frame	Wood	Brown	Intact	0.15	Negative		
438	Interior	HEALTH OFFICE	---	Ceiling	Drywall	White	Intact	0.03	Negative		
439	Interior	INFIRMARY 1	A	Wall	Drywall	Tan	Intact	0.03	Negative		
440	Interior	INFIRMARY 1	B	Wall	Drywall	Tan	Intact	0.07	Negative		
441	Interior	INFIRMARY 1	C	Wall	Drywall	Tan	Intact	0.36	Negative		
442	Interior	INFIRMARY 1	D	Wall	Drywall	Tan	Intact	0.04	Negative		
443	Interior	INFIRMARY 1	B	Door	Wood	White	Intact	0.06	Negative		
444	Interior	INFIRMARY 1	B	Door Frame	Wood	White	Intact	0.03	Negative		
445	Interior	INFIRMARY 1	---	Ceiling	Drywall	White	Intact	0.08	Negative		
446	Interior	RESTROOM	A	Wall	Drywall	White	Intact	0.07	Negative		
447	Interior	RESTROOM	B	Wall	Drywall	White	Intact	0.31	Negative		
448	Interior	RESTROOM	C	Wall	Drywall	White	Intact	0.14	Negative		
449	Interior	RESTROOM	D	Wall	Drywall	White	Intact	0.05	Negative		
450	Interior	RESTROOM	A	Door	Wood	White	Intact	0.19	Negative		
451	Interior	RESTROOM	A	Door Frame	Wood	White	Intact	0.26	Negative		
452	Interior	RESTROOM	---	Ceiling	Drywall	White	Intact	0.02	Negative		
453	Interior	RESTROOM	---	Tile	Ceramic Tile	Beige	Intact	11.99	Positive	150 SF	Not a paint
454	Interior	RESTROOM	---	Floor	Ceramic Tile	Yellow	Intact	0.26	Negative		
455	Interior	INFIRMARY 2	A	Wall	Drywall	Pink	Intact	0.08	Negative		
456	Interior	INFIRMARY 2	B	Wall	Drywall	Pink	Intact	0.37	Negative		
457	Interior	INFIRMARY 2	C	Wall	Drywall	Pink	Intact	0.14	Negative		
458	Interior	INFIRMARY 2	D	Wall	Drywall	Pink	Intact	0.05	Negative		
459	Interior	INFIRMARY 2	A	Door	Wood	White	Intact	-0.20	Negative		
460	Interior	INFIRMARY 2	A	Door Frame	Wood	White	Intact	-0.36	Negative		
461	Interior	INFIRMARY 2	---	Ceiling	Drywall	White	Intact	0.08	Negative		
462	Interior	INFIRMARY 2	B	Upper-Cabinet	Wood	Brown	Intact	0.04	Negative		
463	Interior	INFIRMARY 2	B	Lower-Cabinet	Wood	Brown	Intact	0.03	Negative		
464	Interior	WOMAN'S RESTROOM	A	Wall	Drywall	Yellow	Intact	0.11	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
465	Interior	WOMAN'S RESTROOM	B	Wall	Drywall	Yellow	Intact	0.07	Negative		
466	Interior	WOMAN'S RESTROOM	C	Wall	Drywall	Yellow	Intact	0.14	Negative		
467	Interior	WOMAN'S RESTROOM	D	Wall	Drywall	Yellow	Intact	0.09	Negative		
468	Interior	WOMAN'S RESTROOM	A	Baseboard	Ceramic Tile	Tan	Intact	13.37	Positive	50 LF	Not a paint
469	Interior	WOMAN'S RESTROOM	C	Door	Wood	White	Intact	0.06	Negative		
470	Interior	WOMAN'S RESTROOM	C	Door Frame	Wood	White	Intact	0.11	Negative		
471	Interior	WOMAN'S RESTROOM	---	Ceiling	Drywall	Yellow	Intact	0.07	Negative		
472	Interior	WOMAN'S RESTROOM	---	Stall	Metal	White	Intact	0.31	Negative		
473	Interior	JANITOR CLOSET	A	Wall	Plaster	Green	Intact	0.24	Negative		
474	Interior	JANITOR CLOSET	B	Wall	Plaster	Green	Intact	0.13	Negative		
475	Interior	JANITOR CLOSET	C	Wall	Plaster	Green	Intact	0.20	Negative		
476	Interior	JANITOR CLOSET	D	Wall	Plaster	Green	Intact	0.07	Negative		
477	Interior	JANITOR CLOSET	B	Door	Wood	Brown	Intact	0.06	Negative		
478	Interior	JANITOR CLOSET	B	Door Frame	Wood	Brown	Intact	0.03	Negative		
479	Interior	JANITOR CLOSET	---	Ceiling	Plaster	Green	Intact	0.02	Negative		
480	Interior	MEN'S RESTROOM	A	Wall	Plaster	White	Intact	0.06	Negative		
481	Interior	MEN'S RESTROOM	B	Wall	Plaster	White	Intact	0.03	Negative		
482	Interior	MEN'S RESTROOM	C	Wall	Plaster	White	Intact	0.14	Negative		
483	Interior	MEN'S RESTROOM	D	Wall	Plaster	White	Intact	0.26	Negative		
484	Interior	MEN'S RESTROOM	D	Door	Wood	Brown	Intact	0.30	Negative		
485	Interior	MEN'S RESTROOM	D	Door Frame	Wood	Brown	Intact	0.06	Negative		
486	Interior	MEN'S RESTROOM	---	Ceiling	Drywall	White	Intact	-0.38	Negative		
487	Interior	MEN'S RESTROOM	---	Tile	Ceramic Tile	Brown	Intact	13.50	Positive	70 SF	Not a paint
488	Interior	MEN'S RESTROOM	---	Stall	Metal	White	Intact	0.02	Negative		
489	Interior	ADMINISTRATIVE LOBBY	A	Wall	Drywall	Tan	Intact	0.17	Negative		
490	Interior	ADMINISTRATIVE LOBBY	B	Wall	Drywall	Tan	Intact	0.14	Negative		
491	Interior	ADMINISTRATIVE LOBBY	C	Wall	Drywall	Tan	Intact	0.00	Negative		
492	Interior	ADMINISTRATIVE LOBBY	D	Wall	Drywall	Tan	Intact	-0.04	Negative		
493	Interior	ADMINISTRATIVE LOBBY	C	Door	Metal	Black	Intact	-0.06	Negative		
494	Interior	ADMINISTRATIVE LOBBY	C	Door Frame	Metal	Black	Intact	-0.13	Negative		
495	Interior	ADMINISTRATIVE LOBBY	A	Window Frame	Metal	Black	Intact	-0.01	Negative		
496	Interior	ADMINISTRATIVE LOBBY	A	Window Sill	Metal	Black	Intact	-0.03	Negative		
497	Interior	ADMINISTRATIVE LOBBY	---	Ceiling	Drywall	White	Intact	-0.36	Negative		
498	Interior	ADMINISTRATIVE LOBBY	---	Rail	Wood	Brown	Intact	-0.30	Negative		
499	Interior	ADMINISTRATIVE LOBBY	---	Stairway Door	Metal	Black	Intact	-0.10	Negative		
500	Interior	DEVELOPMENT	A	Wall	Drywall	White	Intact	0.20	Negative		
501	Interior	DEVELOPMENT	B	Wall	Drywall	White	Intact	0.04	Negative		
502	Interior	DEVELOPMENT	C	Wall	Drywall	White	Intact	0.15	Negative		
503	Interior	DEVELOPMENT	D	Wall	Drywall	White	Intact	0.38	Negative		
504	Interior	DEVELOPMENT	A	Door Frame	Metal	White	Intact	0.04	Negative		
505	Interior	DEVELOPMENT	---	Ceiling	Drywall	White	Intact	0.00	Negative		
506	Interior	ADMISSIONS OFFICE	A	Wall	Drywall	Tan	Intact	-0.33	Negative		
507	Interior	ADMISSIONS OFFICE	B	Wall	Drywall	Tan	Intact	0.07	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/cm²)	Results	Quantities For Entire Area	Comments
508	Interior	ADMISSIONS OFFICE	C	Wall	Drywall	Tan	Intact	0.11	Negative		
509	Interior	ADMISSIONS OFFICE	D	Wall	Drywall	Tan	Intact	0.22	Negative		
510	Interior	ADMISSIONS OFFICE	C	Door	Wood	Brown	Intact	0.06	Negative		
511	Interior	ADMISSIONS OFFICE	C	Door Frame	Metal	White	Intact	0.03	Negative		
512	Interior	ADMISSIONS OFFICE	A	Window Frame	Wood	White	Intact	0.01	Negative		
513	Interior	ADMISSIONS OFFICE	A	Window Sill	Wood	White	Intact	0.05	Negative		
514	Interior	ADMISSIONS OFFICE	---	Ceiling	Drywall	White	Intact	-0.10	Negative		
515	Interior	ADMISSIONS/DEVELOPMENT	A	Wall	Drywall	White	Intact	0.06	Negative		
516	Interior	ADMISSIONS/DEVELOPMENT	B	Wall	Drywall	White	Intact	0.03	Negative		
517	Interior	ADMISSIONS/DEVELOPMENT	C	Wall	Drywall	White	Intact	-0.41	Negative		
518	Interior	ADMISSIONS/DEVELOPMENT	D	Wall	Drywall	White	Intact	-0.37	Negative		
519	Interior	ADMISSIONS/DEVELOPMENT	A	Door	Wood	Brown	Intact	-0.18	Negative		
520	Interior	ADMISSIONS/DEVELOPMENT	A	Door Frame	Metal	White	Intact	-0.20	Negative		
521	Interior	ADMISSIONS/DEVELOPMENT	C	Window Frame	Wood	White	Intact	-0.35	Negative		
522	Interior	ADMISSIONS/DEVELOPMENT	C	Window Sill	Wood	White	Intact	-0.26	Negative		
523	Interior	ADMISSIONS/DEVELOPMENT	---	Ceiling	Drywall	White	Intact	0.08	Negative		
524	Interior	ASSISTANT HEAD OF SCHOOL	A	Wall	Drywall	Tan	Intact	0.09	Negative		
525	Interior	ASSISTANT HEAD OF SCHOOL	B	Wall	Drywall	Tan	Intact	0.10	Negative		
526	Interior	ASSISTANT HEAD OF SCHOOL	C	Wall	Drywall	Tan	Intact	0.04	Negative		
527	Interior	ASSISTANT HEAD OF SCHOOL	D	Wall	Drywall	Tan	Intact	-0.21	Negative		
528	Interior	ASSISTANT HEAD OF SCHOOL	A	Window Frame	Wood	White	Intact	0.03	Negative		
529	Interior	ASSISTANT HEAD OF SCHOOL	A	Window Sill	Wood	White	Intact	0.27	Negative		
530	Interior	HEAD OF SCHOOL	A	Wall	Drywall	Tan	Intact	0.20	Negative		
531	Interior	HEAD OF SCHOOL	B	Wall	Drywall	Tan	Intact	0.03	Negative		
532	Interior	HEAD OF SCHOOL	C	Wall	Drywall	Tan	Intact	0.14	Negative		
533	Interior	HEAD OF SCHOOL	D	Wall	Drywall	Tan	Intact	0.05	Negative		
534	Interior	HEAD OF SCHOOL	D	Door	Wood	Brown	Intact	0.06	Negative		
535	Interior	HEAD OF SCHOOL	D	Door Frame	Metal	White	Intact	0.01	Negative		
536	Interior	HEAD OF SCHOOL	B	Window Frame	Wood	White	Intact	0.08	Negative		
537	Interior	HEAD OF SCHOOL	B	Window Sill	Wood	White	Intact	0.01	Negative		
538	Interior	HEAD OF SCHOOL	---	Ceiling	Drywall	White	Intact	0.07	Negative		
539	Interior	ASSISTANT HEAD OF SCHOOL	A	Wall	Drywall	Tan	Intact	-0.16	Negative		
540	Interior	ASSISTANT HEAD OF SCHOOL	B	Wall	Drywall	Tan	Intact	-0.64	Negative		
541	Interior	ASSISTANT HEAD OF SCHOOL	C	Wall	Drywall	Tan	Intact	-0.37	Negative		
542	Interior	ASSISTANT HEAD OF SCHOOL	D	Wall	Drywall	Tan	Intact	-0.20	Negative		
543	Interior	ASSISTANT HEAD OF SCHOOL	D	Door	Wood	Brown	Intact	0.13	Negative		
544	Interior	ASSISTANT HEAD OF SCHOOL	D	Door Frame	Metal	White	Intact	0.08	Negative		
545	Interior	ASSISTANT HEAD OF SCHOOL	C	Window Frame	Wood	White	Intact	-0.32	Negative		
546	Interior	ASSISTANT HEAD OF SCHOOL	C	Window Sill	Wood	White	Intact	-0.29	Negative		
547	Interior	ASSISTANT HEAD OF SCHOOL	---	Ceiling	Drywall	White	Intact	0.08	Negative		
548	Interior	SERVER ROOM	A	Wall	Concrete	Pink	Intact	0.30	Negative		
549	Interior	SERVER ROOM	B	Wall	Concrete	Pink	Intact	0.26	Negative		
550	Interior	SERVER ROOM	C	Wall	Drywall	Pink	Intact	0.04	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
551	Interior	SERVER ROOM	D	Wall	Drywall	Pink	Intact	0.15	Negative		
552	Interior	SERVER ROOM	D	Door	Wood	White	Intact	0.01	Negative		
553	Interior	SERVER ROOM	D	Door Frame	Wood	White	Intact	0.26	Negative		
554	Interior	SERVER ROOM	---	Ceiling	Drywall	White	Intact	0.06	Negative		
555	Interior	ROOM 147	A	Wall	Drywall	Pink	Intact	0.01	Negative		
556	Interior	ROOM 147	B	Wall	Drywall	Pink	Intact	0.27	Negative		
557	Interior	ROOM 147	C	Wall	Drywall	Pink	Intact	0.38	Negative		
558	Interior	ROOM 147	D	Wall	Drywall	Pink	Intact	0.19	Negative		
559	Interior	ROOM 147	C	Door	Wood	White	Intact	0.22	Negative		
560	Interior	ROOM 147	C	Door Frame	Wood	White	Intact	0.06	Negative		
561	Interior	ROOM 147	---	Ceiling	Drywall	White	Intact	0.09	Negative		
562	Interior	ROOM 141	A	Wall	Drywall	White	Intact	0.26	Negative		
563	Interior	ROOM 141	B	Wall	Drywall	White	Intact	0.08	Negative		
564	Interior	ROOM 141	C	Wall	Drywall	White	Intact	0.09	Negative		
565	Interior	ROOM 141	D	Wall	Drywall	White	Intact	0.14	Negative		
566	Interior	ROOM 141	D	Door	Wood	White	Intact	0.00	Negative		
567	Interior	ROOM 141	D	Door Frame	Metal	White	Intact	0.01	Negative		
568	Interior	ROOM 141	---	Ceiling	Drywall	White	Intact	0.30	Negative		
569	Interior	ROOM 142	A	Wall	Drywall	White	Intact	-0.20	Negative		
570	Interior	ROOM 142	B	Wall	Drywall	White	Intact	-0.37	Negative		
571	Interior	ROOM 142	C	Wall	Drywall	White	Intact	0.08	Negative		
572	Interior	ROOM 142	D	Wall	Drywall	White	Intact	0.19	Negative		
573	Interior	ROOM 142	C	Door	Wood	White	Intact	0.15	Negative		
574	Interior	ROOM 142	C	Door Frame	Metal	White	Intact	0.09	Negative		
575	Interior	ROOM 142	A	Window Frame	Metal	White	Intact	0.06	Negative		
576	Interior	ROOM 142	---	Ceiling	Drywall	White	Intact	0.00	Negative		
577	Interior	ROOM 143	A	Wall	Drywall	White	Intact	0.06	Negative		
578	Interior	ROOM 143	B	Wall	Drywall	White	Intact	0.08	Negative		
579	Interior	ROOM 143	C	Wall	Drywall	White	Intact	0.31	Negative		
580	Interior	ROOM 143	D	Wall	Drywall	White	Intact	0.24	Negative		
581	Interior	ROOM 143	A	Door	Wood	White	Intact	0.22	Negative		
582	Interior	ROOM 143	A	Door Frame	Metal	White	Intact	0.06	Negative		
583	Interior	ROOM 143	---	Ceiling	Drywall	White	Intact	0.08	Negative		
584	Interior	LOWER LEVEL MECHANICAL RM.	B	Wall	Plaster	Green	Fair	0.06	Negative		
585	Interior	LOWER LEVEL MECHANICAL RM.	C	Wall	Plaster	Green	Fair	0.08	Negative		
586	Interior	LOWER LEVEL MECHANICAL RM.	D	Wall	Plaster	Green	Fair	0.09	Negative		
587	Interior	LOWER LEVEL MECHANICAL RM.	C	Door	Wood	Tan	Fair	0.02	Negative		
588	Interior	LOWER LEVEL MECHANICAL RM.	C	Door Frame	Wood	Tan	Fair	0.22	Negative		
589	Interior	LOWER LEVEL MECHANICAL RM.	D	Closet Wall	Drywall	White	Intact	0.07	Negative		
590	Interior	LOWER LEVEL MECHANICAL RM.	B	Closet Door	Wood	Green	Fair	0.13	Negative		
591	Interior	LOWER LEVEL MECHANICAL RM.	---	Valve Closet	Metal	Green	Intact	0.14	Negative		
592	Interior	ROOM 144	A	Wall	Drywall	White	Intact	0.06	Negative		
593	Interior	ROOM 144	B	Wall	Drywall	White	Intact	0.12	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantifies For Entire Area	Comments
594	Interior	ROOM 144	C	Wall	Drywall	White	Intact	0.31	Negative		
595	Interior	ROOM 144	D	Wall	Wood	Brown	Intact	0.15	Negative		
596	Interior	ROOM 144	A	Door	Wood	White	Fair	0.25	Negative		
597	Interior	ROOM 144	A	Door Frame	Metal	White	Fair	0.18	Negative		
598	Interior	ROOM 144	C	Window Frame	Metal	Black	Intact	0.04	Negative		
599	Interior	ROOM 144	C	Window Sill	Metal	Black	Intact	0.13	Negative		
600	Interior	ROOM 144	---	Ceiling	Drywall	White	Intact	0.08	Negative		
601	Interior	CUSTODIAN	A	Wall	Plaster	Green	Fair	0.14	Negative		
602	Interior	CUSTODIAN	B	Wall	Plaster	Green	Fair	0.22	Negative		
603	Interior	CUSTODIAN	C	Wall	Plaster	Green	Fair	0.13	Negative		
604	Interior	CUSTODIAN	D	Wall	Plaster	Green	Fair	0.20	Negative		
605	Interior	CUSTODIAN	D	Door	Wood	White	Intact	0.09	Negative		
606	Interior	CUSTODIAN	D	Door Frame	Metal	White	Intact	0.11	Negative		
607	Interior	CUSTODIAN	---	Ceiling	Plaster	Green	Intact	0.00	Negative		
608	Interior	RESTROOM	A	Wall	Drywall	White	Intact	0.04	Negative		
609	Interior	RESTROOM	B	Wall	Drywall	White	Intact	0.05	Negative		
610	Interior	RESTROOM	C	Wall	Drywall	White	Intact	0.12	Negative		
611	Interior	RESTROOM	D	Wall	Drywall	White	Intact	0.08	Negative		
612	Interior	RESTROOM	D	Door	Wood	White	Intact	0.13	Negative		
613	Interior	RESTROOM	D	Door Frame	Metal	White	Intact	0.08	Negative		
614	Interior	RESTROOM	---	Ceiling	Drywall	White	Intact	0.15	Negative		
615	Interior	RESTROOM	---	Tile	Ceramic Tile	White	Intact	0.09	Negative		
616	Interior	RESTROOM	---	Floor	Ceramic Tile	White	Intact	0.13	Negative		
617	Interior	RESTROOM	A	Wall	Drywall	White	Intact	0.13	Negative		
618	Interior	RESTROOM	B	Wall	Drywall	White	Intact	0.20	Negative		
619	Interior	RESTROOM	C	Wall	Drywall	White	Intact	0.09	Negative		
620	Interior	RESTROOM	D	Wall	Drywall	White	Intact	0.11	Negative		
621	Interior	RESTROOM	C	Door	Wood	White	Intact	0.32	Negative		
622	Interior	RESTROOM	C	Door Frame	Metal	White	Intact	0.21	Negative		
623	Interior	RESTROOM	---	Ceiling	Drywall	White	Intact	0.20	Negative		
624	Interior	RESTROOM	---	Tile	Ceramic Tile	White	Intact	0.21	Negative		
625	Interior	RESTROOM	---	Floor	Ceramic Tile	White	Intact	0.28	Negative		
626	Interior	HALL	A	Wall	Drywall	White	Intact	0.08	Negative		
627	Interior	HALL	B	Wall	Drywall	White	Intact	0.09	Negative		
628	Interior	HALL	C	Wall	Drywall	White	Intact	0.33	Negative		
629	Interior	HALL	D	Wall	Drywall	White	Intact	0.26	Negative		
630	Interior	HALL	A	Door	Wood	White	Intact	0.03	Negative		
631	Interior	HALL	A	Door Frame	Wood	White	Intact	0.12	Negative		
632	Interior	HALL	---	Ceiling	Drywall	White	Intact	0.02	Negative		
633	Interior	HALL	B	Closet Door	Wood	White	Intact	0.04	Negative		
634	Interior	ROOM 145	A	Wall	Drywall	White	Intact	0.08	Negative		
635	Interior	ROOM 145	B	Wall	Wood	Tan	Intact	0.12	Negative		
636	Interior	ROOM 145	C	Wall	Drywall	White	Intact	-0.41	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
637	Interior	ROOM 145	D	Wall	Drywall	White	Intact	-0.31	Negative		
638	Interior	ROOM 145	A	Door	Wood	White	Intact	0.06	Negative		
639	Interior	ROOM 145	A	Door Frame	Metal	White	Intact	0.02	Negative		
640	Interior	ROOM 145	C	Window Frame	Metal	Black	Intact	-0.09	Negative		
641	Interior	ROOM 145	C	Window Sill	Metal	Black	Intact	-0.23	Negative		
642	Interior	ROOM 145	---	Ceiling	Drywall	White	Intact	-0.34	Negative		
643	Interior	ROOM 146 PUBLICATION	A	Wall	Drywall	Tan	Intact	0.07	Negative		
644	Interior	ROOM 146 PUBLICATION	B	Wall	Drywall	Tan	Intact	0.34	Negative		
645	Interior	ROOM 146 PUBLICATION	C	Wall	Drywall	Tan	Intact	0.26	Negative		
646	Interior	ROOM 146 PUBLICATION	D	Wall	Drywall	Tan	Intact	0.04	Negative		
647	Interior	ROOM 146 PUBLICATION	B	Door	Wood	White	Intact	0.25	Negative		
648	Interior	ROOM 146 PUBLICATION	B	Door Frame	Metal	White	Intact	0.39	Negative		
649	Interior	ROOM 146 PUBLICATION	---	Ceiling	Drywall	White	Intact	-0.32	Negative		
650	Interior	ROOM 149 COMPUTER LAB	A	Wall	Drywall	Tan	Intact	0.06	Negative		
651	Interior	ROOM 149 COMPUTER LAB	B	Wall	Drywall	Tan	Intact	0.03	Negative		
652	Interior	ROOM 149 COMPUTER LAB	C	Wall	Drywall	Tan	Intact	0.29	Negative		
653	Interior	ROOM 149 COMPUTER LAB	D	Wall	Drywall	Tan	Intact	0.14	Negative		
654	Interior	ROOM 149 COMPUTER LAB	B	Door	Wood	White	Intact	0.11	Negative		
655	Interior	ROOM 149 COMPUTER LAB	B	Door Frame	Metal	White	Intact	0.28	Negative		
656	Interior	ROOM 149 COMPUTER LAB	---	Ceiling	Drywall	White	Intact	-0.30	Negative		
657	Interior	COPY ROOM	A	Wall	Drywall	White	Intact	0.30	Negative		
658	Interior	COPY ROOM	B	Wall	Drywall	White	Intact	0.16	Negative		
659	Interior	COPY ROOM	C	Wall	Drywall	White	Intact	0.04	Negative		
660	Interior	COPY ROOM	D	Wall	Drywall	White	Intact	0.09	Negative		
661	Interior	COPY ROOM	C	Door	Wood	White	Intact	0.02	Negative		
662	Interior	COPY ROOM	C	Door Frame	Metal	White	Intact	0.03	Negative		
663	Interior	COPY ROOM	---	Ceiling	Drywall	White	Intact	0.08	Negative		
664	Interior	COPY ROOM	A	Closet Wall	Concrete	Green	Intact	-0.22	Negative		
665	Interior	COPY ROOM	B	Closet Door	Metal	Green	Intact	-0.12	Negative		
666	Interior	COPY ROOM	B	Elevator Door	Metal	White	Intact	0.46	Negative		
667	Interior	DIRECTOR OF TECHNOLOGY	A	Wall	Drywall	Tan	Intact	0.16	Negative		
668	Interior	DIRECTOR OF TECHNOLOGY	B	Wall	Drywall	Tan	Intact	0.09	Negative		
669	Interior	DIRECTOR OF TECHNOLOGY	C	Wall	Drywall	Tan	Intact	0.01	Negative		
670	Interior	DIRECTOR OF TECHNOLOGY	D	Wall	Drywall	Tan	Intact	0.26	Negative		
671	Interior	DIRECTOR OF TECHNOLOGY	B	Door	Wood	White	Intact	-0.45	Negative		
672	Interior	DIRECTOR OF TECHNOLOGY	B	Door Frame	Metal	Tan	Intact	0.11	Negative		
673	Interior	DIRECTOR OF TECHNOLOGY	---	Ceiling	Drywall	White	Intact	0.14	Negative		
674	Interior	SUPPLY ROOM	A	Wall	Concrete	Green	Intact	0.15	Negative		
675	Interior	SUPPLY ROOM	B	Wall	Drywall	Green	Intact	0.26	Negative		
676	Interior	SUPPLY ROOM	C	Wall	Drywall	Green	Intact	0.08	Negative		
677	Interior	SUPPLY ROOM	D	Wall	Drywall	Green	Intact	0.13	Negative		
678	Interior	SUPPLY ROOM	D	Door	Wood	White	Intact	0.00	Negative		
679	Interior	SUPPLY ROOM	D	Door Frame	Wood	White	Intact	0.03	Negative		

DETAILED XRF TESTING RESULTS

3900 Stansbury Avenue, Sherman Oaks, CA 91423

Sample	Area	Room Equivalent	Side Tested	Component	Substrate	Color	Condition	Lead (mg/ cm²)	Results	Quantities For Entire Area	Comments
680	Interior	SUPPLY ROOM	—	Ceiling	Drywall	Green	Intact	0.01	Negative		
681	Interior	TECHNOLOGY ROOM	A	Wall	Drywall	Tan	Intact	0.20	Negative		
682	Interior	TECHNOLOGY ROOM	B	Wall	Drywall	Tan	Intact	0.16	Negative		
683	Interior	TECHNOLOGY ROOM	C	Wall	Drywall	Tan	Intact	0.04	Negative		
684	Interior	TECHNOLOGY ROOM	D	Wall	Drywall	Tan	Intact	0.30	Negative		
685	Interior	TECHNOLOGY ROOM	D	Door	Wood	White	Intact	0.07	Negative		
686	Interior	TECHNOLOGY ROOM	D	Door Frame	Wood	White	Intact	0.31	Negative		
687	Interior	TECHNOLOGY ROOM	—	Ceiling	Drywall	White	Intact	0.08	Negative		
688	Interior	LOWER LEVEL HALL	A	Wall	Drywall	White	Intact	0.01	Negative		
689	Interior	LOWER LEVEL HALL	B	Wall	Drywall	White	Intact	0.16	Negative		
690	Interior	LOWER LEVEL HALL	C	Wall	Drywall	White	Intact	-0.21	Negative		
691	Interior	LOWER LEVEL HALL	D	Wall	Drywall	White	Intact	-0.03	Negative		
692	Interior	LOWER LEVEL HALL	C	Door	Wood	White	Intact	0.16	Negative		
693	Interior	LOWER LEVEL HALL	C	Door Frame	Metal	White	Intact	0.03	Negative		
694	Interior	LOWER LEVEL HALL	—	Ceiling	Drywall	White	Intact	0.08	Negative		

ALLSTATE SERVICES ENVIRONMENTAL XRF CALIBRATION FORM

Address/Unit: The Buckley School, 3900 Stansbury Avenue, Sherman Oaks, CA 91423

Device: EDAX/MAP-4 M41316

Date: April 26, 2006

Inspector: James Hantgin & George Munoz

Calibration Check Tolerance Used: 0.6 mg/cm² - 1.2 mg/cm² (Inclusive)

Use Level III (1.02 mg/cm²) NIST SRM Paint film

First Calibration Check Time: 3:00 pm

1st Reading	2nd Reading	3rd Reading	**1st Average**
1.07	1.03	1.03	**1.04**

Second Calibration Check Time: 7:00 pm

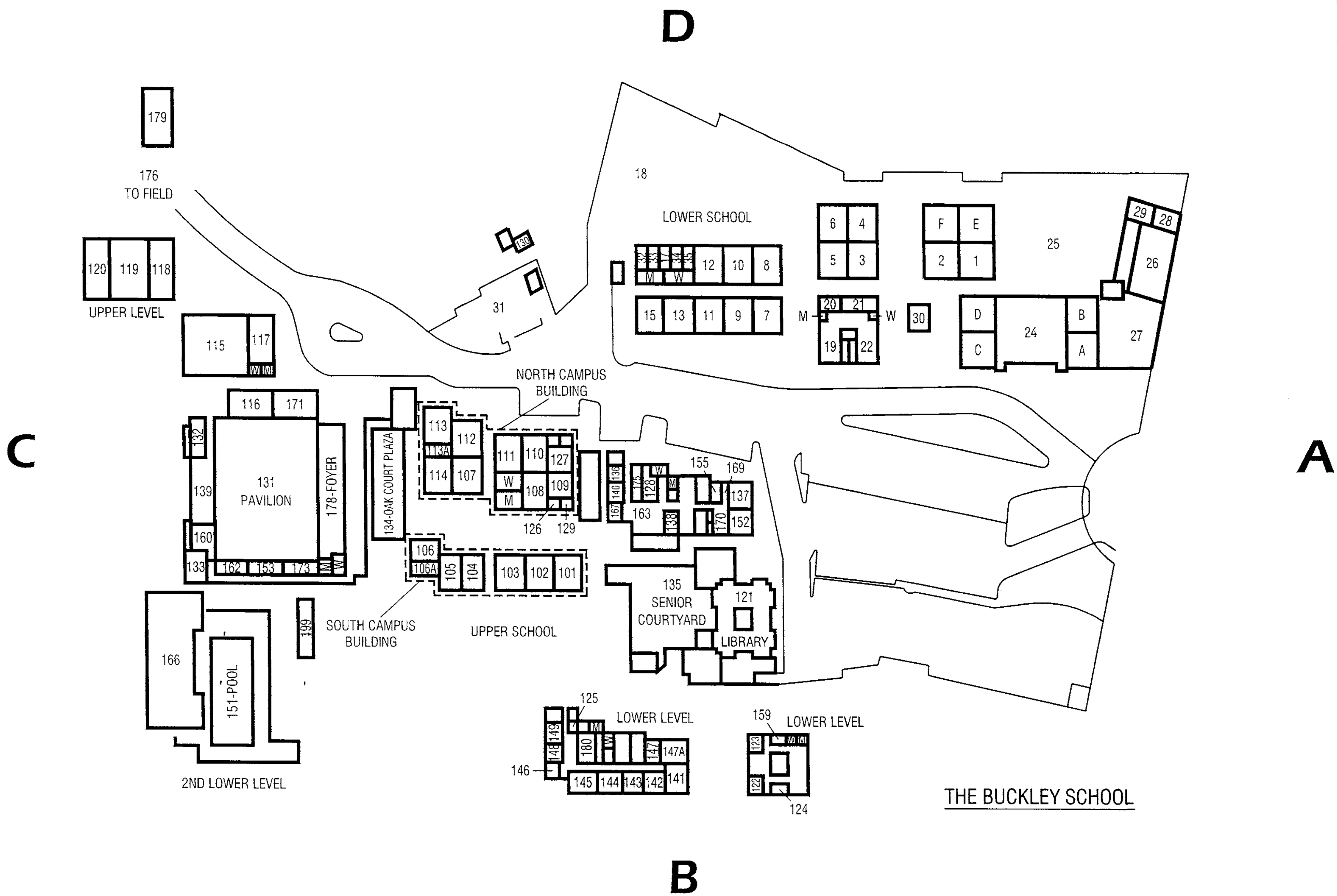
1st Reading	2nd Reading	3rd Reading	**2nd Average**
1.01	1.05	0.99	**1.02**

Third Calibration Check (If Needed) Time: 8:30 pm

1st Reading	2nd Reading	3rd Reading	**3rd Average**
1.05	1.01	1.03	**1.03**

- **Use the Test Mode Reading**
- **Tolerance Values for EDAX/MAP-4: 0.6 mg/cm² to 1.2 mg/cm² (Inclusive)**

APPENDIX C
FLOOR PLAN



ALLSTATE SERVICES ENVIRONMENTAL, INC.

1826 POMONA ROAD
CORONA, CA 92880
(800) 320-5323

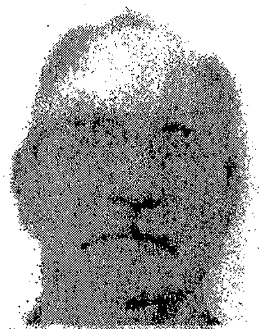
LEAD-BASED PAINT TESTING AT:
3900 STANSBURY AVENUE
SHERMAN OAKS, CALIFORNIA 91423

DATE	4/26/06
JOB #	06-109
SCALE	N.T.S.

APPENDIX D
INSPECTOR/ASSESSOR CERTIFICATIONS

State of California Department of Health Services

Lead-Related Construction Certificate	Certificate Type	Expiration Date
	Inspector/Assessor	05/27/2007

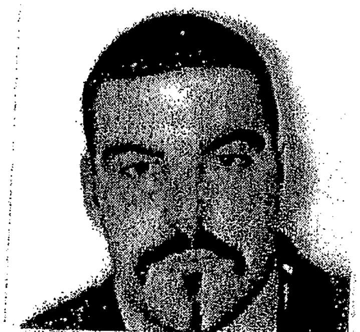


James R. Hantgin ID #: 6259

State of California Department of Health Services

Lead-Related
Construction
Certificate

Certificate Type	Expiration Date
Inspector/Assessor	11/11/2006
Supervisor	11/11/2006
Project Monitor	11/11/2006



George A. Munoz ID #: 11268

APPENDIX E
DHS FORM 8552 - LEAD HAZARD EVALUATION REPORT

LEAD HAZARD EVALUATION REPORT

Section 1: Date of Lead Hazard Evaluation 4/26/06

Section 2:

A. Type of Lead Hazard Evaluation (**Check One Box and Mark the Necessary Option**):

- [x] Lead Inspection
  - [ ] No lead-based paint detected
  - [ ] Intact lead-based paint detected
  - [x] Deteriorated lead-based paint detected
- [ ] Risk Assessment
  - [ ] No lead hazards detected
  - [ ] Lead hazards detected
- [ ] Clearance Inspection
  - [ ] No lead hazards detected
  - [ ] Lead hazards detected
- [ ] Environmental Investigation
  - [ ] No lead hazards detected
  - [ ] No lead-based paint detected
  - [ ] Lead hazards detected
  - [ ] Lead-based paint detected

B. Method of Lead Hazard Evaluation (**Check All That Apply**):

- [ ] Soil
- [ ] Wipe(s)
- [ ] Paint Chips
- [x] XRF (Brand and Serial Number) EDAX/MAP-4 M41316

Section 3: Structure Where Lead Hazard Evaluation Was Conducted

Name of Structure (if applicable):	Construction Date (Year) of Structure:		
Buckley School	1/1/60		
Address [number, street, apartment number (if applicable)]:	**City:**	**County:**	**Zip Code:**
3900 Stansbury Avenue	Sherman Oaks	Los Angeles	91423

Type of Structure (**Check One Box Only**):

- [x] School, Day Care, or Other Child-Occupied Facility
- [ ] Single Family Dwelling
- [ ] Multi-Unit Building
- [ ] Public Building
- [ ] Commercial Facility
- [ ] Other ______

Section 4: Owner of Structure (if business/agency/school, list contact person)

Name of Organization (if any):	First Name:	Last Name:	Telephone Number:
Applied Toxicology	Ken	Medici	( )(760) 212-8857
Address [number, street, apartment number (if any)]:	**City:**	**State:**	**Zip Code:**
1450 North Sants Fe Suite # C, PMB # 144	Vista	California	92083

Section 5: Individual Conducting Lead Hazard Evaluation

Last Name:	First Name:	Telephone Number:	
Hantgin	James	( ) (951) 340-1717	
Address [number, street, apartment (if applicable)]	**City:**	**State:**	**Zip Code:**
1826 Pomona Road	Corona	California	92880
DHS Certification Number (Required)	**Signature:**		**Date:**
I-6259	James Hantgin		4/27/06

Section 6: Attachments (Submit By Request Only)

A. A foundation diagram or sketch of the structure indicating the specific locations of each lead hazard or presence of lead-based paint;

B. Each testing method, device, and sampling procedures used;

C. All data collected, including quality control data, laboratory results, including laboratory name, address, and phone number.

First copy and attachments retained by inspector
Second copy and attachments retained by owner

Third copy must be submitted to DHS (NO Attachments)

This form shall be mailed or faxed to:
Childhood Lead Poisoning Prevention Branch
Reports
850 Marina Bay Parkway, Bldg. P, Third Floor
Phone: (510) 620-5600
Fax: (510) 620-5656

LEAD HAZARD EVALUATION REPORT

Section 1: Date of Lead Hazard Evaluation 4/26/06

Section 2:

A. Type of Lead Hazard Evaluation (**Check One Box and Mark the Necessary Option**):

- [x] Lead Inspection
  - [ ] No lead-based paint detected
  - [ ] Intact lead-based paint detected
  - [x] Deteriorated lead-based paint detected
- [ ] Risk Assessment
  - [ ] No lead hazards detected
  - [ ] Lead hazards detected
- [ ] Clearance Inspection
  - [ ] No lead hazards detected
  - [ ] Lead hazards detected
- [ ] Environmental Investigation
  - [ ] No lead hazards detected
  - [ ] No lead-based paint detected
  - [ ] Lead hazards detected
  - [ ] Lead-based paint detected

B. Method of Lead Hazard Evaluation (**Check All That Apply**):

- [ ] Soil - [ ] Wipe(s) - [ ] Paint Chips - [x] XRF (Brand and Serial Number) EDAX/MAP-4 M41316

Section 3: Structure Where Lead Hazard Evaluation Was Conducted

Name of Structure (if applicable):	Construction Date (Year) of Structure:		
Buckley School	1/1/60		
Address [number, street, apartment number (if applicable)]:	City:	County:	Zip Code:
3900 Stansbury Avenue	Sherman Oaks	Los Angeles	91423

Type of Structure (**Check One Box Only**): [x] School, Day Care, or Other Child-Occupied Facility

[ ] Single Family Dwelling [ ] Multi-Unit Building [ ] Public Building [ ] Commercial Facility [ ] Other ____________

Section 4: Owner of Structure (if business/agency/school, list contact person)

Name of Organization (if any):	First Name:	Last Name:	Telephone Number:
Applied Toxicology	Ken	Medici	( )(760) 212-8857
Address [number, street, apartment number (if any)]:	City:	State:	Zip Code:
1450 North Sants Fe Suite # C, PMB # 144	Vista	California	92083

Section 5: Individual Conducting Lead Hazard Evaluation

Last Name:	First Name:	Telephone Number:	
Munoz	George	( ) (951) 340-1717	
Address [number, street, apartment (if applicable)]	City:	State:	Zip Code:
1826 Pomona Road	Corona	California	92880
DHS Certification Number (Required)	Signature:		Date:
I-11268	George M...		4/27/06

Section 6: Attachments (Submit By Request Only)

A. A foundation diagram or sketch of the structure indicating the specific locations of each lead hazard or presence of lead-based paint;

B. Each testing method, device, and sampling procedures used;

C. All data collected, including quality control data, laboratory results, including laboratory name, address, and phone number.

First copy and attachments retained by inspector
Second copy and attachments retained by owner

Third copy must be submitted to DHS (NO Attachments)
This form shall be mailed or faxed to:
Childhood Lead Poisoning Prevention Branch
Reports
850 Marina Bay Parkway, Bldg. P, Third Floor
Phone: (510) 620-5600
Fax: (510) 620-5656

APPENDIX 2.0

CADHS Form 8552

Kenneth Medici

LEAD HAZARD EVALUATION REPORT

Section 1: Date of Lead Hazard Evaluation 4/26/06

Section 2:

A. Type of Lead Hazard Evaluation (**Check One Box and Mark the Necessary Option**):

- ☐ Lead Inspection
  - ☐ No lead-based paint detected
  - ☐ Intact lead-based paint detected
  - ☐ Deteriorated lead-based paint detected
- ☐ Risk Assessment
  - ☐ No lead hazards detected
  - ☐ Lead hazards detected
- ☐ Clearance Inspection
  - ☐ No lead hazards detected
  - ☐ Lead hazards detected
- ☑ Environmental Investigation
  - ☑ No lead hazards detected
  - ☐ No lead-based paint detected
  - ☐ Lead hazards detected
  - ☑ Lead-based paint detected

B. Method of Lead Hazard Evaluation (**Check All That Apply**):

☐ Soil ☐ Wipe(s) ☐ Paint Chips ☐ XRF (Brand and Serial Number)

Section 3: Structure Where Lead Hazard Evaluation Was Conducted

Name of Structure (if applicable): The Buckley School

Construction Date (Year) of Structure: 1/1/60

Address [number, street, apartment number (if applicable)]: 3900 Stansbury Ave

City: Sherman Oaks

County: Los Angeles

Zip Code: 91423

Type of Structure (**Check One Box Only**): ☑ School, Day Care, or Other Child-Occupied Facility

☐ Single Family Dwelling ☐ Multi-Unit Building ☐ Public Building ☐ Commercial Facility ☐ Other

Section 4: Owner of Structure (if business/agency/school, list contact person)

Name of Organization (if any): The Buckley School

First Name:

Last Name:

Telephone Number: ( )(818) 783-1610

Address [number, street, apartment number (if any)]: 3900 Stansbury Avenue

City: Sherman Oaks

State: CA

Zip Code: 91423

Section 5: Individual Conducting Lead Hazard Evaluation

Last Name: Medici

First Name: Kenneth

Telephone Number: ( ) (760) 212-8857

Address [number, street, apartment (if applicable)] 1450 North Santa Fe Avenue #C-144

City: Vista

State: CA

Zip Code: 92083

DHS Certification Number (Required) 1629

Signature:

Date:

Section 6: Attachments (Submit By Request Only)

A. A foundation diagram or sketch of the structure indicating the specific locations of each lead hazard or presence of lead-based paint;

B. Each testing method, device, and sampling procedures used;

C. All data collected, including quality control data, laboratory results, including laboratory name, address, and phone number.

First copy and attachments retained by inspector
Second copy and attachments retained by owner

Third copy must be submitted to DHS (NO Attachments)

This form shall be mailed or faxed to:
Childhood Lead Poisoning Prevention Branch
Reports
850 Marina Bay Parkway, Bldg. P, Third Floor
Phone: (510) 620-5600
Fax: (510) 620-5656

Asbestos Report

ASBESTOS

ABATEMENT

REPORT

Prepared for:

The Buckley School
3900 Stansbury Road
Sherman Oaks, CALIFORNIA 91423

Curtis Covington, Director of Physical Plant
(818).783-1610 Office
(818).461-6712 Fax

Prepared by:
Ken Medici 1/7/06
Kenneth Medici
Certified Asbestos Consultant
California DOSH #92-0007

CERTIFIED ASBESTOS CONSULTANT ★ KENNETH MEDICI KM No 92-0007 Exp 6-17-07 STATE OF CALIFORNIA

Site: **The Buckley School, Sherman Oaks Campus - Administration Bldg MR Cleaning (Basement) & Lower School Buildings - O&M Clean-up Work - Assembly Room Boiler Room Attic Work - Attic above Kindergarten Rooms**

&

Pavilion Stairwell Flooring Abatement (Stairs located at Stage area up to Mech Rm)

Dates:	June 2001	Comprehensive Asbestos Survey
	December 2005	Background air tests
	December 2005	Asbestos Abatement
	December 2005	TEM Air Clearance Testing
	(Winter Break 2005)	

TABLE OF CONTENTS

The Buckley School Records

SECTION 1.0

Comprehensive Asbestos Survey on file with administration office. Not included in this report.

SECTION 2.0

ASBESTOS CONSULTANT RECORDS

ASBESTOS CONSULTANT RECORDS

SECTION 2.0

PART 1.0

WORK SUMMARY

SECTION 2.0 - PART 1.0 (page one of one)
SUMMARY OF THE ASBESTOS ABATEMENT WORK

Background: The Buckley School continued to conduct O&M work within the Attics of the Lower School Building above Kindergarten rooms and Assembly Boiler room. Also, asbestos abatement of the flooring materials at the Pavilion Stairwell (located at the stage area up to the Mech room) was begun. Also, O&M cleaning of the Main Campus Administration Bldg Mechanical room was begun. The Buckley School contacted Applied Toxicology for management of the asbestos abatement project. Ken Medici, CAC #92-0007 was designated as the primary Asbestos Abatement Consultant for The Buckley School. Subsequently, directives were prepared regarding the asbestos AHERA regulations in which only the most stringent abatement procedures be followed and only the most stringent air clearance tests were to be performed prior to release of the asbestos abatement contractor from his cleaning liability. This school policy would maximize construction safety and minimize asbestos fiber release.

Asbestos Survey: Applied Toxicology conducted a comprehensive asbestos survey of the entire school; this survey is on file with the school at the Superintendents office. Additional samples of attic area stucco-related debris were collected August 2004 which found <1% asbestos ("Trace") Asbestos present. Additional samples of floor glue were collected at the stairwell which found no asbestos detected.

Asbestos Abatement Plan: An abatement plan was prepared and issued by Ken Medici of Applied Toxicology for bidding by California Licensed Contractors, Certified in Asbestos Abatement.

Asbestos Abatement Job Walk/Bid Award: A job walk with Fresh Air Environmental Contractors qualified contractors was performed via telephone December 2005 prior to contract ward. The Buckley School collected quoted labor rates from the bidding contractor and selected Fresh Air for the work.

Pre-construction meeting: A meeting was conducted on-site with Romeo Hernandez of Fresh Air. Paperwork submittals were pending for review at this pre-construction meeting. A planned asbestos abatement date was set for December 22, 2005 at 9am.

Abatement & Clearance Work: On Thursday, December 22, 2005 (7am) Applied Toxicology met at Buckley and conducted background air tests. Work began at approximately 9:10am. Fresh Air provided workers for this job and their names are found in the Contractor submittal section of this report. Applied Toxicology provided one worker for this job- Kenneth Medici, CAC #92-0007. Fresh Air Set-up the work area at the Stairs with with plastic sheeting barriers (containment area). After set-up the workers began abating floor tile from the base landing and upper landing and stairwell stairs. Friday December 23, 2005 Fresh Air went into the Boiler room attic adjacent to the Assembly Room and set-up plastic to conduct cleaning at the Admin Bldg Basement Mech Room. Air tests were conducted throughout the project. Air tests were collected from within each work area and outside each work area. Review of the air tests found that all work was conducted safely and in compliance with all laws and regulations regarding asbestos.
Other asbestos-related work:

1. PLM Bulk suspect asbestos samples were collected within the Pavilion Building at the stairs for glue found under the floor tile . The Analytical laboratory reported no asbestos found.
   One sample of the Admin Bldg elevator linoleum found no asbestos detected.

ASBESTOS CONSULTANT RECORDS

SECTION 2.0

PART 2.0

COMPREHENSIVE ASBESTOS SURVEY

Comprehensive asbestos survey on file with administration office. Not included in this report.

ASBESTOS CONSULTANT RECORDS

SECTION 2.0

PART 3.0

ABATEMENT PLAN

ASBESTOS

ABATEMENT

PROJECT DESIGN PLAN

Prepared for:

THE BUCKLEY SCHOOL
3900 Stansbury Ave
Sherman Oaks, CA 91423-4699

Curtis Covington, Director of Physical Plant
(818).783-1610 Office
(818).990-4516 Fax

Kenneth Medici
Management Planner for The Buckley School
California DOSH #92-0007
1450 North Santa Fe #C-144
Vista, CA 92083
(888).999-7908 toll-free
Fax (760).414-1183

Site: **THE BUCKLEY SCHOOL SHERMAN OAKS, CALIFORNIA**
Pavilion Stairwell to upper Mech Rm
Associated Floor Tile, Mastic, Baseboards
Approx 150 sq ft floor tile and associated black mastic floor adhesive
&
Lower School Assembly attic cleaning- O&M work

Planned Abatement Time Frame: **December 22, 23, 26, 27, 28, 2005**

BID FORM

JOB SPECIFICATION REQUIREMENTS - Pavilion Stairwell to Mech room Flooring ABATEMENT: Submit this completed bid form and your work contract to Kenneth Medici, Buckley School Management Planner for written approval. The Buckley School Management Planner will then submit approved contract to The Buckley School - Curtis Covington for final approval and final signature.

(ACM's) Removal and Disposal & Attic cleaning:

1. Disposal of floor tile/black mastic: Asbestos Hazardous Waste Disposal only.
   Contractor to assist owner in obtaining applicable Hazardous Waste Generator ID's
   Keep all in-place cabinets(if applicable) as original- **Sand off mastic from wood stairs!**
   Remove stair metal lips and sidewall baseboard and sidewall mastic with sander.
   - Construct full containment with negative air pressure enclosure-4 or more air changes/hr.
   - Use wet methods , notify applicable agencies and pay applicable permit fees
   - If emergency notification is required, Buckley School will issue a letter confirming such
   - Complete all removal work in two shifts or less, request an air clearance from Applied Toxicology. Asbestos abatement may be monitored during asbestos abatement work. Air Clearance will be performed by Applied Toxicology . If air test fails, re-clean the work area. Applied Toxicology will re-test work area.
   - Within 30 days of demobilization submit copies of Supervisor logs, air testing results, copy of waste manifest that was signed on-site at time of transport, copies of worker and supervisor documentation not obtained by The Buckley School on-site.

2. Send a final invoice to The Buckley School, attention Curtis Covington c/o Ken Medici, Applied Toxicology after work and paperwork are complete.

3. All of the above flooring removal work must be completed in 1-2 work shift time frame so air clearances can be completed during winter break with enough time for Buckley to install new flooring. Complete removal and disposal with two men and a supervisor in two or less shifts.

4. Attic cleaning consists of HEPA vac and wet wiping of walking boards, no air clearance tests planned. Set-up a negative pressure enclosure inside the boiler room with decon unit. Complete cleaning using one man and a supervisor in three or less shifts.

Bid Time and Material Rates:

Bid per hour per worker: Fresh Air - $55/hr Worker
Bid per hour per supervisor: Fresh Air - $65/hr Supervisor
above labor includes all disposal costs, related mgt costs, transportation costs, materials, Labor Overtime Costs, etc.

Project costs: 5 days two men and one supervisor 10hrs/day = $3250 -Supervisor plus $5500 workers
Total = $8750.00

Submitted by:

Signature: X ______________________________

Print Name - X DATE

The Buckley School Approval: Signed by: Faxed back:

THE BUCKLEY SCHOOL - Abatement of flooring at the Pavilion Stairs to Mech room & O&M Work at Lower School Attic areas near the Boiler Room of the Assembly Room

UP TO 150 sq ft of floor tile/associated black mastic (layered flooring)

Up to 45 ft of attic boards to be cleaning with HEPA Vac/wet wipe

SUMMARY OF THE ASBESTOS ABATEMENT WORK

PART 1 GENERAL:

1.01 RELATED WORK REQUIREMENTS: Related requirements and conditions required by the Contract Documents include, but are not necessarily limited to the following:

A. Drawing and general provisions of Contract Documents, including General and Supplementary and Special Conditions, apply to work of this section.

B. Asbestos is a generic term applied to a number of mineral silicates which are separable into fibers. There is evidence to support the fact that the inhaling of the fibers can result in various diseases to those exposed. Some of the diseases that have been associated with exposure to airborne asbestos are: asbestosis; mesothelioma; and cancers of the lung, esophagus, stomach, colon, and other organs. The US EPA and the scientific community believe that any level of exposure to asbestos involves some health risks, although the exact degree of the risk is not readily measurable or known. The Contractor acknowledges the danger and the health risk associated with working in and around asbestos and assumes said risk by entering into the Contract. The Contractor shall secure a copy of and familiarize himself with EPA Document No. 560/5-85-024, published June 1985, titled "Guidance for Controlling Asbestos-Containing Materials in Buildings," and applicable State, Federal, and Local, asbestos rules and regulations.

C. The Contractor under this Contract has the care, custody, and control of the premises and is solely responsible for all persons entering the work areas to be attired and protected as specified herein. The Contractor has the option to establish OSHA-defined Regulated Areas or to use glovebags and/or mini-enclosures to contain the work areas where asbestos-containing materials may be disturbed or removed. Regardless of the containment methods used, the Contractor is liable for constructing air-tight containments and for compliance with all current applicable regulations and guidelines relevant to this work.

1. The contractor must remove/dispose and clean areas of asbestos identified above, etc. and allow the asbestos consultant/others to test or inspect for asbestos.
2. This work must be completed within the TIME specified.
3. Work hours are pre-determined by the School.
4. Clearance will be by TEM or PCM by the asbestos consultant as applicable.
5. Include stairs, hallways, mastic on wood within the scope of work at the project location; include walking boards and vertical wood members.

D. The Contractor shall submit evidence of the following: 1) successful completion of at least three comparable asbestos removal projects accomplished by the firm to perform the work specified herein; 2) Asbestos Certification from the State Contractor's License Board; and 3) registration from Cal-OSHA as an Asbestos Abatement Contractor; 4) Applicable Insurance.

E. Comply with all Applicable codes and regulations.

F. Pay for and submit all required Notices and permits (Cal-OSHA and AQMD, etc)

G. Comply with applicable existing site conditions and restrictions on use of the site.

H. Patents: of negative air machines.
Contractor shall either be licensed by GPAC, Inc. for use of the patented Reduced Pressure and Filtration System, or indemnify Owner and Owner's Representative against any and all potential liability from patent infringement or use of this system.

1.02 DEFINITIONS:

A.	Owner:	The Buckley School	
B.	Owner's Representative:	Curtis Covington The Buckley School	
C.	Asbestos Consultant: (Management Planner)	Kenneth Medici CAC #92-0007	1-888-999-7908 Fax-(760).414-1183

D. Site Surveillance Technician - TBD, if applicable
E. AIHA Accredited Laboratory Analysis Firm: TBD
F. Work to be performed at this Facility Address:

The Buckley School
3900 Stansbury Ave
Sherman Oaks, California 91423

Work Area: The location where asbestos abatement work will occur. The "work area" is considered contaminated during the abatement work and must be isolated from the balance of the building, and decontaminated at the completion of the removal of asbestos. The work area must be isolated from the balance of the building by constructing a negatively pressurized containment around the work area. The containment must be constructed in a manner which prevents dust or debris from passing beyond the work area. Should the area beyond the work area containment become contaminated (as determined by a statistically significant increase in airborne fiber levels measured outside the containment barriers) with ACM dust or debris as a consequence of the work, immediately stop all abatement work. The Contractor shall clean any contaminated areas using wet-wiping and HEPA vacuuming techniques.

G. ACM: Asbestos-containing material.

1.03 SUMMARY OF WORK:

A. This abatement plan covers the removal of asbestos-containing materials which have been previously identified and which have not been previously identified. It is the sole responsibility of the Asbestos Abatement Contractor to thoroughly investigate periodically along with the Asbestos Consultant newly discovered suspect building materials not accessible or tested in previous surveys. Applicable change order approvals will be authorized upon completion of a written review by the Asbestos Consultant/Project Management. The contractor must adjust their bid to accommodate all interaction with the asbestos consultant and other project management and assumes risk for estimation of this additional time required to allow for owner's rep. or owner interaction.

B. All bidders shall attend the pre-bid walk-through inspection and measure amounts of material to be removed and thoroughly familiarize themselves with existing conditions that affect the work.

C. The objective of the project is to "clean" the areas designated of all asbestos-containing materials and to provide an atmosphere inside the building that is free from airborne fibers within limits specified in these specifications.

D. Work specified in this section includes furnishing all labor, equipment, services, insurance, materials, etc., in accordance with the requirements of EPA, OSHA, and other regulatory agencies, to complete removal of designated ACMs at the Owner's facility specified herein.
The asbestos consultant will perform air monitoring within the work area, outside the work area as deemed applicable during asbestos abatement work. The asbestos consultant will perform visual inspections and final visual and clearance inspections and air testing independent of the contractor. Allow two days for lab results as a worst case, if applicable. We anticipate 5 hour lab turnarounds as our goal, if possible!

1.04 DESCRIPTION OF WORK: Briefly and without force and effect upon the Contract Documents, the work of the contract can be summarized as follows:

A. Upon acceptance of asbestos removal plan and with prior authorization from the Asbestos-Consultant, secure and post areas where asbestos removal will take place.

B. Setup negative air system prior to start of cleaning (try to establish negative pressure within the proposed abatement area). Clean each individual designated work space using a high-efficiency particulate air (HEPA) vacuum system and wet-wiping techniques prior to beginning removal operations.

C. Prepare work areas for removal of existing ACMs in accordance with applicable laws.

D. Remove, clean, and properly package all ACM waste on a daily basis for proper disposal. Transport, prior to the end of each work shift, all packaged ACM waste to a fully enclosed (no open top) locked dumpster for overnight storage or other equivalent. All waste ACM must be disposed of as hazardous waste!

E. After final air clearance for unrestricted occupancy, dispose of all asbestos waste remaining and other items used in the work as applicable.

F. Conduct all work otherwise in accordance with these requirements, and, prior to submittal for final payment, deduct all costs due the Owner. Do not submit partial payment final requests.

1.05 GENERAL AND ADMINISTRATIVE REQUIREMENTS are set forth by Project Management and by this abatement plan:

CODES AND REGULATIONS: Sets forth governmental regulations and industry standards which are included and incorporated herein by reference and made a part of the Specifications. This section also sets forth those notices and permits which are known to the Owner and which either must be applied for and received, or which must be given to governmental agencies before start of work.

1.06 WORK AREA ACM REMOVAL: Requirements are set forth in the following section, listed here according to the sequence of the work:

A. Prepare a working decontamination unit. 3 stage only with hot running water for the Asbestos Consultant to shower with, every hour. Provide towels, waste bags, non-slip floors outside shower and in clean room. Provide a locked containment, use wood barriers as needed. Contractor may be forced to stop work and pay for the owner to install a locked barrier system if contractor fails to set up a locked regulated area.
B. HEPA vacuum and wet wipe as needed.
C. Prepare a regulated area as applicable.
D. Remove and properly package as ACMs. Dispose of ACM's.
The Buckley School Policy is to dispose of all waste generated as Hazardous Material Asbestos waste.

1.07 AIR MONITORING SURVEILLANCE: The protocol for the Site Surveillance Technician or asbestos consultant to use for conducting Baseline, Periodic, and Clearance air monitoring of the work area. Does not include Contractor's employee exposure monitoring.

WORK AREA CLEARANCE: The protocol to determine if the work area has been successfully cleaned of contamination, and is "cleared" for re-entry by building occupants. The asbestos consultant will perform his independent work area clearance as applicable and use PCM **or** TEM air analysis protocols.

A. The disturbance or dislocation of ACMs may cause the asbestos fibers to be released. Apprise all workers, supervisory personnel, subcontractors and consultants who will be at the job site of the seriousness of the hazard and of proper work procedures which must be followed.

B. Whereas in the performance of the work, workers, supervisory personnel, subcontractors, or consultants may encounter, disturb, or otherwise function in the immediate vicinity of any identified ACMs, take appropriate continuous measures as necessary to protect human health and the environment from the potential hazard and exposure to airborne asbestos. Such measures shall include the procedures and methods described herein, and compliance with regulations of applicable federal, state and local agencies.

1.08 ASBESTOS-CONTAINING MATERIALS/OTHER HAZARDS:

The following asbestos-containing materials are known to be present at the worksite. If any other materials are found which are suspected of containing asbestos, notify the Owner's representative immediately. These materials are not to be disturbed without prior written authorization from the Owner's Representative. Floor Tile, Black Mastic, Drywall, Stucco, stucco overspray, roofing, attic debris, drywall mud, plaster, TSI elbows, TSI, etc.............

A. Please see comprehensive asbestos survey for the entire school at Buckley office as a background reference.

B. The Contractor shall be responsible for removing all ACM as identified in this abatement plan and during the "job walk."

C. See above addendum work sheet and bid sheet.

1.09 CONTRACTOR USE OF PREMISES:

A. General: The Contractor shall limit his use of the premises to the work indicated, so as to allow for Owner occupancy, and use by the public. (Use of the premises is unrestricted if indicated so by the "Job Walk").

B. Keep existing driveways and entrances serving the premises available to the Owner and his employees, etc., at all times. Do not use these areas for parking or storage of materials.

C. Lock automotive-type vehicles, such as passenger cars and trucks and other mechanized or motorized construction equipment, when parked and unattended, so as to prevent unauthorized use. Do not leave such vehicles or equipment unattended with motor running or ignition key in place or accessible to unauthorized persons.

1.10 CONTRACTOR'S USE OF THE EXISTING BUILDING:

Maintain existing building in a safe and weather-tight condition throughout the construction period. Take all precautions necessary to protect human health and the environment during the construction period. These protective measures shall be provided by the Contractor 24 hours per day and 7 days per week until the work area or portion of the premises exposed by work under this contract has been deemed safe by the Asbestos Consultant.

PART 2 PRODUCTS (NOT APPLICABLE)

PART 3 EXECUTION (NOT APPLICABLE)

ASBESTOS CONSULTANT RECORDS

SECTION 2.0

PART 7.0

ANALYTICAL LABORATORY RESULTS

CHAIN OF CUSTODY FORMS

Laboratory Analytical Methods

PLM - Bulk Sample Analysis (Polarized Light Microscopy):
The bulk material samples were submitted to an accredited laboratory in California.
Bulk material samples were analyzed using dispersion staining techniques in accordance with the 40 CFR, Part 763, Appendix A, Subpart F, AHERA regulations.

PCM - Air Analysis (Phase Contrast Microscopy):
The air samples were analyzed for airborne fibers by a regular light microscope per NIOSH Method 7400 A (as applicable).

TEM - Air Analysis (Transmission Electron Microscopy):
The air samples were analyzed for airborne asbestos by a Transmission Electron Microscope per AHERA protocol .

Sample ID #	**Location/description**	**Result Summary**

Background Air Tests at Pavilion Stairwell:

December 22, 2005, Thursday at 6:20am:

1222T-01	Work Area - base of stairs	Pass
1222T-02	Work Area -middle of stairs	Pass
1222T-03	Work Area - Top of Stairs	Pass
1222T-04	Work Area - Stage Corridor	Pass
1222T-05	Work Area - Basketball stage area	Pass
1222T-06	Work Area - Door to stairwell at end of lower corridor	Pass

Bulk Suspect Flooring Glue tests at Pavilion Stairwell: 6 total tests:

December 22, 2005:

A-01	Stair mastic, brown mixture, top landing	None detected
A-02	Stair mastic, brown mixture, random stair	None Detected
A-03	Stair mastic, random stair, stair mixture	None Detected
A-03L-2	Layer #2 mastic	None Detected
A-04	Stair Mastic, random stair, stair mixture	None Detected
A-05	Stiar Mastic, random mixture,	None Detected

Laboratory Analytical Methods

PLM - Bulk Sample Analysis (Polarized Light Microscopy):
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Bulk material samples were analyzed using dispersion staining techniques in accordance with the 40 CFR, Part 763, Appendix A, Subpart F, AHERA regulations.

PCM - Air Analysis (Phase Contrast Microscopy):
The air samples were analyzed for airborne fibers by a regular light microscope per NIOSH Method 7400 A (as applicable).

TEM - Air Analysis (Transmission Electron Microscopy):
The air samples were analyzed for airborne asbestos by a Transmission Electron Microscope per AHERA methods.

Sample ID #	Location/Description	Result Summary
======	===========	========
PAVILION STAIRS FLOORING AREA		
Thursday, Dec 22, 2005		
1222-1	Stage Corridor Entry area	Pass
1222-2	Stage exit area	Pass
1222-3	Decon Clean Room	Pass
1222-4	Middle Stage Corridor area	Pass
1222-5	Blank Zefon Lot #11292	Pass
1222-6	Stage corridor exit area	Pass
1222-7	Stage exit area	Pass
1222-8	Decon Clean Room	Pass
1222-9	Middle stage corridor area	Pass
1222-10	Stage Corridor Entry area	Pass
1222-11	Stage exit area	Pass
1222-12	Decon Clean Room	Pass
1222-13	Middle of corrdior area	Pass

Contractors abated ACMs and finished by 3pm December 22, 2005.

Laboratory Analytical Methods

PLM - Bulk Sample Analysis (Polarized Light Microscopy):
The bulk material samples were submitted to an accredited laboratory in California.
Bulk material samples were analyzed using dispersion staining techniques in accordance with the 40 CFR, Part 763, Appendix A, Subpart F, AHERA regulations.

PCM - Air Analysis (Phase Contrast Microscopy):
The air samples were analyzed for airborne fibers by a regular light microscope per NIOSH Method 7400 A (as applicable).

TEM - Air Analysis (Transmission Electron Microscopy):
The air samples were analyzed for airborne asbestos by a Transmission Electron Microscope per AHERA methods.

Sample ID #	Location/Description	Result Summary
======	===========	========
LOWER SCHOOL ASSEMBLY ROOM AREA		
Thursday - -December 22, 2005		
22-01	**Lower School Assembly Boiler room**	**Pass**
22-02	**Lower School Assembly Room**	**Pass**
22-03	**Lower School Assembly Kindergarten Room**	**Pass**
22-04	**Blank - Zefon lot #11292**	**0**
22-05	**Blank - Zefon Lot #11292**	**0**
Lower School Assembly Room Area		
Background Air Tests		
Thursday, December 22, 2005		
AR-1	**Boiler Room adjacent to Assembly Room**	**pass**
AR-2	**Assembly Room**	**Pass**
AR-3	**Kindergarten Rooms adjacent to Boiler Room**	**pass**
Main Campus Administration Building		
Friday - - December 23, 2005		
X-01	Elevator Admin Bldg Floor Linoleum	none detected

Laboratory Analytical Methods

PLM - Bulk Sample Analysis (Polarized Light Microscopy):
The bulk material samples were submitted to an accredited laboratory in California.
Bulk material samples were analyzed using dispersion staining techniques in accordance with the 40 CFR, Part 763, Appendix A, Subpart F, AHERA regulations.

PCM - Air Analysis (Phase Contrast Microscopy):
The air samples were analyzed for airborne fibers by a regular light microscope per NIOSH Method 7400 A (as applicable).

TEM - Air Analysis (Transmission Electron Microscopy):
The air samples were analyzed for airborne asbestos by a Transmission Electron Microscope per AHERA methods.

Sample ID #	Location/Description	Result Summary
======	===========	========
PAVILION STAIRS FLOORING AREA		
Friday, December 23, 2005		
AHERA CLEARANCE TESTING Post Mastic Abatement:		
1223T-01	Pavilion Stairwell up to Mech Room @ top landing	pass
1223T-02	Pavilion Stairwell up to Mech Room @ top stairs	pass
1223T-03	Pavilion Stairwell up to Mech Room @ middle stairs	pass
1223T-04	Pavilion Stairwell up to Mech Room @ base of stairs	pass

Main Campus Administration Building
O&M Cleaning of Basement Mechanical Room
Friday, December 23, 2005

1223-1	Basement at hallway at Mech room	Pass
1223-2	Basement at middle hallway at Mech room	Pass
1223-3	Basement at Mech Room at Stairs (Neg air exhaust area)	Pass
1223-4	Blank - Zef lot #11292	0

Laboratory Analytical Methods

PLM - Bulk Sample Analysis (Polarized Light Microscopy):
The bulk material samples were submitted to an accredited laboratory in California.
Bulk material samples were analyzed using dispersion staining techniques in accordance with the 40 CFR, Part 763, Appendix A, Subpart F, AHERA regulations.

PCM - Air Analysis (Phase Contrast Microscopy):
The air samples were analyzed for airborne fibers by a regular light microscope per NIOSH Method 7400 A (as applicable).

TEM - Air Analysis (Transmission Electron Microscopy):
The air samples were analyzed for airborne asbestos by a Transmission Electron Microscope per AHERA methods.

Sample ID #	Location/Description	Result Summary
======	==================	========
Main Campus Mechanical Room - Basement		
O & M Cleaning of Mech Room		
Tuesday, December 27, 2005		
1227-1	Outside - ambient air at stairs near elevator entry	pass
1227-2	Inside- Top of stairs at elevator	Pass
1227-3	Inside-Top of stairs at Headmaster office hjall	pass
1227-4	Inside- Neg Air exhaust near tube	Pass
1227-5	Inside-Decon Dirty room	Pass
1227-6	Inside-Basement hallway near decon unit	Pass
1227-7	Inside-Basement area at elevator	Pass
1227-8	Outside - ambient air at stairs near elevator entry	pass
1227-9	Inside- Top of stairs at elevator	Pass
1227-10	Inside-Top of stairs at Headmaster office hjall	pass
1227-11	Inside- Neg Air exhaust near tube	Pass
1227-12	Inside-Decon Dirty room	Pass
1227-13	Inside-Basement hallway near decon unit	Pass
1227-14	Inside-Basement area at elevator	Pass
1227-15	Blank - Zefon lot #11292	0
1227-16	Blank - Zefon lot #11292	0
1227-17	Basement near decon	Pass
1227-18	Hallway near decon	Pass

90512162З-

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

RUSH

Client: The Buckley School Date THURS 22DEC05 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area:

24 HR

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

PLMS

Sample ID	Sample Description/Location/Condition of Material
1 A-01	STAIR MASTIC @ TOP LANDING
2 A-02	@ random stair
3 A-03	@
4 A-04	@
5 A-05	@ random stair
6	
7	
8	Pavilion stair mastic req'd tests
9	since previous consultant did not
10	test mastics.
11	
12	Black mastic found at base
13	of stairs.
14	
15	
16	
17	
18	

Brown Glue

Relinquished by/Date: K Medici

Received by / Date: [signature] 12/23/05 @ 06:00

Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+
+ AA flame for lead
+

24 HR

AmeriSci

AmeriSci Los Angeles
24416 SOUTH MAIN STREET • SUITE 308
CARSON, CA 90745
TEL: (310) 834-4868 • FAX: (310) 834-4772

PLM Bulk Asbestos Report

Applied Toxicology
Attn: Kenneth Medici
1450 North Santa Fe Avenue
PMB #144
Vista, CA 92083

Date Received 12/23/05
Date Examined 12/23/05

AmeriSci Job No. 905121623
P.O. # The Buckley School
Page 1 **of** 2

RE The Buckley School; Sherman Oaks Campus / Sample ID's A-01 Through A-05

Client No. / HGA	Lab No.	Asbestos Present	Total % Asbestos
A-01	905121623-01	*No*	NAD

Location: Stair Mastic @ Top Landing/Brown Glue

Description: Brown, Heterogeneous, Non-Fibrous, Bulk Material
Asbestos Types:
Other Material: Non-fibrous 100. %

A-02	905121623-02	*No*	NAD

Location: Stair Mastic @ Random Stair/Brown Glue

Description: Brown, Heterogeneous, Non-Fibrous, Bulk Material
Asbestos Types:
Other Material: Non-fibrous 100. %

A-03	905121623-03L1	*No*	NAD

Location: Stair Mastic @ Random Stair/Brown Glue

Description: Brown, Heterogeneous, Non-Fibrous, Mastic
Asbestos Types:
Other Material: Non-fibrous 100. %

A-03	905121623-03L2	*No*	NAD

Location: Stair Mastic @ Random Stair/Brown Glue

Description: White, Heterogeneous, Non-Fibrous, Joint Compound
Asbestos Types:
Other Material: Non-fibrous 100. %

A-04	905121623-04	*No*	NAD

Location: Stair Mastic @ Random Stair/Brown Glue

Description: Brown, Heterogeneous, Non-Fibrous, Bulk Material
Asbestos Types:
Other Material: Non-fibrous 100. %

AMERI SCI

AmeriSci Los Angeles
24416 SOUTH MAIN STREET • SUITE 308
CARSON, CA 90745
TEL: (310) 834-4868 • FAX: (310) 834-4772

PLM Bulk Asbestos Report

Applied Toxicology
Attn: Kenneth Medici
1450 North Santa Fe Avenue
PMB #144
Vista, CA 92083

Date Received 12/23/05
Date Examined 12/23/05

AmeriSci Job No. 905121623
P.O. # The Buckley School
Page 2 **of** 2

RE The Buckley School; Sherman Oaks Campus / Sample ID's A-01 Through A-05

Client No. / HGA	Lab No.	Asbestos Present	Total % Asbestos
A-05	905121623-05	*No*	NAD

Location: Stair Mastic @ Random Stair/Brown Glue

Description: Brown, Heterogeneous, Non-Fibrous, Bulk Material
Asbestos Types:
Other Material: Non-fibrous 100. %

Reporting Notes:
Analyzed By: David G. Baseman David Baseman; Date Analyzed: <Date Examined> 12/23/05
*NAD = no asbestos detected; Detection Limit <1%; Reporting Limits: CVES = 1%, 400 Pt Ct = 0.25%, 1000 Pt Ct = 0.1%; "Present" or "NVA" = "No Visible Asbestos" are observations made during a qualitative analysis; NA = not analyzed; NA/PS = not analyzed / positive stop; PLM Bulk Asbestos Analysis by EPA 600/M4-82-020 per 40 CFR 763 (NVLAP Lab #200346-0, CA ELAP lab #2322); Note: PLM is not consistently reliable in detecting asbestos in floor coverings and similar NOB materials. TEM is currently the only method that can be used to determine if this material can be considered or treated as non-asbestos-containing in New York State (also see EPA Advisory for floor tile, FR 59, 146, 38970, 8/1/94). NIST Accreditation requirements mandate that this report must not be reproduced except in full without the approval of the laboratory. This PLM report relates ONLY to the items tested.
Reviewed By: JPA 12/23/05

90512161O

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date THURS 22 DEC 05 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area: LOWR SCHOOL ASSEMBLY ROOM

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

TEM

Sample ID	Sample Description/Location/Condition of Material
1 AR-01	BOILER ROOM
2 AR-02	ASSEMBLY ROOM
3 AR-03	KINDERGARTEN ROOM
4	
5	
6	
7	BACKGROUND AIR TESTS
8	
9	Fresh Air plans to clean attic
10	boards and encap.
11	
12	
13	
14	
15	
16	
17	
18	

10^{03} AM / 11^{08} AM
F = 10 LPM
Vol =

Relinquished by/Date: [signature]

Received by / Date: [signature] 12/23/05 @ 06:00

+ Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+
+ AA flame for lead
+

AHERA
24 HR

AmeriSci Job #: **905121610**
Client Name: Applied Toxicology

Table I

Summary of Transmission Electron Microscopy (TEM) Results for Asbestos (air)

The Buckley school; Sherman Oaks Campus / Lower School Assembly Room

AmeriSci Sample #	Client Sample #	Dilution Factor	Air Filtered (liters)	Area Analyzed (sq. mm.)	* Analytical Sensitivity (struc/cc air)	Asbestos Structures Detected (Microns) 0.5-5.0	>=5.0	Total	Structure Density (struc/sq. mm.) >=5.0	Total	Structure Concentration (struc/cc air) >=5.0	Total	Type of Asbestos
01 inside	AR-01 Boiler Room		650	.100	0.0059	0.0	0.0	0.0	<10	<10	<0.0059	<0.0059	NSD
02 inside	AR-02 Assembly Room		650	.100	0.0059	0.0	0.0	0.0	<10	<10	<0.0059	<0.0059	NSD
03 inside	AR-03 Kindergarten Room		650	.100	0.0059	0.0	0.0	0.0	<10	<10	<0.0059	<0.0059	NSD

* concentration represented by the detection of 1 structure
** not analyzed
NSD: No Asbestos Structures Detected

Reviewed By: ____________________ ; Analyzed By: Javier Cortes Date: 12/23/2005

NVLAP#: 200346-0

905121611

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date 22 DEC 05 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area: PAVILION STAIRS (TO UPPR MECH RM)

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

	Sample ID	Sample Description/Location/Condition of Material	
1	1222T-01	BASE OF STAIRS	23 / 43 6 AM / 8 AM
2	1222T-02	MIDDLE STAIRS	
3	1222T-03	TOP OF STAIRS	F = 10 LPM
4	1222T-04	STAGE CORRIDOR	Vol =
5	1222T-05	BASKETBALL/STAGE AREA	
6	122T-06	DOOR TO STAIRWELL @ STAGE	
7	BACKGROUND TESTS		
8			
9	Stairwell Tile/MASTIC ACMS are		
10	planned for abatement.		
11			
12	Condition of stairs = poor.		
13	Holes and overall deterioration		
14	of stairwell materials noted.		
15			
16			
17			
18			

Relinquished by/Date: [signature] 12/22/05

Received by / Date: [signature] 12/23/05 @ 06:09

Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+ AA flame for lead

24 HR

AmeriSci Job #: **905121611**
Client Name: Applied Toxicology

Table I

Summary of Transmission Electron Microscopy (TEM) Results for Asbestos (air)

The Buckly School; Sherman Oaks Campus / Pavilion Stairs (To Upper Mech Rm)

AmeriSci Sample #	Client Sample #	Dilution Factor	Air Filtered (liters)	Area Analyzed (sq. mm.)	* Analytical Sensitivity (struc/cc air)	Asbestos Structures Detected (Microns) 0.5-5.0	>=5.0	Total	Structure Density (struc/sq. mm.) >=5.0	Total	Structure Concentration (struc/cc air) >=5.0	Total	Type of Asbestos
01 inside	1222T-01 Base Of Stairs		1400	.060	0.0046	0.0	0.0	0.0	<16.6	<16.6	<0.0046	<0.0046	NSD
02 inside	1222T-02 Middle Stairs		1400	.060	0.0046	0.0	0.0	0.0	<16.6	<16.6	<0.0046	<0.0046	NSD
03 inside	1222T-03 Top Of Stairs		1400	.060	0.0046	0.0	0.0	0.0	<16.6	<16.6	<0.0046	<0.0046	NSD
04 inside	1222T-04 Stage Corridor		1400	.060	0.0046	0.0	0.0	0.0	<16.6	<16.6	<0.0046	<0.0046	NSD
05 inside	1222T-05 Basket Ball / Stage Area		1400	.060	0.0046	0.0	0.0	0.0	<16.6	<16.6	<0.0046	<0.0046	NSD
06 inside	1222T-06 Door To Stairwell @ Stage		1400	.060	0.0046	0.0	0.0	0.0	<16.6	<16.6	<0.0046	<0.0046	NSD

* concentration represented by the detection of 1 structure
** not analyzed
NSD: No Asbestos Structures Detected

Reviewed By: ______________________ ; Analyzed By: Javier Cortes   Date: 12/23/2005

NVLAP#: 200346-0

905121625-

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date THURS 22 DEC 05 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area:

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

PCM

Sample ID	Sample Description/Location/Condition of Material	
1 1222-1	STAGE CORRIDOR ENTRY	9^{08}AM/11^{08}
2 1222-2	STAGE EXIT	F=10LPM
3 1222-3	DECON CLEAN RM	V=1200L
4 1222-4	MIDDLE STAGE CORRIDOR	
5 1222-5	BLANK Zefon lot #11292	
6 1222-6	STAGE CORRIDOR ENTRY	11^{08}Am/1^{08}pm
7 1222-7	STAGE EXIT	F=10LPM
8 1222-8	DECON CLEAN RM	V=1200L
9 1222-9	MIDDLE STAGE CORRIDOR	
10 1222-10	STAGE CORRIDOR ENTRY	108pm/3^{08}pm
11 1222-11	STAGE EXIT	10LPM
12 1222-12	DECON CLEAN RM	V=1200L
13 1222-13	MIDDLE STAGE CORRIDOR	
14		
15	Contractors abated ACMs 10:30Am-3pm.	
16	Encap @ 3pm.	
17		
18		

Relinquished by/Date: [signature]

Notes:
Asbestos or Lead:
PCM/ TEM PLM
AA flame for lead

24HR

Received by / Date: [signature] 12/23/05 @ 06:00

AmeriSci Job #: 905121625
Client Name: Applied Toxicology

Phase Contrast Microscopy (PCM) Fiber Results

The Buckley School; Sherman Oaks Campus / Sample ID's 1222-1 Through 1222-13

AmeriSci Sample #	Client Sample # / Location	Date Collected	Flow Rate (liters/min.)	Duration (min.)	Air Filtered (liters)	Fields	Fibers	Fiber Density (Fibers/mm ^{2})	Fibers Conc. (Fibers/cc)	TWA
01	1222-1 Stage Corridor Entry	12/22/2005	10	120	1200	100	41	52.23	0.017	
02	1222-2 Stage Exit	12/22/2005	10	120	1200	92	101	139.85	0.045	
03	1222-3 Decon Clean Rm	12/22/2005	10	120	1200	100	36	45.86	0.015	
04	1222-4 Middle Stage Corridor	12/22/2005	10	120	1200	90	103	145.79	0.047	
05	1222-5 Blank Zefon Lot #11292	12/22/2005	0	0	0	100	0	ND	Footnotes: /	
06	1222-6 Stage Corridor Entry	12/22/2005	10	120	1200	100	21	26.75	0.009	
07	1222-7 Stage Exit	12/22/2005	10	120	1200	100	10	12.74	0.004	
08	1222-8 Decon Clean Rm	12/22/2005	10	120	1200	100	20	25.48	0.008	
09	1222-9 Middle Stage Corridor	12/22/2005	10	120	1200	100	12	15.29	0.005	
10	1222-10 Stage Corridor Entry	12/22/2005	10	120	1200	100	7	8.92	0.003	
11	1222-11 Stage Exit	12/22/2005	10	120	1200	100	5	6.37	< 0.002	
12	1222-12 Decon Clean Rm	12/22/2005	10	120	1200	100	6	7.64	0.002	

See Reporting notes on last page

AmeriSci Job #: 905121625

Client Name: Applied Toxicology

Phase Contrast Microscopy (PCM) Fiber Results

The Buckley School; Sherman Oaks Campus / Sample ID's 1222-1 Through 1222-13

AmeriSci Sample #	Client Sample # / Location	Date Collected	Flow Rate (liters/min.)	Duration (min.)	Air Filtered (liters)	Fields	Fibers	Fiber Density (Fibers/mm^2)	Fibers Conc. (Fibers/cc)	TWA
13	1222-13 Middle Stage Corridor	12/22/2005	10	120	1200	100	9	11.46	0.004	

Reporting Notes:

(1) Fibers/cc cannot be calculated for samples (or blanks) with no air volume.

Analyzed By: Javier Cortes ____________; Date Analyzed: 12/24/2005

Samples analyzed by NIOSH 7400(A) METHOD, Issue #2, 8/15/94; Limit of Detection = 5.5 fibers per 100 fields or 7 fibers / mm2; This report relates ONLY to the sample analysis expressed as fibers/sq mm of filter area; ND = no fibers observed; NA = Not Analyzed; Walton - Beckett gradicule field area 0.00785 mm2; Duration in minutes; TWA = 8Hr TWA, calculation assumes zero exposure for remainder of 8 hour period not sampled; Upper 95% Confidence Limit (Employer's Compliance Test) - Calculated as a one sided UCL to determine 95% certainty of compliance with the 0.01 fiber/cc standard; Estimated relative standard deviation: Intralab Sr = 0.405, Interlab Sr = 0.45.

Reviewed By: ____________

905121624-

Kenneth Medici, CAC #92-0007 **1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083**
Fax: (760).414-1183 **Office: 1-888-999-7908 Toll-Free**

Client: The Buckley School Date 22 DEC 05 THURS Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area:

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

PCM
2 pm 04 / 4pm 04
10 LPM
V=

Sample ID	***Sample Description/Location/Condition of Material***
1 22-01	Lwr School - Boiler Rm @ Assmbly Hall
2 22-02	Lwr School - Assmbly Room
3 22-03	Lwr School - Kindergarten
4 22-04	BLANK Zefon lot #11292
5 22-05	BLANK Zefon lot # 11292
6	
7	
8	
9	
10	
11	
12	
13	
14	
15	
16	
17	
18	

Relinquished by/Date:

Received by / Date: 12/23/05 @ 06:00

Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+
+ AA flame for lead
+

24 HR

AmeriSci Job #: 905121624

Client Name: Applied Toxicology

Phase Contrast Microscopy (PCM) Fiber Results

The Buckley School; Sherman Oaks Campus / Sample ID's 22-04 Through 22-05

AmeriSci Sample #	Client Sample # / Location	Date Collected	Flow Rate (liters/min.)	Duration (min.)	Air Filtered (liters)	Fields	Fibers	Fiber Density (Fibers/mm ^{2})	Fibers Conc. (Fibers/cc)	TWA
01	22-01 Lwn School-Boiler Rm @ Assembly Hall	12/22/2005	10	120	1200	100	16	20.38	0.007	
02	22-02 Lwn School-Assembly Room	12/22/2005	10	120	1200	100	4	5.10	< 0.002	
03	22-03 Lwn School-Kindergarden	12/22/2005	10	120	1200	100	10	12.74	0.004	
04	22-04 Blank Zefon Lot #11292	12/22/2005	0	0	0	100	4	5.10	Footnotes: 1	
05	22-05 Blank Zefon Lot #11292	12/22/2005	0	0	0	100	1	1.27	Footnotes: 1	

Reporting Notes:

(1) Fibers/cc cannot be calculated for samples (or blanks) with no air volume.

Analyzed By: Javier Cortes ________; Date Analyzed: 12/24/2005

Samples analyzed by NIOSH 7400(A) METHOD, Issue #2, 8/15/94; Limit of Detection = 5.5 fibers per 100 fields or 7 fibers / mm2; This report relates ONLY to the sample analysis expressed as fibers/sq mm of filter area; ND = no fibers observed; NA = Not Analyzed; Walton - Beckett gradicule field area 0.00785 mm2; Duration in minutes; TWA = 8Hr TWA, calculation assumes zero exposure for remainder of 8 hour period not sampled; Upper 95% Confidence Limit (Employer's Compliance Test) - Calculated as a one-sided UCL to determine 95% certainty of compliance with the 0.01 fiber/cc standard; Estimated relative standard deviation: Intralab Sr = 0.405, Interlab Sr = 0.45.

Reviewed By: ________

905121650

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date FRI 23 DEC 05 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area: ADMIN BLDG

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

Sample ID	*Sample Description/Location/Condition of Material*
1 X-01	LINO - ADMIN BLDG
2	* Elevator Floor
3	
4	
5	
6	
7	
8	
9	
10 * Note:	
11	THIS FLOOR HAS BEEN
12	ABATED. IT APPEARS
13	THE NEW LINO IS ACM
14	X-01 WILL TEST THIS PAcM.
15	
16	
17	
18	

Relinquished by/Date: [signature]

Received by / Date: KAullano @0903 12/24/05

Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+
+ AA flame for lead
+

48HR

AMERI SCI

AmeriSci Los Angeles
24416 SOUTH MAIN STREET • SUITE 308
CARSON, CA 90745
TEL: (310) 834-4868 • FAX: (310) 834-4772

PLM Bulk Asbestos Report

Applied Toxicology
Attn: Kenneth Medici
1450 North Santa Fe Avenue
PMB #144
Vista, CA 92083

Date Received 12/24/05
Date Examined 12/27/05

AmeriSci Job No. 905121650
P.O. # The Buckley School
Page 1 **of** 1

RE The Buckley School; Sherman Oaks Campus Admin Bldg.

Client No. / HGA	Lab No.	Asbestos Present	Total % Asbestos
X-01	905121650-01	*No*	NAD

Location: Lino. -Admin Bldg. Elevator Floor

Description: Beige, Heterogeneous, Fibrous, Bulk Material
Asbestos Types:
Other Material: Cellulose 22. %, Fibrous glass 3. %, Non-fibrous 75. %

Reporting Notes:

Analyzed By: David G. Baseman ; Date Analyzed: <Date Examined> 12/27/05
*NAD = no asbestos detected; Detection Limit <1%; Reporting Limits: CVES = 1%, 400 Pt Ct = 0.25%, 1000 Pt Ct = 0.1%; "Present" or "NVA" = "No Visible Asbestos" are observations made during a qualitative analysis; NA = not analyzed; NA/PS = not analyzed / positive stop; PLM Bulk Asbestos Analysis by EPA 600/M4-82-020 per 40 CFR 763 (NVLAP Lab #200346-0, CA ELAP lab #2322); Note: PLM is not consistently reliable in detecting asbestos in floor coverings and similar NOB materials. TEM is currently the only method that can be used to determine if this material can be considered or treated as non-asbestos-containing in New York State (also see EPA Advisory for floor tile, FR 59, 146, 38970, 8/1/94). NIST Accreditation requirements mandate that this report must not be reproduced except in full without the approval of the laboratory. This PLM report relates ONLY to the items tested.
Reviewed By: ____________________

905121648

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 FRIDAY Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date 23 DEC 2005 Sampler: K. Medici, CAC #92-0007 TEM 24 HR AHERA
Site Address: Sherman Oaks Campus Site area: PAVILION

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

Sample ID	*Sample Description/Location/Condition of Material*
1 1223T-01	PAVILION - STAIRWELL TO UPPER MECH ROOM
2 1223T-02	PAVILION -
3 1223T-03	PAVILION -
4 1223T-04	PAVILION - DECON @ Base of STAIRS
5	7²³ AM / 9²³ AM Vol = 1200L
6	F = 10 LPM
7	AHERA CLEARANCE
8	FOLLOWING FLOORING ABATEMT.
9	
10	
11	
12	
13	
14	
15	
16	
17	
18	

Relinquished by/Date: K. Medici

Received by / Date:

Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+
+ AA flame for lead
+

24 HR

AmeriSci Job #: **905121648**
Client Name: .Applied Toxicology

Table I

Summary of Transmission Electron Microscopy (TEM) Results for Asbestos (air)

1223T-

AmeriSci Sample #	Client Sample #	Dilution Factor	Air Filtered (liters)	Area Analyzed (sq. mm.)	* Analytical Sensitivity (struc/cc air)	Asbestos Structures Detected (Microns) 0.5-5.0	>=5.0	Total	Structure Density (struc/sq. mm.) >=5.0	Total	Structure Concentration (struc/cc air) >=5.0	Total	Type of Asbestos
01	1223T-01 Pavilion Stairwell To Upper Mech Room		1200	.060	0.0053	0.0	0.0	0.0	<16.6	<16.6	<0.0053	<0.0053	NSD
02	1223T-02 Pavilion Stairwell To Upper Mech Room		1200	.060	0.0053	0.0	0.0	0.0	<16.6	<16.6	<0.0053	<0.0053	NSD
03	1223T-03 Pavilion Stairwell To Upper Mech Room		1200	.060	0.0053	0.0	0.0	0.0	<16.6	<16.6	<0.0053	<0.0053	NSD
04	1223T-04 Pavilion Decon @ Base Of Stairs		1200	.060	0.0053	0.0	0.0	0.0	<16.6	<16.6	<0.0053	<0.0053	NSD

* concentration represented by the detection of 1 structure
** not analyzed
NSD: No Asbestos Structures Detected

Reviewed By: ______________________ ; Analyzed By: Rory S. Tabatt Date: 12/24/2005

Rory S. Tabatt

NVLAP#: 200346-0

905121649-

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 FRIDAY Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date 23 DEC 2005 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area: ~~(illegible)~~ ADMIN BLDG

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

	Sample ID	***Sample Description/Location/Condition of Material***
1	1223-1	Basemt OUTSIDE MECH RM 05/05
2	1223-2	" " 9AM / 11AM
3	1223-3	@ STAIRS 10LPM
4	1223-4	BLANK lot 11292
5		
6		
7		
8		
9		
10		
11		
12		
13		
14		
15		
16		
17		
18		

Relinquished by/Date: K Medici

Received by / Date: KAulliano @ L903 12/24/05

Notes:
+ Asbestos or Lead:
+ PCM TEM PLM
+ AA flame for lead
+

24HR PCM

AmeriSci Job #: 905121649

Client Name: Applied Toxicology

Phase Contrast Microscopy (PCM) Fiber Results

The Buckley School; Sherman Oaks Campus Admin Bldg.

AmeriSci Sample #	Client Sample # / Location	Date Collected	Flow Rate (liters/min.)	Duration (min.)	Air Filtered (liters)	Fields	Fibers	Fiber Density (Fibers/mm ^{2})	Fibers Conc. (Fibers/cc)	TWA
01	1223-1 Basemt Outside Mech. Rm.	12/23/2005	10	120	1200	100	7	8.92	0.003	
02	1223-2 Basemt Outside Mech. Rm.	12/23/2005	10	120	1200	100	6	7.64	0.002	
03	1223-3 Basemt Outside Mech. Rm.	12/23/2005	10	120	1200	100	9	11.46	0.004	
04	1223-4 Blank Lot 11292	12/23/2005	10	120	1200	100	1	1.27	< 0.002	

Reporting Notes:

Footnotes: 1

(1) Fibers/cc cannot be calculated for samples (or blanks) with no air volume.

Analyzed By: Karrie Chan ______________________; Date Analyzed: 12/26/2005

Samples analyzed by NIOSH 7400(A) METHOD, Issue #2, 8/15/94; Limit of Detection = 5.5 fibers per 100 fields or 7 fibers / mm2; This report relates ONLY to the sample analysis expressed as fibers/sq mm of filter area; ND = no fibers observed; NA = Not Analyzed; Walton - Beckett gradicule field area 0.00785 mm2; Duration in minutes; TWA = 8Hr TWA, calculation assumes zero exposure for remainder of 8 hour period not sampled; Upper 95% Confidence Limit (Employer's Compliance Test) - Calculated as a one sided UCL to determine 95% certainty of compliance with the 0.01 fiber/cc standard; Estimated relative standard deviation: Intralab Sr = 0.405, Interlab Sr = 0.45.

Reviewed By: ______________________

105121507

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

TUES

Client: The Buckley School Date 27 DEC 2005 Sampler: K. Medici, CAC #92-0007
Site Address: Sherman Oaks Campus Site area:

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

ADMIN BLDG - M.R. AHERA CLEANING

Sample ID	Sample Description/Location/Condition of Material	@ 10 LPM:
1 1227-01	Outside Ambient. @ Admin Entry	6:53 AM / 9:01 AM Vol=
2 1227-02	Inside - @ Top of STAIRS @ elevator	
3 1227-03	Inside @ Top of STAIRS @ Headmaster office	
4 1227-04	Inside @ Neg Air Exhaust near -03	
5 1227-05	Inside - @ Decon Dirty Room	
6 1227-06	Inside @ Basement Hallway	
7 1227-07	Inside @ Basement Elevator	
8 1227-08	@ -01	9:05 AM / 11:08 AM Vol=
9 1227-09	@ -02	
10 1227-10	@ -03	
11 1227-11	@ -04	
12 1227-12	@ -05	
13 1227-13	@ -06	
14 1227-14	@ -07	
15 1227-15	Blank Zefon 11292	
16 1227-16	Blank Zefon 11292	
17 1227-17	Near Decon	11:08 AM / 1:10 PM Vol=
18 1227-18	Near Neg Air Exhaust STAIRS	
19 1227-19	Hallway near Decon	

RECEIVED DEC 29 2005 By: PL

Relinquished by/Date: K Medici

Notes:
Asbestos or Lead:
PCM TEM PLM
AA flame for lead

PCM 24HR

Received by / Date:

CONTRACTORS WET-WIPING & HEPA VAC
ADMIN BUILDING MECHANICAL ROOM.

105121507

Kenneth Medici, CAC #92-0007 1450 North Santa Fe Ave, Suite #C PMB #144 Vista, CA 92083
Fax: (760).414-1183 TUES Office: 1-888-999-7908 Toll-Free

Client: The Buckley School Date 27 DEC 05 Sampler: K. Medici, CAC #92-0007 24HR
Site Address: Sherman Oaks Campus Site area: TEM AHERA

FIELD DATA AND CHAIN OF CUSTODY FORM

Please fax lab results to 760.414-1183; call Ken Medici with verbal results at 760-212-8857 and return original chain of custody to Ken Medici at above address. Your laboratory must be NVLAP certified as applicable to complete this work (asbestos, lead or other). If your laboratory is not certified please stop and call Ken Medici at phone #760-212-8857.

Sample ID	***Sample Description/Location/Condition of Material***
1	After PCM analyses please
2	
3	run AHERA TEM's on
4	samples
5	
6	#1227-05
7	#1227-12 TEM also
8	#1227-19
9	
10	
11	
12	
13	
14	
15	RECEIVED
16	DEC 29 2005
17	By
18	

Relinquished by/Date: 12/28/05

Received by / Date:

+ *Notes:*
+ Asbestos or Lead:
+ PCM TEM PLM
+
+ AA flame for lead
+

AHERA 24HR

AmeriSci Job #: **105121507**

Client Name: Applied Toxicology

Phase Contrast Microscopy (PCM) Fiber Results

CAC#92-0007; The Buckley School; 12/27/2005; 1227-01 thru 1227-19; The Buckley School

AmeriSci Sample #	Client Sample # / Location	Date Collected	Flow Rate (liters/min.)	Duration (min.)	Air Filtered (liters)	Fields	Fibers	Fiber Density (Fibers/mm ^{2})	Fibers Conc. (Fibers/cc)	TWA
01	1227-01 Outside Ambient At Admin Entry	12/27/2005	10	127	1270	100	1	1.27	< 0.002	
02	1227-02 Inside At Top Of Stairs At Elevator	12/27/2005	10	127	1270	100	4.5	5.73	< 0.002	
03	1227-03 Inside At Top Of Stairs At Head Master Office	12/27/2005	10	127	1270	100	4	5.10	< 0.002	
04	1227-04 Inside At Neg Air Exhaust Near-03	12/27/2005	10	127	1270	100	2.5	3.18	< 0.002	
05	1227-05 Inside At Decon Dirty Room	12/27/2005	10	127	1270	100	3.5	4.46	< 0.002	
06	1227-06 Inside At Basement Hallway	12/27/2005	10	127	1270	100	13.5	17.20	0.005	
07	1227-07 Inside At Basement Elevator	12/27/2005	10	127	1270	100	12	15.29	0.005	
08	1227-08 At 01	12/27/2005	10	123	1230	100	1.5	1.91	< 0.002	
09	1227-09 At 02	12/27/2005	10	123	1230	100	11.5	14.65	0.005	
10	1227-10 At 03	12/27/2005	10	123	1230	100	9	11.46	0.004	
11	1227-11 At 04	12/27/2005	10	123	1230	100	3	3.82	< 0.002	
12	1227-12 At 05	12/27/2005	10	123	1230	100	3	3.82	< 0.000	
13	1227-13 At 06	12/27/2005	10	123	1230	100	6.5	8.28	0.000	
14	1227-14 At 07	12/27/2005	10	123	1230	100	11.5	14.65	0.000	
15	1227-15 Blank Zefon 11292	12/27/2005	0	0	0	100	0	ND		

See Reporting notes on last page

AmeriSci Job #: 105121507

Client Name: Applied Toxicology

Phase Contrast Microscopy (PCM) Fiber Results

CAC#92-0007; The Buckley School; 12/27/2005; 1227-01 thru 1227-19; The Buckley School

AmeriSci Sample #	Client Sample # / Location	Date Collected	Flow Rate (liters/min.)	Duration (min.)	Air Filtered (liters)	Fields	Fibers	Fiber Density (Fibers/mm^2)	Fibers Conc. (Fibers/cc)	TWA
16	1227-16 Blank Zefon 11292	12/27/2005	0	0	0	100	0	ND		
17	1227-17 Near Decon	12/27/2005	10	122	1220	100	6.5	8.28	0.000	
18	1227-18 Near Neg Air Exhaust Stairs	12/27/2005	10	122	1220	100	5.5	7.01	0.000	
19	1227-19 Hallway Near Decon	12/27/2005	10	122	1220	100	6	7.64	0.000	

Reporting Notes:

Reviewed by: ______________________; Analyzed by: Rebekah J. Swanson ______________________, Date Analyzed: 12/29/2005

Samples analyzed by NIOSH 7400(A) METHOD, Issue #2, 8/15/94; Limit of Detection = 5.5 fibers per 100 fields or 7 fibers / mm2; This report relates ONLY to the sample analysis expressed as fibers/sq mm of filter area; ND = no fibers observed; NA = Not Analyzed; Walton - Beckett graticule field area 0.00785 mm2; Duration in minutes; TWA = 8Hr TWA calculation assumes zero exposure for remainder of 8 hour period not sampled; Upper 95% Confidence Limit (Employer's Compliance Test) - Calculated as a one sided UCL to determine 95% certainty of compliance with the 0.01 fiber/cc standard; Estimated relative standard deviation: Intralab Sr = 1.354, Interlab Sr = 14.688. , NYSDOH ELAP Lab#10984

The Buckley School

3-year AHERA Re-inspection for Asbestos — 27December2005
Inspector: Ken Medici, CAC #92-0007 -Phone 1-888-999-7908 — Tuesday, 1:00pm-3pm

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Previous Re-Inspection: 23Dec03 by K. Medici. Areas inspected include all areas of the school accessible at time of survey. Most attic areas were not inspected thoroughly because the original Asbestos Management plan determined that these areas were off limits until proper assessment methods could be performed to determine safety.

The site was inspected on Tuesday, December 27, 2005 between the hours of 1pm and 3 pm by Ken Medici an AHERA Accredited Building Inspector and Management Planner.

FIELDHOUSE

Ceiling material was found to be water damaged in selected areas. Discolorations and warping could best describe the surface appearances. Locations included the Boys locker room and girls locker room approx 30 sq ft may be affected. Attic areas were assumed contaminated with asbestos.

LOWER SCIENCE BUILDING ROOMS #115

Mechanical Room #1:	Plaster wall damage, delamination approx 2 sq ft (Elbows assumed ACM)
Mechanical Room #2:	Same as #1
Room #115:	Flooring is black mastic only - no floor covering to protect mastic - approx 200sq ft

UPPER SCHOOL AREAS & ROBERT YOUNG LIBRARY

Attic areas may have ACM debris from pipe elbows, etc.,

LOWER SCHOOL AREA

Room #5:	Delamination of Ceiling Tiles at center room / 3 locations approx 12 sq ft total
Room #24:	Minor damage to ceiling tile 1x1, classrooms B and D
Lwr School Office:	2 sq ft of ceiling tiles delamination/missing at xerox room; water damaged

ADMINISTRATION BUILDING

Attic spaces contain hard elbows and are assumed as ACM.
Basement area: at xerox machine in hall-ceiling tile 2 sq ft of water-damage....(found painted upon inspection)

RECOMMENDATIONS

1. Follow the AHERA Management Plan, inform LEA Designee Asbestos Program Manager, Ken Medici of any upcoming construction work so that applicable bulk sampling may be performed. Inform Ken Medici of any emergency work or plans to enter attic spaces anywhere on campus. Continue to conduct employee Awareness Training and other formal training as needed. Perform a suspects materials audit and update the AHERA Management Plan. Update the AHERA Management Plan as needed. Send out notifications to PTA members, parents, school employees as per the Management Plan and make available the AHERA Management Plan for review. Keep asbestos abatement records and organize into a readable file. Organize the Management Plan into a readable and user friendly document. The Management Plan is a working document and The Buckley School is required by AHERA to actively work with the asbestos concerns specified by the document.
2. The Buckley School should not pull up and replace carpet without the written approval of a Certified Asbestos Consultant even if The Buckley School believes newly installed carpet is free of Asbestos debris. (i.e. Lower school area rooms) nor disturb drywall of stucco matls.
3. If air testing is out of compliance with the Education Code, complete air testing to be in compliance with the Education Code. See the State of California internet web page (Education)
4. Address the damaged materials identified within the 6 month re-inspection.
5. Only AHERA accredited persons can work within the Asbestos Management Program and work within the Asbestos Abatement Program.
6. Roof materials should also be included as asbestos-containing materials.
   Attic areas, as mentioned in the original management plan should remain off limits and be considered as contaminated with asbestos until proven not to be contaminated with asbestos.

General Comments

Extensive air monitoring of all campus rooms and hallways was completed in July 2001. All air samples were analyzed by an AIHA accredited laboratory which reported no asbestos detected. During other asbestos abatement work and clean-up , air monitoring was again performed in which all air samples collected were delivered to an AIHA accredited laboratory which again reported no asbestos detected in the air. Because all inspections are up to date and all previous air testing samples found no asbestos airborne fibers present, we conclude that the Buckley Campus in Sherman Oaks, CA is safe and presently free from any air-borne asbestos fiber hazards.

CERTIFICATION OF ASBESTOS SAFE FACILITY :

Ken Medici

Kenneth Medici
Certified Asbestos Consultant #92-0007

Dated: 12/27/05

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: STUCCO **Lab % Asbestos:** 2%
Building Description: UPPER SCHOOL BLDGS **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: OUTSIDE & ATTICS OVERHANGS
Estimated square feet or linear feet of Material: 10K ft2 **Approx Thickness:** 3"

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable
ATTIC WALLS

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing** - ATTIC AREAS
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: **Greater/Less than 10% Distributed/ Greater/Less than 25% localized**
Explanation: DUST, DEBRIS FROM ORIGINAL INSTALL

Cause of Damage: **Wear and Tear Mechanical Weather Water Other**
Explanation: Mech Install caused dust & debris

Accessibility: **Always Periodic Rare**
Explanation: MAINT & CONSTRUCTION ONLY

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation: A CAC SHOULD DIRECT & MANAGE ANY ENTRY INTO ATTIC AREAS.

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: K. Medici
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: EXTERIOR STUCCO **Lab % Asbestos:** 2%
Building Description: ALL LOWER SCHOOL BLDGS **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: ATTIC OVERSPRAY, EXT WALLS & OVERHANGS
Estimated square feet or linear feet of Material: 10K ft2 **Approx Thickness:** 3" MIN.

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable
ATTIC WALLS

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing** - ATTIC AREAS
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed/Greater/Less than 25% localized
Explanation: DUST, DEBRIS FROM ORIGINAL INSTALLATION

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation: Mech Install created dust & debris

Accessibility: Always Periodic Rare
Explanation: MAINT ONLY, CAC & ASB CONTRACTORS

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation: ENTER UNDER DIRECT SUPERVISION OF CAC WITH PROTECTIVE GEAR

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature:
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007

Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: DRYWALL SYSTEM **Lab % Asbestos:** TRACE
Building Description: LOWER SCHOOL BLDGS **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: CLASSROOMS & OFFICE
Estimated square feet or linear feet of Material: 10K ft2 **Approx Thickness:** 5/8"

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed/Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation: MINOR H2O STAINS

Accessibility: Always Periodic Rare
Explanation:

Potential for Disturbance: Potential for significant damage Potential for damage Low Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation:
Follow AHERA MGT PLAN

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: Ken Medici
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: PIPING ELBOWS **Lab % Asbestos:** 10%
Building Description: ALL LOWER SCH. BLDGS **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: ATTIC AREAS
Estimated square feet or linear feet of Material: 100 ft **Approx Thickness:** 5"

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable

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Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed//Greater/Less than 25% localized
Explanation: SOME DETERIORATION - VARIOUS ELBOWS

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation: AGE DETERIORATION

Accessibility: Always Periodic Rare
Explanation:

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation:
Follow AHERA MGT PLAN

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: Ken Medici
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: LINOLEUM & FLOOR TILE **Lab % Asbestos:** 10% A&B
Building Description: ADMINIST. & LIBARY **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: ALL ROOMS
Estimated square feet or linear feet of Material: 10K ft2(+) **Approx Thickness:** 1"

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable
LINO. TILE

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed///Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation:

Accessibility: Always **Periodic Rare**
Explanation:

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation:
Follow AHERA MGT Plan

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature:
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: WALL SYSTEMS -DRYWALL **Lab % Asbestos:** TRACE
Building Description: UPPER SCHOOL BLDGS **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: ALL AREAS-ALL ROOMS
Estimated square feet or linear feet of Material: 10K ft² (+) **Approx Thickness:** 5/8"

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed///Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation:

Accessibility: Always **Periodic Rare**
Explanation:

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation:
Follow AHERA MGT PLAN

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: Ken Medici
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007

Fax: (760).414-1183   Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: STUCCO   **Lab % Asbestos:** TRACE ASB
Building Description: FIELDHOUSE   **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: ATTIC AREAS & OFFICE
Estimated square feet or linear feet of Material: 3000 ft2 **Approx Thickness:** 3''

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable
ATTIC WALLS

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing** ~ ATTIC
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed//Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation: ORIGINAL APPLICATION

Accessibility: Always Periodic Rare
Explanation: O+M

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation: ENTER ATTIC ONLY UNDER DIRECT SUPERVISION OF A CAC.

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: [signature]
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: BLACK MASTIC GLUE **Lab % Asbestos:** 10% asbestos
Building Description: ALL BUILDINGS **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description: Glue under carpet or linoleums, etc
Estimated square feet or linear feet of Material: 120K ft2 **Approx Thickness:** 1/8"

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed///Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation:

Accessibility: Always Periodic Rare
Explanation: NORMAL OCCUPANCY

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation: FOLLOW AHERA MGT PLAN
DO NOT DISTURB FLOOR TILE, LINO OR MASTICS

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: [signature]
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007

Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: ROOF CAP SHEETS, MASTICS **Lab % Asbestos:**
Building Description: ALL BUILDINGS **Or** **PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space **Other** ROOF
Functional Space Description:
Estimated square feet or linear feet of Material: 120K ft^2 **Approx Thickness:** Layered

---

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable

---

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed///Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation:

Accessibility: Always Periodic Rare
Explanation: ROOF AREAS NORMALLY NOT ACCESSIBLE

Potential for Disturbance: Potential for significant damage Potential for damage Low Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation:
TAKE ALL PRECAUTIONS PER APPLICABLE LAWS

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature: Ken Medici
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

THE BUCKLEY SCHOOL

c/o Kenneth Medici, CAC #92-0007
Fax: (760).414-1183 Office: 1-888-999-7908 Toll-Free

AHERA FIELD DATA RE-INSPECTION ASSESSMENT FORM

Type of Material: **Lab % Asbestos:**
Building Description: **Or PACM**

Functional Space: classrooms Office hallway mech rm Attic Crawl-Space Other
Functional Space Description:
Estimated square feet or linear feet of Material: **Approx Thickness:**

Homogeneous Area: Surfacing TSI Miscellaneous +++++ Friable Non-Friable

---

Condition of Material: Good Fair Poor Damaged Significantly Damaged
AHERA Category required by 40CFR763.88 :

1. **Damaged or significantly damaged TSI**
2. **Damaged friable surfacing**
3. **Significantly damaged friable surfacing**
4. **Damaged or significantly damaged friable miscellaneous**
5. **Any ACBM with potential for damage**
6. **Any ACBM with potential for significant damage**
7. **Any friable ACBM**

Type of Damage: Greater/Less than 10% Distributed///Greater/Less than 25% localized
Explanation:

Cause of Damage: Wear and Tear Mechanical Weather Water Other
Explanation:

Accessibility: Always Periodic Rare
Explanation:

Potential for Disturbance: Potential for significant damage Potential for damage Low
Vibration Air Erosion Weather Normal O&M

Preventative Damage Measures Explanation:

Date of AHERA Assessment: DECEMBER 27, 2005
Inspector Name: Kenneth Medici Signature:
Phone: 1-888-999-7908
Inspector Accreditation Information: CAC #92-0007

APPENDIX H:

PHASE I ENVIRONMENTAL SITE ASSESSMENT

Phase I and Phase II Environmental Site Assessment

Buckley School
3900 Stansbury Avenue
Sherman Oaks, California

Prepared for:

Latham and Watkins LLP

Prepared by:

Rincon Consultants, Inc.
March 25, 2005

rincon

Environmental Scientists Planners Engineers rincon

Rincon Consultants, Inc.

790 East Santa Clara Street
Ventura, California 93001

805 641 1000
FAX 641 1072

info@rinconconsultants.com
www. rinconconsultants.com

March 25, 2005
Project Numbers 04-17840 and 04-17841

Maria Hoye
Latham & Watkins LLP
633 West Fifth Street, Suite 4000
Los Angeles, California 90071

Phase I and Phase II Environmental Site Assessment
Buckley School
3900 Stansbury Avenue
Sherman Oaks, California

Dear Ms. Hoye:

This report presents the findings of a Phase I and Phase II Environmental Site Assessment (ESA) completed by Rincon Consultants, Inc. (Rincon) for the Buckley School, located at 3900 Stansbury Avenue, Sherman Oaks.. The assessment was performed in accordance with our proposals and contracts dated November 3, 2004 and December 20, 2004.

If you have any questions or if we can be of any future assistance, please contact us.

Sincerely,
RINCON CONSULTANTS, INC.

Tricia Ainsworth, REA I
Associate, Environmental Engineer

Walter Hamann, RG, CEG, REA II
Vice President, Environmental Services

REGISTERED GEOLOGIST
WALTER E. HAMANN
No. EG 1635
CERTIFIED ENGINEERING GEOLOGIST
STATE OF CALIFORNIA

EXECUTIVE SUMMARY

This report presents the findings of a Phase I and Phase II Environmental Site Assessment (ESA) for an irregular shaped, approximately 18-acre property located at 3900 Stansbury Avenue in Sherman Oaks, California (Figure 1, Vicinity Map). The site is currently developed with educational and recreational facilities comprising approximately 16 structures. The site was previously used as a golf course and country club.

The current educational and recreational facilities include a two-story administration building, two-story library, two-story gym and performing arts building (including two basement levels with a swimming pool on the lowest level), a two-story art and science building, several single-story classroom structures, a one-story athletic field house, two-story maintenance building, several paved parking lots, a baseball field, a basketball court, and tennis courts. Several storage sheds, used for storing electrical, mechanical, and janitorial supplies, paints, groundskeeping equipment, fertilizer and earthquake supplies are located south of the baseball field. The storage sheds are used to store small quantities of the following hazardous substances: gasoline, diesel fuel, paint, spray paint, adhesives, coatings, stains, seals, compressed gases, and fertilizer. Two 55-gallon drums of waste oil and two 30-gallon drums of waste paint are stored on secondary containment pallets outside the paint shed. Small quantities of various chemicals, glazes and stains are stored in the science and art classrooms. Chlorine and other pool chemicals are stored in the swimming pool maintenance area. The print shop contains small quantities of printing chemicals. Slight staining was observed on the wood floor beneath a small diesel can in the groundskeeping shed.

A bus maintenance garage was formerly located in the vicinity of the current print shop. An underground storage tank (UST) was formerly located in the trash compactor/parking lot area southwest of the science building. According to Curtis Covington, Director of Facilities, the UST was removed in the 1980s. Mr. Covington also indicated that the hydraulic lift in the former bus maintenance garage was removed, a clarifier was abandoned in place, and there is the potential that a UST is still located outside the former garage.

The project site is located in an area that is primarily composed of residential land uses and open space. Surrounding properties in the vicinity of the site include single-family homes and undeveloped land preserved by the Santa Monica Mountains Conservancy.

Review of an environmental database records search (EDR) indicated that a release from a UST had occurred on the site. Files maintained by Los Angeles City Fire Department (LAFD) and Los Angeles Regional Water Quality Control Board (RWQCB) indicate that a 10,000-gallon gasoline UST was removed from the subject property in 1988, after a leak was detected. Soil and groundwater were reportedly impacted with total petroleum hydrocarbons (TPH), based on soil and soil gas samples collected from the base of the excavation pit and surrounding areas and gasoline observed in the groundwater in the downgradient swimming pool sump pump. According to an Engineering Report on Soil Gas Investigation, prepared by Enviropro Inc., TPH was detected at a concentration of 46,600 milligrams per kilogram (mg/kg) in a soil sample collected from UST excavation pit. The LAFD and RWQCB files did not have any information regarding any soil or groundwater remediation at the site. Additionally, there is no indication that the soil samples were analyzed for methyl tertiary butyl ether (MTBE). The RWQCB granted case closure for the UST release and removal in 1996.

Historical sources reviewed as part of the Phase I include aerial photographs (1928, 1940, 1952, 1960, 1971, 1982, and 1994) and topographic maps (1898, 1902, 1913, 1921, 1926, 1932, 1953, 1966, and 1972). The photos and maps reviewed indicate the site was undeveloped from 1898 through 1921, developed with a few structures between 1926 and 1932, developed with a golf course and country club in 1940, developed with a few structures from 1952 through 1966, and developed as a school from 1971 through 1994.

Based on the findings of the Phase I ESA, two recognized environmental conditions were identified for the project site: the former presence of a UST and associated gasoline release on the project site, and the former presence of a bus maintenance garage on the project site.

To evaluate the potential site impact associated with the recognized environmental conditions identified in this Phase I ESA, a Phase II ESA was conducted at the site. The Phase II included the completion of a geophysical survey to investigate the potential presence of a UST at the former bus maintenance garage, the collection of subsurface soil samples from ten boring locations in the vicinity of the former UST, clarifier, and hydraulic hoist, and the collection of groundwater from the pool sump pump. Select soil samples were analyzed for the presence of total petroleum hydrocarbons (TPH), volatile organic compounds (VOCs), lead, metals, and polychlorinated biphenyls (PCBs). The groundwater sample from the sump pump was analyzed for hydrocarbons and VOCs. The Phase II geophysical survey was conducted on December 21, 2004. The results of the geophysical survey indicate that a small UST remains in the vicinity of the observed tank vent and covered tank fill access. Based on the dimensions of the detected anomaly, the tank is believed to be a waste oil tank. The Phase II soil sampling was conducted on December 27 and 30, 2004 (Figure 4, Soil Sampling Location Map). The results of laboratory analyses of these samples are presented in Tables 3 through 5.

The laboratory data indicate that TPH – gasoline (TPH-g), VOCs, oxygenates and metals were detected in the soil samples. None of the soil samples tested for TPH-diesel range organics (DRO), TPH-oil range organics (ORO), and PCBs had detectable levels of these constituents. Metals were detected at varying concentrations in the soil samples collected and analyzed for metals. A maximum concentration of 1,080 mg/kg TPH-g was detected in B1 at 25 feet below grade. Maximum concentrations of 8.4 mg/kg benzene, 31 mg/kg toluene, 13.7 mg/kg ethylbenzene and 104.2 mg/kg total xylenes were detected in B1 at 25 feet below grade. A maximum concentration of 0.798 mg/kg tert-butyl alcohol (TBA) was detected in B1 at 20 feet below grade and a maximum concentration of 6.95 mg/kg MTBE was detected in B4 at 20 feet below grade. A maximum concentration of 0.12 mg/kg acetone and 0.27 mg/kg tetrachloroethylene (PCE) was detected in B6 at a depth of 5 feet below grade. Various metal compounds were detected in B1 through B3, B5 through B7, B9 and B10.

To evaluate the significance of the reported hydrocarbon and VOC levels in the soil samples, we compared these levels to threshold levels established by RWQCB. TPH-g and benzene were detected at concentrations exceeding the RWQCB maximum soil screening levels (SSLs) in sample B1 at 25 feet below grade. BTEX and MTBE were detected in soil samples collected at various depths in borings B1, B3, and B4 at concentrations that could potentially exceed the

RWQCB SSLs. Without actual depth to groundwater data for these locations, exact SSLs cannot be calculated to determine whether these thresholds have been exceeded. TBA was detected in several samples in the former UST area. The SSL for TBA could not be determined as there is no Maximum Contaminant Level (MCL) for this constituent. Low concentrations of PCE and acetone were detected near the waste oil tank in soil samples B5 and B6 at 5 feet below grade. However, based on the shallow depth of the detected PCE, it is not likely that the PCE SSL would be exceeded for this location. The acetone SSL could not be determined as there is no MCL for this constituent.

The metals concentrations were compared to the United States Environmental Protection Agency (USEPA) soil cleanup thresholds and the State of California Department of Toxic Substances Control (DTSC) hazardous waste thresholds. The metal concentrations detected in the soil samples tested for these constituents did not exceed total threshold limit concentration (TTLC) levels or ten times soluble threshold limit concentration (STLC) levels. Therefore, if soil were to be excavated from this location, the metals content in the resulting soil would be considered non-hazardous for disposal purposes. With the exception of arsenic, metals were well below their respective PRGs. Although the levels of arsenic detected in the soil samples analyzed during this assessment exceed the arsenic PRGs, they were within the published ranges for arsenic in soils in the Western United States (Shacklette, H.T. and Boerngen, J.G., 1984) and appear to be within normal background levels. As discussed in the Shacklette and Boerngen report, the range of arsenic observed in background soil in the Western United States was between 0.10 mg/kg and 97 mg/kg. Overall, the levels of metals detected in the soil samples were low and likely represent naturally occurring background concentrations of metals in soil.

PHASE I ENVIRONMENTAL SITE ASSESSMENT

INTRODUCTION

This report presents the findings of a Phase I ESA conducted for the property located at 3900 Stansbury Avenue, Sherman Oaks, California, APN 2274-027-003. The Phase I ESA was performed by Rincon Consultants, Inc. (Rincon) for Latham & Watkins LLP in general conformance with ASTM E 1527-00 and our proposal and contract dated November 3, 2004. The following sections present our findings and provide our opinion as to the potential presence and impact of environmental site conditions.

PURPOSE

The purpose of this Phase I ESA was to identify the possible presence of recognized environmental conditions (RECs) associated with possible soil and groundwater contamination at the site.

A REC is defined pursuant to ASTM E 1527-00 as the presence or likely presence of any hazardous substances or petroleum products on a property under conditions that indicate an existing release, a past release, or a material threat of a release of any hazardous substances or petroleum products into structures on the property or into the ground, groundwater, or surface water of the property. The term includes hazardous substances or petroleum products even under conditions in compliance with laws. The term is not intended to include de minimis conditions that generally do not present a material risk of harm to public health or the environment and that generally would not be the subject of an enforcement action if brought to the attention of appropriate governmental agencies.

SCOPE OF SERVICES

The scope of services conducted for this study is outlined below:

- Perform an on-site reconnaissance to identify obvious indicators of the existence of hazardous materials.
- Observe adjacent or nearby properties from public thoroughfares in an attempt to see if such properties are likely to use, store, generate, or dispose of hazardous materials.
- Obtain and review an environmental records database search from Environmental Data Resources (EDR), Inc. to obtain information about the potential for hazardous materials to exist at the site or at properties located in the vicinity of the site.
- Review files for the subject site as identified in the EDR report.
- Review the current U.S. Geological Survey (USGS) topographic map to obtain information about the site's topography and uses of the site and properties in the vicinity of the site.
- Review historic aerial photographs and topographic maps to obtain information about historic uses of the subject property and adjacent properties.
- Review California Division of Oil and Gas records to obtain information about historic oil and gas activity in the vicinity of the site.
- Provide an interview questionnaire to the designated site representative identified to Rincon by Latham & Watkins LLP.
- Conduct a site interview with the designated representative.

Our scope of services, pursuant to ASTM E 1527 practice, did not include any inquiries with respect to asbestos, lead-based paint, lead in drinking water, wetlands, regulatory compliance, cultural and historic resources, industrial hygiene, health and safety, ecological resources, endangered species, indoor air quality, or high voltage power lines.

LIMITATIONS, ASSUMPTIONS AND USER RELIANCE

This Phase I ESA was prepared for use solely and exclusively by Latham & Watkins LLP and the Buckley School. This report shall not be relied upon by or transferred to any other party without the express written authorization of Rincon Consultants.

Latham & Watkins LLP has requested this assessment and will use the assessment for the purposes of a facilities modernization project. No other use or disclosure is intended or authorized by Rincon. Also, this report is issued with the understanding that it is to be used only in its entirety. It is intended for use only by the client, and no other person or entity may rely upon the report without the express written consent of Rincon.

This work has been performed in accordance with good commercial, customary, and generally accepted environmental investigation practices for similar investigations conducted at this time and in this geographic area. No other guarantee or warranties, expressed or implied are provided.

The findings and opinions conveyed in this report are based on findings derived from a site reconnaissance, review of an environmental database report, specified regulatory records and historical sources, and comments made by interviewees. This report is not intended as a comprehensive site characterization and should not be construed as such. Standard data sources relied upon during the completion of Phase I ESAs may vary with regard to accuracy and completeness. Although Rincon believes the data sources are reasonably reliable, Rincon cannot and does not guarantee the authenticity or reliability of the data sources it has used. Additionally, pursuant to our contract, the data sources reviewed included only those that are practically reviewable without the need for extraordinary analysis.

Rincon has identified evidence that suggests that petroleum products exist at the site at levels that could require mitigation. In accordance with our authorized work scope and contract and the general provisions of ASTM E1527-00, no attempt was made to check for the presence of asbestos, lead-based paint, lead in drinking water, wetlands, regulatory compliance, cultural and historic resources, industrial hygiene, health and safety, ecological resources, endangered species, indoor air quality, or high voltage power lines.

SITE DESCRIPTION

LOCATION AND LEGAL DESCRIPTION

The site is an approximately 18-acre property located at 3900 Stansbury Avenue, Sherman Oaks, California (Figure 2, Site and Adjacent Land Use Map). The site is located at the south end of Stansbury Avenue, adjacent to the east of Camino De La Cumbre. The property is identified as APN 2274-027-003.

SITE AND VICINITY GENERAL CHARACTERISTICS

The site is located in an area that is comprised of residential land uses and open space. Properties north and west of the site include single-family homes. Properties east and south are generally open space.

CURRENT USES OF THE PROPERTY

The site is currently developed with the Buckley School, a private school (elementary through high school).

DESCRIPTIONS OF STRUCTURES, ROADS AND OTHER IMPROVEMENTS ON THE SITE

The Buckley School campus is currently developed with approximately 16 structures, including a two-story administration building, two-story library, two-story gym and performing arts building (Pavilion), a two-story art and science building, and several single-story classroom structures. A large paved parking lot is located on the northern end of the property, near the entrance gate. Smaller paved parking areas are located throughout campus. A baseball field is located on the southern end of the property. A basketball court is located along the southeast boundary of the property, adjacent to the baseball field. Several storage sheds, used for storing electrical, mechanical, and janitorial supplies, paints, groundskeeping equipment, fertilizer and earthquake supplies are located adjacent to the south of the baseball field. According to Curtis Covington, Director of Facilities, most facility structures are about 35 years old, with the exception of the gymnasium (pavilion), which is about 32 years old.

Access to the site is available through a guard kiosk entrance located at the southern end of Stansbury Avenue. Water service is provided by Los Angeles Department of Water and Power (LADWP) and sewer service is provided by City of Los Angeles. Los Angeles Department of Water and Power (LADWP) provides electrical service and the Southern California Gas Company provides natural gas service. Solid waste collection and disposal services are provided by Crown Disposal.

CURRENT USES OF THE ADJACENT PROPERTIES

Current adjacent land uses are described in Table 1 and depicted on Figure 2, Site and Adjacent Land Use Map.

Table 1 - Current Uses of Adjacent Properties

Area	Use
Northern Property	residential
Eastern Property	open space (Santa Monica Mountains Conservancy)
Western Property	Camino de la Cumbre/then residential
Southern Property	open space (Santa Monica Mountains Conservancy)

USER PROVIDED INFORMATION

TITLE RECORDS

Latham & Watkins LLP and the Buckley School did not provide Rincon with a copy of title records for the subject site.

ENVIRONMENTAL LIENS OR ACTIVITY AND USE LIMITATIONS

Latham & Watkins LLP and the Buckley School did not provide Rincon with any information pertaining to environmental liens or activity and use limitations for the subject site.

SPECIALIZED KNOWLEDGE

Latham & Watkins LLP and the Buckley School did not provide Rincon with any specialized knowledge that would be material to recognized environmental conditions in connection with the property.

VALUATION REDUCTION FOR ENVIRONMENTAL ISSUES

Latham & Watkins LLP and the Buckley School did not provide Rincon with any information pertaining to a valuation reduction for the subject site relative to any known environmental issues.

OWNER, PROPERTY MANAGER, AND OCCUPANT INFORMATION

The school Director of Facilities was interviewed regarding the current and former uses of the site. The information obtained from this interview is described in the Site Reconnaissance and Interviews section of this report.

RECORDS REVIEW

PHYSICAL SETTING SOURCES

Topography

The current USGS topographic map (Van Nuys Quadrangle, 1966, photorevised 1972) indicates that the site is situated at an elevation ranging from about 800 to 900 feet above mean sea level with topography sloping generally to the west-northwest on the eastern portion of the site and to the east-southeast on the western portion of the site.

Geology and Hydrogeology

Geology

The project area is near the southern boundary of the San Fernando Valley alluvial basin. The sediments in this area are erosional remnants of the sedimentary rocks found along the southern boundary of the Santa Monica Mountains. These sedimentary rocks consist of claystones and siltstones. Erosion of these sediments generally results in fine-grained alluvial deposits.

According to the Geologic Map of the Beverly Hills and Van Nuys (South 1/2) Quadrangles (Dibblee, 1991), the site is underlain by Quaternary-age alluvium and Miocene-age unnamed shale and Monterey Formation. The alluvium is comprised of unconsolidated deposits of gravel, sand and silt-clay, derived mostly from Santa Monica Mountains and including gravel and sand from stream channels. The unnamed shale is comprised of soft, white-weathering diatomaceous shale to diatomite. The Monterey Formation is comprised of white-weathering, thin bedded, moderately hard, dark siliceous shale and tan to light gray semi-friable bedded sandstone.

The GeoCheck summary report provided in the attached EDR report (Appendix 1, page A-4) indicates that the site is underlain by Tertiary age stratified sequence. The USDA soil survey for the general area of the property indicates that the soil types present in the site vicinity are primarily gravelly loam.

Hydrogeology

The site is located in the southern portion of the Los Angeles River Watershed. In the San Fernando Valley area, groundwater depths range from near land surface to 100 feet below ground surface. According to the October 1988 Engineering Report on Soil Gas Investigation prepared by Enviropro Inc., groundwater is reportedly at about 35 feet below grade at the Pavilion building (gym), where the sump pump is used to protect the structural integrity of the swimming pool. Based on the Enviropro report, the ground surface drops in elevation by about 40 feet from the former UST area/trash compactor/parking lot to the Pavilion building. Therefore, the estimated depth to groundwater beneath the former UST area is between 60 and 90 feet below grade. As the subject site has a wide range of hillside elevations, the groundwater depths will vary beneath the site. Groundwater flow direction has not been established for this site. However, based on the assumption that the groundwater flow direction in the area parallels the topographic gradient, the general anticipated groundwater flow directions near the subject site would be to the west-northwest on the eastern portion of the site and to the east-southeast on the western portion of the site.

STANDARD ENVIRONMENTAL RECORDS SOURCES

Environmental Data Resources, Inc. (EDR) was contracted to provide a database search of public lists of sites that generate, store, treat or dispose of hazardous materials or sites for which a release or incident has occurred. The EDR search was conducted for the subject site and included data from surrounding sites within a specified radius of the property. A copy of the EDR report, which specifies the ASTM search distance for each public list, is included as Appendix 1. As shown on the attached EDR report, Federal, State and County lists were reviewed as part of the research effort. The subject site was listed as a RCRIS-SQG, FINDS, HAZNET, CA FID UST, LUST, Cortese and ERNS site in the EDR database.

Sites that were identified within a one-mile radius of the subject site are listed in Table 2, EDR Listing Summary of Sites Within One Mile of the Subject Property (see Appendix 1 for a complete listing of sites reported by EDR) and include sites that appear in the following databases:

> **FINDS**: Facility Index System. Contains both facility information and pointers to other sources that contain more detail.
>
> **LUST**: LUST records contain an inventory of reported leaking underground storage tank incidents. This database is maintained by the State Water Resources Control Board.

RCRIS-(TSD, LQG, SQG): Resource Conservation and Recovery Information System. The RCRIS database includes selected information on sites that generate, store, treat, or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act. TSD refers to transfer, storage or disposal facility. LQG refers to large quantity generator. SQG refers to small quantity generator. The source of this database is the U.S. EPA.

CORTESE: Identified Hazardous Waste and Substance Sites. This database (from the CAL EPA/Office of Emergency Information) identifies public drinking water wells with detectable levels of contamination, hazardous substance sites selected for remedial action, sites with known toxic material identified through the abandoned site assessment program, sites with USTs having a reportable release and all solid waste disposal facilities from which there is known migration.

Ca. FID: California Facilities Inventory Database contains active and inactive underground storage tank locations as provided by the California State Water Resources Control Board.

HistUST: The Hazardous Substance Storage Container Database is a historical listing of UST sites. This database is maintained by the State Water Resources Control Board.

ERNS: Emergency Response Notification System. This database records and stores information on reported releases of oil and hazardous substances.

NOTIFY 65: Proposition 65 notification reports. Notify 65 contains facility notifications about any release which could impact drinking water and thereby expose the public to a potential health risk (information is provided by the State Water Resources Control Board).

HAZNET: Hazardous Waste Information System. Data that is extracted from the copies of hazardous waste manifests received each year by the DTSC (information is provided by the Department of Toxic Substances Control).

Table 2 - EDR Listing Summary of Sites Within One Mile of the Subject Site

Site Name	Site Address	Distance from Subject Site (miles)	Database Reference
Buckley School Bus Garage / Buckley School	3900 Stansbury Ave.	Subject Site	RCRIS-SQG, FINDS, HAZNET, CA FID UST, LUST, Cortese, ERNS
Service Station	14478 Ventura Blvd.	1/2 – 1 mile	Notify 65, HAZNET, LUST, Cortese, CA FID UST, HIST UST

The RCRIS-SQG listing for the subject site indicates that small quantities (more than 100 and less than 1,000 kilograms per calendar month) of unspecified solvent mixture waste, unspecified organic liquid mixture, oil/water separation sludge, organic liquids (nonsolvents) with halogens, laboratory waste chemicals, asbestos containing waste and aqueous waste with less than 10%

total organic residues are generated onsite. There is no indication of any unauthorized release regarding the wastes generated by the subject site. The LUST and Cortese listings for the subject site indicate that there was a gasoline release due to leaking piping in 1988. The EDR indicates the release was to soil only, the site was not tested for MTBE and the case was closed in 1996.

REVIEW OF AGENCY FILES

As a follow-up to the database search and the site reconnaissance, we filed a request with Los Angeles City Fire Department (LAFD) and Los Angeles Regional Water Quality Control Board (RWQCB) to review documents and obtain copies of documents pertaining to the subject site. Rincon reviewed UST files at LAFD and RWQCB for the subject site on December 2, 2004.

Review of LAFD Files

According to an LAFD Fire/Life Safety Violation notice, dated May 27, 1988, Buckley School was directed to remove product from the leaking UST, monitor the groundwater sump (located beneath the swimming pool, downgradient of the UST area) for flammable vapors, provide an integrity test of the UST, and provide the LAFD with a report of analysis from soil borings to determine whether or not an unauthorized release has occurred.

According to a June 2, 1988 LAFD Fire/Life Safety Violation notice, Buckley School was required to provide a site assessment including the extent of contamination, location of groundwater, groundwater flow direction and cleanup recommendations.

According to an Engineering Report on Soil Gas Investigation, prepared by Enviropro Inc. on October 31, 1988, one 10,000-gallon gasoline tank was removed in July of 1988. During the excavation of the tank, two soil samples were collected and analyzed for total petroleum hydrocarbons (TPH) during the tank removal (July 1998). TPH was detected at a concentration of 46,600 mg/kg in the soil sample collected from the north end of the excavation (Sample #1). Hydrocarbon contamination was observed in the groundwater being pumped from a sump near the swimming pool located on the basement floor of the Pavilion building. A preliminary soil gas investigation was conducted by Enviropro Inc. on August 11, 1988 using a photoionization detector (PID). A total of 29 boreholes were drilled to depths from 1 to 1.5 feet below grade. The boreholes were covered with a plastic film and vapors were allowed to collect in the borehole. PID readings were collected from the boreholes by penetrating the plastic film with the PID sampling probe. The report states that the results of the soil gas investigation are only qualitative, because no direct measurement of soil or groundwater contamination has been provided. The report proposes that a subsequent detailed remedial investigation be conducted, including the installation of three groundwater monitoring wells. PID readings collected from various locations near the tank excavation area and the Pavilion area, downgradient of the former tank area, indicate the highest volatile organic compound concentration was detected near the tank excavation to the east. A copy of the soil gas investigation report is included in Appendix 2.

An LAFD letter, dated April 12, 1989, states that groundwater beneath the site has been impacted and the case has been referred to the State Regional Water Quality Control Board (SRWQCB).

Review of RWQCB Files

A May 27, 1988 State of California Hazardous Substance Spill Report indicates that the LAFD notified the state of the gasoline UST release. The spill report indicates that the UST leaked an unknown quantity of gasoline into the swimming pool and school grounds sump pump, causing fuel to be pumped into a drainage ditch, which flows to the Los Angeles River.

According to a June 2, 1988 Underground Storage Tank Unauthorized Release (Leak) / Contamination Site Report, an unknown quantity of gasoline was released from the UST. The leak was discovered on May 27, 1988 during a tank test. The discharge was reportedly stopped by removal of tank contents. A piping leak was the determined source of discharge of the 10,000-gallon, 16 year-old steel tank.

A RWQCB case closure letter, dated July 22, 1996, indicates site closure was granted and no further action was required related to the UST release. Copies of the RWQCB files are included in Appendix 2.

ADDITIONAL ENVIRONMENTAL RECORDS SOURCES

State of California Division of Oil and Gas Records

A review of the Division of Oil and Gas Munger Map Book (2001) indicates that no oil or gas wells are or have been located on or within at least two miles of the subject site.

HISTORICAL USE INFORMATION

Review of Historic Aerial Photographs

Copies of aerial photographs were obtained from UCSB Map and Imagery Department's aerial photograph collection and reviewed. Copies of the aerial photographs are included in Appendix 3 (Historical Documents).

- ***1928, Fairchild (Scale: 1" = 600')*** – The subject site appears to have graded areas and structures or foundations surrounded by undeveloped property. Camino De La Cumbre is depicted as a dirt road adjacent to the west. Beverly Glen Boulevard and Mulholland Highway are depicted to the south. The adjacent properties are depicted as undeveloped. Several surrounding properties are depicted as residential.

- ***1940, Fairchild (Scale: 1" = 600')*** –The subject site appears to be developed as a country club and golf course. The adjacent property to the north, wrapping around to the east and then south, is depicted as the remainder of the golf course. With the exception of the golf course, the adjacent properties are depicted similar to the 1928 photograph. Substantial residential development is depicted in the surrounding properties to the north.

- ***1952, ASCS-USDA (Scale: 1" = 600')*** – The subject site appears to be graded and under development, with several smaller structures or trailers onsite. The former adjacent golf course property to the north (wrapping around to the east and south) now appears to be depicted as residential. Additional residential development is depicted in surrounding properties to the north and south.

- ***1960, Fairchild (Scale: 1" = 600')*** – The subject site and adjacent properties are depicted similar to the 1952 photograph. Additional residential development is depicted in surrounding properties in all directions.

- ***1971, Teledyne (Scale: 1" = 600')*** – The subject site appears to be developed with three large classroom buildings, paved parking lots, and graded areas under development. Adjacent properties are depicted similar to the 1960 photograph. Additional residential development is depicted in surrounding properties in all directions.

- ***1982, Aerial Map Industries (Scale: 1" = 600')*** – The subject site appears to be developed with approximately thirteen educational facility structures and a sports field and track. Adjacent and surrounding properties are depicted similar to the 1971 photograph.

- ***1994, USGS (Scale: 1" = 600')*** – The subject site and adjacent properties are depicted similar to the 1982 photograph. A large residential development is depicted on a nearby property to the east.

Review of Historic Topographic Maps

Historic topographic maps from the UCSB Map and Imagery Department map collection were reviewed. Copies of the historic topographic maps are included in Appendix 3 (Historical Documents). Following is a summary of our review of these maps.

- ***1898 Santa Monica Quadrangle Map*** – The map depicts the subject site and adjacent properties as being undeveloped. A road (currently Ventura Boulevard) and the Los Angeles River appear to the north of the subject property. The Southern Pacific Railroad is depicted further to the north.

- ***1902 Santa Monica Quadrangle Map*** – The subject site and adjacent properties are depicted similar to the 1898 map.

- ***1902, reprinted 1913, Santa Monica Quadrangle Map*** – The subject site and adjacent properties are depicted similar to the 1902 map.

- ***1921 Santa Monica Quadrangle Map*** – The subject site and adjacent properties are depicted similar to the 1913 map.

- ***1926 Van Nuys Quadrangle Map*** – The subject site is depicted as being developed with one structure. A road (currently Stansbury Avenue) is depicted on the subject property, connecting to Mulholland Highway further south.

- ***1926, reprinted 1932, Van Nuys Quadrangle Map*** – The subject site and adjacent properties are depicted similar to the 1926 map.
- ***1953 Van Nuys Quadrangle Map*** – The subject site is depicted as being developed with two structures. A road (currently Camino De La Cumbre) is depicted adjacent to the west.
- ***1966 Van Nuys Quadrangle Map*** – The subject site and adjacent properties are depicted similar to the 1953 map. Highway 101 (Ventura Freeway) is depicted north of Ventura Boulevard.
- ***1966, photorevised 1972, Van Nuys Quadrangle Map*** – The subject site is depicted as Buckley School, with several structures shown.

SITE RECONNAISSANCE AND INTERVIEWS

Rincon Consultants performed a reconnaissance of the site on November 22, 2004 accompanied by Curtis Covington, Director of Facilities with the Buckley School. The purpose of the reconnaissance was to observe existing site conditions and to identify obvious indicators of hazardous materials that could affect the subject site. An interview questionnaire was provided to Mr. Covington prior to the site reconnaissance. A copy of the completed questionnaire is included in Appendix 4.

The following information is based on observations noted or information obtained during the November 22, 2004 site reconnaissance and our review of the completed questionnaire.

HISTORICAL USE INFORMATION

Mr. Covington indicated that the on-site structures are about 35 years old, with the exception of the gymnasium (Pavilion), which is about 32 years old. The Buckley School reportedly obtained ownership of the site in 1968. He did not know who owned or leased the site property prior to the Buckley School. However, Mr. Covington indicated that the subject property was previously used as a golf course and country club.

Mr. Covington indicated a UST was formerly located onsite, in the trash compactor/parking lot area southwest of the science building. He indicated the tank had been removed in the 1980s, however, he was not aware of the details of any unauthorized releases associated with the tank. Mr. Covington indicated that the print shop was formerly a bus maintenance garage, with an abandoned three-stage clarifier, former hydraulic lift, and possible underground storage tank. The three-stage clarifier located in the former bus garage was pumped out, abandoned and filled with sand less than 2 years ago. The hydraulic lift was removed more than 5 years ago. A possible tank vent and tank fill access observed near the bus garage indicate the possible current presence of an underground storage tank in the former bus garage vicinity. Mr. Covington was not aware of any hazardous materials releases or other environmental liabilities associated with the site or surrounding properties.

CURRENT USES OF THE PROPERTY

Mr. Covington indicated that the current operation on the site involves uses that are typical of an educational facility and includes operation and maintenance of buildings, surrounding landscape, tennis courts, basketball court, baseball fields and swimming pool. Maintenance and storage sheds/containers located on the subject site are used to store electrical, mechanical, and janitorial supplies, paints, groundskeeping equipment, fertilizer and earthquake supplies. Site photographs are provided as Figure 3.

STORAGE TANKS

During the site reconnaissance, Rincon did not observe above-ground tanks. A possible underground tank vent and covered tank fill access were observed near the print shop (former bus garage). Mr. Covington had no knowledge of the status of this possible tank. Mr. Covington indicated on his questionnaire, Appendix 4, that former underground storage tank has been removed.

HAZARDOUS SUBSTANCES AND PETROLEUM PRODUCTS IN CONNECTION WITH IDENTIFIED USES

- The art classroom contains small quantities of lead-free glazes (i.e., iron oxide and copper carbonate) and stains in the supply cabinet.
- The chemistry supply room contains a 1-gallon container of kerosene, a 16-ounce container of linseed oil, and several small containers of various laboratory chemicals (i.e., phosphorous pentoxide, sodium dithionite, sodium peroxide, acids, and nitrates).
- The pool maintenance area contains various pool chemicals including muriatic acid, Alkalinity Up, a 55-gallon plastic drum of chlorine in secondary containment and a small quantity of boxes of liquid chlorine.
- The print shop contains two 3-gallon containers of blanket wash, one 3-gallon container of Rubber Rejuvenator, one 5-gallon hazardous waste container serviced by Safety Kleen, and small quantities of WD40, spray adhesive, and other print products.
- The athletic office and associated storage shed contain small quantities of rubbing alcohol, hydrogen peroxide, disinfectant, cleaning products, and chlorine for the whirlpool.
- The electrical storage shed contains two 5-gallon containers of gasoline for the two generators stored in the shed.
- The paint storage shed contains approximately fifty 1-gallon cans of paint, fifteen 5-gallon buckets of paint, and small quantities of adhesive and coating.
- Outside of the paint shed, two 55-gallon waste oil drums and two 30-gallon waste paint drums are stored on secondary containment pallets. No staining was observed in the waste drum area.
- The air compressor shed contains compressed acetylene and oxygen tanks and torches, and an air compressor. About thirty 12 and 15-ounce cans of spray paint, ten 1-quart containers of stains and seals, and one gallon of contact cement are stored in a flammables cabinet.

- The parts shed stores small containers of WD40, liquid nails, caulk, spackling paste, primer, and PVC pipe cement.
- The groundskeeping shed contains one 30-gallon diesel drum, two 5-gallon and two 3-gallon containers of gasoline, two 2.5-gallon containers of diesel. Slight staining was observed on the wood floor beneath on the small diesel containers, however, the shed sits atop a concrete pad.
- The fertilizer shed contains about forty 50-pound bags of Nitrex (nitrate and iron mixture).
- The field maintenance shed contains about ten 5-gallon buckets of athletic field striping paint.

UNIDENTIFIED HAZARDOUS SUBSTANCE AND PETROLEUM PRODUCT CONTAINERS

Unidentified hazardous substance containers or unidentified containers that might contain hazardous substances were not observed during the site reconnaissance. The possible tank vent and covered fill access were the only visible components of the possible petroleum product tank near the bus garage. Therefore, Rincon could not observe indications of potential releases from the possible tank.

Rincon observed two 55-gallon waste oil drums stored on secondary containment pallets outside paint shed, one 30-gallon diesel drum in the groundskeeping shed, and several small containers storing gasoline and diesel in storage sheds. Slight staining was observed on the wood floor beneath the small diesel containers, however, the shed sits atop a concrete pad.

INDICATIONS OF POLYCHLORINATED BIPHENYLS (PCBs)

Curtis Covington, the Director of Facilities, indicated that there are 13 transformers onsite. During the site reconnaissance, Rincon observed several of the transformers located inside and outside campus buildings. There was no indication of a release in the vicinity of the transformers observed. With the exception of the main high voltage transformer, the onsite transformers are owned by the Buckley School and are maintained as necessary by private contractors. The main transformer on campus is owned and maintained by LADWP.

The hydraulic equipment for one elevator and one dumb waiter were identified during the site reconnaissance. These hydraulic systems are maintained under a private service contract. The elevator equipment is located in the basement of the administration building and the dumbwaiter equipment is located on the bottom floor of the library. An oil leak was observed beneath the hydraulic equipment for the elevator. However, the concrete floor appeared to be in good condition (i.e., no apparent cracking) in the vicinity of the oil leak. No indications of recent spills or leaks were observed beneath the library's dumbwaiter equipment.

OTHER CONDITIONS OF CONCERN

During the site reconnaissance, Rincon did not observe or note any of the following possible indicators of a hazardous materials release:

- *stressed vegetation*
- *solid waste/debris*
- *odors*

However, during the site reconnaissance, Rincon observed the following possible indicators of a hazardous materials release or the presence of the following indicators of such a release: small pool of liquid beneath the elevator equipment and slight staining of wood floor in the groundskeeping shed.

A small pool of oil was observed beneath the hydraulic equipment for the elevator in the administrative building. However, the concrete floor did not appear to be cracked in the vicinity of the oil leak.

Slight staining was observed on the wood floor in the groundskeeping shed beneath two small containers of diesel fuel. However, this shed sits atop a concrete pad.

FINDINGS OF PHASE I ESA

Known or suspect environmental conditions associated with the property include the following:

- Former presence of UST and associated gasoline release on the subject site.
- Former presence of an onsite bus maintenance garage, with a former hydraulic lift, abandoned clarifier, and possible underground storage tank.
- Former use of subject site as golf course.
- Slight staining of wood floor in the groundskeeping shed on the subject site.
- Presence of leaking elevator equipment on the subject site.

OPINIONS AND CONCLUSIONS OF PHASE I ESA

It is our opinion that the former UST and associated gasoline release is a recognized environmental condition (REC). Although the UST was removed and site closure was granted by the RWQCB, TPH was detected in the soil at the base of the excavation and files reviewed at the LAFD and RWQCB do not indicate that any soil remediation was conducted. Contaminated groundwater was reportedly observed in the nearby sump for the swimming pool and case closure was granted before a groundwater assessment was conducted. Additionally, there is no indication that the soil samples were analyzed for MTBE.

It is our opinion that the former presence of a bus maintenance garage is a REC because of the potential for soil or groundwater to be impacted with hydrocarbons, solvents, and other chemicals in the vicinity of the former hydraulic lift, abandoned clarifier, or possible underground storage tank.

It is our opinion that the former use of the subject property as a golf course is a de minimis condition. The potential for fertilizers and pesticides to impact the underlying soil or groundwater should be considered low.

Based on the minimal amount of staining of the wood floor in the groundskeeping shed set atop a concrete pad, the potential to impact the underlying soil should be considered low. It is our opinion that the slight staining beneath the small diesel containers is a de minimis condition.

It is our opinion that the small pool of oil beneath elevator equipment is a de minimis condition. As the concrete floor appeared to be in good condition, the potential to impact the underlying soil should be considered low.

Rincon has performed a Phase I ESA in general conformance with the scope and limitations of ASTM Practice E 1527 of 3900 Stansbury Avenue, Sherman Oaks. This assessment has revealed evidence of the following recognized environmental conditions in connection with the property: the former presence of a UST and associated gasoline release on the subject site and the former presence of a bus maintenance garage on the subject site.

PHASE II ENVIRONMENTAL SITE ASSESSMENT

To evaluate the potential site impact associated with the former UST release and the former presence of a bus maintenance garage, a geophysical survey was conducted in the vicinity of the former garage and a Geoprobe drill rig was used to collect soil samples in the vicinity of the former UST, clarifier, and hydraulic hoist (Figure 4). Select soil samples were analyzed for the presence of hydrocarbons, volatile organic compounds (VOCs, EPA 8260B), oxygenates, and PCBs (see Table 3) and metals (see Table 4). A sample was also collected from the pool sump pump groundwater and analyzed for hydrocarbons and VOCs (see Table 5).

PHASE II METHODOLOGY

GEOPHYSICAL SURVEY

A geophysical survey was conducted in the vicinity of the former bus maintenance garage on December 21, 2004 by GeoVision Geophysical Services. The purpose of the geophysical survey was to determine if there is a UST present in this area. The survey included investigation in the vicinity of the observed tank vent and covered tank fill access near the former bus garage using a ground-penetrating radar (GPR) instrument. Additionally, GPR profiles were collected at 5-foot intervals in both the north-south and east-west directions in the parking lot area adjacent to the former bus garage. See Appendix 5 for a copy of the documentation provided by GeoVision.

GEOPROBE SAMPLING

A Geoprobe sampling rig was used to collect soil samples from ten locations at the subject site (samples B1 through B10; see Figure 4 for sample locations). The Geoprobes were drilled by Core Probe International, Inc. of Irwindale, California on December 27 and 30, 2005 under the responsible oversight of a California registered geologist.

The probes were advanced by hydraulically driving a two-inch diameter rod equipped with a soil sampling tool. The Geoprobe borings were advanced to depths of between 8 and 30 feet below grade. Where possible, soil samples were collected from each probe at 5-foot intervals. When the target sampling depth was reached, a decontaminated, stainless steel soil sampler was attached to the end of the rod. The soil sampler was comprised of a one-inch diameter tube containing four 6-inch long brass sample liners. By advancing this sampler into the soil, soil was forced into the opening of the sampling tube and a sample was obtained. Once the sampler was filled, it was retrieved and the brass sample liners were removed. The bottom brass liners were retained for laboratory analysis and preserved onsite using EPA method 5035. Soil was collected from the bottom brass liner using a disposable EnCore sampling device. The EnCore soil sample was then placed into 40-milliliter (ml) VOA vials containing either sodium bisulfate preservative or a methanol preservative. The remaining soil from the bottom brass liner was sealed with Teflon, capped, labeled. All samples were stored in a cooler with blue ice pending delivery to the analytical laboratory. A total of 33 soil samples were collected from the Geoprobe borings during this assessment. Soil within the sampling tip and the other liners was used for soil classification and to screen for volatile organics using a photoionization detector (PID). Copies of the soil boring logs are included in Appendix 6.

Upon completion of the sampling program, all probe holes were backfilled with bentonite chips. Sampling equipment was decontaminated between use by washing with a non-phosphate detergent solution followed by a potable water rinse.

POOL SUMP PUMP GROUNDWATER SAMPLING

On December 27, 2005, a groundwater grab sample was collected from the pool sump pump using a disposable bailer. The groundwater collected was placed in a one-liter glass amber bottle and three 40- ml glass vials. Care was taken to ensure no headspace or bubbles were created within the vials. The groundwater sample containers were sealed, placed on ice, and delivered under chain of custody documentation to a state certified laboratory via courier.

LABORATORY ANALYSIS

The soil and groundwater samples were transported to American Scientific Laboratories of Los Angeles, California under chain-of-custody documentation. The following analyses were performed:

Sampling Area	TPH-g[1]	TPH-DRO/ TPH-ORO[2]	VOCs[1]	BTEX only[1]	Oxygenates[1]	PCBs[3]	Lead[4]	Metals[5]
Former UST Area	14	7		14	14		5	
Waste Oil Tank		6	6					6
Hoist Area		3				2		3
Clarifier		2	2					
Pool Sump	1	1	1					

1 – EPA Method 8260B
2 – EPA Method 8015M
3 – EPA Method 8082
4 – EPA Method 6010B
5 – EPA Method 6010B/7471A

PHASE II RESULTS

GEOPHYSICAL SURVEY

The results of the geophysical survey conducted on December 21, 2004 indicate that a small UST remains in the vicinity of the observed tank vent and covered tank fill access. GeoVision Geophysical Services marked the outline of the UST with marking paint. However, the entire outline of the tank was not identified due to a large storage pile of school equipment. Based on the identified tank dimensions and the location of the tank vent, the tank dimensions are assumed to be about 10 feet long by 4 feet wide. Therefore, based on the size and location of the identified UST, this was assumed to be a waste oil tank.

A copy of the geophysical survey documentation is included in Appendix 5.

SOIL SAMPLING

Soil discoloration and elevated PID readings were noted in soil samples collected from B1 at a depth of 20 feet below grade and B3 at depths of 15, 20, and 25 feet below grade. A gasoline odor was noted in soil samples collected from B1 at a depth of 25 feet below grade and B3 at depths of 20, 25, and 30 feet below grade. A sweet chemical odor was noted in soil samples collected from B1, B2, and B4 at 20 feet below grade and in B3 at 15 feet below grade. The maximum PID reading of 985 was measured in the soil sample collected from B1 at 25 feet below grade. Soil was comprised primarily of sandy, silty clay mixtures and siltstone. Groundwater was not encountered in the Geoprobe borings. Copies of the soil boring logs are included in Appendix 6.

A summary of the soil analytical testing program is included in Tables 3 and 4. Copies of the laboratory analytical reports are included in Appendix 7. A maximum concentration of 1,080 mg/kg TPH-g was detected in B1 at 25 feet below grade. Maximum concentrations of 8.4 mg/kg benzene, 31 mg/kg toluene, 13.7 mg/kg ethylbenzene and 104.2 mg/kg total xylenes were detected in B1 at 25 feet below grade. A maximum concentration of 0.798 mg/kg tert-butyl alcohol (TBA) was detected in B1 at 20 feet below grade and a maximum concentration of 6.95 mg/kg MTBE was detected in B4 at 20 feet below grade. A maximum concentration of 0.12 mg/kg acetone and 0.27 mg/kg tetrachloroethylene (PCE) was detected in B6 at a depth of 5 feet below grade. None of the soil samples tested for TPH-DRO, TPH-ORO, and PCBs had detectable levels of these constituents. Metals were detected at varying concentrations in the soil samples collected and analyzed for metals.

GROUNDWATER SAMPLING

A summary of the pool sump water analytical testing program is included in Table 5. Copies of the laboratory analytical reports are included in Appendix 7. The water sample had no detectable levels of TPH-g, TPH-DRO, TPH-ORO, and VOCs.

DISCUSSION

To evaluate the significance of the reported contaminant levels in the soil samples, we compared these levels to threshold levels established by RWQCB, the United States Environmental Protection Agency (USEPA), and the State of California Department of Toxic Substances Control (DTSC). The TPH, BTEX, MTBE and PCE concentrations were compared to the RWQCB thresholds. The metals concentrations were compared to the USEPA soil cleanup thresholds and DTSC hazardous waste thresholds.

HYDROCARBONS IN SOIL

The RWQCB maximum soil screening level (SSL) for TPH-g ranges from 100 to 1,000 mg/kg, depending on distance above groundwater. Assuming that the depth to groundwater beneath the former UST area is between 60 and 90 feet below grade (based on the 1988 Enviropro, Inc. report), the soil samples collected from the former UST area would be in the range of 30 to 85 feet above groundwater. The RWQCB SSL for TPH-g detected in the soil from 20 to 150 feet above groundwater is 500 mg/kg. Of the 14 soil samples tested for TPH-g, the RWQCB SSL was exceeded in one sample. TPH-g was detected in B1 at a concentration of 1,080 mg/kg at a depth of 25 feet below grade (approximately 35 to 65 feet above groundwater).

VOLATILE ORGANIC COMPOUNDS IN SOIL

The RWQCB SSLs for BTEX are determined using site-specific distance above groundwater and lithology. Without specific depth to groundwater data for the site, we cannot calculate specific SSLs for BTEX. However, the ranges of BTEX SSLs for various soil types and distances above groundwater are provided below:

	Benzene	Toluene	Ethylbenzene	Xylenes
SSL	0.011-0.8 mg/kg	0.15-43 mg/kg	0.7-170 mg/kg	1.75-465 mg/kg

Using the above SSL ranges as a guideline, concentrations of BTEX detected in soil beneath the site could potentially exceed these levels in the following samples: B1-20, B3-20, B3-25 and B4-20. The benzene concentration detected in B1-25 exceeds the highest SSL range value for benzene. Therefore, regardless of soil type or distance above groundwater, the concentration of benzene at this location exceeds the RWQCB SSL.

The RWQCB SSL for MTBE is calculated using the California drinking water Maximum Contaminant Level (MCL) level and site-specific distance above groundwater and lithology. For various soil types and distances above groundwater, the MTBE SSL ranges from 0.013 mg/kg to 3.315 mg/kg. Using the SSL range as a guideline, concentrations of MTBE detected in soil beneath the site could potentially exceed these levels in the following samples: B1-20, B1-25, B3-15, B3-20, B3-25, B3-30, B4-10, B4-15 and B4-20. The calculated SSL for PCE ranges from 0.005 to 1.275 mg/kg for various soil types and distances above groundwater. Low concentrations of PCE were detected near the waste oil tank in soil samples B5 and B6 at 5 feet below grade. Based on the shallow depth of the detected PCE, it would not be likely that the

PCE SSL would be exceeded in the B5 and B6 boring locations. SSL ranges for acetone and TBA could not be determined as there are no MCLs for these constituents.

METALS IN SOIL

The levels of metals detected were compared to soluble threshold limit concentration (STLC) levels and total threshold limit concentration (TTLC) levels established by the State of California DTSC. The STLC and the TTLC are used to determine whether soil or other solid waste would be classified as a hazardous or non-hazardous waste for disposal purposes. STLC and TTLC levels for metals are listed in Table 4. The metal concentrations detected in the soil samples tested for these constituents did not exceed TTLC levels or ten times STLC levels (Table 4). Therefore, if soil were to be excavated from this location, the metals content in the resulting soil would be considered non-hazardous for disposal purposes.

In addition to TTLC/STLC values, the metals concentrations in the soil sample were compared to USEPA PRGs. The PRG-R and PRG-I values for metals are listed in Table 4. With the exception of arsenic, the detected concentrations of metals were all below their respective PRG-R and PRG-I values.

For arsenic, normal background concentrations found in California soils are typically above the USEPA PRGs for both residential and industrial settings. The PRGs for residential and industrial settings for arsenic are 0.062 and 0.25 mg/kg, respectively. The USEPA states that generally they do not require cleanup below natural background levels. In light of this fact and in our experience, regulatory agencies typically consider the use of local or regional background concentrations as the threshold concentration. Although the levels of arsenic detected in the soil samples analyzed during this assessment exceed the arsenic PRGs, they were within the published ranges for arsenic in soils in the Western United States (Shacklette, H.T. and Boerngen, J.G., 1984) and appear to be within normal background levels. As discussed in the Shacklette and Boerngen report, the range of arsenic observed in background soil in the Western United States was between 0.10 mg/kg and 97 mg/kg. Overall, the levels of metals detected in the soil samples were low and likely represent naturally occurring background concentrations of metals in soil.

PHASE II CONCLUSIONS

The following conclusions are based on the geophysical survey and soil and groundwater sampling and analysis for this assessment:

- The results of the geophysical survey conducted on December 21, 2004 indicate that a small UST remains in the vicinity of the observed tank vent and covered tank fill access in the former bus garage area. Based on the size and location of the identified UST, this was assumed to be a waste oil tank.

- The non-detectable levels of TPH-DRO, TPH-ORO, and PCBs in the soil samples collected from beneath the subject property indicate that soil at the locations tested have not been impacted by these contaminants.

- TPH-g and benzene were detected at concentrations exceeding the RWQCB SSL in sample B1 at 25 feet below grade (former UST area). As drilling refusal was encountered at 25 feet below grade, no deeper soil samples were collected from this boring, and the vertical extent of the contamination was not determined.

- BTEX was detected at concentrations that could potentially exceed the RWQCB SSLs in samples B1-20, B3-20, B3-25 and B4-20 (former UST area). MTBE was detected at concentrations that could potentially exceed the RWQCB SSLs in samples B1-20, B1-25, B3-15, B3-20, B3-25, B3-30, B4-10, B4-15 and B4-20. Actual depth to groundwater data is needed to calculate exact SSLs to determine whether SSLs have been exceeded in these samples.

- TBA was detected in several samples in the former UST area. The SSL for TBA could not be determined as there is no MCL for this constituent.

- Low concentrations of PCE and acetone were detected near the waste oil tank in soil samples B5 and B6 at 5 feet below grade. However, based on the shallow depth of the detected PCE, it is not likely that the PCE SSL would be exceeded at these locations. However, it is possible that the low concentrations of PCE detected could be an indication of potentially higher concentrations of PCE existing in the vicinity. The acetone SSL could not be determined as there is no MCL for this constituent.

- The metal concentrations detected in the soil samples tested for these constituents did not exceed TTLC levels or ten times STLC levels. Therefore, if soil were to be excavated from this location, the metals content in the resulting soil would be considered non-hazardous for disposal purposes. With the exception of arsenic, metals were well below their respective PRGs. Although the levels of arsenic detected in the soil samples analyzed during this assessment exceed the arsenic PRGs, they were within the published ranges for arsenic in soils in the Western United States (Shacklette, H.T. and Boerngen, J.G., 1984) and appear to be within normal background levels. We also believe that the other metals are within naturally occurring background concentrations for metals in soil.

- The pool sump groundwater sample had no detectable levels of TPH-g, TPH-DRO, TPH-ORO, and VOCs.

LIMITATIONS

This Phase II ESA has been prepared for and is intended for the exclusive use of Latham & Watkins LLP and the Buckley School. The contents of this report should not be relied upon by any other party without the written consent of Rincon Consultants, Inc.

Our conclusions regarding the site are based on the results of a limited subsurface sampling program. The results of this evaluation are qualified by the fact that only limited sampling and analytical testing was conducted during this assessment.

This scope was not intended to completely establish the quantities and distribution of contaminants present at the site or to determine the cost to remediate the site. The concentrations of contaminants measured at any given location may not be representative of conditions at other locations. Further, conditions may change at any particular location as a function of time in response to natural conditions, chemical reactions and other events. Conclusions regarding the condition of the site do not represent a warranty that all areas within the site are similar to those sampled.

REFERENCES

The following published reference materials were used in preparation of this Phase I and Phase II ESA:

Environmental database: Environmental Data Resources (EDR) report dated November 23, 2004.
Geology: Geologic Map of the Beverly Hills and Van Nuys (South 1/2) Quadrangles (Dibblee 1991) and EDR report.
Groundwater: Engineering Report on Soil Gas Investigation at Buckley School, Enviropro Inc., October 31, 1988.
Topography: USGS topographic map, Van Nuys Quadrangle (1966, photorevised 1972)
Oil and gas records: Division of Oil and Gas Munger Map Book (2001)
Aerial photographs: Photos maintained by UCSB Map and Imagery Department
Historic topographic maps: Maps maintained by UCSB Map and Imagery Department
Other:

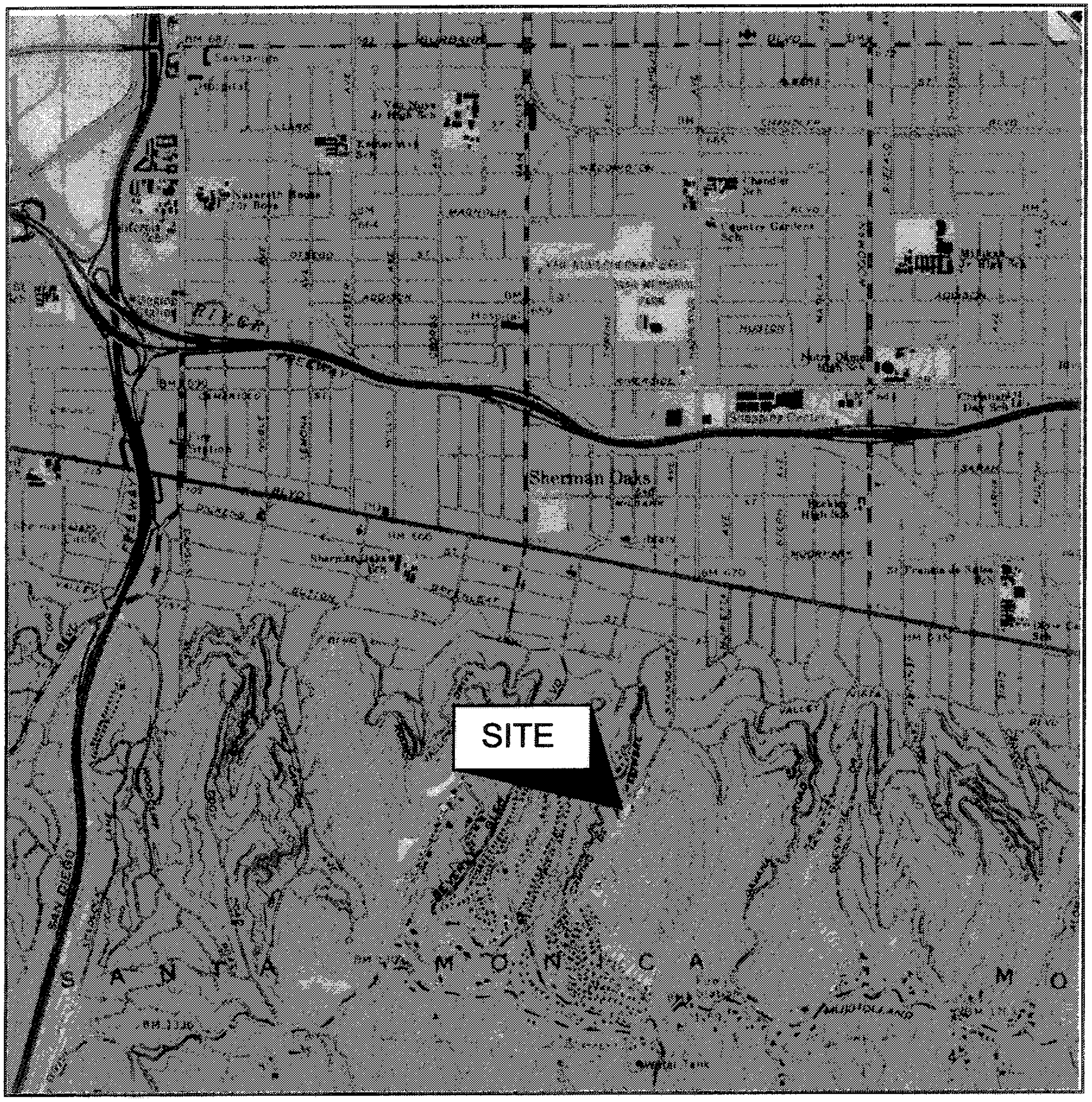
- Engineering Report on Soil Gas Investigation at Buckley School, Enviropro Inc., October 31, 1988.
- Background Concentrations of Trace and Major Elements in California Soils, Kearney Foundation Special Report, UC-Riverside and CAL-EPA DTSC, Bradford et al, March 1996

QUALIFICATIONS

The environmental professionals responsible for conducting this Phase I ESA and preparing the report include Tricia Bartholome and Walt Hamann. Their qualifications are summarized below.

Walt Hamann, RG, CEG, CHG, REA II, is a Principal and Senior Geologist with Rincon Consultants. He holds a Bachelor of Science degree in geology from the University of California, Santa Barbara and a Master of Science degree in geology from the University of California, Los Angeles. He has over 17 years of experience conducting assessment and remediation projects and has prepared or overseen the preparation of hundreds of Phase I and Phase II Environmental Site Assessments throughout California. Mr. Hamann is a Registered Geologist (#4742), Certified Engineering Geologist (#1635), Certified Hydrogeologist (#208) and Registered Environmental Assessor II (#20063) with the State of California.

Tricia Ainsworth, REA I, is an Associate Environmental Engineer with Rincon Consultants. She holds a Bachelor of Science degree in environmental engineering from California Polytechnic State University, San Luis Obispo. Ms. Bartholome has experience with regulatory compliance and reporting in the fields of air, water, and hazardous waste management, as well as environmental assessment and remediation of soil and groundwater. Ms. Bartholome's responsibilities at Rincon include implementation of site assessments and development of site remediation programs within the Environmental Site Assessment and Remediation Group. Ms. Bartholome is a certified Engineer-in-Training (#XE105131) with the State of California.



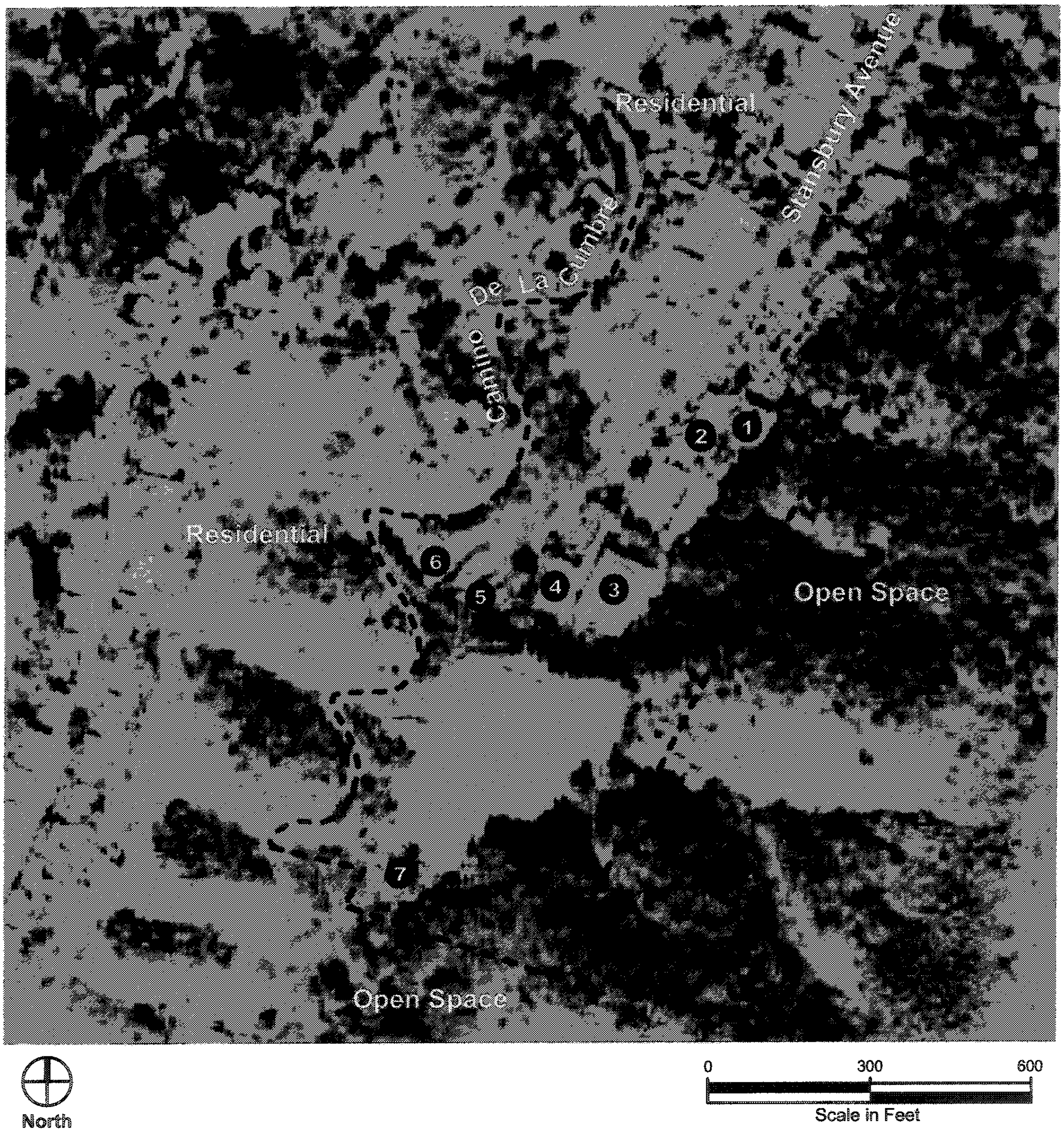
Printed from TOPO!, 2001 National Geographic Holdings

0 1/2 1
Scale in Miles

NORTH

Vicinity Map

Figure 1



Legend

- Site Boundary
- 1 Library
- 2 Administration Building
- 3 Pavilion (gym)
- 4 Art/Science Building
- 5 Former UST Area
- 6 Former Bus Maintenance Garage
- 7 Storage Sheds

Site & Adjacent Land Use Map

Figure 2

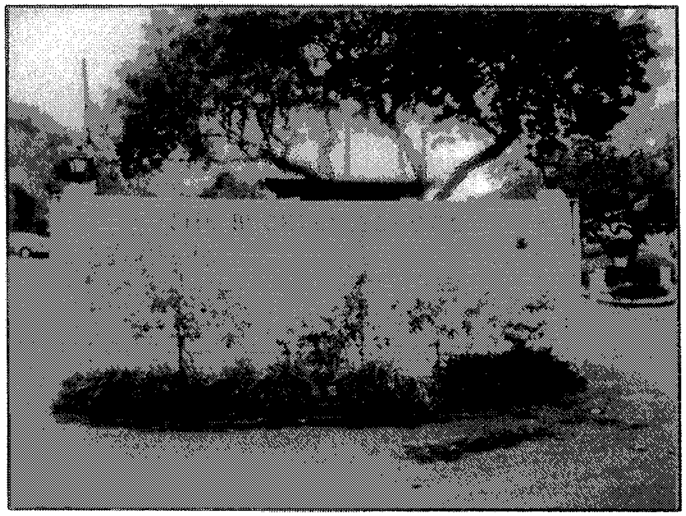


Photo 1 - View of entrance to subject property at the south end of Stansbury Avenue.

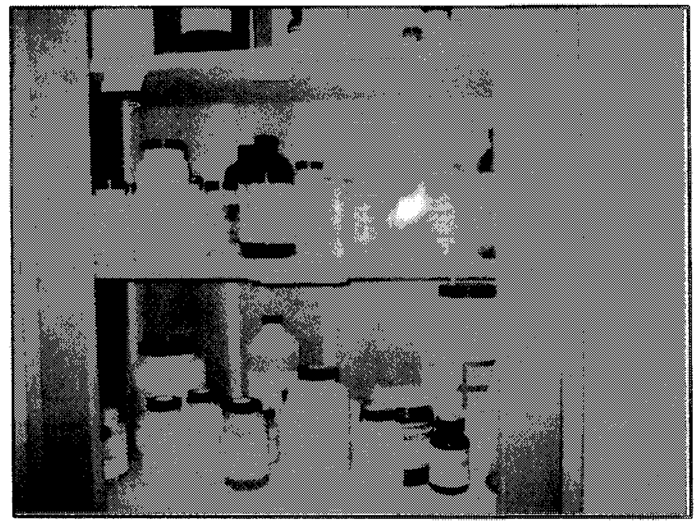


Photo 2 - Laboratory chemicals stored in the chemistry supply room.

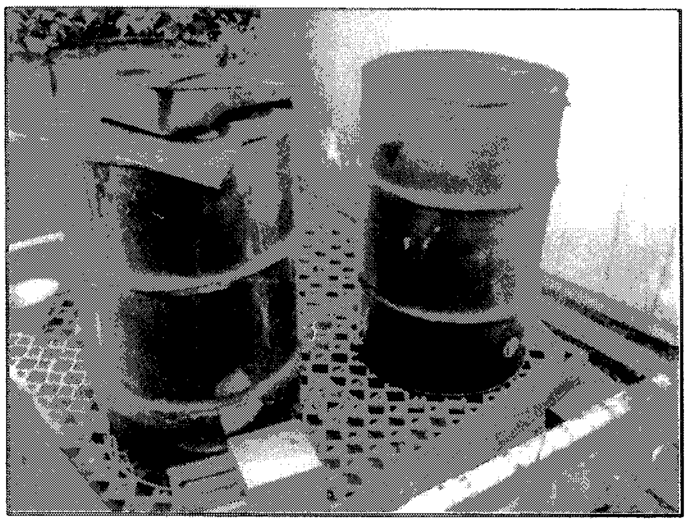


Photo 3 - View of 55-gallon waste paint and waste oil drums in the storage shed area.

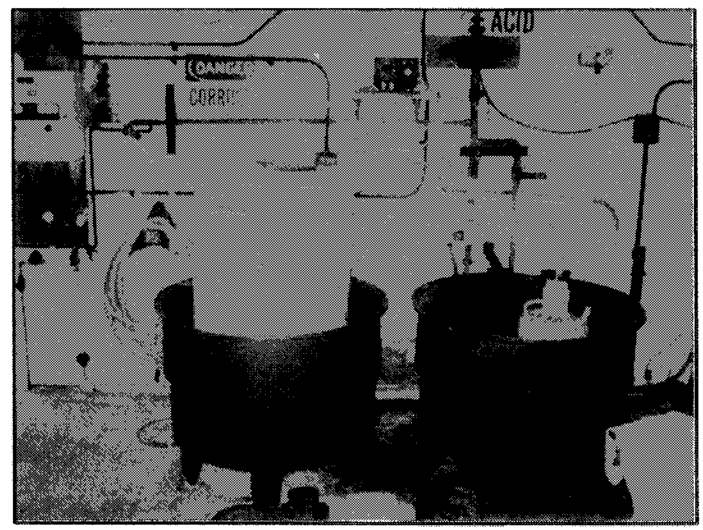


Photo 4 - View of swiming pool chemicals stored in the basement of the Pavilion building.

Site Photographs

Figure 3

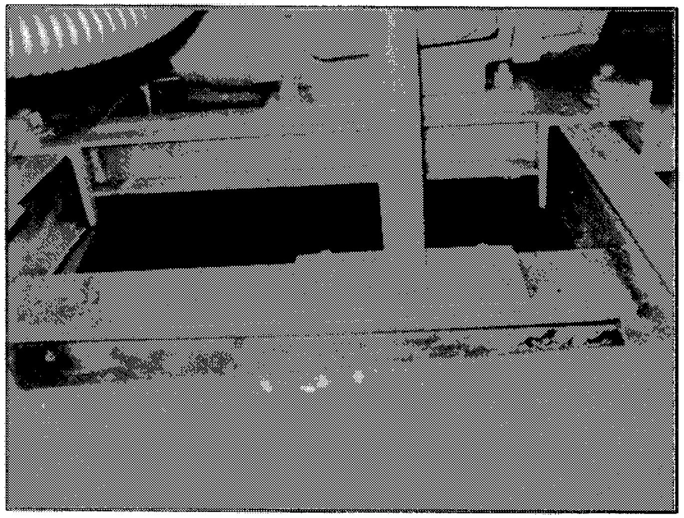


Photo 5 - View of leaking elevator equipment in the Administration building.

Photo 6 - View of 30-gallon diesel drum and small containers of gasoline.

Photo 7 - View of possible underground storage tank vent near the former bus maintenance garage.

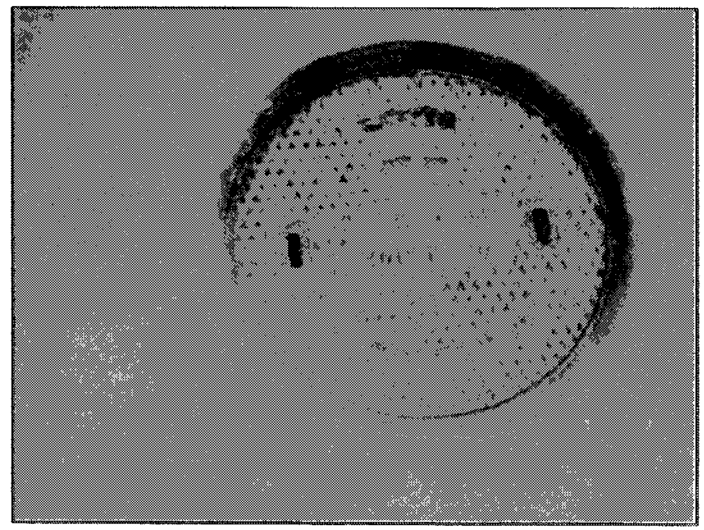


Photo 8 - View of possible tank fill access located near possible tank vent.

Site Photographs

Figure 3

Table 3 - Analytical Testing Summary - TPH, VOCs, Oxygenates and PCBs
December 27 and 30, 2004

Boring	Depth (feet)	TPH (mg/kg)			Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	Other VOCs (mg/kg)	Oxygenates (mg/kg)	PCBs (mg/kg)
		Gasoline (C4-C12)	DRO (C13-C22)	ORO (C22+)							
December 27, 2004 Sampling Event											
Former UST Area											
B1	5	-	-	-	-	-	-	-	-	-	-
	10	ND	ND	ND	0.002	0.002	ND	ND	-	ND	-
	15	ND	ND	ND	ND	ND	ND	ND	-	ND	-
	20	2.05	-	-	0.032	0.09	0.024	0.195	-	MTBE - 0.816 TBA - 0.798	-
	25	1,080	ND	ND	8.4	31	13.7	104.2	-	MTBE - 3.13	-
B2	5	-	-	-	-	-	-	-	-	-	-
	10	-	-	-	-	-	-	-	-	-	-
	15	ND	-	-	0.002	ND	ND	ND	-	ND	-
	20	ND	-	-	ND	ND	ND	ND	-	ND	-
B3	5	-	-	-	-	-	-	-	-	-	-
	10	93.4	ND	ND	ND	ND	ND	ND	-	ND	-
	15	0.646	ND	ND	0.007	0.003	ND	ND	-	MTBE - 0.206 TBA - 0.32	-
	20	2.55	ND	ND	0.07	ND	0.019	ND	-	MTBE - 1.05 TBA - 0.792	-
	25	28.5	ND	ND	0.295	1.98	0.67	3.79	-	MTBE - 2.74	-
	30	1.93	-	-	0.013	ND	0.053	0.054	-	MTBE - 1.05 TBA - 0.302	-
B4	5	-	-	-	-	-	-	-	-	-	-
	10	0.55	-	-	ND	0.002	ND	ND	-	MTBE - 0.129 TBA - 0.392	-
	15	2.02	-	-	0.004	0.002	ND	ND	-	MTBE - 1.27 TBA - 0.346	-
	20	10.2	-	-	0.027	0.054	0.053	0.245	-	MTBE - 6.95	-
Detection Limit		0.5-50	10	50	0.002-0.2	0.002-0.2	0.002-0.2	varies	varies	varies	varies

Table 3 - Analytical Testing Summary - TPH, VOCs, Oxygenates and PCBs
December 27 and 30, 2004

Boring	Depth (feet)	TPH (mg/kg) Gasoline (C4-C12)	TPH (mg/kg) DRO (C13-C22)	TPH (mg/kg) ORO (C22+)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	Other VOCs (mg/kg)	Oxygenates (mg/kg)	PCBs (mg/kg)
December 27, 2004 Sampling Event											
Waste Oil Tank											
B5	5	-	ND	ND	ND	ND	ND	ND	acetone - 0.106 PCE - 0.018	-	-
	10	-	ND	ND	ND	ND	ND	ND	ND	-	-
	15	-	ND	ND	ND	ND	ND	ND	ND	-	-
B6	5	-	ND	ND	ND	ND	ND	ND	acetone - 0.12 PCE - 0.027	-	-
	10	-	ND	ND	ND	ND	ND	ND	ND	-	-
	15	-	ND	ND	ND	ND	ND	ND	ND	-	-
Hoist Area											
B7	5	-	ND	ND	-	-	-	-	-	-	-
	10	-	ND	ND	-	-	-	-	-	-	ND
December 30, 2004 Sampling Event											
Hoist Area											
B8	5	-	-	-	-	-	-	-	-	-	-
	9	-	ND	ND	-	-	-	-	-	-	ND
Clarifier											
B9	8	-	-	-	-	-	-	-	-	-	-
	10	-	ND	ND	ND	ND	0.004	ND	ND	-	-
B10	5	-	-	-	-	-	-	-	-	-	-
	10	-	ND	ND	ND	ND	0.003	ND	ND	-	-
Detection Limit		0.5-50	10	50	0.002-0.2	0.002-0.2	0.002-0.2	varies	varies	varies	varies

\- Not analyzed
ND - Not detected
mg/kg - milligrams per kilogram (parts per million)
PCE - tetrachloroethylene

Analyses:

TPH-G (total petroleum hydrocarbons, gasoline range) by EPA Method 8260B
TPH-DRO / TPH-ORO (total petroleum hydrocarbons, diesel range organics / oil range organics) by EPA Method 8015M
BTEX and Oxygenates by EPA Method 8260B
VOCs (volatile organic compounds) by EPA Method 8260B (see attached laboratory report for complete listing of VOCs)
PCBs (Polychlorinated Biphenyls) by EPA Method 8082

Table 4 - Analytical Testing Summary - 17 CCR Metals
December 27 and 30, 2004

Boring/ Depth (ft)	17 CCR Metals Results in milligrams per kilogram (mg/kg)																
	Antimony	Arsenic	Barium	Beryllium	Cadmium	Chromium	Cobalt	Copper	Lead	Mercury	Molyb	Nickel	Selenium	Silver	Thallium	Vanadium	Zinc
December 27, 2004 Sampling Event																	
Former UST Area																	
B1-15	-	-	-	-	-	-	-	-	1.40	-	-	-	-	-	-	-	-
B1-20	-	-	-	-	-	-	-	-	2.14	-	-	-	-	-	-	-	-
B1-25	-	-	-	-	-	-	-	-	ND	-	-	-	-	-	-	-	-
B3-20	-	-	-	-	-	-	-	-	1.40	-	-	-	-	-	-	-	-
B3-25	-	-	-	-	-	-	-	-	1.91	-	-	-	-	-	-	-	-
Waste Oil Tank																	
B5-5	1.03	11.8	155	ND	0.50	34.5	10.3	24.0	4.63	ND	0.68	25.6	ND	ND	ND	60.1	55.9
B5-10	ND	3.14	72.1	ND	0.91	16.2	4.73	29.1	0.74	ND	3.00	38.9	ND	ND	ND	66.5	69.3
B5-15	0.51	6.45	138	ND	1.88	12.2	3.40	15.5	ND	ND	5.14	22.3	ND	ND	ND	66.6	47.3
B6-5	0.90	12.2	178	ND	0.57	35.0	13.7	26.5	4.25	ND	0.74	28.6	ND	ND	ND	62.4	61.0
B6-10	1.03	9.51	222	ND	1.72	27.5	7.87	23.7	2.31	ND	1.06	26.6	ND	ND	ND	57.6	57.7
B6-15	0.64	6.67	113	ND	2.76	23.9	2.48	20.0	ND	ND	5.61	29.7	ND	ND	ND	76.6	60.4
Hoist Area																	
B7-10	ND	14.1	50.8	ND	1.24	11.3	4.26	17.5	0.58	ND	3.82	24.2	ND	ND	ND	71.5	36.0
December 30, 2004 Sampling Event																	
B9-10	0.63	0.90	64.1	ND	2.87	10.7	3.23	19.8	0.38	ND	1.92	22.8	ND	0.84	ND	40.1	55.5
B10-10	0.75	3.57	125	ND	0.81	10.4	4.31	20.0	2.18	ND	1.58	19.4	ND	0.70	ND	44.6	51.8
Detection Limit	0.50	0.25	0.50	0.50	0.50	0.50	0.50	0.50	0.25	0.20	0.50	0.50	0.50	0.50	0.50	0.50	0.50
STLC	15	5	100	0.75	1	5 or 560^	80	25	5	0.2	350	20	1	5	7	24	250
TTLC	500	500	10,000	75	100	500 or 2500	8,000	2,500	1,000	20	3,500	2,000	100	500	700	2,400	5,000
PRG-R	31	0.062	5,400	150	37	210	900	3,100	150	23	390	1,600	390	390	5.2	78	23,000
PRG-I	410	0.25	67,000	1,900	450	450	1,900	41,000	800	310	5,100	20,000	5,100	5,100	67	1,000	100,000

\- Not analyzed
ND - Not detected
STLC - Soluble threshold limit concentration
TTLC - Total threshold limit concentration
PRG - United States Environmental Protection Agency Region 9 Preliminary Remediation Goal for residential (R) and industrial (I) sites (October 2004)
^ - STLC for Cr 3+ is 560 mg/L; STLC for Cr 6+ (Hexavalent Chromium) is 5 mg/L

Table 5 - Pool Sump Water Analytical Testing Summary - TPH and VOCs
December 27, 2004

Sample Designation	TPH-g (C4-C12) (µg/L)	TPH-DRO (C13-C22) (µg/L)	TPH-ORO (C22+) (µg/L)	Benzene (µg/L)	Toluene (µg/L)	Ethyl-benzene (µg/L)	Total Xylenes (µg/L)	Other VOCs (µg/L)
Pool Sump*	ND	ND	ND	ND	ND	ND	ND	ND
Detection Limit	50	500	500	1.0	1.0	1.0	varies	varies

µg/L - milligrams per liter
ND - not detected at or above detection limit
TPH-g (total petroleum hydrocarbons, gasoline range)
TPH-DRO / TPH-ORO (total petroleum hydrocarbons, diesel range organics / oil range organics)
* Pool sump water sample collected using a disposable bailer

Analyses:
TPH-g and VOCs by EPA Method 8260B
TPH-DRO / TPH-ORO by EPA Method 8015M

Appendix 1

Environmental Database Search Report

EDR™ Environmental
Data Resources Inc

The EDR Radius Map
with GeoCheck®

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA 91423

Inquiry Number: 01313273.1r

November 23, 2004

The Standard in Environmental Risk Management Information

440 Wheelers Farms Road
Milford, Connecticut 06460

Nationwide Customer Service

Telephone: 1-800-352-0050
Fax: 1-800-231-6802
Internet: www.edrnet.com

TABLE OF CONTENTS

Thank you for your business.
Please contact EDR at 1-800-352-0050
with any questions or comments.

EXECUTIVE SUMMARY

A search of available environmental records was conducted by Environmental Data Resources, Inc. (EDR). The report meets the government records search requirements of ASTM Standard Practice for Environmental Site Assessments, E 1527-00. Search distances are per ASTM standard or custom distances requested by the user.

TARGET PROPERTY INFORMATION

ADDRESS

3900 STANSBURY AVENUE
SHERMAN OAKS, CA 91423

COORDINATES

Latitude (North):	34.139600 - 34° 8' 22.6"
Longitude (West):	118.443600 - 118° 26' 37.0"
Universal Tranverse Mercator:	Zone 11
UTM X (Meters):	366896.9
UTM Y (Meters):	3778381.0
Elevation:	797 ft. above sea level

USGS TOPOGRAPHIC MAP ASSOCIATED WITH TARGET PROPERTY

Target Property:	34118-B4 VAN NUYS, CA
Source:	USGS 7.5 min quad index

TARGET PROPERTY SEARCH RESULTS

The target property was identified in the following government records. For more information on this property see page 6 of the attached EDR Radius Map report:

Site	Database(s)	EPA ID
BUCKLEY SCHOOL BUS GARAGE 3900 STANSBURY AVE SHERMAN OAKS, CA 91423	RCRIS-SQG FINDS HAZNET	CAD077262558
THE BUCKLEY SCHOOL 3900 STANSBURY AVE SHERMAN OAKS, CA 91403	CA FID UST	N/A
BUCKLEY SCHOOL 3900 STANSBURY AVE SHERMAN OAKS, CA 91423	LUST Cortese	N/A

DATABASES WITH NO MAPPED SITES

No mapped sites were found in EDR's search of available ("reasonably ascertainable ") government records either on the target property or within the ASTM E 1527-00 search radius around the target property for the following databases:

FEDERAL ASTM STANDARD

NPL........................ National Priority List

EXECUTIVE SUMMARY

Proposed NPL	Proposed National Priority List Sites
CERCLIS	Comprehensive Environmental Response, Compensation, and Liability Information System
CERC-NFRAP	CERCLIS No Further Remedial Action Planned
CORRACTS	Corrective Action Report
RCRIS-TSD	RCRAInfo
RCRIS-LQG	RCRAInfo
ERNS	Emergency Response Notification System

STATE ASTM STANDARD

AWP	Annual Workplan Sites
Cal-Sites	Calsites Database
CHMIRS	California Hazardous Material Incident Report System
Toxic Pits	Toxic Pits Cleanup Act Sites
SWF/LF	Solid Waste Information System
WMUDS/SWAT	Waste Management Unit Database
CA BOND EXP. PLAN	Bond Expenditure Plan
UST	List of Underground Storage Tank Facilities
VCP	Voluntary Cleanup Program Properties
INDIAN UST	Underground Storage Tanks on Indian Land
INDIAN LUST	Leaking Underground Storage Tanks on Indian Land
HIST UST	Hazardous Substance Storage Container Database

FEDERAL ASTM SUPPLEMENTAL

CONSENT	Superfund (CERCLA) Consent Decrees
ROD	Records Of Decision
Delisted NPL	National Priority List Deletions
HMIRS	Hazardous Materials Information Reporting System
MLTS	Material Licensing Tracking System
MINES	Mines Master Index File
NPL Liens	Federal Superfund Liens
PADS	PCB Activity Database System
UMTRA	Uranium Mill Tailings Sites
ODI	Open Dump Inventory
FUDS	Formerly Used Defense Sites
DOD	Department of Defense Sites
INDIAN RESERV	Indian Reservations
RAATS	RCRA Administrative Action Tracking System
TRIS	Toxic Chemical Release Inventory System
TSCA	Toxic Substances Control Act
SSTS	Section 7 Tracking Systems
FTTS INSP	FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)

STATE OR LOCAL ASTM SUPPLEMENTAL

AST	Aboveground Petroleum Storage Tank Facilities
CLEANERS	Cleaner Facilities
CA WDS	Waste Discharge System
DEED	List of Deed Restrictions
NFE	Properties Needing Further Evaluation
SCH	School Property Evaluation Program

EXECUTIVE SUMMARY

EMI .... Emissions Inventory Data
REF .... Unconfirmed Properties Referred to Another Agency
NFA .... No Further Action Determination
CA SLIC .... Statewide SLIC Cases
LOS ANGELES CO. HMS .... HMS: Street Number List
LA Co. Site Mitigation .... Site Mitigation List
AOCONCERN .... San Gabriel Valley Areas of Concern

EDR PROPRIETARY HISTORICAL DATABASES

Coal Gas .... Former Manufactured Gas (Coal Gas) Sites

BROWNFIELDS DATABASES

US BROWNFIELDS .... A Listing of Brownfields Sites
VCP .... Voluntary Cleanup Program Properties

SURROUNDING SITES: SEARCH RESULTS

Surrounding sites were identified.

Elevations have been determined from the USGS Digital Elevation Model and should be evaluated on a relative (not an absolute) basis. Relative elevation information between sites of close proximity should be field verified. Sites with an elevation equal to or higher than the target property have been differentiated below from sites with an elevation lower than the target property.
Page numbers and map identification numbers refer to the EDR Radius Map report where detailed data on individual sites can be reviewed.

Sites listed in ***bold italics*** are in multiple databases.

Unmappable (orphan) sites are not considered in the foregoing analysis.

STATE ASTM STANDARD

NOTIFY 65: Notify 65 records contain facility notifications about any release that could impact drinking water and thereby expose the public to a potential health risk. The data come from the State Water Resources Control Board's Proposition 65 database.

A review of the Notify 65 list, as provided by EDR, has revealed that there is 1 Notify 65 site within approximately 1 mile of the target property.

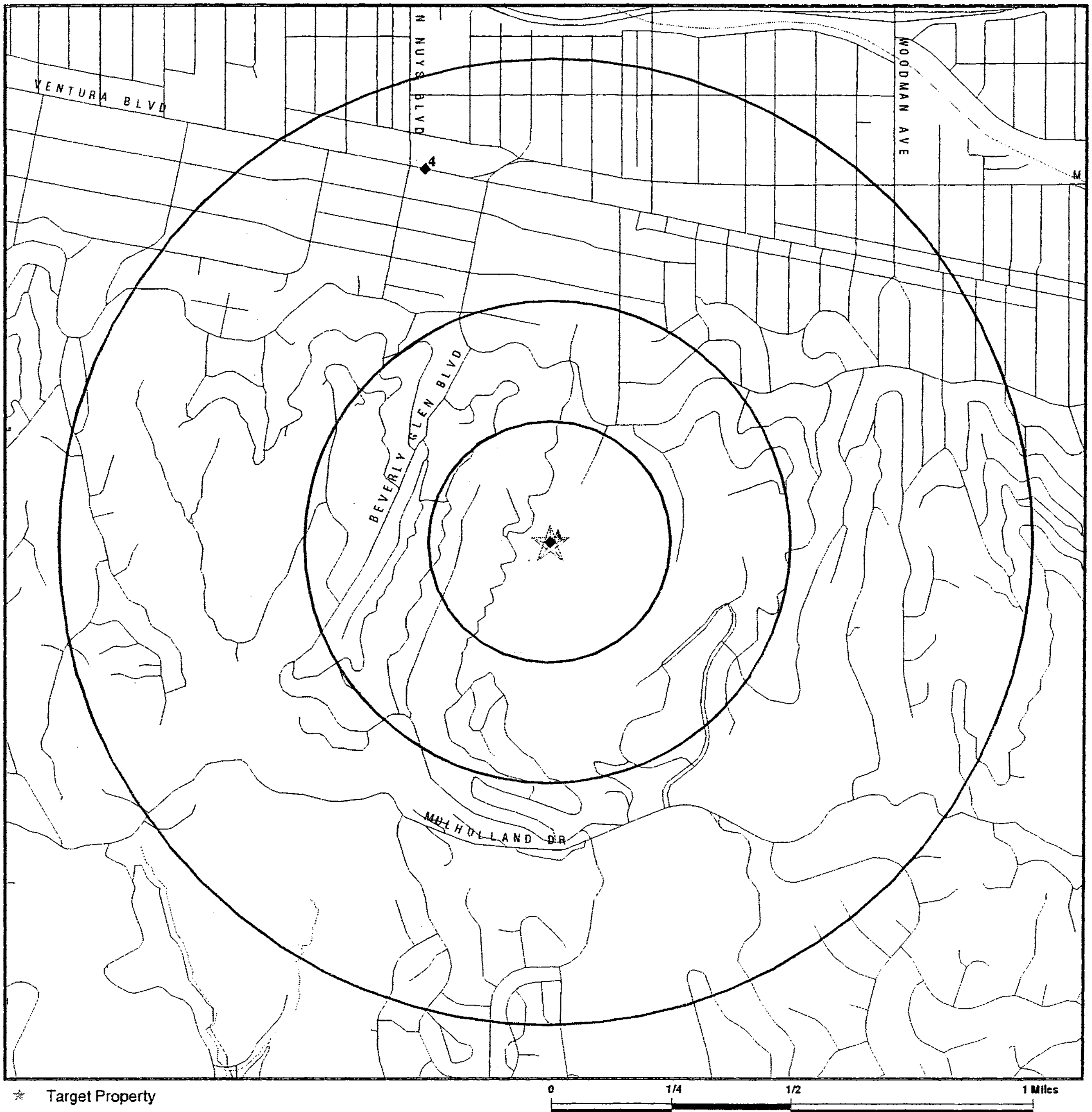
Lower Elevation	Address	Dist / Dir	Map ID	Page
SERVICE STATION	*14478 VENTURA BLVD*	*1/2 - 1 NNW*	*4*	*10*

EXECUTIVE SUMMARY

Due to poor or inadequate address information, the following sites were not mapped:

Site Name	Database(s)
BUILDING #8 LONG BEACH NAVAL	LUST, CHMIRS
BUCKLEY SCHOOL	ERNS

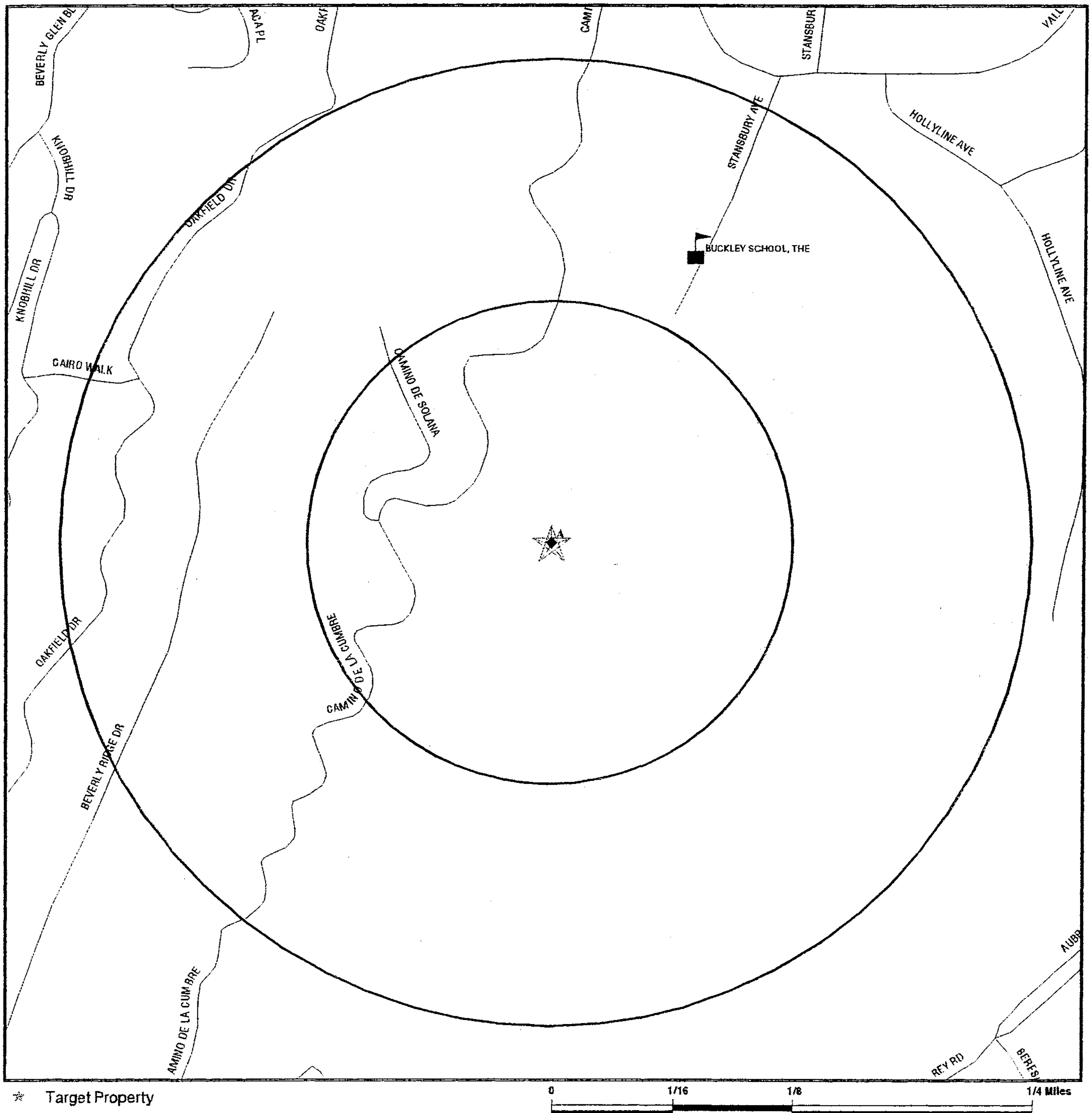
OVERVIEW MAP - 01313273.1r - Rincon



- ☆ Target Property
- ▲ Sites at elevations higher than or equal to the target property
- ◆ Sites at elevations lower than the target property
- Coal Gasification Sites
- National Priority List Sites
- Landfill Sites
- Dept. Defense Sites
- Indian Reservations BIA
- Oil & Gas pipelines
- 100-year flood zone
- 500-year flood zone
- Areas of Concern

TARGET PROPERTY:	Buckley School	CUSTOMER:	Rincon
ADDRESS:	3900 Stansbury Avenue	CONTACT:	Tricia Bartholome
CITY/STATE/ZIP:	Sherman Oaks CA 91423	INQUIRY #:	01313273.1r
LAT/LONG:	34.1396 / 118.4436	DATE:	November 23, 2004 12:38 pm

DETAIL MAP - 01313273.1r - Rincon



☆ Target Property
▲ Sites at elevations higher than or equal to the target property
◆ Sites at elevations lower than the target property
Coal Gasification Sites
Sensitive Receptors
National Priority List Sites
Landfill Sites
Dept. Defense Sites

Indian Reservations BIA
Oil & Gas pipelines
100-year flood zone
500-year flood zone

Areas of Concern

TARGET PROPERTY:	Buckley School	CUSTOMER:	Rincon
ADDRESS:	3900 Stansbury Avenue	CONTACT:	Tricia Bartholome
CITY/STATE/ZIP:	Sherman Oaks CA 91423	INQUIRY #:	01313273.1r
LAT/LONG:	34.1396 / 118.4436	DATE:	November 23, 2004 12:39 pm

MAP FINDINGS SUMMARY

Database	Target Property	Search Distance (Miles)	< 1/8	1/8 - 1/4	1/4 - 1/2	1/2 - 1	> 1	Total Plotted
FEDERAL ASTM STANDARD								
NPL		1.000	0	0	0	0	NR	0
Proposed NPL		1.000	0	0	0	0	NR	0
CERCLIS		0.500	0	0	0	NR	NR	0
CERC-NFRAP		0.250	0	0	NR	NR	NR	0
CORRACTS		1.000	0	0	0	0	NR	0
RCRA TSD		0.500	0	0	0	NR	NR	0
RCRA Lg. Quan. Gen.		0.250	0	0	NR	NR	NR	0
RCRA Sm. Quan. Gen.	X	0.250	0	0	NR	NR	NR	0
ERNS		TP	NR	NR	NR	NR	NR	0
STATE ASTM STANDARD								
AWP		1.000	0	0	0	0	NR	0
Cal-Sites		1.000	0	0	0	0	NR	0
CHMIRS		TP	NR	NR	NR	NR	NR	0
Cortese	X	0.500	0	0	0	NR	NR	0
Notify 65		1.000	0	0	0	1	NR	1
Toxic Pits		1.000	0	0	0	0	NR	0
State Landfill		0.500	0	0	0	NR	NR	0
WMUDS/SWAT		0.500	0	0	0	NR	NR	0
LUST	X	0.500	0	0	0	NR	NR	0
CA Bond Exp. Plan		1.000	0	0	0	0	NR	0
UST		0.250	0	0	NR	NR	NR	0
VCP		0.500	0	0	0	NR	NR	0
INDIAN UST		0.250	0	0	NR	NR	NR	0
INDIAN LUST		0.500	0	0	0	NR	NR	0
CA FID UST	X	0.250	0	0	NR	NR	NR	0
HIST UST		0.250	0	0	NR	NR	NR	0
FEDERAL ASTM SUPPLEMENTAL								
CONSENT		1.000	0	0	0	0	NR	0
ROD		1.000	0	0	0	0	NR	0
Delisted NPL		1.000	0	0	0	0	NR	0
FINDS	X	TP	NR	NR	NR	NR	NR	0
HMIRS		TP	NR	NR	NR	NR	NR	0
MLTS		TP	NR	NR	NR	NR	NR	0
MINES		0.250	0	0	NR	NR	NR	0
NPL Liens		TP	NR	NR	NR	NR	NR	0
PADS		TP	NR	NR	NR	NR	NR	0
UMTRA		0.500	0	0	0	NR	NR	0
ODI		0.500	0	0	0	NR	NR	0
FUDS		1.000	0	0	0	0	NR	0
DOD		1.000	0	0	0	0	NR	0
INDIAN RESERV		1.000	0	0	0	0	NR	0
RAATS		TP	NR	NR	NR	NR	NR	0
TRIS		TP	NR	NR	NR	NR	NR	0

MAP FINDINGS SUMMARY

Database	Target Property	Search Distance (Miles)	< 1/8	1/8 - 1/4	1/4 - 1/2	1/2 - 1	> 1	Total Plotted
TSCA		TP	NR	NR	NR	NR	NR	0
SSTS		TP	NR	NR	NR	NR	NR	0
FTTS		TP	NR	NR	NR	NR	NR	0
STATE OR LOCAL ASTM SUPPLEMENTAL								
AST		TP	NR	NR	NR	NR	NR	0
CLEANERS		0.250	0	0	NR	NR	NR	0
CA WDS		TP	NR	NR	NR	NR	NR	0
DEED		TP	NR	NR	NR	NR	NR	0
NFE		0.250	0	0	NR	NR	NR	0
SCH		0.250	0	0	NR	NR	NR	0
EMI		TP	NR	NR	NR	NR	NR	0
REF		0.250	0	0	NR	NR	NR	0
NFA		0.250	0	0	NR	NR	NR	0
SLIC		0.500	0	0	0	NR	NR	0
HAZNET	X	TP	NR	NR	NR	NR	NR	0
Los Angeles Co. HMS		TP	NR	NR	NR	NR	NR	0
LA Co. Site Mitigation		TP	NR	NR	NR	NR	NR	0
AOCONCERN		1.000	0	0	0	0	NR	0
EDR PROPRIETARY HISTORICAL DATABASES								
Coal Gas		1.000	0	0	0	0	NR	0
BROWNFIELDS DATABASES								
US BROWNFIELDS		0.500	0	0	0	NR	NR	0
VCP		0.500	0	0	0	NR	NR	0

NOTES:

AQUIFLOW - see EDR Physical Setting Source Addendum

TP = Target Property

NR = Not Requested at this Search Distance

Sites may be listed in more than one database

Map ID Direction Distance Distance (ft.) Elevation	Site	Database(s)	EDR ID Number EPA ID Number

MAP FINDINGS

Coal Gas Site Search: No site was found in a search of Real Property Scan's ENVIROHAZ database.

A1 **Target** **Property**	**BUCKLEY SCHOOL BUS GARAGE** **3900 STANSBURY AVE** **SHERMAN OAKS, CA 91423**	**RCRIS-SQG** **FINDS** **HAZNET**	**1000591085** **CAD077262558**

Actual:
792 ft.

Site 1 of 3 in cluster A

RCRIS:

Owner: THE BUCKLEY SCHOOL DIST
(818) 783-1613
EPA ID: CAD077262558

Contact: RAY GOURVTAN
(818) 783-1613

Classification: Small Quantity Generator
TSDF Activities: Not reported

Violation Status: No violations found

FINDS:

Other Pertinent Environmental Activity Identified at Site:
National Compliance Data Base
Resource Conservation and Recovery Act Information system

HAZNET:

Gepaid: CAD077262558
TSD EPA ID: CAD093459485
Gen County: Los Angeles
Tsd County: Fresno
Tons: .0665
Waste Category: Unspecified solvent mixture Waste
Disposal Method: Transfer Station
Contact: NON-PROFIT SCHOOL OPERATED UND
Telephone: (818) 783-1610
Mailing Address: 3900 STANSBURY AVE
SHERMAN OAKS, CA 91423 - 4618
County Los Angeles

Gepaid: CAD077262558
TSD EPA ID: CAT000613893
Gen County: Los Angeles
Tsd County: Los Angeles
Tons: .2400
Waste Category: Unspecified organic liquid mixture
Disposal Method: Transfer Station
Contact: NON-PROFIT SCHOOL OPERATED UND
Telephone: (818) 783-1610
Mailing Address: 3900 STANSBURY AVE
SHERMAN OAKS, CA 91423 - 4618
County Los Angeles

Map ID Direction Distance Distance (ft.) Elevation	Site	Database(s)	EDR ID Number EPA ID Number

BUCKLEY SCHOOL BUS GARAGE (Continued) **1000591085**

Gepaid: CAD077262558
TSD EPA ID: CAD981696420
Gen County: Los Angeles
Tsd County: Los Angeles
Tons: 5.8380
Waste Category: Oil/water separation sludge
Disposal Method: Transfer Station
Contact: NON-PROFIT SCHOOL OPERATED UND
Telephone: (818) 783-1610
Mailing Address: 3900 STANSBURY AVE
SHERMAN OAKS, CA 91423 - 4618
County Los Angeles

Gepaid: CAD077262558
TSD EPA ID: CAT000613893
Gen County: Los Angeles
Tsd County: Los Angeles
Tons: .1940
Waste Category: Unspecified organic liquid mixture
Disposal Method: Transfer Station
Contact: NON-PROFIT SCHOOL OPERATED UND
Telephone: (818) 783-1610
Mailing Address: 3900 STANSBURY AVE
SHERMAN OAKS, CA 91423 - 4618
County Los Angeles

Gepaid: CAD077262558
TSD EPA ID: CAT000613893
Gen County: Los Angeles
Tsd County: Los Angeles
Tons: .2400
Waste Category: Organic liquids (nonsolvents) with halogens
Disposal Method: Transfer Station
Contact: NON-PROFIT SCHOOL OPERATED UND
Telephone: (818) 783-1610
Mailing Address: 3900 STANSBURY AVE
SHERMAN OAKS, CA 91423 - 4618
County Los Angeles

Click this hyperlink while viewing on your computer to access
6 additional CA HAZNET record(s) in the EDR Site Report.

A2 **Target** **Property**	**THE BUCKLEY SCHOOL** **3900 STANSBURY AVE** **SHERMAN OAKS, CA 91403**	**CA FID UST**	**S101582919** **N/A**

Site 2 of 3 in cluster A

Actual:
792 ft.

Map ID Direction Distance Distance (ft.) Elevation	Site	Database(s)	EDR ID Number EPA ID Number

THE BUCKLEY SCHOOL (Continued) **S101582919**

FID:

Facility ID:	19001850	Regulate ID:	Not reported
Reg By:	Inactive Underground Storage Tank Location		
Cortese Code:	Not reported	SIC Code:	Not reported
Status:	Inactive	Facility Tel:	(818) 783-1610
Mail To:	Not reported 3900 STANSBURY AVE SHERMAN OAKS, CA 91403		
Contact:	Not reported	Contact Tel:	Not reported
DUNs No:	Not reported	NPDES No:	Not reported
Creation:	10/22/93	Modified:	00/00/00
EPA ID:	Not reported		
Comments:	Not reported		

A3
Target
Property

BUCKLEY SCHOOL
3900 STANSBURY AVE
SHERMAN OAKS, CA 91423

LUST **1006890270**
Cortese **N/A**

Site 3 of 3 in cluster A

Actual:
792 ft.

State LUST:

Cross Street:	Not reported		
Qty Leaked:	Not reported		
Case Number	9160615		
Reg Board:	Los Angeles Region		
Chemical:	Gasoline		
Lead Agency:	Regional Board		
Local Agency :	19050		
Case Type:	Soil only		
Status:	Case Closed		
Review Date:	Not reported	Confirm Leak:	Not reported
Workplan:	Not reported	Prelim Assess:	Not reported
Pollution Char:	Not reported	Remed Plan:	Not reported
Remed Action:	Not reported		
Monitoring:	Not reported		
Close Date:	1996-07-22 00:00:00		
Release Date:	1988-06-02 00:00:00		
Cleanup Fund Id :	Not reported		
Discover Date :	1988-05-27 00:00:00		
Enforcement Dt :	Not reported		
Enf Type:	Not reported		
Enter Date :	1988-09-16 00:00:00		
Funding:	Not reported		
Staff Initials:	PEJ		
How Discovered:	Nuisance Conditions		
How Stopped:	Not reported		
Interim :	Not reported		
Leak Cause:	Structure Failure		
Leak Source:	Piping		
MTBE Date :	Not reported		
Max MTBE GW :	Not reported		
MTBE Tested:	Site NOT Tested for MTBE.Includes Unknown and Not Analyzed.		
Priority:	Not reported		
Local Case # :	Not reported		
Beneficial:	Not reported		
Staff :	UNK		
GW Qualifier :	Not reported		
Max MTBE Soil :	Not reported		

BUCKLEY SCHOOL (Continued) **1006890270**

Soil Qualifier : Not reported
Hydr Basin #: UNNAMED BASIN
Operator : BAUMHOFF
Oversight Prgm: LUST
Review Date : 1988-09-21 00:00:00
Stop Date : Not reported
Work Suspended :Not reported
Responsible PartyBUCKLEY SCHOOL
RP Address: 3900 STANSBURY AVE, SHERMAN
Global Id: T0603702598
Org Name: Not reported
Contact Person: Not reported
MTBE Conc: 0
Mtbe Fuel: 1
Water System Name: Not reported
Well Name: Not reported
Distance To Lust: 0
Waste Discharge Global ID: Not reported
Waste Disch Assigned Name: Not reported

LUST Region 4:
Report Date: 6/2/1988
Lead Agency: Regional Board
Local Agency: 19050
Substance: Gasoline
Case Type: Soil
Status: Case Closed
Region: 4
Staff: UNK
Date Case Last Changed on Database: 9/21/1988
Date Leak Record Entered: 9/16/1988
Historical Max MTBE Date: Not reported
GW Qualifier: Not reported
Soil Qualifier: Not reported
Hist Max MTBE Conc in Groundwater: Not reported
Hist Max MTBE Conc in Soil : Not reported
County: Los Angeles
Organization : Not reported
Regional Board: 04
Owner Contact: Not reported
Responsible Party: BUCKLEY SCHOOL
RP Address: 3900 STANSBURY AVE, SHERMAN OAKS CA 91423
Significant Interim Remedial Action Taken: Not reported
Program : LUST
Lat / Long : 34.1417876 / -1
Local Agency Staff: PEJ
Beneficial Use : Not reported
Priority : Not reported
Cleanup Fund Id : Not reported
Suspended : Not reported
Local Case No : Not reported
Substance Quantity : Not reported
Abatement Method Used at the Site: Not reported
Operator : BAUMHOFF, WALTER
Water System : Not reported
Well Name : Not reported
Approx. Dist To Production Well (ft) : 20003.840185590122796404012591
Assigned Name : Not reported

BUCKLEY SCHOOL (Continued) **1006890270**

W Global ID :	Not reported
Source of Cleanup Funding:	Not reported
Date the Leak was Discovered:	5/27/1988
How the Leak was Discovered:	Nuisance Conditions
How the Leak was Stopped:	Not reported
Cause of Leak:	Structure Failure
Leak Source:	Piping
Date The Leak was Stopped:	Not reported
Date Confirmation Leak Began:	Not reported
Preliminary Site Assessment Workplan Submitted:	Not reported
Preliminary Site Assessment Began:	Not reported
Pollution Characterization Began:	9/21/1988
Remediation Plan Submitted:	Not reported
Remedial Action Underway:	Not reported
Post Remedial Action Monitoring Began:	Not reported
Date the Case was Closed:	7/22/1996
Enforcement Action Date:	Not reported
Date Leak First Reported:	6/2/1988
Enforcement Type:	Not reported
Global ID :	T0603702598
Cross Street:	Not reported
Summary :	ENVIROPRO HAS SENT WORKPLAN

CORTESE:

Region:	CORTESE
Fac Address 2:	3900 STANSBURY AVE

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4 **SERVICE STATION** **Notify 65** **1000166679**
NNW **14478 VENTURA BLVD** **HAZNET** **N/A**
1/2-1 **SHERMAN OAKS, CA 91423** **LUST**
4304 ft. **Cortese**
CA FID UST
HIST UST

Relative:
Lower

Actual:
662 ft.

State LUST:

Cross Street:	VAN NUYS BLVD		
Qty Leaked:	Not reported		
Case Number	9142303		
Reg Board:	Los Angeles Region		
Chemical:	Gasoline		
Lead Agency:	Regional Board		
Local Agency :	19050		
Case Type:	Other ground water affected		
Status:	Pollution Characterization		
Review Date:	Not reported	Confirm Leak:	Not reported
Workplan:	Not reported	Prelim Assess:	Not reported
Pollution Char:	Not reported	Remed Plan:	Not reported
Remed Action:	Not reported		
Monitoring:	Not reported		
Close Date:	Not reported		
Release Date:	1988-04-14 00:00:00		
Cleanup Fund Id :	Not reported		
Discover Date :	1988-04-12 00:00:00		
Enforcement Dt :	Not reported		
Enf Type:	DLSEL		
Enter Date :	1988-04-21 00:00:00		
Funding:	Not reported		
Staff Initials:	PEJ		
How Discovered:	OM		

SERVICE STATION (Continued) **1000166679**

How Stopped: Not reported
Interim : Not reported
Leak Cause: Other Cause
Leak Source: Piping
MTBE Date : 2000-04-06 00:0
Max MTBE GW : 50000 Parts per Billion
MTBE Tested: MTBE Detected. Site tested for MTBE & MTBE detected
Priority: Not reported
Local Case # : Not reported
Beneficial: Not reported
Staff : AT
GW Qualifier : Not reported
Max MTBE Soil : Not reported
Soil Qualifier : Not reported
Hydr Basin #: SAN FERNANDO VALLEY
Operator : NAMSON,
Oversight Prgm: LUST
Review Date : 2002-07-15 00:00:00
Stop Date : 1988-04-12
Work Suspended :Not reported
Responsible PartySHARI LONDON
RP Address: 3611 HARBOR BLVD., SUITE #20
Global Id: T0603702483
Org Name: Not reported
Contact Person: Not reported
MTBE Conc: 1
Mtbe Fuel: 1
Water System Name: Not reported
Well Name: Not reported
Distance To Lust: 0
Waste Discharge Global ID: Not reported
Waste Disch Assigned Name: Not reported

LUST Region 4:
Report Date: 4/14/1988
Lead Agency: Regional Board
Local Agency: 19050
Substance: Gasoline
Case Type: Groundwater
Status: Pollution Characterization
Region: 4
Staff: AT
Date Case Last Changed on Database: 7/15/2002
Date Leak Record Entered: 4/21/1988
Historical Max MTBE Date: 4/6/2000
GW Qualifier: Not reported
Soil Qualifier: Not reported
Hist Max MTBE Conc in Groundwater: 50000
Hist Max MTBE Conc in Soil : Not reported
County: Los Angeles
Organization : Not reported
Regional Board: 04
Owner Contact: Not reported
Responsible Party: SHARI LONDON
RP Address: 3611 HARBOR BLVD., SUITE #200
Significant Interim Remedial Action Taken: Not reported
Program : LUST
Lat / Long : 34.1506913 / -1

SERVICE STATION (Continued) **1000166679**

Local Agency Staff:	PEJ
Beneficial Use :	Not reported
Priority :	Not reported
Cleanup Fund Id :	Not reported
Suspended :	Not reported
Local Case No :	Not reported
Substance Quantity :	Not reported
Abatement Method Used at the Site:	Not reported
Operator :	NAMSON, JOSEPH N.
Water System :	Not reported
Well Name :	Not reported
Approx. Dist To Production Well (ft) :	17639.953186757741589545141318
Assigned Name :	Not reported
W Global ID :	Not reported
Source of Cleanup Funding:	Not reported
Date the Leak was Discovered:	4/12/1988
How the Leak was Discovered:	OM
How the Leak was Stopped:	Not reported
Cause of Leak:	Other Causes
Leak Source:	Piping
Date The Leak was Stopped:	4/12/1988
Date Confirmation Leak Began:	Not reported
Preliminary Site Assessment Workplan Submitted:	3/1/1999
Preliminary Site Assessment Began:	Not reported
Pollution Characterization Began:	7/25/2000
Remediation Plan Submitted:	Not reported
Remedial Action Underway:	Not reported
Post Remedial Action Monitoring Began:	Not reported
Date the Case was Closed:	Not reported
Enforcement Action Date:	Not reported
Date Leak First Reported:	4/14/1988
Enforcement Type:	DLSEL
Global ID :	T0603702483
Cross Street:	VAN NUYS BLVD

Summary : ABANDONED PIPE CONNECTED TO OLD PUMP ISLAND WAS NOT CAPPED. CONTRACTOR DISCOVERED LEAKING UG PIPE.; 7/14/00 2ND QTR GW MON RPT; 10/30/00 SUPPLE. SITE ASESSM. RPT AND REMED. TESTING PROPOSAL; 12/31/00 4TH QTR GW MON RPT 2000

HAZNET:

Gepaid:	CAD981645377
TSD EPA ID:	CAD050099696
Gen County:	Los Angeles
Tsd County:	Los Angeles
Tons:	.4170
Waste Category:	Aqueous solution with less than 10% total organic residues
Disposal Method:	Recycler
Contact:	UNION OIL COMPANY OF CALIFORNI
Telephone:	(714) 428-6560
Mailing Address:	PO BOX 25376 SANTA ANA, CA 92799 - 5376
County	Los Angeles

SERVICE STATION (Continued) **1000166679**

Gepaid:	CAD981645377
TSD EPA ID:	CAT080011059
Gen County:	Los Angeles
Tsd County:	Los Angeles
Tons:	1.6680
Waste Category:	Waste oil and mixed oil
Disposal Method:	Recycler
Contact:	UNION OIL COMPANY OF CALIFORNI
Telephone:	(714) 428-6560
Mailing Address:	PO BOX 25376
	SANTA ANA, CA 92799 - 5376
County	Los Angeles

Gepaid:	CAD981645377
TSD EPA ID:	CAT080011059
Gen County:	Los Angeles
Tsd County:	Los Angeles
Tons:	.3085
Waste Category:	Aqueous solution with 10% or more total organic residues
Disposal Method:	Recycler
Contact:	UNION OIL COMPANY OF CALIFORNI
Telephone:	(714) 428-6560
Mailing Address:	PO BOX 25376
	SANTA ANA, CA 92799 - 5376
County	Los Angeles

Gepaid:	CAD981645377
TSD EPA ID:	CAD099452708
Gen County:	Los Angeles
Tsd County:	Los Angeles
Tons:	4.3785
Waste Category:	Waste oil and mixed oil
Disposal Method:	Recycler
Contact:	UNION OIL COMPANY OF CALIFORNI
Telephone:	(714) 428-6560
Mailing Address:	PO BOX 25376
	SANTA ANA, CA 92799 - 5376
County	Los Angeles

Gepaid:	CAD981645377
TSD EPA ID:	CAD028409019
Gen County:	Los Angeles
Tsd County:	Los Angeles
Tons:	3.7862
Waste Category:	Aqueous solution with less than 10% total organic residues
Disposal Method:	Treatment, Tank
Contact:	UNION OIL COMPANY OF CALIFORNI
Telephone:	(714) 428-6560
Mailing Address:	PO BOX 25376
	SANTA ANA, CA 92799 - 5376
County	Los Angeles

Click this hyperlink while viewing on your computer to access
7 additional CA HAZNET record(s) in the EDR Site Report.

SERVICE STATION (Continued) **1000166679**

NOTIFY 65:

Date Reported:	Not reported Staff Initials: Not reported
Board File Number:	Not reported
Facility Type:	Not reported
Discharge Date:	Not reported
Incident Description:	91423-2607

CORTESE:

Region:	CORTESE
Fac Address 2:	14478 VENTURA BLVD

FID:

Facility ID:	19001622	Regulate ID:	00029443
Reg By:	Active Underground Storage Tank Location		
Cortese Code:	Not reported	SIC Code:	Not reported
Status:	Active	Facility Tel:	(818) 784-2275
Mail To:	Not reported 3701 WILSHIRE BLVD SHERMAN OAKS, CA 91403		
Contact:	Not reported	Contact Tel:	Not reported
DUNs No:	Not reported	NPDES No:	Not reported
Creation:	10/22/93	Modified:	00/00/00
EPA ID:	Not reported		
Comments:	Not reported		

UST HIST:

Facility ID:	29443	Owner Name:	UNION OIL COMPANY OF CALIFORNI
Total Tanks:	3	Region:	STATE
Owner Address:	3701 WILSHIRE BOULEVARD-SUITE LOS ANGELES, CA 90010		
Tank Used for:	PRODUCT		
Tank Num:	1	Container Num:	2421-1
Tank Capacity:	00009950	Year Installed:	1967
Type of Fuel:	UNLEADED	Tank Construction:	Not Reported
Leak Detection:	Stock Inventor, Pressure Test		
Contact Name:	JOSEPH N NAMSON	Telephone:	(818) 784-2275
Facility Type:	Gas Station	Other Type:	Not reported

Facility ID:	29443	Owner Name:	UNION OIL COMPANY OF CALIFORNI
Total Tanks:	3	Region:	STATE
Owner Address:	3701 WILSHIRE BOULEVARD-SUITE LOS ANGELES, CA 90010		
Tank Used for:	PRODUCT		
Tank Num:	2	Container Num:	2421-2
Tank Capacity:	00009950	Year Installed:	1967
Type of Fuel:	PREMIUM	Tank Construction:	Not Reported
Leak Detection:	Stock Inventor, Pressure Test		
Contact Name:	JOSEPH N NAMSON	Telephone:	(818) 784-2275
Facility Type:	Gas Station	Other Type:	Not reported

Facility ID:	29443	Owner Name:	UNION OIL COMPANY OF CALIFORNI
Total Tanks:	3	Region:	STATE
Owner Address:	3701 WILSHIRE BOULEVARD-SUITE LOS ANGELES, CA 90010		
Tank Used for:	PRODUCT		
Tank Num:	3	Container Num:	2421-4
Tank Capacity:	00000550	Year Installed:	1967
Type of Fuel:	WASTE OIL	Tank Construction:	Not Reported

Map ID Direction Distance Distance (ft.) Elevation	Site	Database(s)	EDR ID Number EPA ID Number

SERVICE STATION (Continued) **1000166679**

Leak Detection:	Stock Inventor, Pressure Test		
Contact Name:	JOSEPH N NAMSON	Telephone:	(818) 784-2275
Facility Type:	Gas Station	Other Type:	Not reported

ORPHAN SUMMARY

City	EDR ID	Site Name	Site Address	Zip	Database(s)
LOS ANGELES COUNTY	S105632075		BUILDING #8 LONG BEACH NAVAL		LUST, CHMIRS
SHERMAN OAKS	8872808	BUCKLEY SCHOOL	BUCKLEY SCHOOL		ERNS

GOVERNMENT RECORDS SEARCHED / DATA CURRENCY TRACKING

To maintain currency of the following federal and state databases, EDR contacts the appropriate governmental agency on a monthly or quarterly basis, as required.

Elapsed ASTM days: Provides confirmation that this EDR report meets or exceeds the 90-day updating requirement of the ASTM standard.

FEDERAL ASTM STANDARD RECORDS

NPL: National Priority List
Source: EPA
Telephone: N/A
National Priorities List (Superfund). The NPL is a subset of CERCLIS and identifies over 1,200 sites for priority cleanup under the Superfund Program. NPL sites may encompass relatively large areas. As such, EDR provides polygon coverage for over 1,000 NPL site boundaries produced by EPA's Environmental Photographic Interpretation Center (EPIC) and regional EPA offices.

Date of Government Version: 07/30/04
Date Made Active at EDR: 09/09/04
Database Release Frequency: Semi-Annually
Date of Data Arrival at EDR: 08/03/04
Elapsed ASTM days: 37
Date of Last EDR Contact: 11/02/04

NPL Site Boundaries

Sources:

EPA's Environmental Photographic Interpretation Center (EPIC)
Telephone: 202-564-7333

EPA Region 1
Telephone 617-918-1143

EPA Region 3
Telephone 215-814-5418

EPA Region 4
Telephone 404-562-8033

EPA Region 6
Telephone: 214-655-6659

EPA Region 8
Telephone: 303-312-6774

Proposed NPL: Proposed National Priority List Sites
Source: EPA
Telephone: N/A

Date of Government Version: 07/22/04
Date Made Active at EDR: 09/09/04
Database Release Frequency: Semi-Annually
Date of Data Arrival at EDR: 08/03/04
Elapsed ASTM days: 37
Date of Last EDR Contact: 11/02/04

CERCLIS: Comprehensive Environmental Response, Compensation, and Liability Information System
Source: EPA
Telephone: 703-413-0223
CERCLIS contains data on potentially hazardous waste sites that have been reported to the USEPA by states, municipalities, private companies and private persons, pursuant to Section 103 of the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA). CERCLIS contains sites which are either proposed to or on the National Priorities List (NPL) and sites which are in the screening and assessment phase for possible inclusion on the NPL.

Date of Government Version: 08/10/04
Date Made Active at EDR: 10/27/04
Database Release Frequency: Quarterly
Date of Data Arrival at EDR: 09/21/04
Elapsed ASTM days: 36
Date of Last EDR Contact: 09/21/04

CERCLIS-NFRAP: CERCLIS No Further Remedial Action Planned
Source: EPA
Telephone: 703-413-0223
As of February 1995, CERCLIS sites designated "No Further Remedial Action Planned" (NFRAP) have been removed from CERCLIS. NFRAP sites may be sites where, following an initial investigation, no contamination was found, contamination was removed quickly without the need for the site to be placed on the NPL, or the contamination was not serious enough to require Federal Superfund action or NPL consideration. EPA has removed approximately 25,000 NFRAP sites to lift the unintended barriers to the redevelopment of these properties and has archived them as historical records so EPA does not needlessly repeat the investigations in the future. This policy change is part of the EPA's Brownfields Redevelopment Program to help cities, states, private investors and affected citizens to promote economic redevelopment of unproductive urban sites.

Date of Government Version: 08/10/04
Date Made Active at EDR: 10/27/04
Database Release Frequency: Quarterly

Date of Data Arrival at EDR: 09/21/04
Elapsed ASTM days: 36
Date of Last EDR Contact: 09/21/04

CORRACTS: Corrective Action Report
Source: EPA
Telephone: 800-424-9346
CORRACTS identifies hazardous waste handlers with RCRA corrective action activity.

Date of Government Version: 09/23/04
Date Made Active at EDR: 11/18/04
Database Release Frequency: Semi-Annually

Date of Data Arrival at EDR: 10/07/04
Elapsed ASTM days: 42
Date of Last EDR Contact: 09/07/04

RCRIS: RCRAInfo
Source: EPA
Telephone: 800-424-9346
RCRAInfo is EPA's comprehensive information system, providing access to data supporting the Resource Conservation and Recovery Act (RCRA) of 1976 and the Hazardous and Solid Waste Amendments (HSWA) of 1984. RCRAInfo replaces the data recording and reporting abilities of the Resource Conservation and Recovery Information System (RCRIS). The database includes selective information on sites which generate, transport, store, treat and/or dispose of hazardous waste as defined by the Resource Conservation and Recovery Act (RCRA). Conditionally exempt small quantity generators (CESQGs): generate less than 100 kg of hazardous waste, or less than 1 kg of acutely hazardous waste per month. Small quantity generators (SQGs): generate between 100 kg and 1,000 kg of hazardous waste per month. Large quantity generators (LQGs): generate over 1,000 kilograms (kg) of hazardous waste, or over 1 kg of acutely hazardous waste per month. Transporters are individuals or entities that move hazardous waste from the generator off-site to a facility that can recycle, treat, store, or dispose of the waste. TSDFs treat, store, or dispose of the waste.

Date of Government Version: 08/10/04
Date Made Active at EDR: 10/11/04
Database Release Frequency: Varies

Date of Data Arrival at EDR: 08/24/04
Elapsed ASTM days: 48
Date of Last EDR Contact: 08/24/04

ERNS: Emergency Response Notification System
Source: National Response Center, United States Coast Guard
Telephone: 202-260-2342
Emergency Response Notification System. ERNS records and stores information on reported releases of oil and hazardous substances.

Date of Government Version: 12/31/03
Date Made Active at EDR: 03/12/04
Database Release Frequency: Annually

Date of Data Arrival at EDR: 01/26/04
Elapsed ASTM days: 46
Date of Last EDR Contact: 10/25/04

FEDERAL ASTM SUPPLEMENTAL RECORDS

BRS: Biennial Reporting System
Source: EPA/NTIS
Telephone: 800-424-9346
The Biennial Reporting System is a national system administered by the EPA that collects data on the generation and management of hazardous waste. BRS captures detailed data from two groups: Large Quantity Generators (LQG) and Treatment, Storage, and Disposal Facilities.

Date of Government Version: 12/01/01
Database Release Frequency: Biennially

Date of Last EDR Contact: 09/20/04
Date of Next Scheduled EDR Contact: 12/13/04

CONSENT: Superfund (CERCLA) Consent Decrees
Source: Department of Justice, Consent Decree Library
Telephone: Varies
Major legal settlements that establish responsibility and standards for cleanup at NPL (Superfund) sites. Released periodically by United States District Courts after settlement by parties to litigation matters.

Date of Government Version: 03/05/04
Database Release Frequency: Varies
Date of Last EDR Contact: 10/25/04
Date of Next Scheduled EDR Contact: 01/24/05

ROD: Records Of Decision
Source: EPA
Telephone: 703-416-0223
Record of Decision. ROD documents mandate a permanent remedy at an NPL (Superfund) site containing technical and health information to aid in the cleanup.

Date of Government Version: 09/09/04
Database Release Frequency: Annually
Date of Last EDR Contact: 10/06/04
Date of Next Scheduled EDR Contact: 01/03/05

DELISTED NPL: National Priority List Deletions
Source: EPA
Telephone: N/A
The National Oil and Hazardous Substances Pollution Contingency Plan (NCP) establishes the criteria that the EPA uses to delete sites from the NPL. In accordance with 40 CFR 300.425.(e), sites may be deleted from the NPL where no further response is appropriate.

Date of Government Version: 07/30/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 11/02/04
Date of Next Scheduled EDR Contact: 01/31/05

FINDS: Facility Index System/Facility Identification Initiative Program Summary Report
Source: EPA
Telephone: N/A
Facility Index System. FINDS contains both facility information and 'pointers' to other sources that contain more detail. EDR includes the following FINDS databases in this report: PCS (Permit Compliance System), AIRS (Aerometric Information Retrieval System), DOCKET (Enforcement Docket used to manage and track information on civil judicial enforcement cases for all environmental statutes), FURS (Federal Underground Injection Control), C-DOCKET (Criminal Docket System used to track criminal enforcement actions for all environmental statutes), FFIS (Federal Facilities Information System), STATE (State Environmental Laws and Statutes), and PADS (PCB Activity Data System).

Date of Government Version: 09/09/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 09/08/04
Date of Next Scheduled EDR Contact: 01/03/05

HMIRS: Hazardous Materials Information Reporting System
Source: U.S. Department of Transportation
Telephone: 202-366-4555
Hazardous Materials Incident Report System. HMIRS contains hazardous material spill incidents reported to DOT.

Date of Government Version: 02/17/04
Database Release Frequency: Annually
Date of Last EDR Contact: 04/20/04
Date of Next Scheduled EDR Contact: 07/19/04

MLTS: Material Licensing Tracking System
Source: Nuclear Regulatory Commission
Telephone: 301-415-7169
MLTS is maintained by the Nuclear Regulatory Commission and contains a list of approximately 8,100 sites which possess or use radioactive materials and which are subject to NRC licensing requirements. To maintain currency, EDR contacts the Agency on a quarterly basis.

Date of Government Version: 07/15/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 10/04/04
Date of Next Scheduled EDR Contact: 01/03/05

MINES: Mines Master Index File
Source: Department of Labor, Mine Safety and Health Administration
Telephone: 303-231-5959

Date of Government Version: 09/13/04
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: 09/28/04
Date of Next Scheduled EDR Contact: 12/27/04

NPL LIENS: Federal Superfund Liens
Source: EPA
Telephone: 202-564-4267
Federal Superfund Liens. Under the authority granted the USEPA by the Comprehensive Environmental Response, Compensation and Liability Act (CERCLA) of 1980, the USEPA has the authority to file liens against real property in order to recover remedial action expenditures or when the property owner receives notification of potential liability. USEPA compiles a listing of filed notices of Superfund Liens.

Date of Government Version: 10/15/91
Database Release Frequency: No Update Planned
Date of Last EDR Contact: 08/23/04
Date of Next Scheduled EDR Contact: 11/22/04

PADS: PCB Activity Database System
Source: EPA
Telephone: 202-564-3887
PCB Activity Database. PADS Identifies generators, transporters, commercial storers and/or brokers and disposers of PCB's who are required to notify the EPA of such activities.

Date of Government Version: 06/29/04
Database Release Frequency: Annually
Date of Last EDR Contact: 08/10/04
Date of Next Scheduled EDR Contact: 11/08/04

DOD: Department of Defense Sites
Source: USGS
Telephone: 703-692-8801
This data set consists of federally owned or administered lands, administered by the Department of Defense, that have any area equal to or greater than 640 acres of the United States, Puerto Rico, and the U.S. Virgin Islands.

Date of Government Version: 10/01/03
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: 08/12/04
Date of Next Scheduled EDR Contact: 11/08/04

UMTRA: Uranium Mill Tailings Sites
Source: Department of Energy
Telephone: 505-845-0011
Uranium ore was mined by private companies for federal government use in national defense programs. When the mills shut down, large piles of the sand-like material (mill tailings) remain after uranium has been extracted from the ore. Levels of human exposure to radioactive materials from the piles are low; however, in some cases tailings were used as construction materials before the potential health hazards of the tailings were recognized. In 1978, 24 inactive uranium mill tailings sites in Oregon, Idaho, Wyoming, Utah, Colorado, New Mexico, Texas, North Dakota, South Dakota, Pennsylvania, and on Navajo and Hopi tribal lands, were targeted for cleanup by the Department of Energy.

Date of Government Version: 04/22/04
Database Release Frequency: Varies
Date of Last EDR Contact: 09/20/04
Date of Next Scheduled EDR Contact: 12/20/04

ODI: Open Dump Inventory
Source: Environmental Protection Agency
Telephone: 800-424-9346
An open dump is defined as a disposal facility that does not comply with one or more of the Part 257 or Part 258 Subtitle D Criteria.

Date of Government Version: 06/30/85
Database Release Frequency: No Update Planned
Date of Last EDR Contact: 05/23/95
Date of Next Scheduled EDR Contact: N/A

FUDS: Formerly Used Defense Sites
Source: U.S. Army Corps of Engineers
Telephone: 202-528-4285
The listing includes locations of Formerly Used Defense Sites properties where the US Army Corps of Engineers is actively working or will take necessary cleanup actions.

Date of Government Version: 12/31/03
Database Release Frequency: Varies
Date of Last EDR Contact: 10/04/04
Date of Next Scheduled EDR Contact: 01/03/05

INDIAN RESERV: Indian Reservations
Source: USGS
Telephone: 202-208-3710
This map layer portrays Indian administered lands of the United States that have any area equal to or greater than 640 acres.

Date of Government Version: 10/01/03
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: 08/12/04
Date of Next Scheduled EDR Contact: 11/08/04

RAATS: RCRA Administrative Action Tracking System
Source: EPA
Telephone: 202-564-4104
RCRA Administration Action Tracking System. RAATS contains records based on enforcement actions issued under RCRA pertaining to major violators and includes administrative and civil actions brought by the EPA. For administration actions after September 30, 1995, data entry in the RAATS database was discontinued. EPA will retain a copy of the database for historical records. It was necessary to terminate RAATS because a decrease in agency resources made it impossible to continue to update the information contained in the database.

Date of Government Version: 04/17/95
Database Release Frequency: No Update Planned
Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/06/04

TRIS: Toxic Chemical Release Inventory System
Source: EPA
Telephone: 202-566-0250
Toxic Release Inventory System. TRIS identifies facilities which release toxic chemicals to the air, water and land in reportable quantities under SARA Title III Section 313.

Date of Government Version: 12/31/02
Database Release Frequency: Annually
Date of Last EDR Contact: 09/20/04
Date of Next Scheduled EDR Contact: 12/20/04

TSCA: Toxic Substances Control Act
Source: EPA
Telephone: 202-260-5521
Toxic Substances Control Act. TSCA identifies manufacturers and importers of chemical substances included on the TSCA Chemical Substance Inventory list. It includes data on the production volume of these substances by plant site.

Date of Government Version: 12/31/02
Database Release Frequency: Every 4 Years
Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/06/04

FTTS INSP: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)
Source: EPA
Telephone: 202-564-2501

Date of Government Version: 04/13/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/20/04

SSTS: Section 7 Tracking Systems
Source: EPA
Telephone: 202-564-5008
Section 7 of the Federal Insecticide, Fungicide and Rodenticide Act, as amended (92 Stat. 829) requires all registered pesticide-producing establishments to submit a report to the Environmental Protection Agency by March 1st each year. Each establishment must report the types and amounts of pesticides, active ingredients and devices being produced, and those having been produced and sold or distributed in the past year.

Date of Government Version: 12/31/01
Database Release Frequency: Annually
Date of Last EDR Contact: 10/18/04
Date of Next Scheduled EDR Contact: 01/17/05

FTTS: FIFRA/ TSCA Tracking System - FIFRA (Federal Insecticide, Fungicide, & Rodenticide Act)/TSCA (Toxic Substances Control Act)
Source: EPA/Office of Prevention, Pesticides and Toxic Substances
Telephone: 202-564-2501
FTTS tracks administrative cases and pesticide enforcement actions and compliance activities related to FIFRA, TSCA and EPCRA (Emergency Planning and Community Right-to-Know Act). To maintain currency, EDR contacts the Agency on a quarterly basis.

Date of Government Version: 09/13/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/20/04

STATE OF CALIFORNIA ASTM STANDARD RECORDS

AWP: Annual Workplan Sites
Source: California Environmental Protection Agency
Telephone: 916-323-3400
Known Hazardous Waste Sites. California DTSC's Annual Workplan (AWP), formerly BEP, identifies known hazardous substance sites targeted for cleanup.

Date of Government Version: 10/05/04
Date Made Active at EDR: 11/03/04
Database Release Frequency: Annually
Date of Data Arrival at EDR: 10/15/04
Elapsed ASTM days: 19
Date of Last EDR Contact: 09/16/04

CAL-SITES: Calsites Database
Source: Department of Toxic Substance Control
Telephone: 916-323-3400
The Calsites database contains potential or confirmed hazardous substance release properties. In 1996, California EPA reevaluated and significantly reduced the number of sites in the Calsites database.

Date of Government Version: 10/05/04
Date Made Active at EDR: 11/03/04
Database Release Frequency: Quarterly
Date of Data Arrival at EDR: 10/15/04
Elapsed ASTM days: 19
Date of Last EDR Contact: 09/16/04

CHMIRS: California Hazardous Material Incident Report System
Source: Office of Emergency Services
Telephone: 916-845-8400
California Hazardous Material Incident Reporting System. CHMIRS contains information on reported hazardous material incidents (accidental releases or spills).

Date of Government Version: 12/31/03
Date Made Active at EDR: 06/25/04
Database Release Frequency: Varies
Date of Data Arrival at EDR: 05/18/04
Elapsed ASTM days: 38
Date of Last EDR Contact: 08/23/04

CORTESE: "Cortese" Hazardous Waste & Substances Sites List
Source: CAL EPA/Office of Emergency Information
Telephone: 916-323-9100
The sites for the list are designated by the State Water Resource Control Board (LUST), the Integrated Waste Board (SWF/LS), and the Department of Toxic Substances Control (Cal-Sites). This listing is no longer updated by the state agency.

Date of Government Version: 04/01/01
Date Made Active at EDR: 07/26/01
Database Release Frequency: No Update Planned
Date of Data Arrival at EDR: 05/29/01
Elapsed ASTM days: 58
Date of Last EDR Contact: 10/28/04

NOTIFY 65: Proposition 65 Records
Source: State Water Resources Control Board
Telephone: 916-445-3846
Proposition 65 Notification Records. NOTIFY 65 contains facility notifications about any release which could impact drinking water and thereby expose the public to a potential health risk.

Date of Government Version: 10/21/93
Date Made Active at EDR: 11/19/93
Database Release Frequency: No Update Planned
Date of Data Arrival at EDR: 11/01/93
Elapsed ASTM days: 18
Date of Last EDR Contact: 10/18/04

TOXIC PITS: Toxic Pits Cleanup Act Sites
Source: State Water Resources Control Board
Telephone: 916-227-4364
Toxic PITS Cleanup Act Sites. TOXIC PITS identifies sites suspected of containing hazardous substances where cleanup has not yet been completed.

Date of Government Version: 07/01/95 | Date of Data Arrival at EDR: 08/30/95
Date Made Active at EDR: 09/26/95 | Elapsed ASTM days: 27
Database Release Frequency: No Update Planned | Date of Last EDR Contact: 11/01/04

SWF/LF (SWIS): Solid Waste Information System
Source: Integrated Waste Management Board
Telephone: 916-341-6320
Active, Closed and Inactive Landfills. SWF/LF records typically contain an inve ntory of solid waste disposal facilities or landfills. These may be active or i nactive facilities or open dumps that failed to meet RCRA Section 4004 criteria for solid waste landfills or disposal sites.

Date of Government Version: 09/13/04 | Date of Data Arrival at EDR: 09/14/04
Date Made Active at EDR: 10/12/04 | Elapsed ASTM days: 28
Database Release Frequency: Quarterly | Date of Last EDR Contact: 09/14/04

WMUDS/SWAT: Waste Management Unit Database
Source: State Water Resources Control Board
Telephone: 916-227-4448
Waste Management Unit Database System. WMUDS is used by the State Water Resources Control Board staff and the Regional Water Quality Control Boards for program tracking and inventory of waste management units. WMUDS is composed of the following databases: Facility Information, Scheduled Inspections Information, Waste Management Unit Information, SWAT Program Information, SWAT Report Summary Information, SWAT Report Summary Data, Chapter 15 (formerly Subchapter 15) Information, Chapter 15 Monitoring Parameters, TPCA Program Information, RCRA Program Information, Closure Information, and Interested Parties Information.

Date of Government Version: 04/01/00 | Date of Data Arrival at EDR: 04/10/00
Date Made Active at EDR: 05/10/00 | Elapsed ASTM days: 30
Database Release Frequency: Quarterly | Date of Last EDR Contact: 09/08/04

LUST: Leaking Underground Storage Tank Information System
Source: State Water Resources Control Board
Telephone: 916-341-5752
Leaking Underground Storage Tank Incident Reports. LUST records contain an inventory of reported leaking underground storage tank incidents. Not all states maintain these records, and the information stored varies by state.

Date of Government Version: 10/13/04 | Date of Data Arrival at EDR: 10/13/04
Date Made Active at EDR: 11/03/04 | Elapsed ASTM days: 21
Database Release Frequency: Quarterly | Date of Last EDR Contact: 10/13/04

CA BOND EXP. PLAN: Bond Expenditure Plan
Source: Department of Health Services
Telephone: 916-255-2118
Department of Health Services developed a site-specific expenditure plan as the basis for an appropriation of Hazardous Substance Cleanup Bond Act funds. It is not updated.

Date of Government Version: 01/01/89 | Date of Data Arrival at EDR: 07/27/94
Date Made Active at EDR: 08/02/94 | Elapsed ASTM days: 6
Database Release Frequency: No Update Planned | Date of Last EDR Contact: 05/31/94

CA UST:

UST: Active UST Facilities
Source: SWRCB
Telephone: 916-341-5752
Active UST facilities gathered from the local regulatory agencies

Date of Government Version: 10/13/04 | Date of Data Arrival at EDR: 10/13/04
Date Made Active at EDR: 11/03/04 | Elapsed ASTM days: 21
Database Release Frequency: Semi-Annually | Date of Last EDR Contact: 10/13/04

GOVERNMENT RECORDS SEARCHED / DATA CURRENCY TRACKING

VCP: Voluntary Cleanup Program Properties
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
Contains low threat level properties with either confirmed or unconfirmed releases and the project proponents have request that DTSC oversee investigation and/or cleanup activities and have agreed to provide coverage for DTSC's costs.

Date of Government Version: 10/05/04
Date Made Active at EDR: 11/03/04
Database Release Frequency: Quarterly
Date of Data Arrival at EDR: 10/15/04
Elapsed ASTM days: 19
Date of Last EDR Contact: 09/16/04

INDIAN LUST: Leaking Underground Storage Tanks on Indian Land
Source: Environmental Protection Agency
Telephone: 415-972-3372
LUSTs on Indian land in Arizona, California, New Mexico and Nevada

Date of Government Version: 10/03/04
Date Made Active at EDR: 11/03/04
Database Release Frequency: Varies
Date of Data Arrival at EDR: 10/06/04
Elapsed ASTM days: 28
Date of Last EDR Contact: 08/23/04

INDIAN LUST: Leaking Underground Storage Tanks on Indian Land
Source: EPA Region 10
Telephone: 206-553-2857
LUSTs on Indian land in Alaska, Idaho, Oregon and Washington.

Date of Government Version: 09/29/04
Date Made Active at EDR: 10/22/04
Database Release Frequency: Varies
Date of Data Arrival at EDR: 10/01/04
Elapsed ASTM days: 21
Date of Last EDR Contact: 08/23/04

INDIAN UST: Underground Storage Tanks on Indian Land
Source: EPA Region 9
Telephone: 415-972-3368

Date of Government Version: 06/18/04
Date Made Active at EDR: 07/26/04
Database Release Frequency: Varies
Date of Data Arrival at EDR: 06/21/04
Elapsed ASTM days: 35
Date of Last EDR Contact: 08/23/04

CA FID UST: Facility Inventory Database
Source: California Environmental Protection Agency
Telephone: 916-445-6532
The Facility Inventory Database (FID) contains a historical listing of active and inactive underground storage tank locations from the State Water Resource Control Board. Refer to local/county source for current data.

Date of Government Version: 10/31/94
Date Made Active at EDR: 09/29/95
Database Release Frequency: No Update Planned
Date of Data Arrival at EDR: 09/05/95
Elapsed ASTM days: 24
Date of Last EDR Contact: 12/28/98

HIST UST: Hazardous Substance Storage Container Database
Source: State Water Resources Control Board
Telephone: 916-341-5700
The Hazardous Substance Storage Container Database is a historical listing of UST sites. Refer to local/county source for current data.

Date of Government Version: 10/15/90
Date Made Active at EDR: 02/12/91
Database Release Frequency: No Update Planned
Date of Data Arrival at EDR: 01/25/91
Elapsed ASTM days: 18
Date of Last EDR Contact: 07/26/01

GOVERNMENT RECORDS SEARCHED / DATA CURRENCY TRACKING

STATE OF CALIFORNIA ASTM SUPPLEMENTAL RECORDS

AST: Aboveground Petroleum Storage Tank Facilities
Source: State Water Resources Control Board
Telephone: 916-341-5712
Registered Aboveground Storage Tanks.

Date of Government Version: 12/01/03 | Date of Last EDR Contact: 11/01/04
Database Release Frequency: Quarterly | Date of Next Scheduled EDR Contact: 01/31/05

CLEANERS: Cleaner Facilities
Source: Department of Toxic Substance Control
Telephone: 916-225-0873
A list of drycleaner related facilities that have EPA ID numbers. These are facilities with certain SIC codes: power laundries, family and commercial; garment pressing and cleaner's agents; linen supply; coin-operated laundries and cleaning; drycleaning plants, except rugs; carpet and upholster cleaning; industrial launderers; laundry and garment services.

Date of Government Version: 04/21/04 | Date of Last EDR Contact: 11/01/04
Database Release Frequency: Annually | Date of Next Scheduled EDR Contact: 01/03/05

CA WDS: Waste Discharge System
Source: State Water Resources Control Board
Telephone: 916-341-5227
Sites which have been issued waste discharge requirements.

Date of Government Version: 10/11/04 | Date of Last EDR Contact: 09/21/04
Database Release Frequency: Quarterly | Date of Next Scheduled EDR Contact: 12/20/04

DEED: List of Deed Restrictions
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
The use of recorded land use restrictions is one of the methods the DTSC uses to protect the public from unsafe exposures to hazardous substances and wastes.

Date of Government Version: 10/04/04 | Date of Last EDR Contact: 10/04/04
Database Release Frequency: Semi-Annually | Date of Next Scheduled EDR Contact: 01/03/05

NFA: No Further Action Determination
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
This category contains properties at which DTSC has made a clear determination that the property does not pose a problem to the environment or to public health.

Date of Government Version: 10/05/04 | Date of Last EDR Contact: 09/16/04
Database Release Frequency: Quarterly | Date of Next Scheduled EDR Contact: 11/29/04

EMI: Emissions Inventory Data
Source: California Air Resources Board
Telephone: 916-322-2990
Toxics and criteria pollutant emissions data collected by the ARB and local air pollution agencies.

Date of Government Version: 12/31/02 | Date of Last EDR Contact: 10/22/04
Database Release Frequency: Varies | Date of Next Scheduled EDR Contact: 01/17/05

REF: Unconfirmed Properties Referred to Another Agency
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
This category contains properties where contamination has not been confirmed and which were determined as not requiring direct DTSC Site Mitigation Program action or oversight. Accordingly, these sites have been referred to another state or local regulatory agency.

Date of Government Version: 10/05/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/16/04
Date of Next Scheduled EDR Contact: 11/29/04

SCH: School Property Evaluation Program
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
This category contains proposed and existing school sites that are being evaluated by DTSC for possible hazardous materials contamination. In some cases, these properties may be listed in the CalSites category depending on the level of threat to public health and safety or the environment they pose.

Date of Government Version: 10/05/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/16/04
Date of Next Scheduled EDR Contact: 11/29/04

NFE: Properties Needing Further Evaluation
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
This category contains properties that are suspected of being contaminated. These are unconfirmed contaminated properties that need to be assessed using the PEA process. PEA in Progress indicates properties where DTSC is currently conducting a PEA. PEA Required indicates properties where DTSC has determined a PEA is required, but not currently underway.

Date of Government Version: 10/05/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/16/04
Date of Next Scheduled EDR Contact: 11/29/04

SLIC: Statewide SLIC Cases
Source: State Water Resources Control Board
Telephone: 916-341-5752
The Spills, Leaks, Investigations, and Cleanups (SLIC) listings includes unauthorized discharges from spills and leaks, other than from underground storage tanks or other regulated sites.

Date of Government Version: 10/13/04
Database Release Frequency: Varies

Date of Last EDR Contact: 10/13/04
Date of Next Scheduled EDR Contact: 01/10/05

HAZNET: Facility and Manifest Data
Source: California Environmental Protection Agency
Telephone: 916-255-1136
Facility and Manifest Data. The data is extracted from the copies of hazardous waste manifests received each year by the DTSC. The annual volume of manifests is typically 700,000 - 1,000,000 annually, representing approximately 350,000 - 500,000 shipments. Data are from the manifests submitted without correction, and therefore many contain some invalid values for data elements such as generator ID, TSD ID, waste category, and disposal method.

Date of Government Version: 12/31/02
Database Release Frequency: Annually

Date of Last EDR Contact: 08/09/04
Date of Next Scheduled EDR Contact: 11/08/04

LOCAL RECORDS

ALAMEDA COUNTY:

Local Oversight Program Listing of UGT Cleanup Sites
Source: Alameda County Environmental Health Services
Telephone: 510-567-6700

Date of Government Version: 08/17/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 10/25/04
Date of Next Scheduled EDR Contact: 01/24/05

Underground Tanks
Source: Alameda County Environmental Health Services
Telephone: 510-567-6700

Date of Government Version: 08/17/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 10/25/04
Date of Next Scheduled EDR Contact: 01/24/05

CONTRA COSTA COUNTY:

Site List
Source: Contra Costa Health Services Department
Telephone: 925-646-2286
List includes sites from the underground tank, hazardous waste generator and business plan/2185 programs.

Date of Government Version: 08/30/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 08/30/04
Date of Next Scheduled EDR Contact: 11/29/04

FRESNO COUNTY:

CUPA Resources List
Source: Dept. of Community Health
Telephone: 559-445-3271
Certified Unified Program Agency. CUPA's are responsible for implementing a unified hazardous materials and hazardous waste management regulatory program. The agency provides oversight of businesses that deal with hazardous materials, operate underground storage tanks or aboveground storage tanks.

Date of Government Version: 07/21/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 08/09/04
Date of Next Scheduled EDR Contact: 11/08/04

KERN COUNTY:

Underground Storage Tank Sites & Tank Listing
Source: Kern County Environment Health Services Department
Telephone: 661-862-8700
Kern County Sites and Tanks Listing.

Date of Government Version: 09/14/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/06/04

LOS ANGELES COUNTY:

List of Solid Waste Facilities
Source: La County Department of Public Works
Telephone: 818-458-5185

Date of Government Version: 06/03/03
Database Release Frequency: Varies

Date of Last EDR Contact: 08/19/04
Date of Next Scheduled EDR Contact: 11/15/04

City of El Segundo Underground Storage Tank
Source: City of El Segundo Fire Department
Telephone: 310-524-2236

Date of Government Version: 09/07/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 08/30/04
Date of Next Scheduled EDR Contact: 11/15/04

City of Long Beach Underground Storage Tank
Source: City of Long Beach Fire Department
Telephone: 562-570-2543

Date of Government Version: 03/28/03
Database Release Frequency: Annually

Date of Last EDR Contact: 08/27/04
Date of Next Scheduled EDR Contact: 11/22/04

City of Torrance Underground Storage Tank
Source: City of Torrance Fire Department
Telephone: 310-618-2973

Date of Government Version: 08/16/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 06/16/04
Date of Next Scheduled EDR Contact: 11/15/04

City of Los Angeles Landfills
Source: Engineering & Construction Division
Telephone: 213-473-7869

Date of Government Version: 03/01/04
Database Release Frequency: Varies

Date of Last EDR Contact: 09/14/04
Date of Next Scheduled EDR Contact: 12/13/04

HMS: Street Number List
Source: Department of Public Works
Telephone: 626-458-3517
Industrial Waste and Underground Storage Tank Sites.

Date of Government Version: 04/29/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 08/16/04
Date of Next Scheduled EDR Contact: 11/15/04

Site Mitigation List
Source: Community Health Services
Telephone: 323-890-7806
Industrial sites that have had some sort of spill or complaint.

Date of Government Version: 02/26/04
Database Release Frequency: Annually

Date of Last EDR Contact: 08/16/04
Date of Next Scheduled EDR Contact: 11/15/04

San Gabriel Valley Areas of Concern
Source: EPA Region 9
Telephone: 415-972-3178
San Gabriel Valley areas where VOC contamination is at or above the MCL as designated by region 9 EPA office.

Date of Government Version: 12/31/98
Database Release Frequency: No Update Planned

Date of Last EDR Contact: 07/06/99
Date of Next Scheduled EDR Contact: N/A

MARIN COUNTY:

Underground Storage Tank Sites
Source: Public Works Department Waste Management
Telephone: 415-499-6647
Currently permitted USTs in Marin County.

Date of Government Version: 08/18/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 11/01/04
Date of Next Scheduled EDR Contact: 01/31/05

NAPA COUNTY:

Sites With Reported Contamination
Source: Napa County Department of Environmental Management
Telephone: 707-253-4269

Date of Government Version: 09/29/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 09/27/04
Date of Next Scheduled EDR Contact: 12/27/04

Closed and Operating Underground Storage Tank Sites
Source: Napa County Department of Environmental Management
Telephone: 707-253-4269

Date of Government Version: 09/29/04
Database Release Frequency: Annually

Date of Last EDR Contact: 09/27/04
Date of Next Scheduled EDR Contact: 12/27/04

ORANGE COUNTY:

List of Underground Storage Tank Cleanups
Source: Health Care Agency
Telephone: 714-834-3446
Orange County Underground Storage Tank Cleanups (LUST).

Date of Government Version: 10/14/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/09/04
Date of Next Scheduled EDR Contact: 12/06/04

List of Underground Storage Tank Facilities
Source: Health Care Agency
Telephone: 714-834-3446
Orange County Underground Storage Tank Facilities (UST).

Date of Government Version: 09/01/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/09/04
Date of Next Scheduled EDR Contact: 12/06/04

List of Industrial Site Cleanups
Source: Health Care Agency
Telephone: 714-834-3446
Petroleum and non-petroleum spills.

Date of Government Version: 09/01/04
Database Release Frequency: Annually

Date of Last EDR Contact: 09/09/04
Date of Next Scheduled EDR Contact: 12/06/04

PLACER COUNTY:

Master List of Facilities
Source: Placer County Health and Human Services
Telephone: 530-889-7312
List includes aboveground tanks, underground tanks and cleanup sites.

Date of Government Version: 10/04/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 09/20/04
Date of Next Scheduled EDR Contact: 12/20/04

RIVERSIDE COUNTY:

Listing of Underground Tank Cleanup Sites
Source: Department of Public Health
Telephone: 909-358-5055
Riverside County Underground Storage Tank Cleanup Sites (LUST).

Date of Government Version: 06/21/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/18/04
Date of Next Scheduled EDR Contact: 01/17/05

Underground Storage Tank Tank List
Source: Health Services Agency
Telephone: 909-358-5055

Date of Government Version: 06/21/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/18/04
Date of Next Scheduled EDR Contact: 01/17/05

SACRAMENTO COUNTY:

CS - Contaminated Sites
Source: Sacramento County Environmental Management
Telephone: 916-875-8406

Date of Government Version: 08/28/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/13/04
Date of Next Scheduled EDR Contact: 01/31/05

ML - Regulatory Compliance Master List
Source: Sacramento County Environmental Management
Telephone: 916-875-8406
Any business that has hazardous materials on site - hazardous material storage sites, underground storage tanks, waste generators.

Date of Government Version: 09/02/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 11/02/04
Date of Next Scheduled EDR Contact: 01/31/05

SAN BERNARDINO COUNTY:

Hazardous Material Permits
Source: San Bernardino County Fire Department Hazardous Materials Division
Telephone: 909-387-3041
This listing includes underground storage tanks, medical waste handlers/generators, hazardous materials handlers, hazardous waste generators, and waste oil generators/handlers.

Date of Government Version: 09/17/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/06/04

SAN DIEGO COUNTY:

Solid Waste Facilities
Source: Department of Health Services
Telephone: 619-338-2209
San Diego County Solid Waste Facilities.

Date of Government Version: 08/01/00
Database Release Frequency: Varies

Date of Last EDR Contact: 08/23/04
Date of Next Scheduled EDR Contact: 11/22/04

Hazardous Materials Management Division Database
Source: Hazardous Materials Management Division
Telephone: 619-338-2268
The database includes: HE58 - This report contains the business name, site address, business phone number, establishment 'H' permit number, type of permit, and the business status. HE17 - In addition to providing the same information provided in the HE58 listing, HE17 provides inspection dates, violations received by the establishment, hazardous waste generated, the quantity, method of storage, treatment/disposal of waste and the hauler, and information on underground storage tanks. Unauthorized Release List - Includes a summary of environmental contamination cases in San Diego County (underground tank cases, non-tank cases, groundwater contamination, and soil contamination are included.)

Date of Government Version: 06/29/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/08/04
Date of Next Scheduled EDR Contact: 01/03/05

SAN FRANCISCO COUNTY:

Local Oversite Facilities
Source: Department Of Public Health San Francisco County
Telephone: 415-252-3920

Date of Government Version: 09/15/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/20/04
Date of Next Scheduled EDR Contact: 12/06/04

Underground Storage Tank Information
Source: Department of Public Health
Telephone: 415-252-3920

Date of Government Version: 09/15/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/20/04
Date of Next Scheduled EDR Contact: 12/26/04

SAN MATEO COUNTY:

Fuel Leak List
Source: San Mateo County Environmental Health Services Division
Telephone: 650-363-1921

Date of Government Version: 10/27/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 10/12/04
Date of Next Scheduled EDR Contact: 01/10/05

Business Inventory
Source: San Mateo County Environmental Health Services Division
Telephone: 650-363-1921
List includes Hazardous Materials Business Plan, hazardous waste generators, and underground storage tanks.

Date of Government Version: 08/19/04
Database Release Frequency: Annually

Date of Last EDR Contact: 10/12/04
Date of Next Scheduled EDR Contact: 01/10/05

SANTA CLARA COUNTY:

Fuel Leak Site Activity Report
Source: Santa Clara Valley Water District
Telephone: 408-265-2600

Date of Government Version: 06/30/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 09/27/04
Date of Next Scheduled EDR Contact: 12/27/04

Hazardous Material Facilities
Source: City of San Jose Fire Department
Telephone: 408-277-4659

Date of Government Version: 10/01/03
Database Release Frequency: Annually

Date of Last EDR Contact: 09/07/04
Date of Next Scheduled EDR Contact: 12/06/04

SOLANO COUNTY:

Leaking Underground Storage Tanks
Source: Solano County Department of Environmental Management
Telephone: 707-421-6770

Date of Government Version: 09/20/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/13/04
Date of Next Scheduled EDR Contact: 12/13/04

Underground Storage Tanks
Source: Solano County Department of Environmental Management
Telephone: 707-421-6770

Date of Government Version: 09/20/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/13/04
Date of Next Scheduled EDR Contact: 12/13/04

SONOMA COUNTY:

Leaking Underground Storage Tank Sites
Source: Department of Health Services
Telephone: 707-565-6565

Date of Government Version: 10/25/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/25/04
Date of Next Scheduled EDR Contact: 01/24/05

SUTTER COUNTY:

Underground Storage Tanks
Source: Sutter County Department of Agriculture
Telephone: 530-822-7500

Date of Government Version: 01/29/04
Database Release Frequency: Semi-Annually

Date of Last EDR Contact: 10/18/04
Date of Next Scheduled EDR Contact: 01/03/05

VENTURA COUNTY:

Inventory of Illegal Abandoned and Inactive Sites
Source: Environmental Health Division
Telephone: 805-654-2813
Ventura County Inventory of Closed, Illegal Abandoned, and Inactive Sites.

Date of Government Version: 08/01/04
Database Release Frequency: Annually

Date of Last EDR Contact: 08/25/04
Date of Next Scheduled EDR Contact: 11/22/04

Listing of Underground Tank Cleanup Sites
Source: Environmental Health Division
Telephone: 805-654-2813
Ventura County Underground Storage Tank Cleanup Sites (LUST).

Date of Government Version: 09/02/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/14/04
Date of Next Scheduled EDR Contact: 12/13/04

Underground Tank Closed Sites List
Source: Environmental Health Division
Telephone: 805-654-2813
Ventura County Operating Underground Storage Tank Sites (UST)/Underground Tank Closed Sites List.

Date of Government Version: 09/29/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/13/04
Date of Next Scheduled EDR Contact: 01/10/05

Business Plan, Hazardous Waste Producers, and Operating Underground Tanks
Source: Ventura County Environmental Health Division
Telephone: 805-654-2813
The BWT list indicates by site address whether the Environmental Health Division has Business Plan (B), Waste Producer (W), and/or Underground Tank (T) information.

Date of Government Version: 09/02/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 09/14/04
Date of Next Scheduled EDR Contact: 12/13/04

YOLO COUNTY:

Underground Storage Tank Comprehensive Facility Report
Source: Yolo County Department of Health
Telephone: 530-666-8646

Date of Government Version: 06/02/04
Database Release Frequency: Annually

Date of Last EDR Contact: 10/18/04
Date of Next Scheduled EDR Contact: 01/17/05

California Regional Water Quality Control Board (RWQCB) LUST Records

LUST REG 1: Active Toxic Site Investigation
Source: California Regional Water Quality Control Board North Coast (1)
Telephone: 707-576-2220
Del Norte, Humboldt, Lake, Mendocino, Modoc, Siskiyou, Sonoma, Trinity counties. For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 02/01/01
Database Release Frequency: No Update Planned

Date of Last EDR Contact: 08/23/04
Date of Next Scheduled EDR Contact: 11/22/04

LUST REG 2: Fuel Leak List
Source: California Regional Water Quality Control Board San Francisco Bay Region (2)
Telephone: 510-286-0457

Date of Government Version: 09/30/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/13/04
Date of Next Scheduled EDR Contact: 01/10/05

LUST REG 3: Leaking Underground Storage Tank Database
Source: California Regional Water Quality Control Board Central Coast Region (3)
Telephone: 805-549-3147

Date of Government Version: 05/19/03
Database Release Frequency: Varies

Date of Last EDR Contact: 08/17/04
Date of Next Scheduled EDR Contact: 11/15/04

LUST REG 4: Underground Storage Tank Leak List
Source: California Regional Water Quality Control Board Los Angeles Region (4)
Telephone: 213-576-6600
Los Angeles, Ventura counties. For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 09/07/04
Database Release Frequency: No Update Planned

Date of Last EDR Contact: 08/16/04
Date of Next Scheduled EDR Contact: 12/27/04

LUST REG 5: Leaking Underground Storage Tank Database
Source: California Regional Water Quality Control Board Central Valley Region (5)
Telephone: 916-464-3291

Date of Government Version: 10/01/04
Database Release Frequency: Quarterly

Date of Last EDR Contact: 10/22/04
Date of Next Scheduled EDR Contact: 01/30/05

LUST REG 6L: Leaking Underground Storage Tank Case Listing
Source: California Regional Water Quality Control Board Lahontan Region (6)
Telephone: 916-542-5424
For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 09/09/03
Database Release Frequency: No Update Planned
Date of Last EDR Contact: 09/08/04
Date of Next Scheduled EDR Contact: 12/06/04

LUST REG 6V: Leaking Underground Storage Tank Case Listing
Source: California Regional Water Quality Control Board Victorville Branch Office (6)
Telephone: 760-346-7491

Date of Government Version: 08/09/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 10/04/04
Date of Next Scheduled EDR Contact: 01/03/05

LUST REG 7: Leaking Underground Storage Tank Case Listing
Source: California Regional Water Quality Control Board Colorado River Basin Region (7)
Telephone: 760-346-7491

Date of Government Version: 02/26/04
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: 09/27/04
Date of Next Scheduled EDR Contact: 12/27/04

LUST REG 8: Leaking Underground Storage Tanks
Source: California Regional Water Quality Control Board Santa Ana Region (8)
Telephone: 951-782-4130
California Regional Water Quality Control Board Santa Ana Region (8). For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 07/01/04
Database Release Frequency: No Update Planned
Date of Last EDR Contact: 08/09/04
Date of Next Scheduled EDR Contact: 11/08/04

LUST REG 9: Leaking Underground Storage Tank Report
Source: California Regional Water Quality Control Board San Diego Region (9)
Telephone: 858-467-2980
Orange, Riverside, San Diego counties. For more current information, please refer to the State Water Resources Control Board's LUST database.

Date of Government Version: 03/01/01
Database Release Frequency: No Update Planned
Date of Last EDR Contact: 10/18/04
Date of Next Scheduled EDR Contact: 01/17/05

California Regional Water Quality Control Board (RWQCB) SLIC Records

SLIC REG 1: Active Toxic Site Investigations
Source: California Regional Water Quality Control Board, North Coast Region (1)
Telephone: 707-576-2220

Date of Government Version: 04/03/03
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: 08/23/04
Date of Next Scheduled EDR Contact: 11/22/04

SLIC REG 2: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: Regional Water Quality Control Board San Francisco Bay Region (2)
Telephone: 510-286-0457
Any contaminated site that impacts groundwater or has the potential to impact groundwater.

Date of Government Version: 09/30/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 10/13/04
Date of Next Scheduled EDR Contact: 01/10/05

SLIC REG 3: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: California Regional Water Quality Control Board Central Coast Region (3)
Telephone: 805-549-3147
Any contaminated site that impacts groundwater or has the potential to impact groundwater.

Date of Government Version: 08/20/04
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: 08/16/04
Date of Next Scheduled EDR Contact: 11/15/04

SLIC REG 4: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: Region Water Quality Control Board Los Angeles Region (4)
Telephone: 213-576-6600
Any contaminated site that impacts groundwater or has the potential to impact groundwater.

Date of Government Version: 07/08/04 — Date of Last EDR Contact: 10/25/04
Database Release Frequency: Quarterly — Date of Next Scheduled EDR Contact: 01/24/05

SLIC REG 5: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: Regional Water Quality Control Board Central Valley Region (5)
Telephone: 916-464-3291
Unregulated sites that impact groundwater or have the potential to impact groundwater.

Date of Government Version: 04/01/04 — Date of Last EDR Contact: 10/06/04
Database Release Frequency: Semi-Annually — Date of Next Scheduled EDR Contact: 01/03/05

SLIC REG 6L: SLIC Sites
Source: California Regional Water Quality Control Board, Lahontan Region
Telephone: 530-542-5574

Date of Government Version: 09/07/04 — Date of Last EDR Contact: 09/07/04
Database Release Frequency: Varies — Date of Next Scheduled EDR Contact: 12/06/04

SLIC REG 6V: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: Regional Water Quality Control Board, Victorville Branch
Telephone: 619-241-6583

Date of Government Version: 04/01/04 — Date of Last EDR Contact: 10/04/04
Database Release Frequency: Semi-Annually — Date of Next Scheduled EDR Contact: 01/03/05

SLIC REG 7: SLIC List
Source: California Regional Quality Control Board, Colorado River Basin Region
Telephone: 760-346-7491

Date of Government Version: 08/25/04 — Date of Last EDR Contact: 08/23/04
Database Release Frequency: Varies — Date of Next Scheduled EDR Contact: 11/22/04

SLIC REG 8: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: California Region Water Quality Control Board Santa Ana Region (8)
Telephone: 951-782-3298

Date of Government Version: 07/01/04 — Date of Last EDR Contact: 10/08/04
Database Release Frequency: Semi-Annually — Date of Next Scheduled EDR Contact: 01/03/05

SLIC REG 9: Spills, Leaks, Investigation & Cleanup Cost Recovery Listing
Source: California Regional Water Quality Control Board San Diego Region (9)
Telephone: 858-467-2980

Date of Government Version: 09/10/04 — Date of Last EDR Contact: 08/30/04
Database Release Frequency: Annually — Date of Next Scheduled EDR Contact: 11/29/04

EDR PROPRIETARY HISTORICAL DATABASES

Former Manufactured Gas (Coal Gas) Sites: The existence and location of Coal Gas sites is provided exclusively to EDR by Real Property Scan, Inc. ©Copyright 1993 Real Property Scan, Inc. For a technical description of the types of hazards which may be found at such sites, contact your EDR customer service representative.

Disclaimer Provided by Real Property Scan, Inc.

The information contained in this report has predominantly been obtained from publicly available sources produced by entities other than Real Property Scan. While reasonable steps have been taken to insure the accuracy of this report, Real Property Scan does not guarantee the accuracy of this report. Any liability on the part of Real Property Scan is strictly limited to a refund of the amount paid. No claim is made for the actual existence of toxins at any site. This report does not constitute a legal opinion.

GOVERNMENT RECORDS SEARCHED / DATA CURRENCY TRACKING

BROWNFIELDS DATABASES

VCP: Voluntary Cleanup Program Properties
Source: Department of Toxic Substances Control
Telephone: 916-323-3400
Contains low threat level properties with either confirmed or unconfirmed releases and the project proponents have request that DTSC oversee investigation and/or cleanup activities and have agreed to provide coverage for DTSC's costs.

Date of Government Version: 10/05/04
Database Release Frequency: Quarterly
Date of Last EDR Contact: 09/16/04
Date of Next Scheduled EDR Contact: 11/29/04

US BROWNFIELDS: A Listing of Brownfields Sites
Source: Environmental Protection Agency
Telephone: 202-566-2777
Included in the listing are brownfields properties addresses by Cooperative Agreement Recipients and brownfields properties addressed by Targeted Brownfields Assessments. Targeted Brownfields Assessments-EPA's Targeted Brownfields Assessments (TBA) program is designed to help states, tribes, and municipalities--especially those without EPA Brownfields Assessment Demonstration Pilots--minimize the uncertainties of contamination often associated with brownfields. Under the TBA program, EPA provides funding and/or technical assistance for environmental assessments at brownfields sites throughout the country. Targeted Brownfields Assessments supplement and work with other efforts under EPA's Brownfields Initiative to promote cleanup and redevelopment of brownfields. Cooperative Agreement Recipients-States, political subdivisions, territories, and Indian tribes become Brownfields Cleanup Revolving Loan Fund (BCRLF) cooperative agreement recipients when they enter into BCRLF cooperative agreements with the U.S. EPA. EPA selects BCRLF cooperative agreement recipients based on a proposal and application process. BCRLF cooperative agreement recipients must use EPA funds provided through BCRLF cooperative agreement for specified brownfields-related cleanup activities.

Date of Government Version: N/A
Database Release Frequency: Semi-Annually
Date of Last EDR Contact: N/A
Date of Next Scheduled EDR Contact: N/A

OTHER DATABASE(S)

Depending on the geographic area covered by this report, the data provided in these specialty databases may or may not be complete. For example, the existence of wetlands information data in a specific report does not mean that all wetlands in the area covered by the report are included. Moreover, the absence of any reported wetlands information does not necessarily mean that wetlands do not exist in the area covered by the report.

Oil/Gas Pipelines: This data was obtained by EDR from the USGS in 1994. It is referred to by USGS as GeoData Digital Line Graphs from 1:100,000-Scale Maps. It was extracted from the transportation category including some oil, but primarily gas pipelines.

Electric Power Transmission Line Data
Source: PennWell Corporation
Telephone: (800) 823-6277
This map includes information copyrighted by PennWell Corporation. This information is provided on a best effort basis and PennWell Corporation does not guarantee its accuracy nor warrant its fitness for any particular purpose. Such information has been reprinted with the permission of PennWell.

Sensitive Receptors: There are individuals deemed sensitive receptors due to their fragile immune systems and special sensitivity to environmental discharges. These sensitive receptors typically include the elderly, the sick, and children. While the location of all sensitive receptors cannot be determined, EDR indicates those buildings and facilities - schools, daycares, hospitals, medical centers, and nursing homes - where individuals who are sensitive receptors are likely to be located.

AHA Hospitals:
Source: American Hospital Association, Inc.
Telephone: 312-280-5991
The database includes a listing of hospitals based on the American Hospital Association's annual survey of hospitals.

Medical Centers: Provider of Services Listing
Source: Centers for Medicare & Medicaid Services
Telephone: 410-786-3000
A listing of hospitals with Medicare provider number, produced by Centers of Medicare & Medicaid Services, a federal agency within the U.S. Department of Health and Human Services.

Nursing Homes
Source: National Institutes of Health
Telephone: 301-594-6248
Information on Medicare and Medicaid certified nursing homes in the United States.

Public Schools
Source: National Center for Education Statistics
Telephone: 202-502-7300
The National Center for Education Statistics' primary database on elementary and secondary public education in the United States. It is a comprehensive, annual, national statistical database of all public elementary and secondary schools and school districts, which contains data that are comparable across all states.

Private Schools
Source: National Center for Education Statistics
Telephone: 202-502-7300
The National Center for Education Statistics' primary database on private school locations in the United States.

Daycare Centers: Licensed Facilities
Source: Department of Social Services
Telephone: 916-657-4041

Flood Zone Data: This data, available in select counties across the country, was obtained by EDR in 1999 from the Federal Emergency Management Agency (FEMA). Data depicts 100-year and 500-year flood zones as defined by FEMA.

NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002 from the U.S. Fish and Wildlife Service.

STREET AND ADDRESS INFORMATION

GEOCHECK ®- PHYSICAL SETTING SOURCE ADDENDUM

TARGET PROPERTY ADDRESS

BUCKLEY SCHOOL
3900 STANSBURY AVENUE
SHERMAN OAKS, CA 91423

TARGET PROPERTY COORDINATES

Latitude (North):	34.139599 - 34˚ 8' 22.6"
Longitude (West):	118.443604 - 118˚ 26' 37.0"
Universal Tranverse Mercator:	Zone 11
UTM X (Meters):	366896.9
UTM Y (Meters):	3778381.0
Elevation:	797 ft. above sea level

EDR's GeoCheck Physical Setting Source Addendum has been developed to assist the environmental professional with the collection of physical setting source information in accordance with ASTM 1527-00, Section 7.2.3. Section 7.2.3 requires that a current USGS 7.5 Minute Topographic Map (or equivalent, such as the USGS Digital Elevation Model) be reviewed. It also requires that one or more additional physical setting sources be sought when (1) conditions have been identified in which hazardous substances or petroleum products are likely to migrate to or from the property, and (2) more information than is provided in the current USGS 7.5 Minute Topographic Map (or equivalent) is generally obtained, pursuant to local good commercial or customary practice, to assess the impact of migration of recognized environmental conditions in connection with the property. Such additional physical setting sources generally include information about the topographic, hydrologic, hydrogeologic, and geologic characteristics of a site, and wells in the area.

Assessment of the impact of contaminant migration generally has two principle investigative components:

1. Groundwater flow direction, and
2. Groundwater flow velocity.

Groundwater flow direction may be impacted by surface topography, hydrology, hydrogeology, characteristics of the soil, and nearby wells. Groundwater flow velocity is generally impacted by the nature of the geologic strata. EDR's GeoCheck Physical Setting Source Addendum is provided to assist the environmental professional in forming an opinion about the impact of potential contaminant migration.

GEOCHECK® - PHYSICAL SETTING SOURCE SUMMARY

GROUNDWATER FLOW DIRECTION INFORMATION

Groundwater flow direction for a particular site is best determined by a qualified environmental professional using site-specific well data. If such data is not reasonably ascertainable, it may be necessary to rely on other sources of information, such as surface topographic information, hydrologic information, hydrogeologic data collected on nearby properties, and regional groundwater flow information (from deep aquifers).

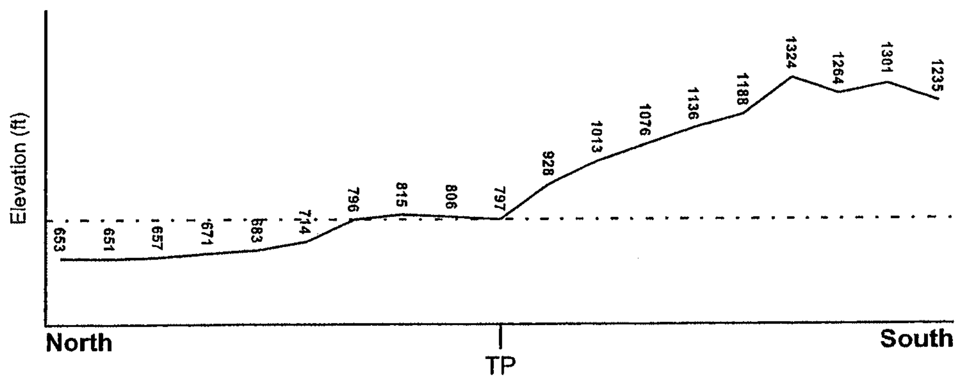
TOPOGRAPHIC INFORMATION

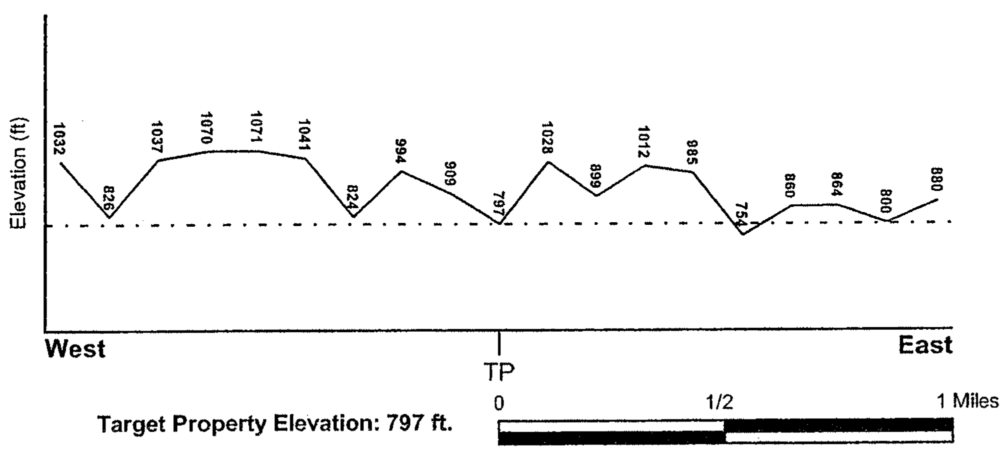
Surface topography may be indicative of the direction of surficial groundwater flow. This information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

TARGET PROPERTY TOPOGRAPHY

USGS Topographic Map:	34118-B4 VAN NUYS, CA
General Topographic Gradient:	General NNE
Source:	USGS 7.5 min quad index

SURROUNDING TOPOGRAPHY: ELEVATION PROFILES





Target Property Elevation: 797 ft.

Source: Topography has been determined from the USGS 7.5' Digital Elevation Model and should be evaluated on a relative (not an absolute) basis. Relative elevation information between sites of close proximity should be field verified.

GEOCHECK® - PHYSICAL SETTING SOURCE SUMMARY

HYDROLOGIC INFORMATION

Surface water can act as a hydrologic barrier to groundwater flow. Such hydrologic information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

Refer to the Physical Setting Source Map following this summary for hydrologic information (major waterways and bodies of water).

FEMA FLOOD ZONE

Target Property County	FEMA Flood Electronic Data
LOS ANGELES, CA	YES - refer to the Overview Map and Detail Map

Flood Plain Panel at Target Property: 0601370045C

Additional Panels in search area: 0601370044C
0601370053C
0601370052C

NATIONAL WETLAND INVENTORY

NWI Quad at Target Property	NWI Electronic Data Coverage
VAN NUYS	YES - refer to the Overview Map and Detail Map

HYDROGEOLOGIC INFORMATION

Hydrogeologic information obtained by installation of wells on a specific site can often be an indicator of groundwater flow direction in the immediate area. Such hydrogeologic information can be used to assist the environmental professional in forming an opinion about the impact of nearby contaminated properties or, should contamination exist on the target property, what downgradient sites might be impacted.

Site-Specific Hydrogeological Data*:

Search Radius: 1.25 miles
Status: Not found

AQUIFLOW®

Search Radius: 1.000 Mile.

EDR has developed the AQUIFLOW Information System to provide data on the general direction of groundwater flow at specific points. EDR has reviewed reports submitted by environmental professionals to regulatory authorities at select sites and has extracted the date of the report, groundwater flow direction as determined hydrogeologically, and the depth to water table.

MAP ID	LOCATION FROM TP	GENERAL DIRECTION GROUNDWATER FLOW
Not Reported		

* ©1996 Site-specific hydrogeological data gathered by CERCLIS Alerts, Inc., Bainbridge Island, WA. All rights reserved. All of the information and opinions presented are those of the cited EPA report(s), which were completed under a Comprehensive Environmental Response Compensation and Liability Information System (CERCLIS) investigation.

GEOCHECK® - PHYSICAL SETTING SOURCE SUMMARY

GROUNDWATER FLOW VELOCITY INFORMATION

Groundwater flow velocity information for a particular site is best determined by a qualified environmental professional using site specific geologic and soil strata data. If such data are not reasonably ascertainable, it may be necessary to rely on other sources of information, including geologic age identification, rock stratigraphic unit and soil characteristics data collected on nearby properties and regional soil information. In general, contaminant plumes move more quickly through sandy-gravelly types of soils than silty-clayey types of soils.

GEOLOGIC INFORMATION IN GENERAL AREA OF TARGET PROPERTY

Geologic information can be used by the environmental professional in forming an opinion about the relative speed at which contaminant migration may be occurring.

ROCK STRATIGRAPHIC UNIT

Era:	Cenozoic
System:	Tertiary
Series:	Miocene
Code:	Tm *(decoded above as Era, System & Series)*

GEOLOGIC AGE IDENTIFICATION

Category: Stratified Sequence

Geologic Age and Rock Stratigraphic Unit Source: P.G. Schruben, R.E. Arndt and W.J. Bawiec, Geology of the Conterminous U.S. at 1:2,500,000 Scale - a digital representation of the 1974 P.B. King and H.M. Beikman Map, USGS Digital Data Series DDS - 11 (1994).

DOMINANT SOIL COMPOSITION IN GENERAL AREA OF TARGET PROPERTY

The U.S. Department of Agriculture's (USDA) Soil Conservation Service (SCS) leads the National Cooperative Soil Survey (NCSS) and is responsible for collecting, storing, maintaining and distributing soil survey information for privately owned lands in the United States. A soil map in a soil survey is a representation of soil patterns in a landscape. Soil maps for STATSGO are compiled by generalizing more detailed (SSURGO) soil survey maps. The following information is based on Soil Conservation Service STATSGO data.

Soil Component Name:	HAMBRIGHT
Soil Surface Texture:	gravelly - loam
Hydrologic Group:	Class D - Very slow infiltration rates. Soils are clayey, have a high water table, or are shallow to an impervious layer.
Soil Drainage Class:	Well drained. Soils have intermediate water holding capacity. Depth to water table is more than 6 feet.

Hydric Status: Soil does not meet the requirements for a hydric soil.

Corrosion Potential - Uncoated Steel:	MODERATE
Depth to Bedrock Min:	> 10 inches
Depth to Bedrock Max:	> 20 inches

Soil Layer Information							
	Boundary			Classification			
Layer	Upper	Lower	Soil Texture Class	AASHTO Group	Unified Soil	Permeability Rate (in/hr)	Soil Reaction (pH)
1	0 inches	7 inches	gravelly - loam	Silt-Clay Materials (more than 35 pct. passing No. 200), Silty Soils.	COARSE-GRAINED SOILS, Gravels, Gravels with fines, Silty Gravel	Max: 2.00 Min: 0.60	Max: 7.30 Min: 6.10
2	7 inches	16 inches	very gravelly - loam	Granular materials (35 pct. or less passing No. 200), Silty, or Clayey Gravel and Sand.	COARSE-GRAINED SOILS, Gravels, Gravels with fines, Silty Gravel. COARSE-GRAINED SOILS, Gravels, Gravels with fines, Clayey Gravel.	Max: 2.00 Min: 0.60	Max: 7.30 Min: 6.10
3	16 inches	20 inches	unweathered bedrock	Not reported	Not reported	Max: 0.00 Min: 0.00	Max: 0.00 Min: 0.00

OTHER SOIL TYPES IN AREA

Based on Soil Conservation Service STATSGO data, the following additional subordinant soil types may appear within the general area of target property.

Soil Surface Textures: loam
silty clay loam
shaly - clay loam
sandy loam
loamy sand
clay
clay loam

Surficial Soil Types: loam
silty clay loam
shaly - clay loam
sandy loam
loamy sand
clay
clay loam

Shallow Soil Types: silty clay

Deeper Soil Types: weathered bedrock
clay loam

GEOCHECK® - PHYSICAL SETTING SOURCE SUMMARY

ADDITIONAL ENVIRONMENTAL RECORD SOURCES

According to ASTM E 1527-00, Section 7.2.2, "one or more additional state or local sources of environmental records may be checked, in the discretion of the environmental professional, to enhance and supplement federal and state sources... Factors to consider in determining which local or additional state records, if any, should be checked include (1) whether they are reasonably ascertainable, (2) whether they are sufficiently useful, accurate, and complete in light of the objective of the records review (see 7.1.1), and (3) whether they are obtained, pursuant to local, good commercial or customary practice." One of the record sources listed in Section 7.2.2 is water well information. Water well information can be used to assist the environmental professional in assessing sources that may impact groundwater flow direction, and in forming an opinion about the impact of contaminant migration on nearby drinking water wells.

WELL SEARCH DISTANCE INFORMATION

DATABASE	SEARCH DISTANCE (miles)
Federal USGS	1.000
Federal FRDS PWS	Nearest PWS within 1 mile
State Database	1.000

FEDERAL USGS WELL INFORMATION

MAP ID	WELL ID	LOCATION FROM TP
No Wells Found		

FEDERAL FRDS PUBLIC WATER SUPPLY SYSTEM INFORMATION

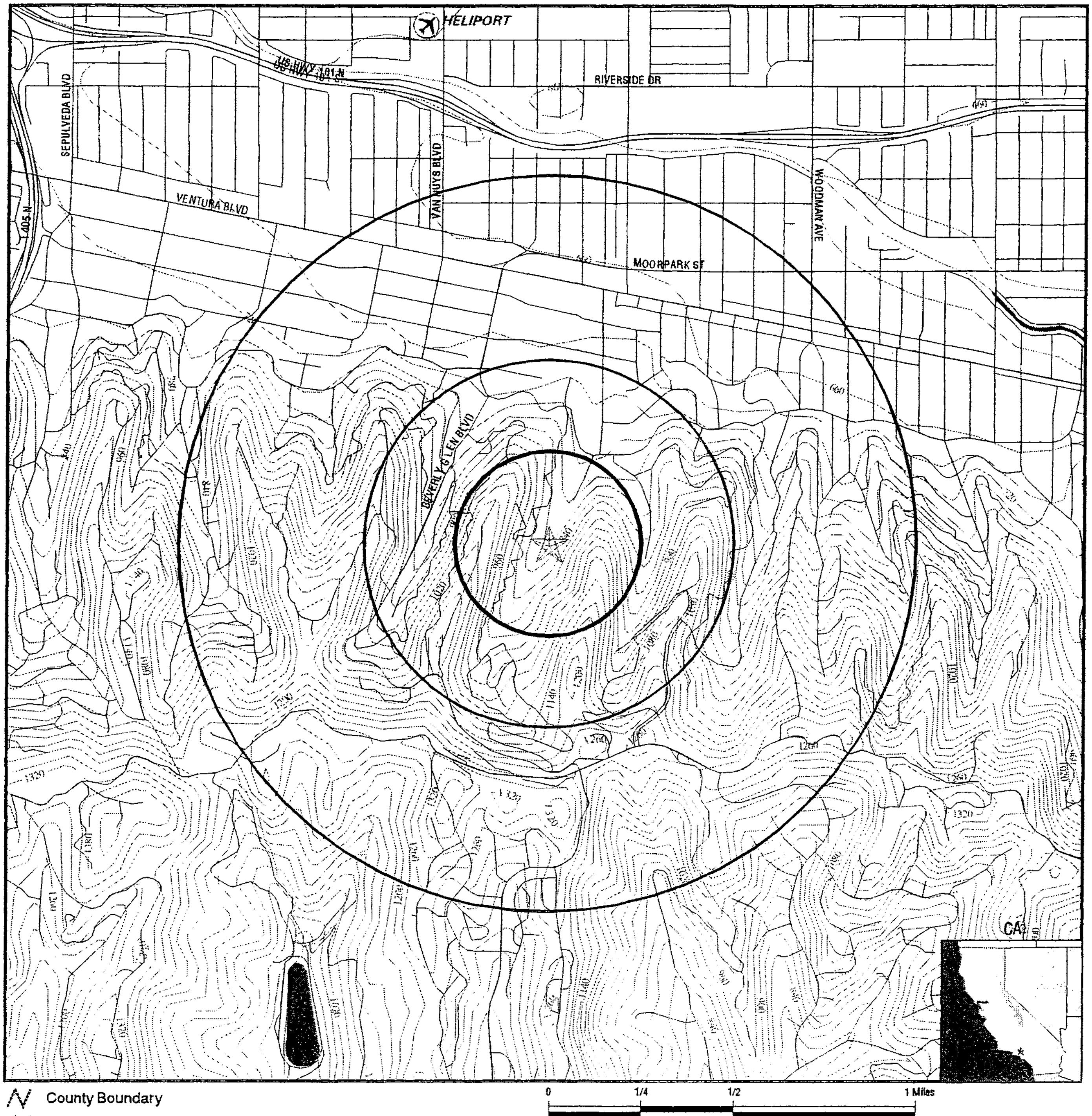
MAP ID	WELL ID	LOCATION FROM TP
No PWS System Found		

Note: PWS System location is not always the same as well location.

STATE DATABASE WELL INFORMATION

MAP ID	WELL ID	LOCATION FROM TP
No Wells Found		

PHYSICAL SETTING SOURCE MAP - 01313273.1r



County Boundary
Major Roads
Contour Lines
Earthquake Fault Lines
Airports
Earthquake epicenter, Richter 5 or greater
Water Wells
Public Water Supply Wells
Cluster of Multiple Icons

Groundwater Flow Direction
(GI) Indeterminate Groundwater Flow at Location
(GV) Groundwater Flow Varies at Location
(HD) Closest Hydrogeological Data
Oil, gas or related wells

TARGET PROPERTY:	Buckley School	CUSTOMER:	Rincon
ADDRESS:	3900 Stansbury Avenue	CONTACT:	Tricia Bartholome
CITY/STATE/ZIP:	Sherman Oaks CA 91423	INQUIRY #:	01313273.1r
LAT/LONG:	34.1396 / 118.4436	DATE:	November 23, 2004 12:39 pm

GEOCHECK® - PHYSICAL SETTING SOURCE MAP FINDINGS
RADON

AREA RADON INFORMATION

State Database: CA Radon

Radon Test Results

Zip	Total Sites	> 4 Pci/L	Pct. > 4 Pci/L
91423	102	14	13.73

Federal EPA Radon Zone for LOS ANGELES County: 2

Note: Zone 1 indoor average level > 4 pCi/L.
: Zone 2 indoor average level >= 2 pCi/L and <= 4 pCi/L.
: Zone 3 indoor average level < 2 pCi/L.

Federal Area Radon Information for Zip Code: 91423

Number of sites tested: 1

Area	Average Activity	% <4 pCi/L	% 4-20 pCi/L	% >20 pCi/L
Living Area - 1st Floor	0.500 pCi/L	100%	0%	0%
Living Area - 2nd Floor	Not Reported	Not Reported	Not Reported	Not Reported
Basement	Not Reported	Not Reported	Not Reported	Not Reported

PHYSICAL SETTING SOURCE RECORDS SEARCHED

TOPOGRAPHIC INFORMATION

USGS 7.5' Digital Elevation Model (DEM)
Source: United States Geologic Survey
EDR acquired the USGS 7.5' Digital Elevation Model in 2002. 7.5-Minute DEMs correspond to the USGS 1:24,000- and 1:25,000-scale topographic quadrangle maps.

HYDROLOGIC INFORMATION

Flood Zone Data: This data, available in select counties across the country, was obtained by EDR in 1999 from the Federal Emergency Management Agency (FEMA). Data depicts 100-year and 500-year flood zones as defined by FEMA.

NWI: National Wetlands Inventory. This data, available in select counties across the country, was obtained by EDR in 2002 from the U.S. Fish and Wildlife Service.

HYDROGEOLOGIC INFORMATION

AQUIFLOW[R] Information System
Source: EDR proprietary database of groundwater flow information
EDR has developed the AQUIFLOW Information System (AIS) to provide data on the general direction of groundwater flow at specific points. EDR has reviewed reports submitted to regulatory authorities at select sites and has extracted the date of the report, hydrogeologically determined groundwater flow direction and depth to water table information.

GEOLOGIC INFORMATION

Geologic Age and Rock Stratigraphic Unit
Source: P.G. Schruben, R.E. Arndt and W.J. Bawiec, Geology of the Conterminous U.S. at 1:2,500,000 Scale - A digital representation of the 1974 P.B. King and H.M. Beikman Map, USGS Digital Data Series DDS - 11 (1994).

STATSGO: State Soil Geographic Database
Source: Department of Agriculture, Natural Resources Conservation Services
The U.S. Department of Agriculture's (USDA) Natural Resources Conservation Service (NRCS) leads the national Conservation Soil Survey (NCSS) and is responsible for collecting, storing, maintaining and distributing soil survey information for privately owned lands in the United States. A soil map in a soil survey is a representation of soil patterns in a landscape. Soil maps for STATSGO are compiled by generalizing more detailed (SSURGO) soil survey maps.

ADDITIONAL ENVIRONMENTAL RECORD SOURCES

FEDERAL WATER WELLS

PWS: Public Water Systems
Source: EPA/Office of Drinking Water
Telephone: 202-564-3750
Public Water System data from the Federal Reporting Data System. A PWS is any water system which provides water to at least 25 people for at least 60 days annually. PWSs provide water from wells, rivers and other sources.

PWS ENF: Public Water Systems Violation and Enforcement Data
Source: EPA/Office of Drinking Water
Telephone: 202-564-3750
Violation and Enforcement data for Public Water Systems from the Safe Drinking Water Information System (SDWIS) after August 1995. Prior to August 1995, the data came from the Federal Reporting Data System (FRDS).

USGS Water Wells: USGS National Water Inventory System (NWIS)
This database contains descriptive information on sites where the USGS collects or has collected data on surface water and/or groundwater. The groundwater data includes information on wells, springs, and other sources of groundwater.

PHYSICAL SETTING SOURCE RECORDS SEARCHED

STATE RECORDS

California Drinking Water Quality Database
Source: Department of Health Services
Telephone: 916-324-2319
The database includes all drinking water compliance and special studies monitoring for the state of California since 1984. It consists of over 3,200,000 individual analyses along with well and water system information.

California Oil and Gas Well Locations for District 2, 3, 5 and 6
Source: Department of Conservation
Telephone: 916-323-1779

RADON

State Database: CA Radon
Source: Department of Health Services
Telephone: 916-324-2208
Radon Database for California

Area Radon Information
Source: USGS
Telephone: 703-356-4020
The National Radon Database has been developed by the U.S. Environmental Protection Agency (USEPA) and is a compilation of the EPA/State Residential Radon Survey and the National Residential Radon Survey. The study covers the years 1986 - 1992. Where necessary data has been supplemented by information collected at private sources such as universities and research institutions.

EPA Radon Zones
Source: EPA
Telephone: 703-356-4020
Sections 307 & 309 of IRAA directed EPA to list and identify areas of U.S. with the potential for elevated indoor radon levels.

OTHER

Airport Landing Facilities: Private and public use landing facilities
Source: Federal Aviation Administration, 800-457-6656

Epicenters: World earthquake epicenters, Richter 5 or greater
Source: Department of Commerce, National Oceanic and Atmospheric Administration

California Earthquake Fault Lines: The fault lines displayed on EDR's Topographic map are digitized quaternary fault lines, prepared in 1975 by the United State Geological Survey. Additional information (also from 1975) regarding activity at specific fault lines comes from California's Preliminary Fault Activity Map prepared by the California Division of Mines and Geology.

Appendix 2

Agency File Review Records

LAFD Files

1. SUMMARY OF SOIL GAS ANALYSIS

1.1 **Date**: August 11, 1988 1.2 **Project No.**: 33501

1.3 **Job Location**:

3900 Stansbury Road, Sherman Oaks, California

1.4 **Current Status of the Job Site**:

A. Currently operating school and related facilities.

B. One 10,000 gallon gasoline tank removed in July 1988.

C. High concentration of hydrocarbons found at the bottom of tank excavation.

1.5 **Reason for Conducting Soil Gas Analysis**:

Preliminary investigation of subsurface soil contamination.

1.6 **Detector Unit Used**: Photovac TIP II

Photoionization Detector With Detection Limit of 50 ppb (for Benzene) and a Performance Range of Up to 2,000 ppm

1.7 **Total No. of Vapor Concentration Readings**: 29

1.8 **Summary of Results**:

Soil gas analysis detected a localized area of potential subsurface contamination near the tank excavation. The soil gas survey did not detect extensive contamination, but the high level of contamination found at the north end of the tank excavation and the hydrocarbon odors detected in the ground water being pumped from the sump beneath the Pavilion building strongly suggests that fuel from the tank and/or piping has migrated downward to the underlying ground water table.

2. TESTING PROCEDURE AND METHODOLOGY

At the site, half-inch diameter boreholes were established throughout the area by drilling through the overlying pavement to a depth of one (1) to one and a half (1.5) feet. However, somewhat more emphasis was placed on certain locations where leakage typically occurs (e.g., around the tank and piping excavation). Boreholes located in areas other than these strategic points were established to detect possible or unexpected subsurface pollution owing to the migration of released fuel, or organic vapor, and to obtain representative background values for comparison purposes.

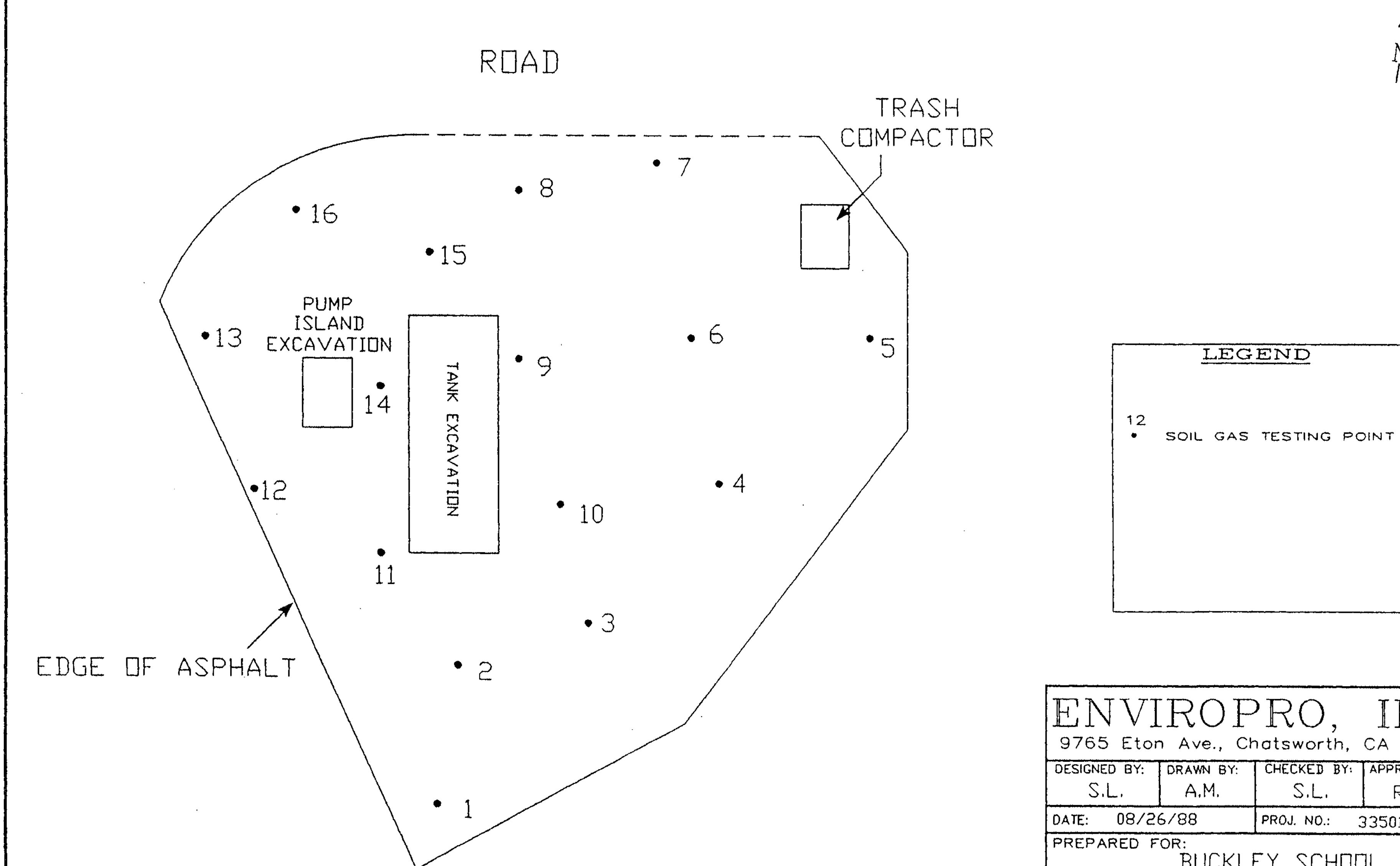
After each boring was drilled, a thin plastic film was placed over each hole to allow vapors to diffuse into and equilibrate within each borehole. After drilling was completed, vapor samples were withdrawn from each borehole in the same order as they were drilled. All samples were obtained by carefully penetrating the plastic film with the detector's sampling probe.

The sensing instrument used in this project is a photoionization detector manufactured by Photovac, Inc. (Photovac TIP II). This unit has a detection limit of 50 ppb (for benzene) and a performance range of up to 2,000 ppm for total ionizable hydrocarbons at 10.6 eV. As recommended by the manufacturer, the span control adjusted to give the Photovac TIP II a mid-range sensitivity. The calibration of Photovac TIP II, and the calculation of approximate actual vapor concentration based on the field Photovac readings, are discussed in Appendix A. The TIP II reading was adjusted to zero with respect to ambient air before taking vapor readings from each borehole.

It is important to recognize that the "soil gas" technique applied here is not a direct measurement of soil and ground water pollution. These results should be used qualitatively to show probable contamination and tendencies of possible leakage and subsurface migration. In addition, they will be useful in the planning of subsequent detailed remedial investigation, which will include soil borings and direct soil sampling at several locations and depths, and chemical analysis of soil and ground water samples. Final decisions should be based on a complete remedial investigation, which will delineate more accurately the nature and extent of subsurface contamination.

3. DISCUSSION OF RESULTS

A total of 29 boreholes were drilled at the site for the soil gas investigation. Drawing 1T shows the locations of the 16 boreholes drilled around the tank excavation area; Drawing 1P shows the locations of the 13 boreholes around the Pavilion (gym). Table 1 and Drawings 2T and 2P present the soil gas sampling data for these areas. Drawings 3T and 3P are the contour maps generated on the basis of field TIP II readings.



ENVIROPRO, INC.

9765 Eton Ave., Chatsworth, CA 91311

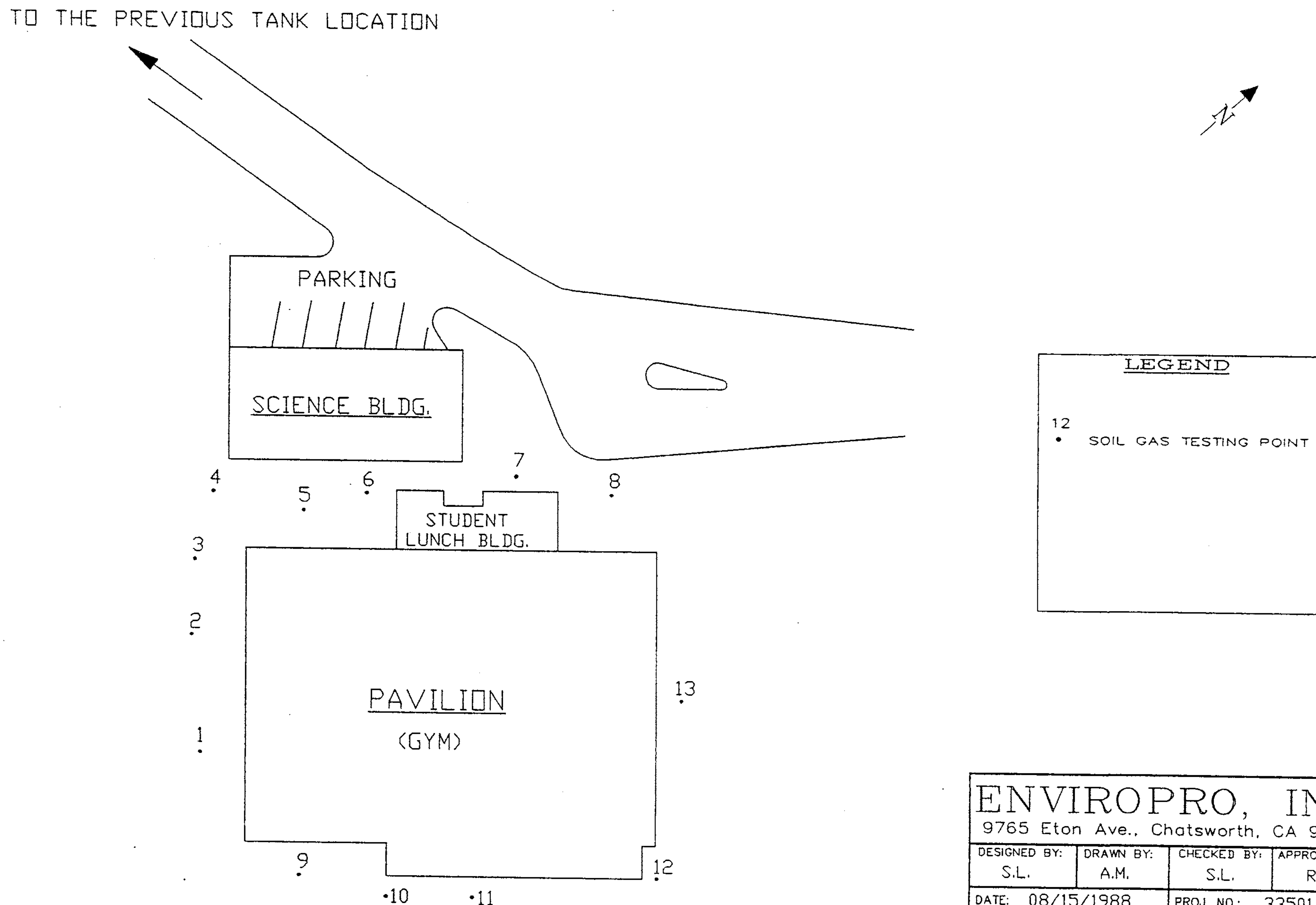
DESIGNED BY:	DRAWN BY:	CHECKED BY:	APPROVED BY:
S.L.	A.M.	S.L.	R.W.
DATE: 08/26/88		PROJ. NO.: 33501	

PREPARED FOR:
BUCKLEY SCHOOL

JOB LOCATION:
3900 STANSBURY AV. SHERMAN OAKS CA. 91423

SITE PLOT PLAN

DRAWING NO. 1T



ENVIROPRO, INC.

9765 Eton Ave., Chatsworth, CA 91311

DESIGNED BY:	DRAWN BY:	CHECKED BY:	APPROVED BY:
S.L.	A.M.	S.L.	R.W.

DATE: 08/15/1988 | PROJ. NO.: 33501

PREPARED FOR: BUCKLEY SCHOOL

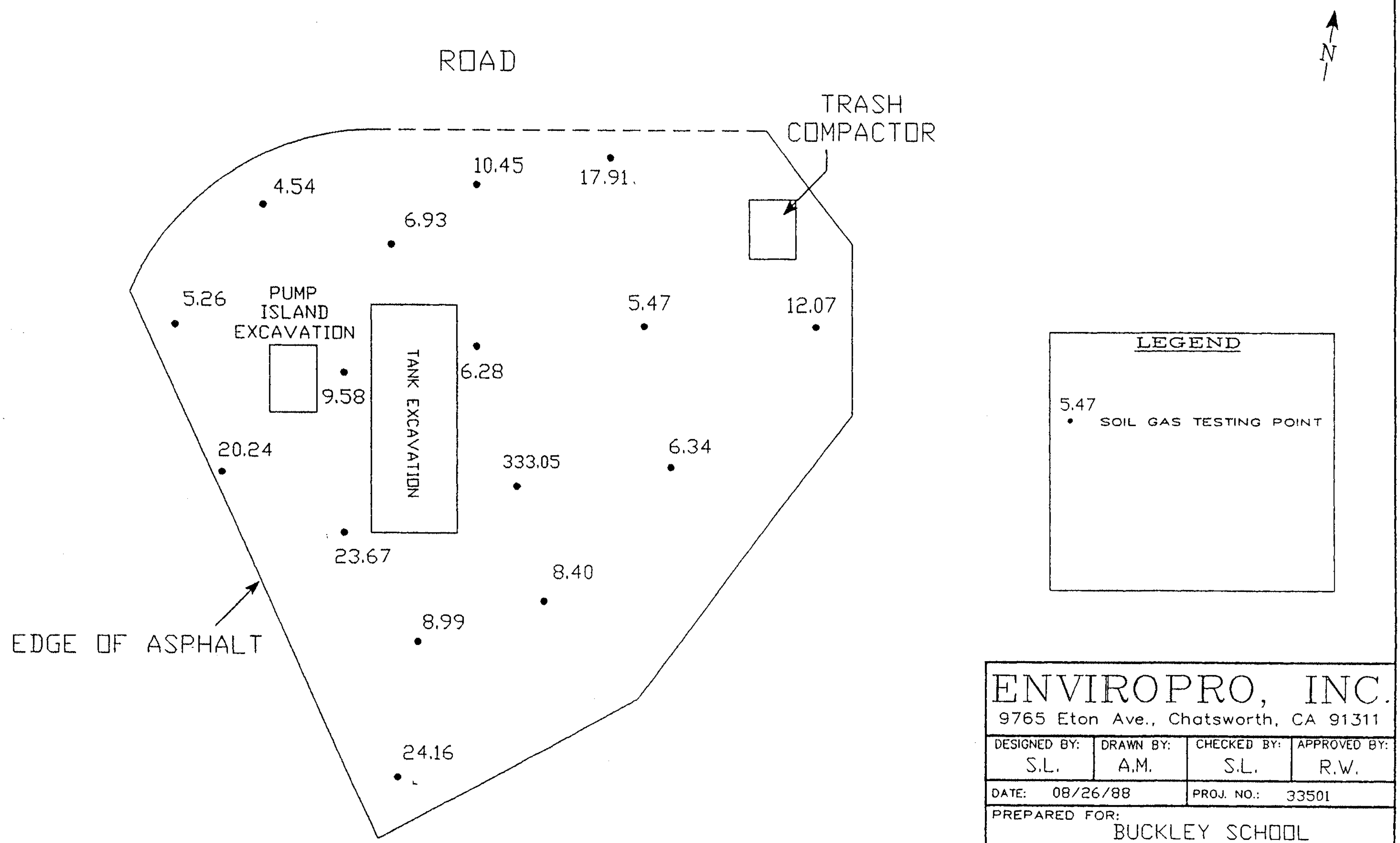
JOB LOCATION: 3900 STANSBURY AV. SHERMAN OAKS CA. 91423

SITE PLOT PLAN | DRAWING NO. 1P

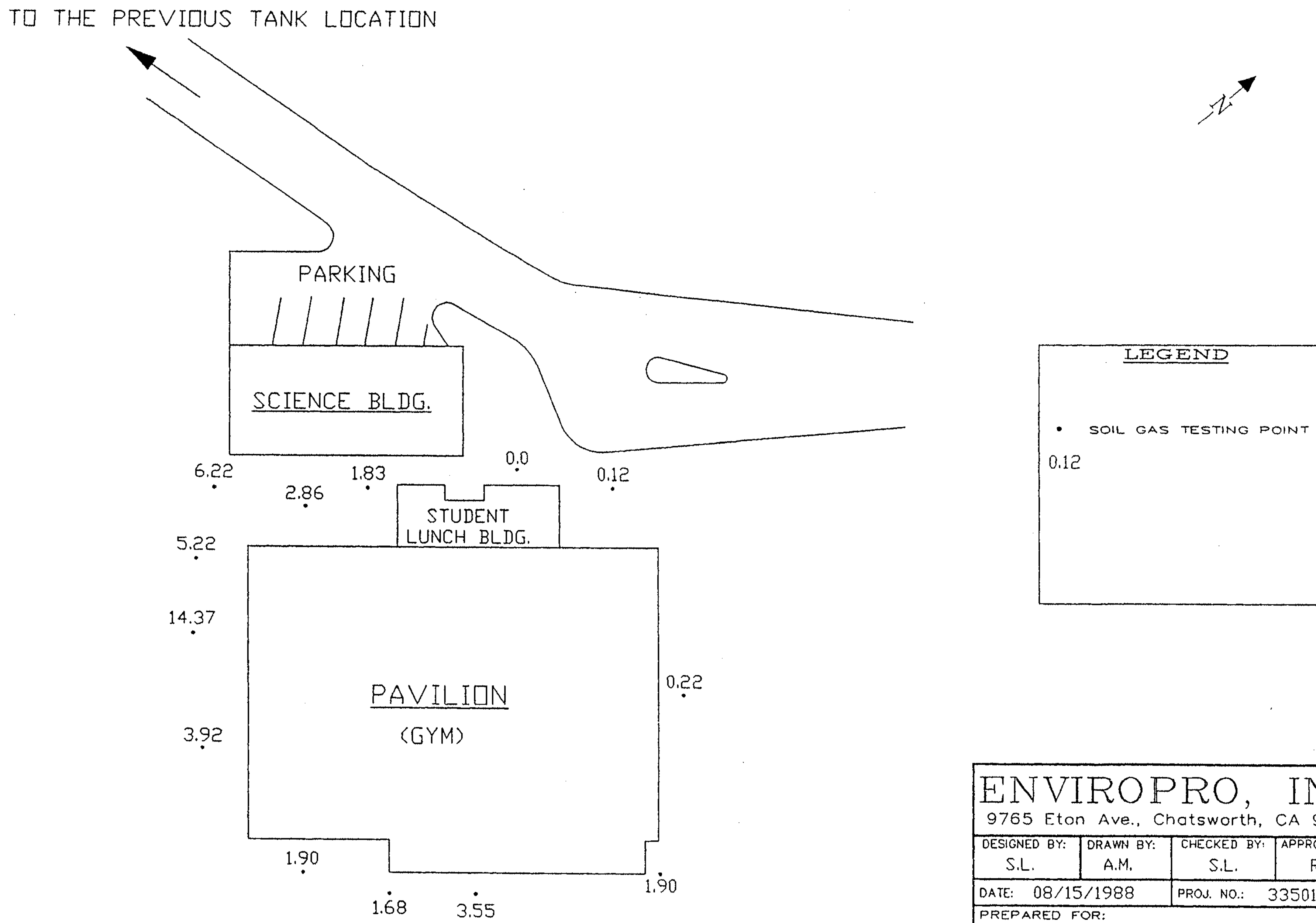
TABLE 1
Soil Gas Sampling Data
Buckley School

Project No.:	33501
Job Location:	3900 Stansbury Road, Sherman Oaks, CA
Detector Unit:	Photovac TIP II
Date of Sampling:	August 11, 1988
PID Span Setting:	1.0

Boring No.	Field PID Reading	Approximate Isobutylene Equivalent Conc. (ppm)
Pavilion Area		
P-1	12.6	3.92
P-2	46.2	14.37
P-3	3.0	0.89
P-4	20.0	6.22
P-5	9.2	2.86
P-6	5.9	1.83
P-7	0.0	0.00
P-8	0.4	0.12
P-9	6.1	1.90
P-10	5.4	1.68
P-11	11.4	3.55
P-12	6.1	1.90
P-13	0.7	0.22
Tank Excavation Area		
T-1	77.7	24.16
T-2	28.9	8.99
T-3	27.0	8.40
T-4	20.4	6.34
T-5	38.8	12.07
T-6	17.6	5.47
T-7	57.6	17.91
T-8	33.6	10.45
T-9	20.2	6.28
T-10	1071.0	333.05
T-11	76.1	23.67
T-12	65.1	20.24
T-13	16.9	5.26
T-14	30.8	9.58
T-15	22.3	6.93
T-16	14.6	4.54



ENVIROPRO, INC. 9765 Eton Ave., Chatsworth, CA 91311			
DESIGNED BY: S.L.	DRAWN BY: A.M.	CHECKED BY: S.L.	APPROVED BY: R.W.
DATE: 08/26/88		PROJ. NO.: 33501	
PREPARED FOR: BUCKLEY SCHOOL			
JOB LOCATION: 3900 STANSBURY AV. SHERMAN OAKS CA. 91423			
SOIL GAS PID READINGS			DRAWING NO. 2T



ENVIROPRO, INC.
9765 Eton Ave., Chatsworth, CA 91311

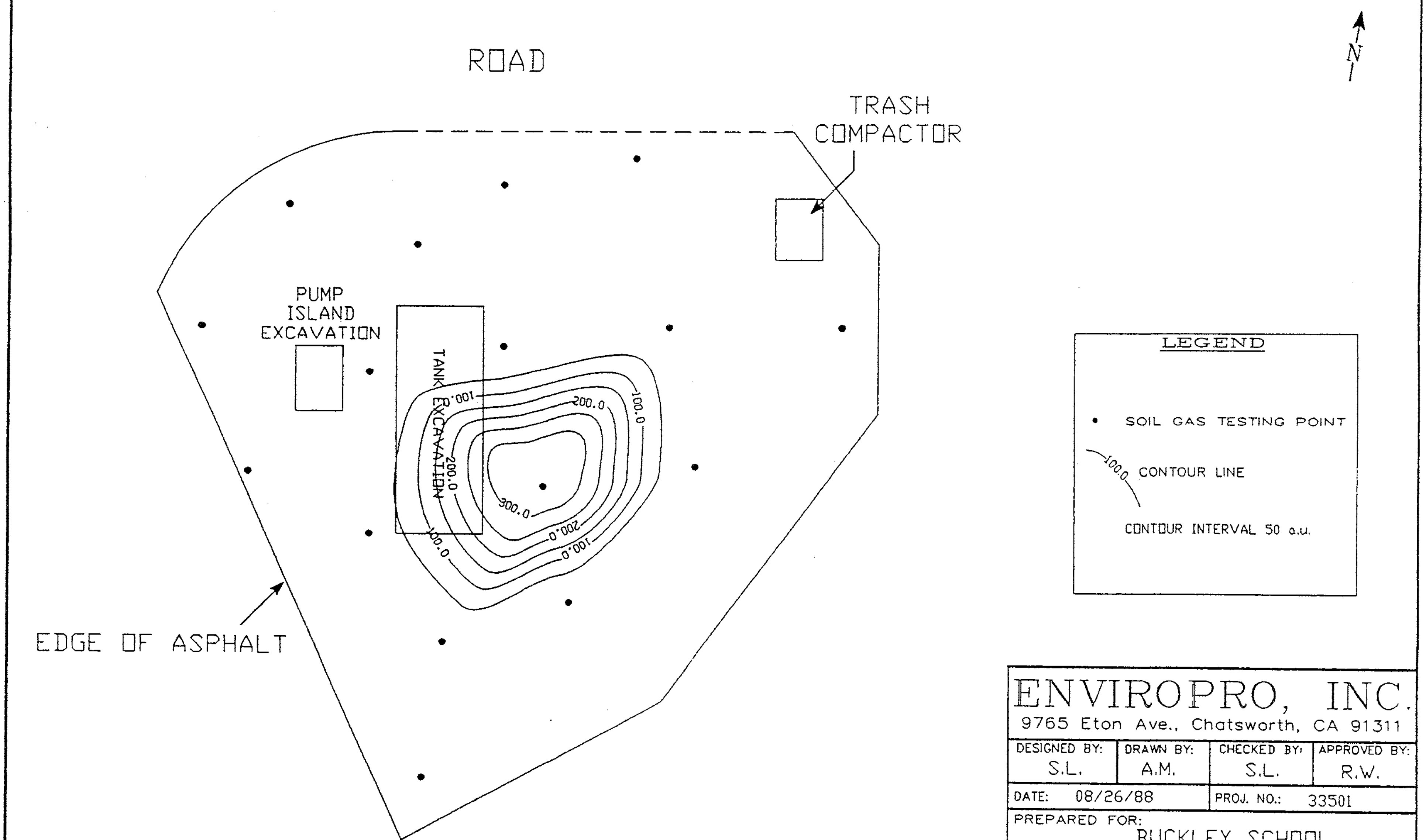
DESIGNED BY:	DRAWN BY:	CHECKED BY:	APPROVED BY:
S.L.	A.M.	S.L.	R.W.

DATE: 08/15/1988 PROJ. NO.: 33501

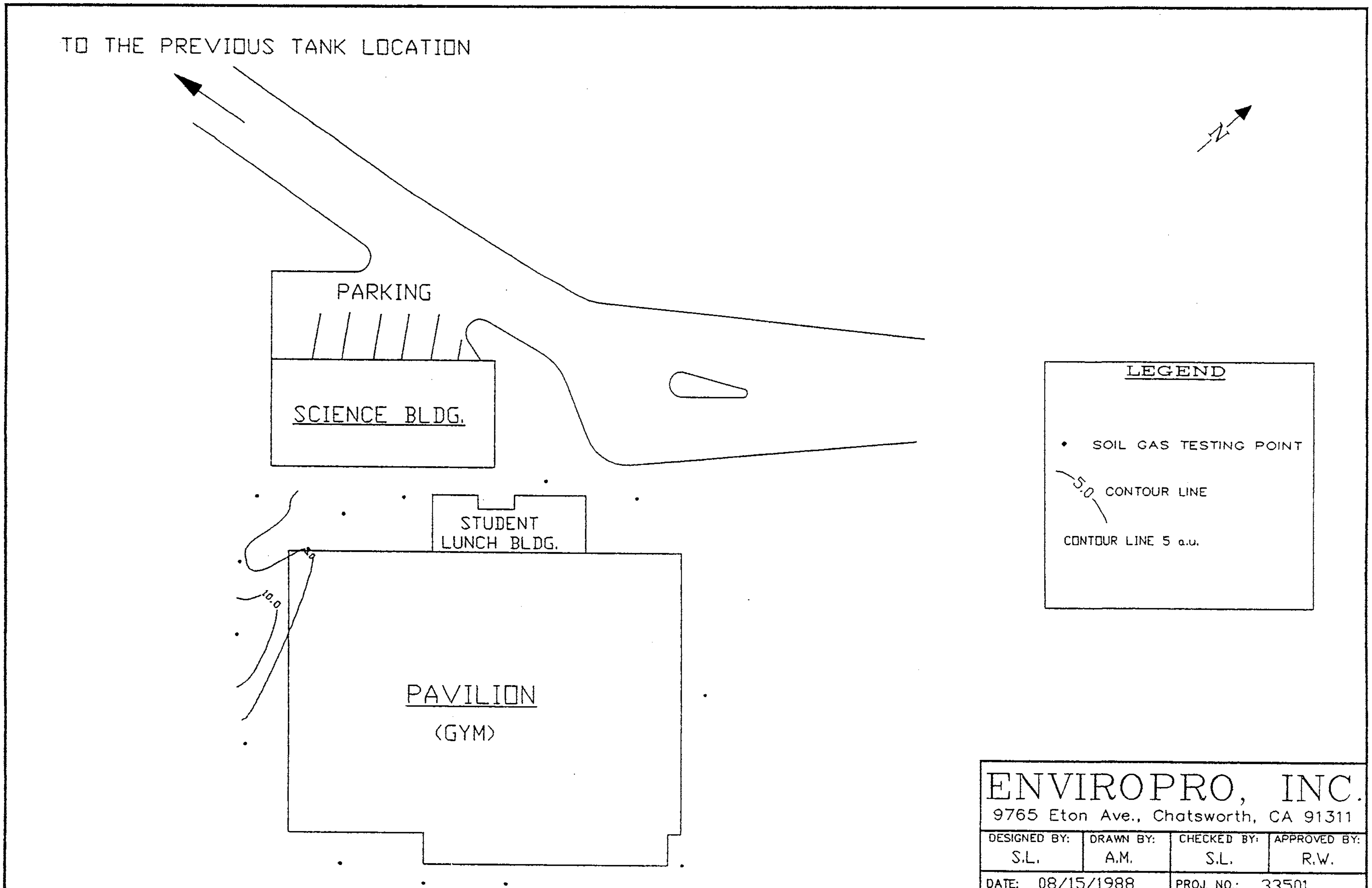
PREPARED FOR: BUCKLEY SCHOOL

JOB LOCATION: 3900 STANSBURY AV. SHERMAN OAKS CA. 91423

SOIL GAS PID READINGS DRAWING NO. 2P



ENVIROPRO, INC. 9765 Eton Ave., Chatsworth, CA 91311			
DESIGNED BY: S.L.	DRAWN BY: A.M.	CHECKED BY: S.L.	APPROVED BY: R.W.
DATE: 08/26/88		PROJ. NO.: 33501	
PREPARED FOR: BUCKLEY SCHOOL			
JOB LOCATION: 3900 STANSBURY AV. SHERMAN OAKS CA. 91423			
CONTOUR MAP OF SOIL GAS READINGS			DRAWING NO. 3T



ENVIROPRO, INC.
9765 Eton Ave., Chatsworth, CA 91311

DESIGNED BY:	DRAWN BY:	CHECKED BY:	APPROVED BY:
S.L.	A.M.	S.L.	R.W.

DATE: 08/15/1988 PROJ. NO.: 33501

PREPARED FOR: BUCKLEY SCHOOL

JOB LOCATION: 3900 STANSBURY AV. SHERMAN OAKS CA. 91423

CONTOUR MAP OF SOIL GAS READINGS

DRAWING NO. 3P

The area between the parking lot where the tank was located (Drawing 3T) and the Pavilion building (Drawing 3P) is a steep hillside, dropping roughly 40 feet in elevation in a lateral distance of 150 feet.

The soil gas survey was proposed as an initial investigation of hydrocarbon contamination discovered in the tank excavation as well as in the ground water being pumped from a sump near the swimming pool located on the lower basement floor of the Pavilion building. Based on pumping records, the ground water level is approximately 35 feet below the ground surface at this building. The pumping is used to keep the buoyant force of the water from structurally damaging the pool by depressing the water table at that location. The water level is depressed at least 8-10 feet at that location due to this activity. This water level drawdown and the resulting cone of depression in the water surface may be locally altering the ground water flow direction and effectively drawing contaminated water from the area beneath the tank excavation.

At the tank excavation area, background vapor readings were in the approximate range of 4 to 10 ppm. A single highly elevated reading of 333 ppm was obtained from Boring T-10 close to the tank excavation. Borings T-1, T-5, T-7, T-11, and T-12 registered slightly elevated readings of 10 to 25 ppm. (See Drawings No. 1T and 2T.)

At the Pavilion building, all soil gas borings registered generally low readings, with Borings T-2, T-3, and T-4 at the west corner of the building registering readings of 14.4 ppm, 5.2 ppm, and 6.22 ppm respectively, which may be slightly above background levels. (See Drawings No. 1P and 2P.)

Although the soil gas survey did not detect extensive contamination, the high level of contamination found at the north end of the tank excavation and the hydrocarbon odors detected in the ground water being pumped from the sump beneath the Pavilion building strongly suggest that fuel from the tank and/or piping has migrated downward to the underlying ground water. Based on the depth to water beneath the Pavilion building, the depth to ground water from the tank area and hence the possible vertical extent of soil contamination is estimated to be 60 to 90 feet.

The single highly elevated reading near the tank excavation (Boring T-14) combined with the lower vapor readings obtained in that same area, suggest that the lateral extent of soil contamination <u>may</u> be limited. However, because of the shallow borings used for soil gas surveys, the permeability of the underlying soils can strongly affect the vapor readings by influencing the upward migration of volatile gases.

A foundation investigation conducted by Converse, Davis and Associates (Appendix B) indicates layers of silts and clayey silts beneath the area of the Science and Pavilion buildings. These layers may be impeding the upward migration of the vapors from the ground water beneath the Pavilion building, which is known to be contaminated. The low vapor readings collected at the west corner of the Pavilion building may be due to contamination migrating via the ground water table from the tank excavation area. Further investigation will be required to determine the nature and extent of the subsurface contamination at this facility. The following section describes the proposed investigative site assessment work.

4. PROPOSAL FOR FURTHER INVESTIGATION

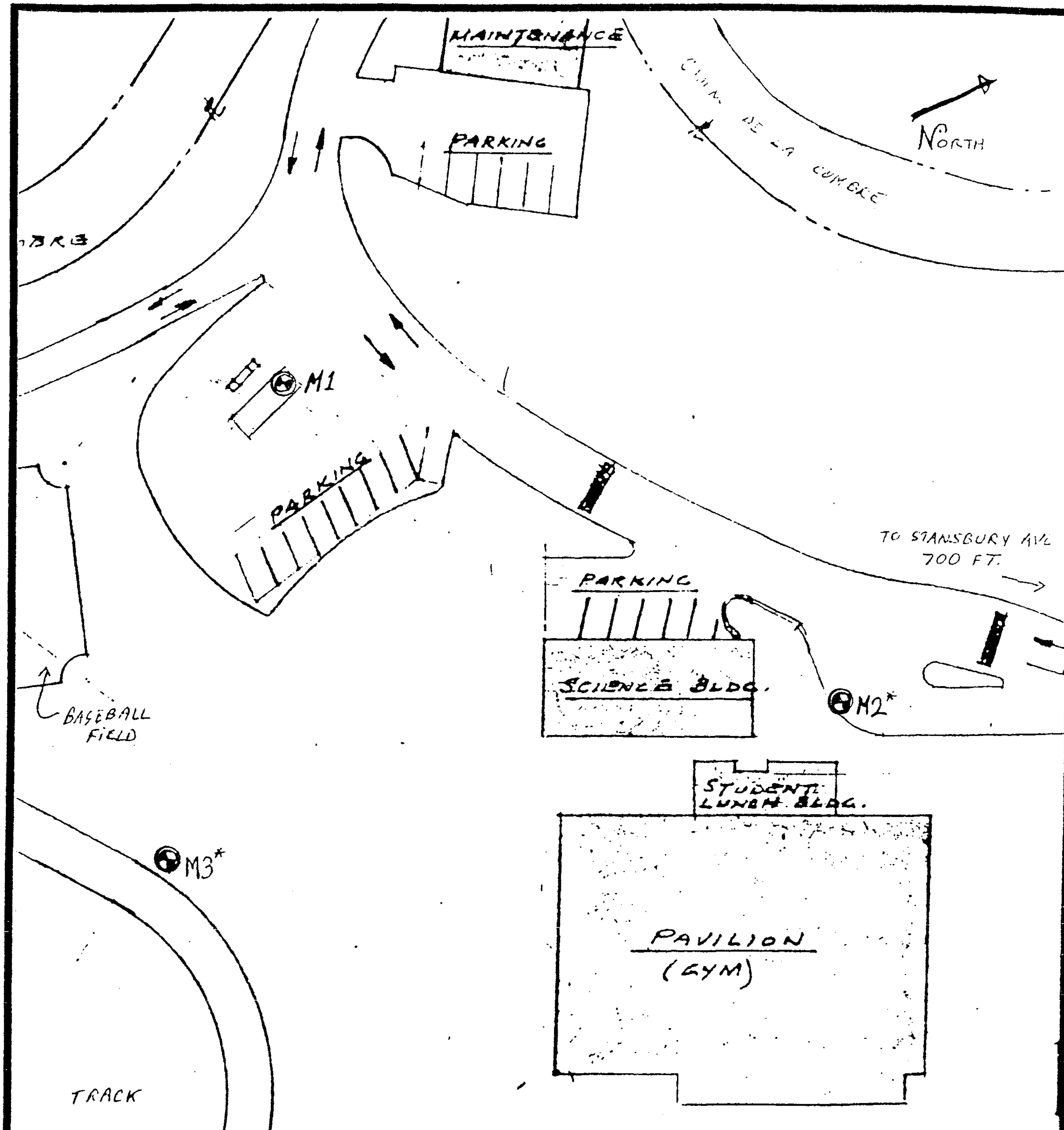
4.1 Introduction

The objective of the proposed work is to investigate and further identify the extent of subsurface soil and ground water contamination previously identified at the site. The work proposed is designed to satisfy Los Angeles City Fire Department requirements for an initial site assessment.

4.2 Monitoring Well Location and Drilling

Three ground water wells (M1, M2, and M3) are proposed for installation at locations shown on Drawing 4. Well M1 will be drilled near the north end of the tank excavation where the previous chemical analysis following tank removal showed the highest concentration of contaminants. (See Table 2.) Well M2 will be located near the perimeter of the Pavilion building, where hydrocarbon odors had been detected in the ground water being pumped. Well M3 will be positioned appropriately to allow a determination of the ground water direction and further define the extent of possible ground water contamination.

A review of the foundation investigation conducted by Converse, Davis & Associates (Appendix B) indicates that bedrock may be encountered during this work. The site also has steep, possibly unstable hillsides and limited access to suitable drilling areas. For these reasons, the most



KEY

PROPOSED WELL LOCATION.

* exact locations to be determined later.

ENVIROPRO, INC
9765 ETON AVE., CHATSWORTH, CA 91311

SCALE: 1" = 50'	APPROVED BY: RW	DRAWN BY: /L
DATE: 10-24-88		
THE BUCKLEY SCHOOL 3700 STANSBURY AVE, SHERMAN OAKS, CA		
PROPOSED WELL LOCATIONS		DRAWING NUMBER 4

appropriate drilling technique and exact well placement will be determined after further review of the conditions at the site.

TABLE 2

Results of Chemical Analysis on Soil Samples Taken During Tank Removal (July 1988)

Sample No.	Depth	Test	Analytical Results
1*	14' B.G. 2' B.I.	8015 M	46,600 mg/kg
2*	14' B.G. 2' B.I.	8015 M	144 mg/kg

B. G. = Below Grade
B. I. = Below Invert

* Sample #1 taken from north end of tank excavation.
Sample #2 taken from south end of tank excavation.

4.3 Soil Sampling Procedures

Soil samples will be obtained during the drilling operation with a split spoon sampler and a standard 140 pound hammer using a 30-inch drop. After each soil sample is obtained the sampler and liner tubes will be cleaned using high pressure steam at 300° F to eliminate the possibility of cross-contamination between samping intervals. After each borehole is drilled, all augers, samplers and liner tubes will be steam cleaned as described above to prevent cross-contamination between borings.

At each prescribed sampling depth, soil samples will be collected in the liner tubes of the split spoon sampler. The sample in the lower liner at each depth will be retained for possible chemical analysis. All soil samples designated for chemical analysis will be kept inside the stainless steel sampling tubes during retrieval. The tubes will be tightly wrapped in aluminum foil, capped and placed inside a ziplock plastic bag. A soil sampling label will be placed on the outside of each bag and the bagged samples with labels will be placed inside a second ziplock plastic bag.

The soil from the remaining upper sample liner tubes will be used for on-site geological classification and organic vapor testing using a Photovac TIP II photoionization detector (PID). The soil will be placed into a ziplock bag and sealed. The soil will be kneaded inside the bag to allow potential vapors to collect in the headspace above the soil. The bagged sample will be kept sealed for five (5) minutes prior to testing. Testing will be accomplished by carefully inserting the sampling probe of the TIP II into the sealed bag. The highest reading obtained will then be noted onto the field boring log. Field PID readings will be obtained at every sampling depth and will be included on the final test boring logs in the final report. Sampling will be conducted at depths of 5, 10, 15, 20, 25, and 30 feet and at 10 foot intervals thereafter until ground water is reached during the well drilling.

It is estimated that 4-5 soil samples obtained during the drilling of M1 (near the tank excavation) will be selected for chemical analysis. This is based upon an estimated ground water depth of 70 feet. The field PID readings obtained will be used to aid in the selection of the most appropriate samples for analysis. Because of the lateral distance of wells M2 and M3 from the previous tank location, analysis of water samples only is proposed unless field PID readings from these borings indicate that soil contamination is present.

All prepared soil and water samples (see section 4) will be immediately placed on ice inside a styrofoam cooler and stored in a refrigerated state for delivery to American Analytics of Chatsworth, California, a California State DOHS certified laboratory, for chemical analysis. All drilling cuttings will be retained on-site until the laboratory analysis work has been completed.

4.4 Monitoring Well Construction

Prior to the drilling for the monitoring wells, well permits will be obtained from the Los Angeles County Department of Health Services, Environmental Management Section.

Based on the field observation of water levels in the sump beneath the Pavilion building, ground water appears to exist at a depth of 30 to 80 feet below the ground surface, depending on the elevation of the well locations (the previous tank area is about 40 feet higher than the Pavilion area). Based upon this depth, soil borings will have to be drilled to a depth of about 40-100 feet to provide for a 10-20 foot deep well screen below the water surface.

If a competent clay layer is encountered (minimum five (5) feet thick) below ground water, drilling will be stopped and the existing borehole will be converted to a ground water monitoring well using the following construction mterials and procedures.

A 4-inch diameter slotted schedule 40 PVC casing with a bottom cap will be installed from the bottom of the borehole to a depth at least 5 feet above the saturated zone. A blank 4-inch casing shall be extended from the upper end of the slotted casing to 4 inches below grade level.

The annular space around the casings will be backfilled with a filter pack of No. 3 Monterey Sand. The filter pack will extend from the well bottom to a distance of 3 feet above the uppermost slots. A 2-foot bentonite seal will be installed above the gravel pack followed by an annular seal of cement grout to fill the remaining annular region.

A watertight, lockable well cover will be installed to protect the wellhead and will be clearly marked with the well identificationn number. The well will be described by well identification number, depth of well and the depths of the perforated interval.

After the construction of each well is complete, well development will be performed to remove sediment collected in the well from the drilling operation. A minimum of eight (8) well volumes will be removed using a Q.E.D. systems ejection pump. The ground water removed will be stored in DOT-approved 55-gallon drums on-site until laboratory analysis of the ground water samples is complete.

Ground water samples will be collected using a clean (previously steam cleaned) teflon bailer. Samples will be put into appropriately sized (per EPA protocol) glass bottles equipped with teflon-lined lids. Each bottle will be filled with the water samples such that all headspace is eliminated.

4.5 Methods of Chemical Analysis

Outlined below in Table 2.4.1 are the methods of chemical analysis that will be performed on the collected ground water and soil samples.

TABLE 2.4.1

EPA Test Methods for Soil and Ground Water Analysis at Buckley School

Sample Type	Locations	Test Method
Water	M1,M2&M3	EPA 602 for Volatile Organics, EPA 8015 for Total Petroleum Hydrocarbons
Soil	M1,M2*,M3*	EPA 8015 Modified for Total Petroleum Hydrocarbons, EPA 8020 for Aromatic Volatile Organics

* A limited number of soil samples will be analyzed based on field PID readings.

4.6 Ground Water Gradient

The existing ground water gradient beneath the site will be determined by measuring the distances from the top of each well casing to the surface of the water table. An arbitrary reference elevation will be established at the site in the vicinity of the wells. The elevation difference between the top of each well casing and the reference elevation will be added to the distance measured from the top of the well casings to the water table.

The distances from the reference elevation to the water table will determine the slope of the water surface and thus the ground water flow direction. Conventional surveying equipment capable of measuring to the nearest 1/10 of an inch will be used to obtain the necessary elevation differences.

5. FINAL REPORT

Upon approval of this work plan, Enviropro, Inc. will implement the work discussed herein. After completion of the field work and receipt of the laboratory analysis, a final report will be prepared for the Los Angeles City Fire Department that will contain the following data/information.

5.1 A plot plan showing final well locations and description of the drilling technique(s) used.

5.2 Chemical analysis results for the three (3) ground water wells M1, M2, and M3 and for at least two (2) soil samples obtained from the drilling of M1.

5.3 Soil boring logs signed by a California Registered Engineering Geologist for each well drilled.

5.4 All field data collected during soil sample collection.

5.5 Ground water monitoring well completion diagrams.

5.6 Ground water monitoring well surveying data and estimate of ground water flow direction.

5.7 Well development information.

5.8 Conclusions and recommendations for further study or remedial action (if necessary).

RWQCB Files

 Pcm 5 PETE WILSON, *Governor*

CALIFORNIA REGIONAL WATER QUALITY CONTROL BOARD
LOS ANGELES REGION
101 CENTRE PLAZA DRIVE
MONTEREY PARK, CA 91754-2156
(213) 266-7500
FAX: (213) 266-7600

July 22, 1996 O/C

RECEIVED
JUL 30 1996
UNDERGROUND TANK

Mr. Walter Baumhoff
Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA 91423

UNDERGROUND STORAGE TANK CASE CLOSURE
BUCKLEY SCHOOL
3900 STANSBURY AVENUE, SHERMAN OAKS (ID #916061598)

Dear Mr. Baumhoff

This letter confirms the completion of the site investigation and remedial action for the underground storage tank(s) formerly located at the above-described location.

Based on the available information and with the provision that the information provided to this agency was accurate and representative of site conditions, no further action related to the underground storage tank release is required.

This notice is issued pursuant to a regulation contained in Title 23, California Code of Regulations, Division 3, Chapter 16, Section 2721(e).

Please contact our office if you have any questions regarding this matter.

Sincerely,

ROBERT P. GHIRELLI, D. Env.
Executive Officer

DAVE DEANER
Acting Assistant Executive Officer
Underground Tanks

cc: Mr. Allan Patton, State Water Resources Control Board, Underground Storage Tank Program
Captain Jesse Pasos, Los Angeles City Fire Department, Underground Tanks

BUCKLEY SCHOOL 111 1705C

88 01589 CM

STATE OF CALIFORNIA
HAZARDOUS SUBSTANCE SPILL REPORT

DTG 1627 27 May 88

COUNTY LA

NOTIFIED OES #29, LA City Fire Dept PHONE 213 485-6185

REPORTED BY ______ PHONE ______

SUBSTANCE gasoline QTY unknown

SPILL SITE: P/L __ SHP __ RD __ O/F __ REF __ R/R __ S/S __ IND PLT __ DTG OCC (FND) 0952

LOCATION 3900 Standbury Van Nuys (private school)

WHAT HAPPENED underground storage tank leaking into swimming pool & school grounds sump pump pumping the fuel into a drainage

CONTAINMENT/CLEANUP/WATER INVOLVED ditch which flows to the LA River ... clean up unknown at this time

LCL AGENCIES ON SCENE (NTFD) FD ✓ SO __ PD __ CO DOH/HW ✓ CO OES __ AIR/Q __ NRC __

FD ntfd Harbor Dept

REC'D BY Carolyn

NOTIFIED	NAME	TIME						
DFG	r/p Untfd		FED R/R			CC CO OES		
RWQCB			CHP			FRESNO CO		
EPA	Cindy	1137	CALTRANS			HUMBOLDT CO		
SFM P/L			F & A			LA CO F/C	r/p Untfd	
DOG			CDF			SBDO CO		
USCG			DPR			SF F/D		
LANDS			USFWS			SOLANO CO		
DOH/ST			E B PARKS			VENTURA CO		
DOH/CO			UC S BARB			FEMA 9		

OES 27 (1/88)

RI 19050   UNA VAC, Ly

UNDERGROUND STORAGE TANK UNAUTHORIZED RELEASE (LEAK) / CONTAMINATION SITE REPORT

EMERGENCY: [ ] YES [X] NO

HAS STATE OFFICE OF EMERGENCY SERVICES REPORT BEEN FILED? [ ] YES [ ] NO

FOR LOCAL AGENCY USE ONLY
I HEREBY CERTIFY THAT I AM A DESIGNATED GOVERNMENT EMPLOYEE AND THAT I HAVE REPORTED THIS INFORMATION TO LOCAL OFFICIALS PURSUANT TO SECTION 25180.7 OF THE HEALTH AND SAFTY CODE.

SIGNED: ____ DATE: ____

REPORT DATE: 0 6 0 2 8 8 (M M D D Y Y)

CASE #:

REPORTED BY

NAME OF INDIVIDUAL FILING REPORT: Andrew M Gutierrez

PHONE: (818) 989 8561

SIGNATURE: Andrew M Gutierrez

REPRESENTING: [ ] OWNER/OPERATOR [ ] REGIONAL BOARD [X] LOCAL AGENCY [ ] OTHER

COMPANY OR AGENCY NAME: L.A. City Fire Dept.

ADDRESS: 200 N Main St (STREET) L.A (CITY) CA (STATE) 90012 (ZIP)

RESPONSIBLE PARTY

NAME: Buckley School [ ] UNKNOWN

CONTACT PERSON: Walter Baumhoff

PHONE: 783-1610

ADDRESS: 3900 Stansbury Ave (STREET) Sherman Oaks (CITY) Cal (STATE) 91616 (ZIP)

SITE LOCATION

FACILITY NAME (IF APPLICABLE): Same as above

OPERATOR:

PHONE: ( )

ADDRESS: STREET / CITY / COUNTY / ZIP

CROSS STREET:

TYPE OF AREA: [ ] COMMERCIAL [ ] INDUSTRIAL [ ] RURAL [X] RESIDENTIAL [ ] OTHER

TYPE OF BUSINESS: [ ] RETAIL FUEL STATION [ ] FARM [ ] OTHER school

IMPLEMENTING AGENCIES

LOCAL AGENCY: Los Angeles Fire Dept

AGENCY NAME: Fire Prevention Bureau

CONTACT PERSON: Andrew M Gutierrez

PHONE: (818) 989-8561

REGIONAL BOARD: State Water Resources

CONTACT: Josh Workman

PHONE: (213) 620-5662

SUBSTANCES INVOLVED

(1) NAME: Gasoline — QUANTITY LOST (GALLONS): [X] UNKNOWN

(2) NAME: — QUANTITY LOST (GALLONS): [ ] UNKNOWN

DISCOVERY/ABATEMENT

DATE DISCOVERED: 0 5 2 7 8 8 (M M D D Y Y)

HOW DISCOVERED: [ ] INVENTORY CONTROL [ ] SUBSURFACE MONITORING [X] NUISANCE CONDITIONS [X] TANK TEST [ ] TANK REMOVAL [ ] OTHER

DATE DISCHARGE BEGAN: ~~0 5 2 7 8 8~~ [X] UNKNOWN

METHOD USED TO STOP DISCHARGE (CHECK ALL THAT APPLY): [X] REMOVE CONTENTS [ ] REPLACE TANK [ ] CLOSE TANK [ ] REPAIR TANK [ ] REPAIR PIPING [ ] CHANGE PROCEDURE [ ] OTHER

HAS DISCHARGE BEEN STOPPED? [X] YES [ ] NO IF YES, DATE M M D D Y Y

SOURCE/CAUSE

SOURCE OF DISCHARGE: [ ] TANK LEAK [ ] UNKNOWN [X] PIPING LEAK [ ] OTHER

TANKS ONLY/CAPACITY: 10,000 GAL. AGE 16 YRS [ ] UNKNOWN

MATERIAL: [ ] FIBERGLASS [X] STEEL [ ] OTHER

CAUSE(S): [ ] OVERFILL [X] RUPTURE/FAILURE [ ] CORROSION [ ] UNKNOWN [ ] SPILL [ ] OTHER

CASE TYPE

CHECK ONE ONLY: [ ] UNDETERMINED [ ] SOIL ONLY [X] GROUNDWATER [ ] DRINKING WATER - (CHECK ONLY IF WATER WELLS HAVE ACTUALLY BEEN AFFECTED)

CURRENT STATUS

CHECK ONE ONLY: [X] SITE INVESTIGATION IN PROGRESS (DEFINING EXTENT OF PROBLEM) [X] CLEANUP IN PROGRESS [ ] SIGNED OFF (CLEANUP COMPLETED OR UNNECESSARY) [ ] NO ACTION TAKEN [ ] POST CLEANUP MONITORING IN PROGRESS [ ] NO FUNDS AVAILABLE TO PROCEED [ ] EVALUATING CLEANUP ALTERNATIVES

REMEDIAL ACTION

CHECK APPROPRIATE ACTION(S) (SEE BACK FOR DETAILS)

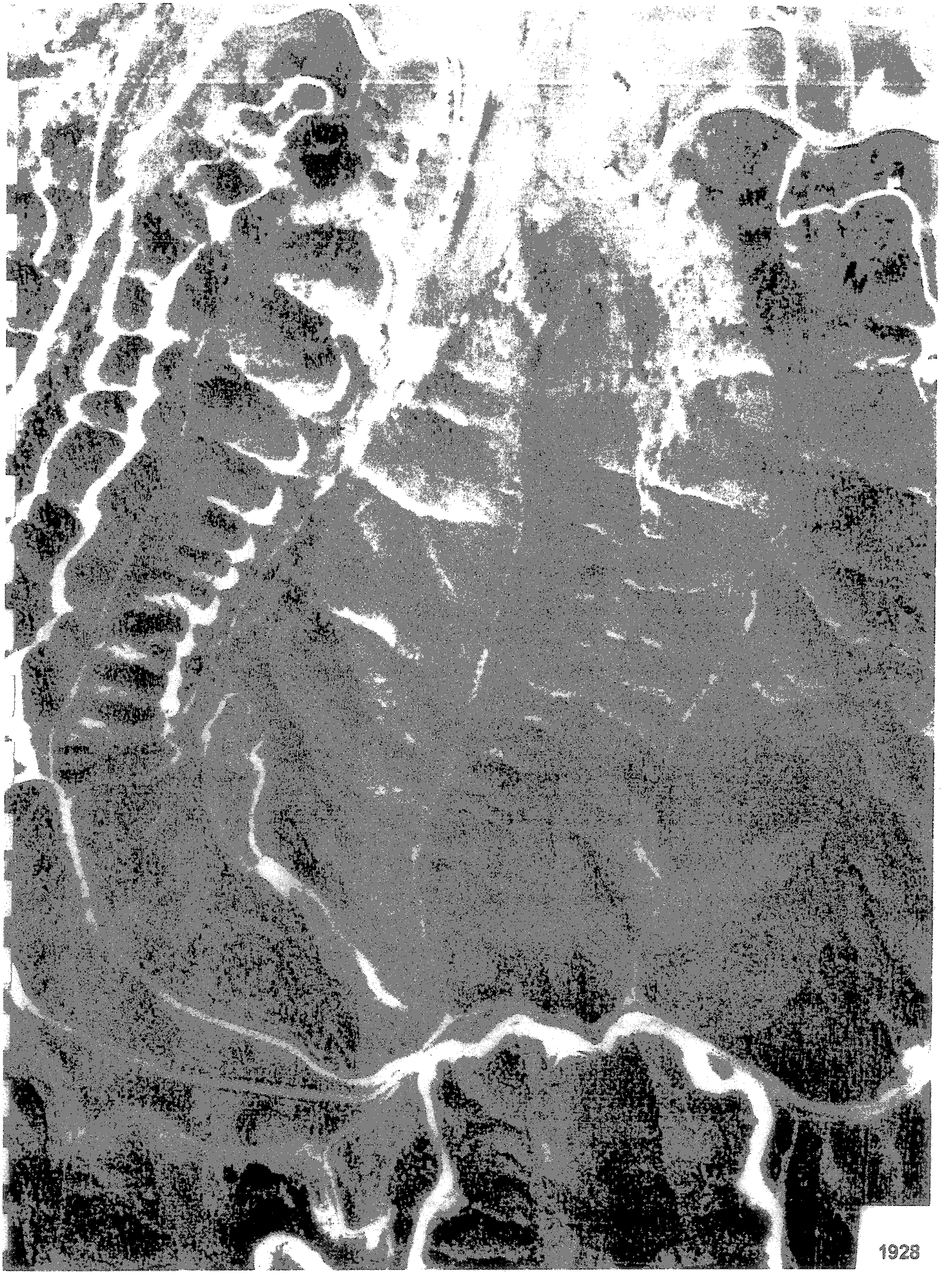
[ ] CAP SITE (CD) [ ] EXCAVATE & DISPOSE (ED) [ ] REMOVE FREE PRODUCT (FP) [ ] ENHANCED BIO DEGRADATION (IT)
[ ] CONTAINMENT BARRIER (CB) [ ] EXCAVATE & TREAT (ET) [X] PUMP & TREAT GROUNDWATER (GT) [ ] REPLACE SUPPLY (RS)
[ ] TREATMENT AT HOOKUP (HU) [ ] NO ACTION REQUIRED (NA) [ ] OTHER (OT)

COMMENTS

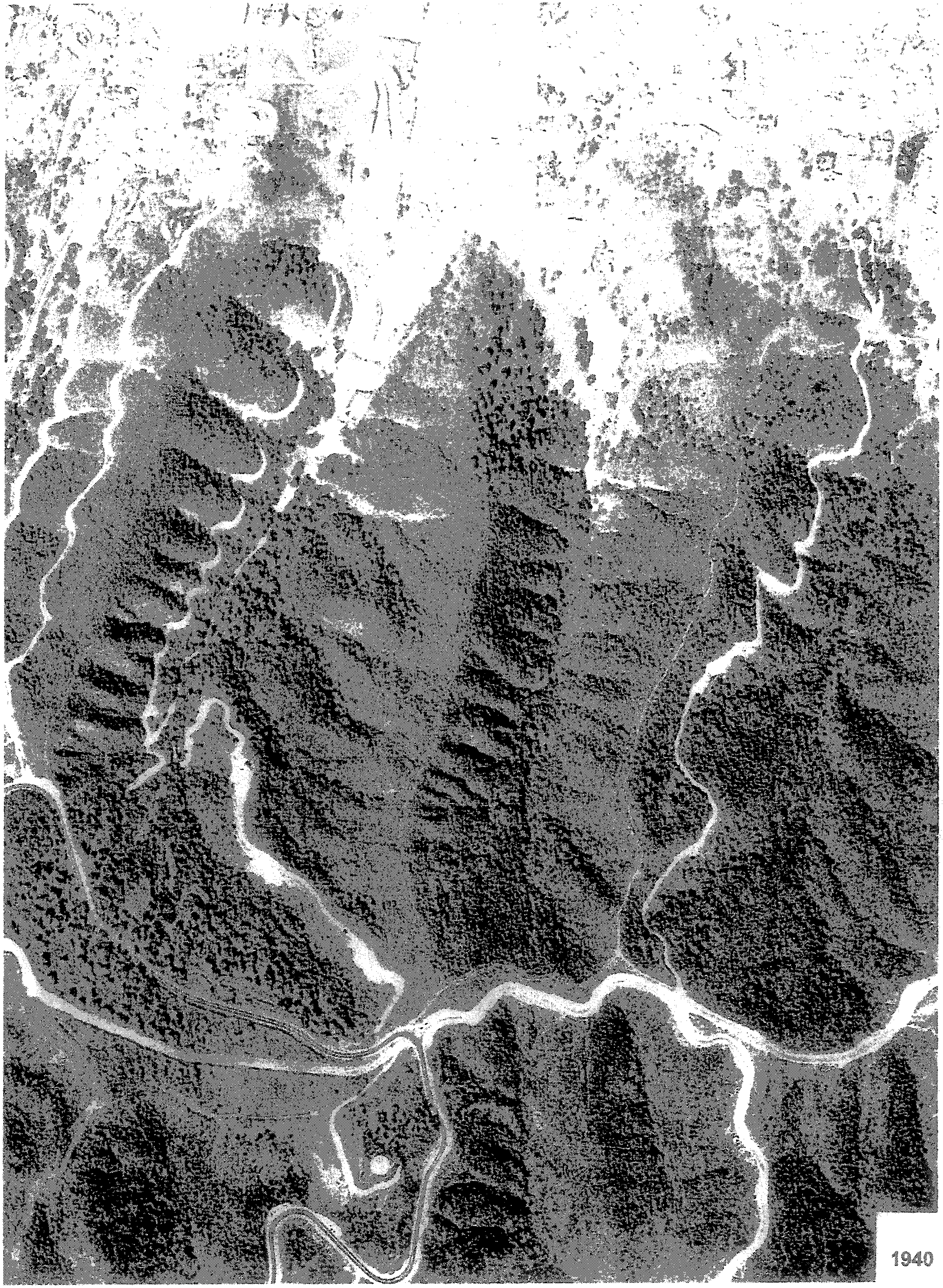
Appendix 3

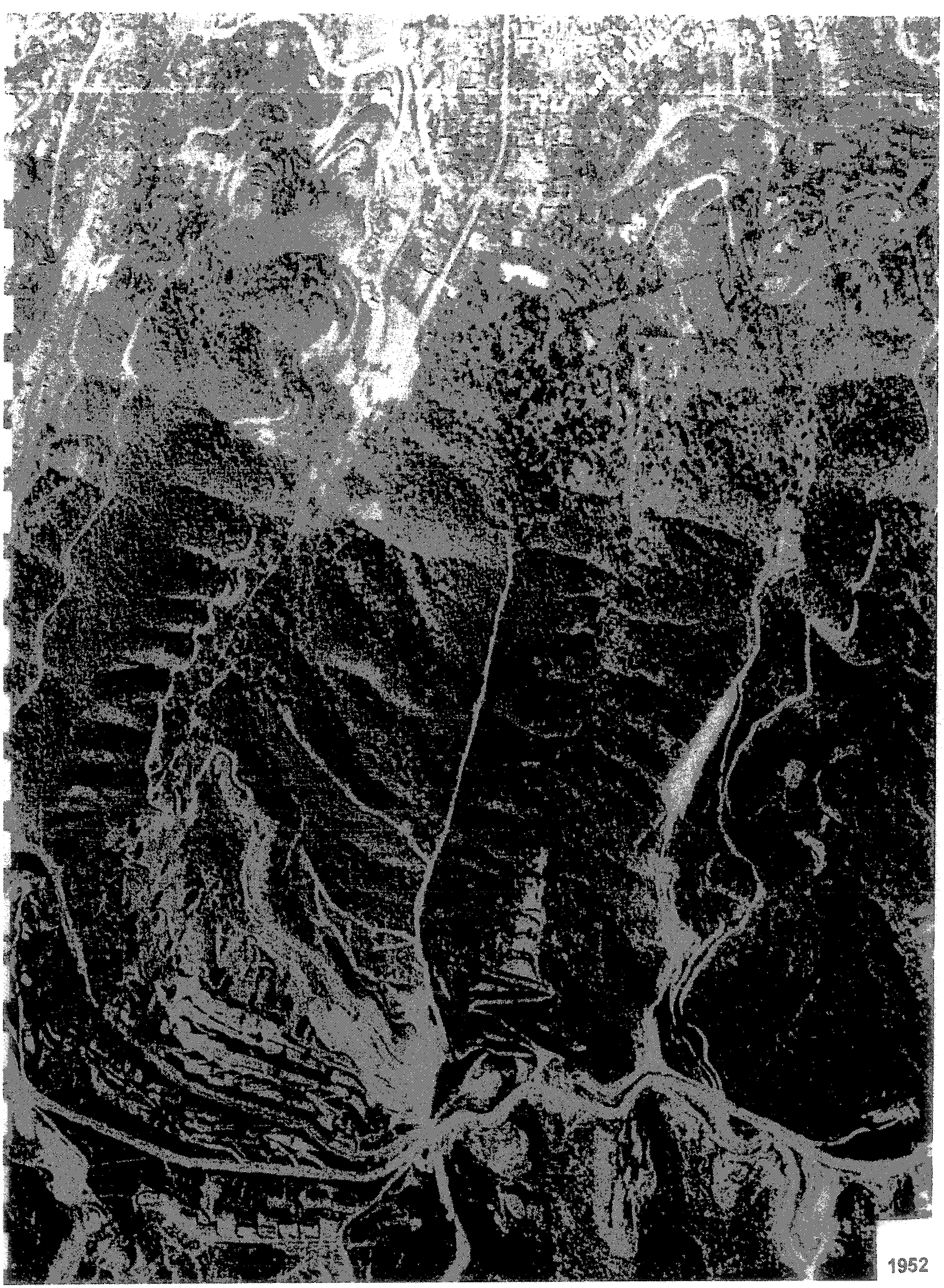
Historical Documents

Historical Aerial Photographs



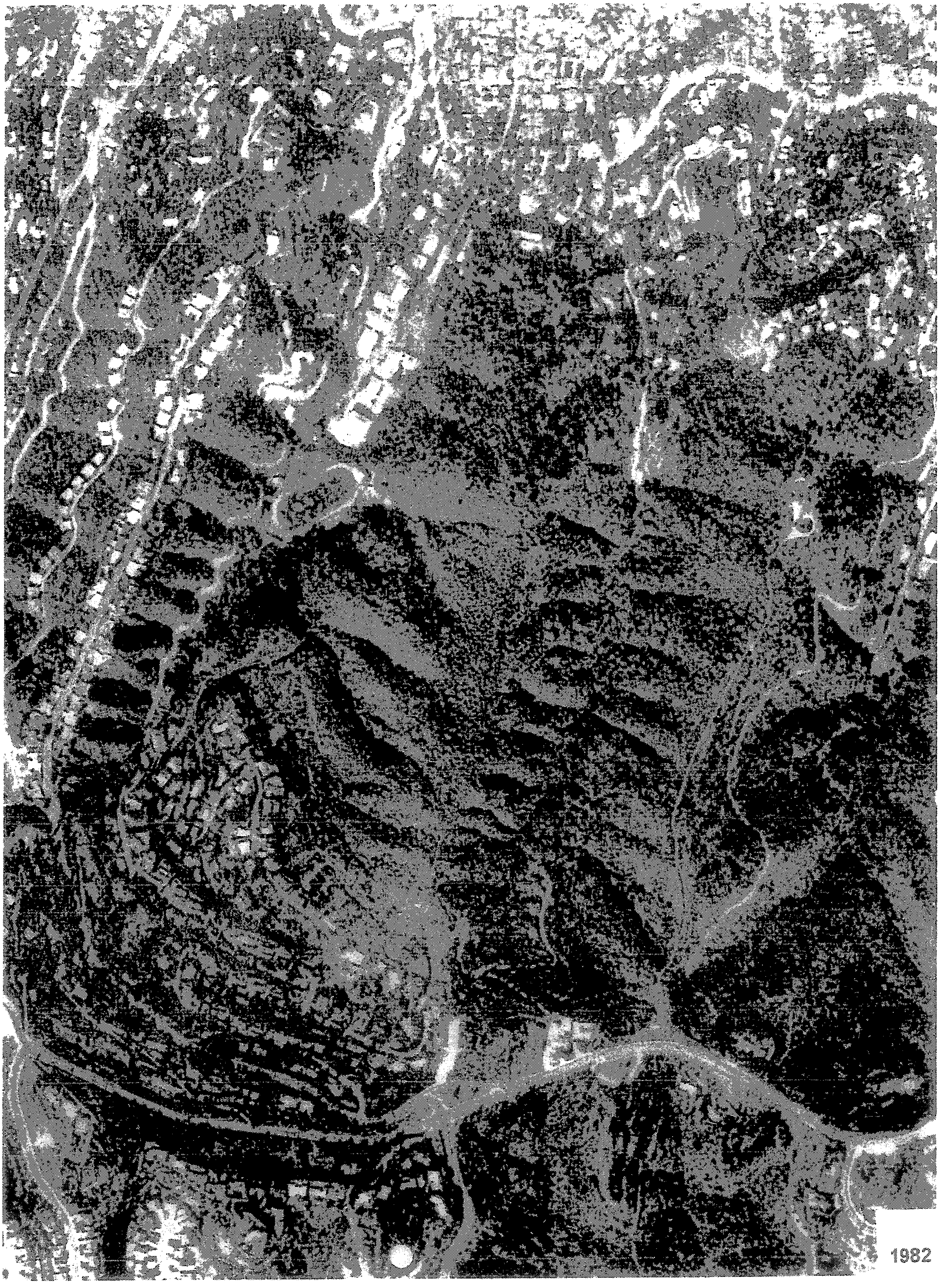
1928


1940

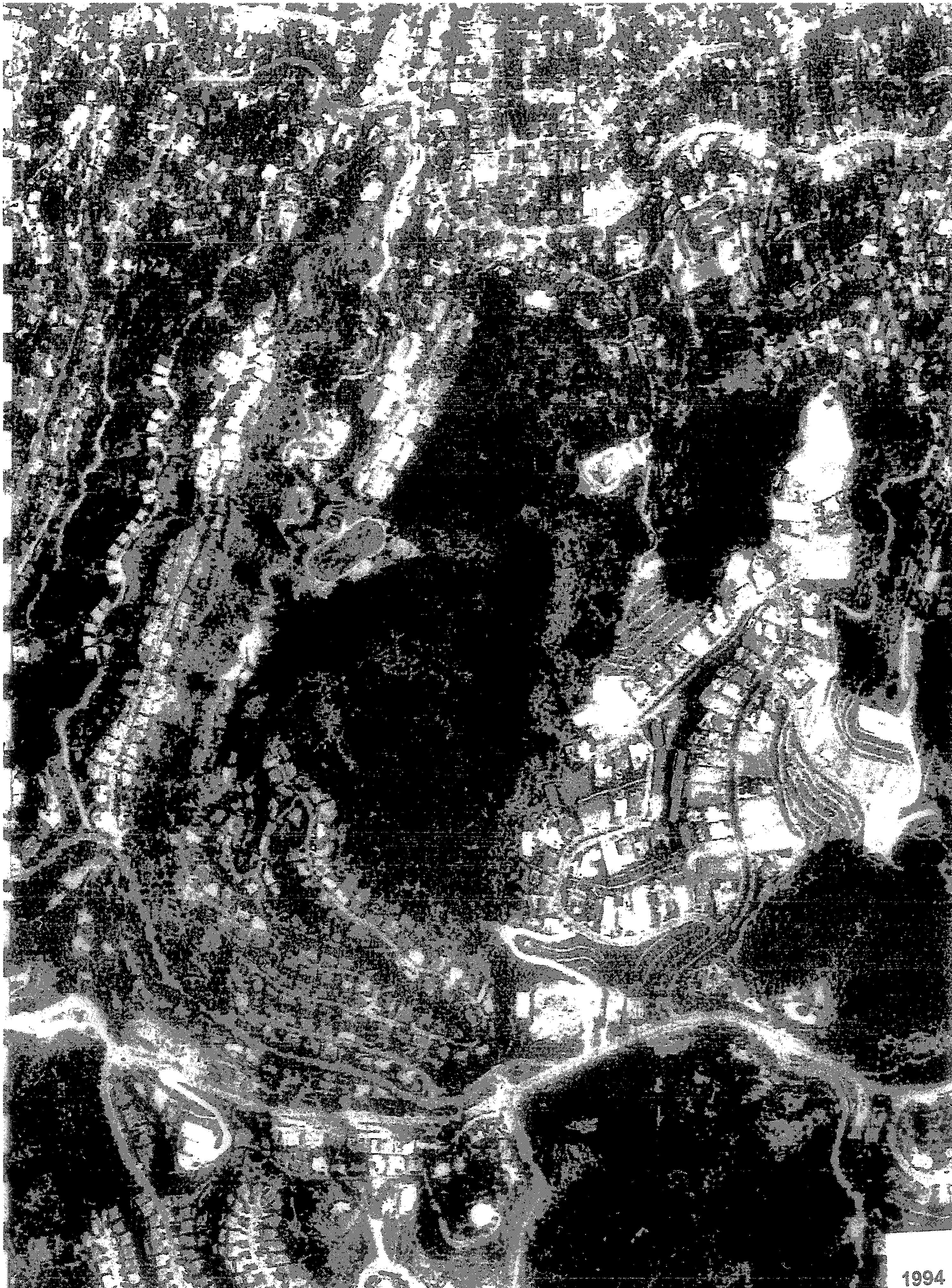

1952


1960

1971

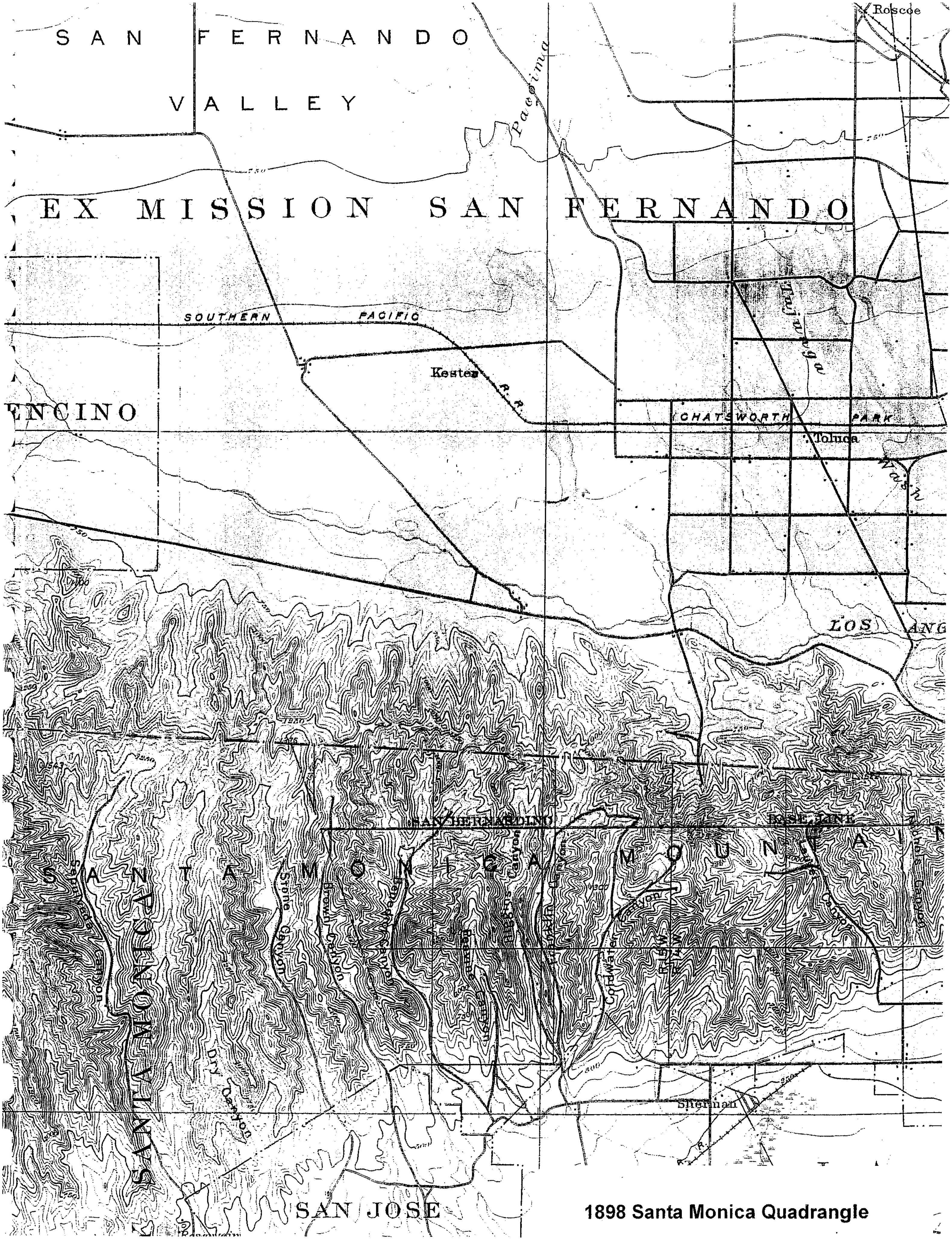


1982

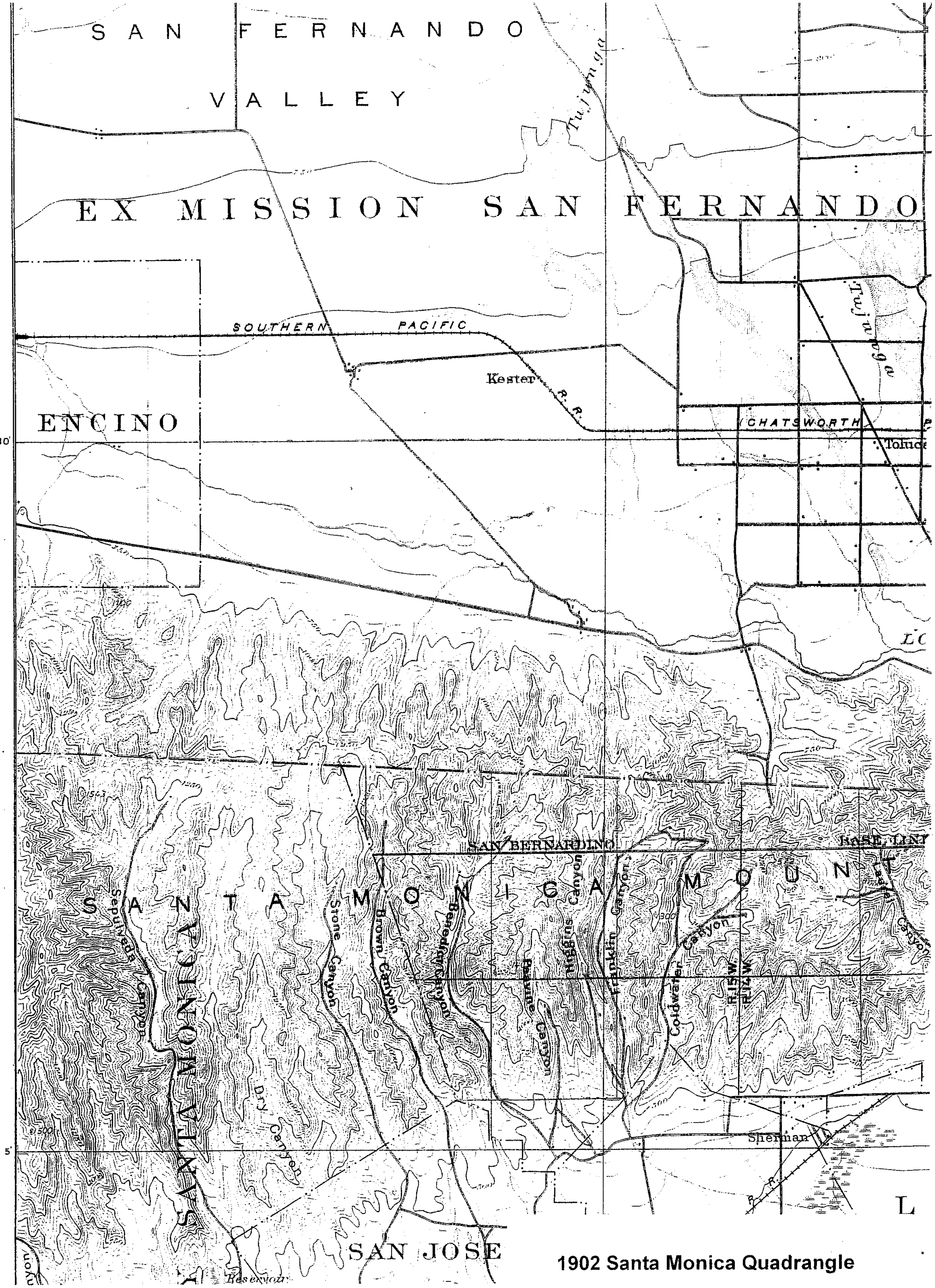


1994

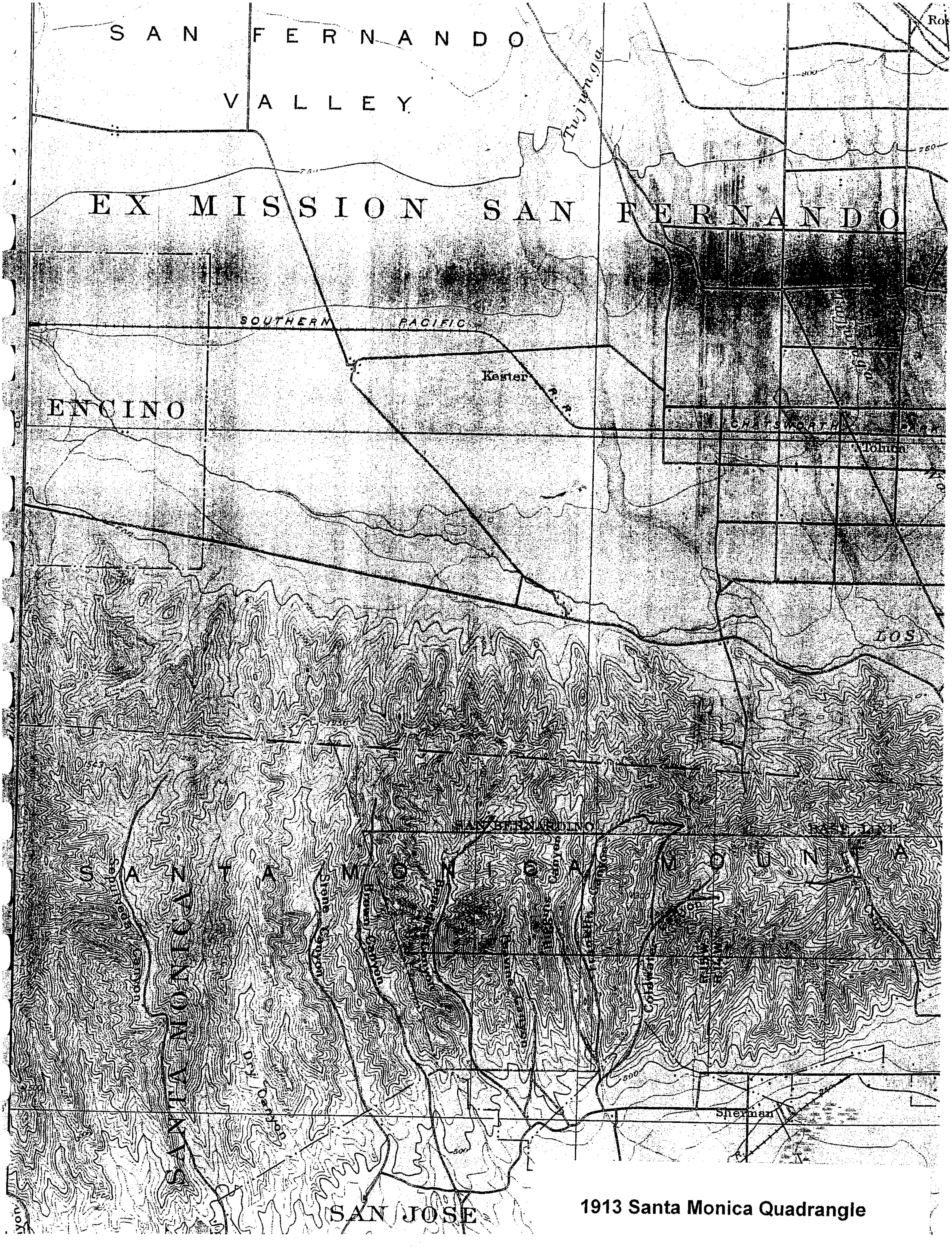
Historical Topographic Maps



1898 Santa Monica Quadrangle

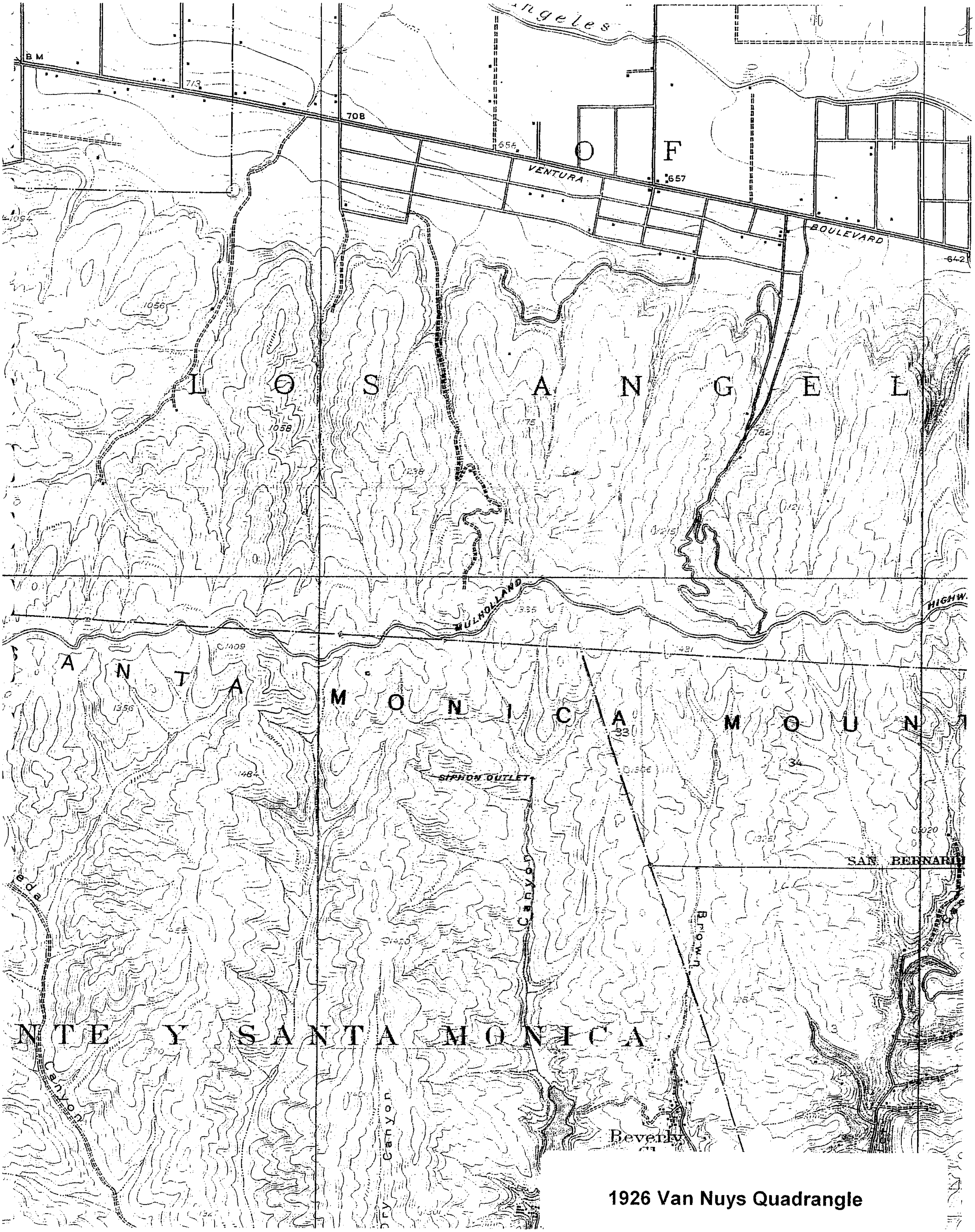


1902 Santa Monica Quadrangle

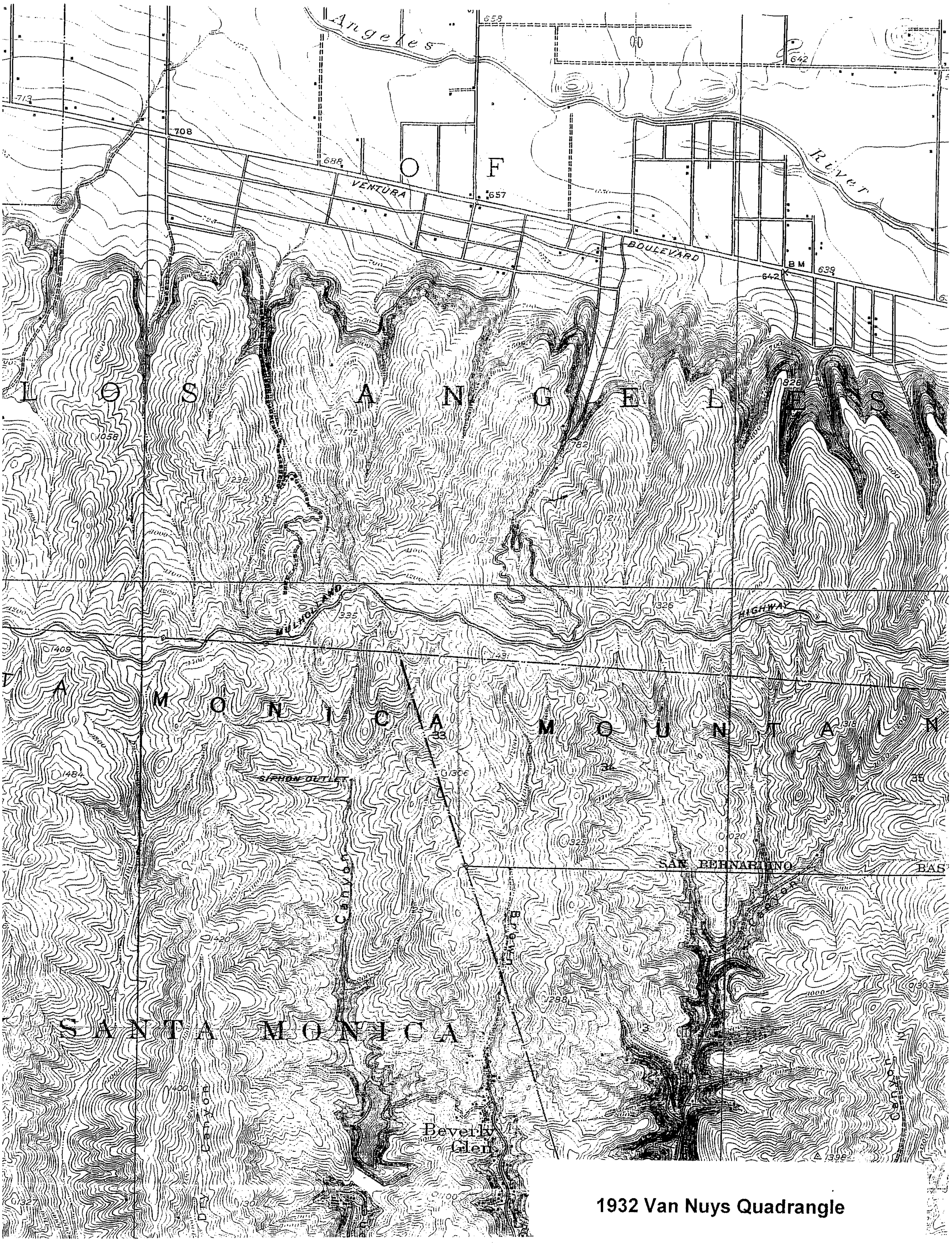


1913 Santa Monica Quadrangle

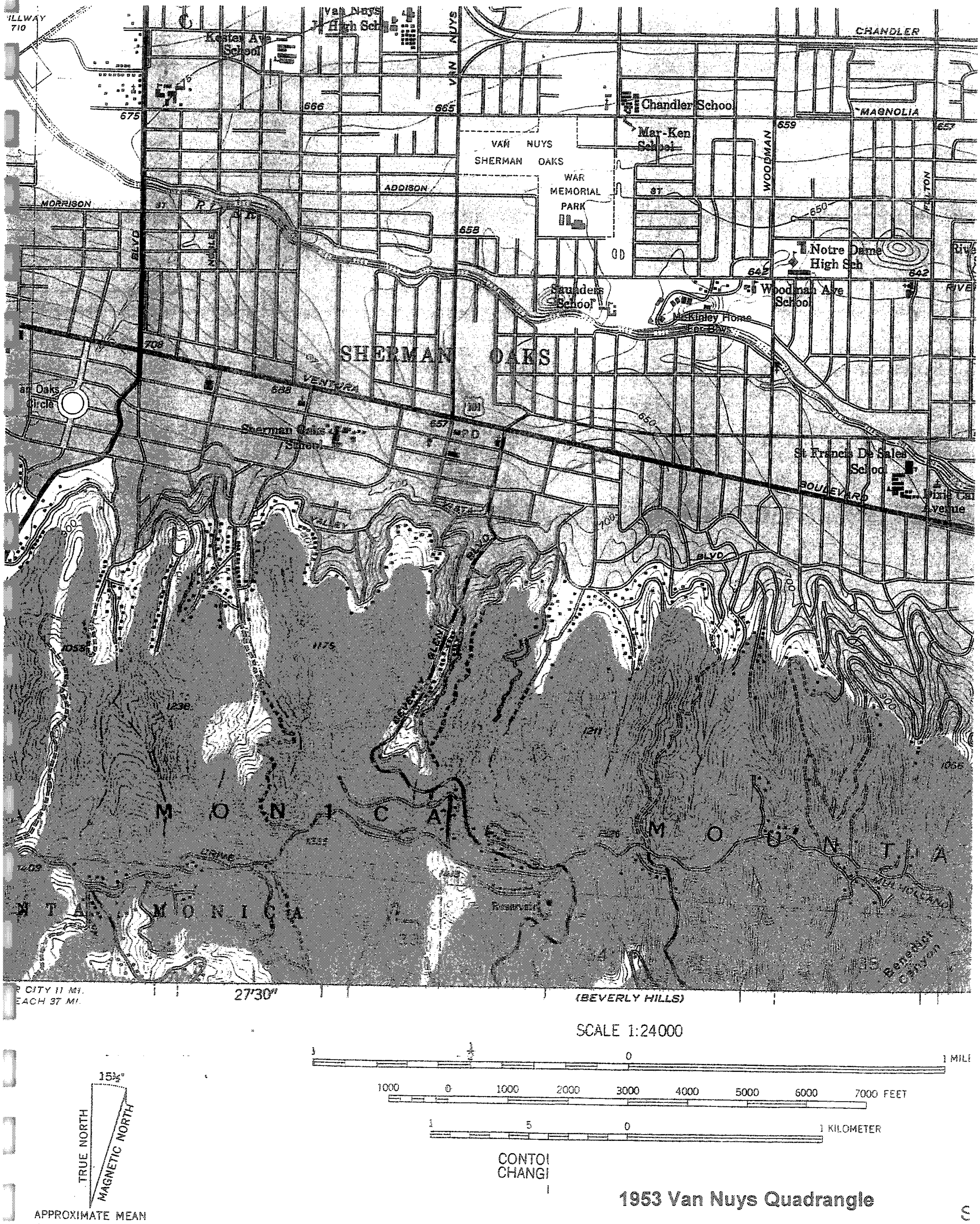
1921 Santa Monica Quadrangle



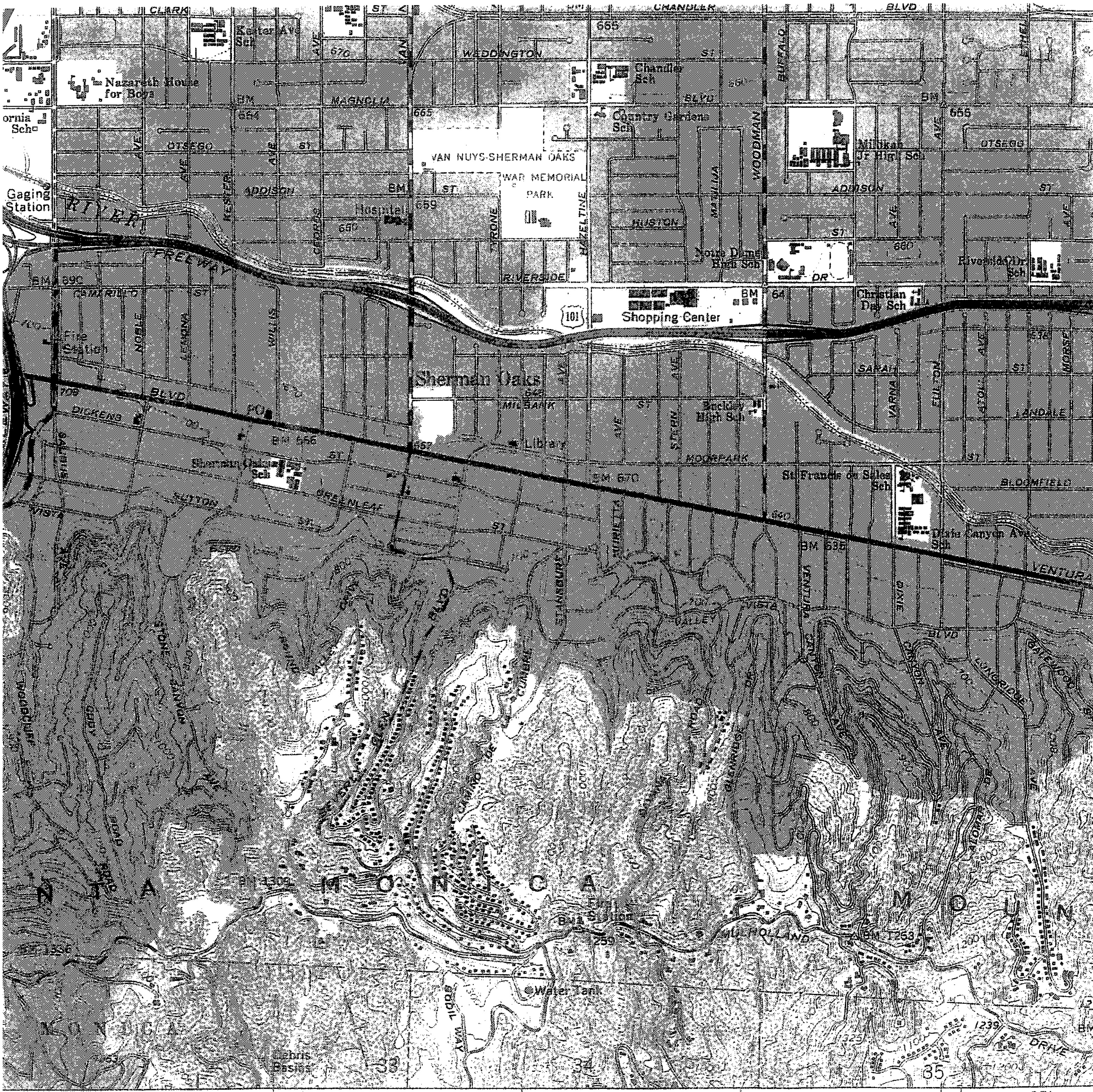
1926 Van Nuys Quadrangle



1932 Van Nuys Quadrangle



1953 Van Nuys Quadrangle



CITY) 10 MI. | 365 | 27'30" | 366 | 367 (BEVERLY HILLS) 2352 III SW | 368 | 369 | 25'

SCALE 1:24 000

1 ½ 0 1 MILE

1000 0 1000 2000 3000 4000 5000 6000 7000 FEET

1 .5 0 1 KILOMETER

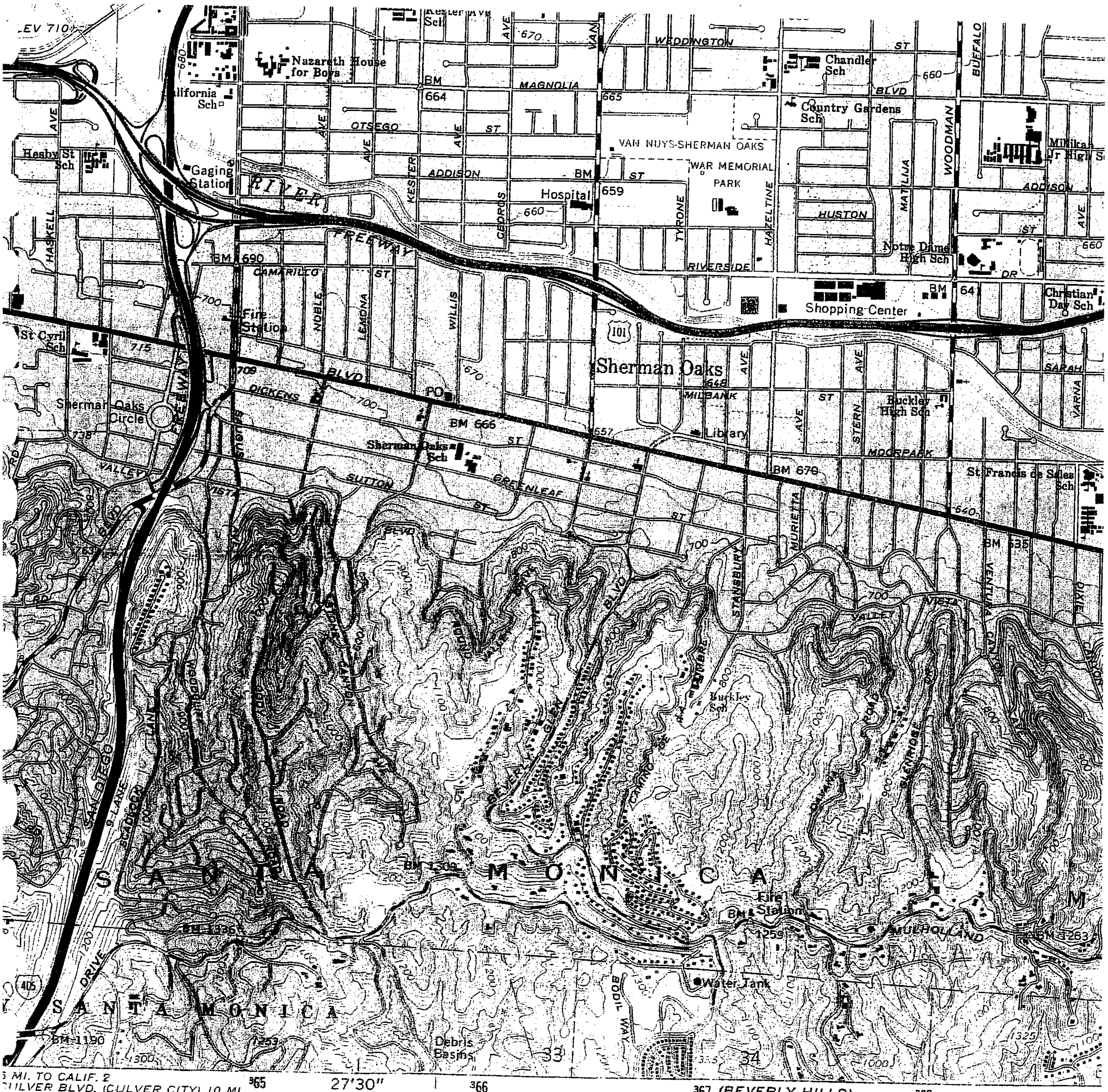
CONTOUR INTERVAL 20 FEET
DOTTED LINES REPRESENT 10-FOOT CONTOURS
DATUM IS MEAN SEA LEVEL

GN MN
0°48'
4 MILS
15½°
276 MILS

AND 1966 MAGNETIC NORTH
ION AT CENTER OF SHEET

THIS MAP COMPLIES WITH NATIONAL
FOR SALE BY U. S. GEOLOGICAL SURVEY, DENVER, C
A FOLDER DESCRIBING TOPOGRAPHIC MAPS AN

1966 Van Nuys Quadrangle

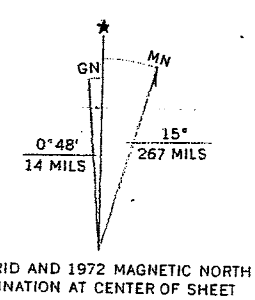


SCALE 1:24 000

1 ½ 0

1000 0 1000 2000 3000 4000 5000 6000 7000 FEET

1 .5 0 1 KILOMETER



UTM GRID AND 1972 MAGNETIC NORTH
DECLINATION AT CENTER OF SHEET

CONTOUR INTERVAL 20 FEET
DOTTED LINES REPRESENT 10-FOOT CONTOURS
NATIONAL GEODETIC VERTICAL DATUM OF 1929

THIS MAP CO
FOR SALE BY U. S. GEOLOGICA
A FOLDER DESCRIBING

1972 Van Nuys Quadrangle

Appendix 4

Transaction Screen Questionnaire

THE BUCKLEY SCHOOL

FAX COVER SHEET

TO: Tricia Bartholome

NAME OF ORGANIZATION: Rincon Consultants

FAX NUMBER: (805) 641-1072

FROM: Curtis Covington

DATE: 12/06/04

NUMBER OF PAGES
Including Cover: 7

RE:

MESSAGE:

☐ MIDDLE/UPPER SCHOOL FAX	818-461-6715	☐ LOWER SCHOOL OFFICE FAX	818-461-6716
☐ ADMISSION/DEVELOPMENT FAX	818-461-6714	☐ BUSINESS OFFICE FAX	818-501-7820
☐ HEAD OF SCHOOL FAX	818-461-6713	☐ PHYSICAL PLANT FAX	818-461-6712
☐ ATHLETICS	818-461-6710	☐ HR/PAYROLL	818-501-7823
		☐ PURCHASING	818-501-7701

3900 Stansbury Avenue • Sherman Oaks, CA 91423-4699 • 818-783-1610

Transaction Screen Questionnaire

Rincon Site Number 04-17840 – Buckley School, 3900 Stansbury, Sherman Oaks, California

This questionnaire should be completed by an individual considered to be knowledgeable of the subject property. We respectfully request that you fill out and return this form (via fax 805-641-1072) to us within one week from the date of this transmittal.

1)	**Was the subject property or any adjoining property ever used as** ☒ a gasoline station or motor repair facility ☐ a commercial printing facility ☐ a dry cleaners ☐ a photo developing laboratory ☐ a junkyard or landfill ☐ a waste treatment, storage, disposal, processing or recycling facility ☐ any other industrial use (please check all that apply and describe) fuel tanks were on site to fuel school buses.

2)	**Please describe the current land uses of the subject property and those surrounding your property. Please indicate all businesses/companies located on property.**	
2a	**Current use of Subject Property** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☐ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☒ Other-Please Describe	(please include a brief description of current operation) K-12 school
2b	**Current use of Northern Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of current operation)
2c	**Current use of Southern Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of current operation)
2d	**Current use of Western Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of current operation)
2e	**Current use of Eastern Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of current operation)

Transaction Screen Questionnaire

Rincon Site Number 04-17840 – Buckley School, 3900 Stansbury, Sherman Oaks, California

3)	**Please describe the previous land uses of your property and those surrounding your property. Include property ownership and dates of operation if known.**	
3a	**Previous use of Subject Property** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☐ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☒ Other-Please Describe	(please include a brief description of previous operations, former property owners, and dates of operation) Golf Course
3b	**Previous use of Northern Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of previous operations)
3c	**Previous use of Southern Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of previous operations)
3d	**Previous use of Western Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of previous operations)
3e	**Previous use of Eastern Adjoining Properties** (please check all that apply) ☐ Commercial (retail, offices, etc.) ☒ Residential (single family or apartments) ☐ Industrial (manufacturing, warehousing, processing) ☐ Other-Please Describe	(please include a brief description of previous operations)

4)	**Who is the current owner of the facility?**	Board of Trustees for The Buckley School
5)	**When did current ownership begin?**	1968
6)	**What is the age of the on-site facility?**	35 yrs.
7)	**Who is the previous owner of the property?**	

Transaction Screen Questionnaire

Rincon Site Number 04-17840 – Buckley School, 3900 Stansbury, Sherman Oaks, California

8)	**Please indicate the properties current...**	
	electrical service provider -	L.A. DWP
	water service provider -	LA DWP
	natural gas service provider -	So Cal Gas
	sewer service provider -	City of L.A.
	solid waste hauler -	Crown Disposal

9)	**To the best of your knowledge has your facility previously or does your facility currently, store or use any of the following in individual containers larger than 5 gallons in volume or 50 gallons in the aggregate?** (If yes or unknown, include how many, type, and size)	
	☐ ***Damaged or discarded automotive or industrial batteries***	no
	☐ ***Pesticides***	no
	☐ ***Paints***	no
	☐ ***Other Chemicals or hazardous substances***	no

10)	**Please indicate any wastes generated at the facility.**		
	Hazardous waste:	**Quantity:**	**Disposal Method:**
	waste oil	55 gal drum	p/u by Safety Kleen
	waste paint	30 gal drum	p/up by Safety Kleen

11)	**Are there currently or to the best of your knowledge have there been previously, any industrial drums (typically 55 gallon) or sacks of chemicals located on the property or at the facility?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

12)	**Are there currently or to the best of your knowledge have there been previously, any evidence of fill dirt having been brought onto the property that originated from a contaminated site or that is of an unknown origin?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

Transaction Screen Questionnaire
Rincon Site Number 04-17840 – Buckley School, 3900 Stansbury, Sherman Oaks, California

13)	**Are there currently or to the best of your knowledge have there been previously, any pits, ponds or lagoons located on the property in connection with waste treatment or waste disposal?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe
14)	**Are there currently or to the best of your knowledge have there been previously, any stained soil on the property?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe
15)	**Are there currently or to the best of your knowledge have there been previously, any storage tanks (above or below ground) located on the property?**	
	☒ Yes ☐ No ☐ Unknown	If Yes or Unknown, please describe Fuel tanks were underground - they have been removed
16)	**Are there currently or to the best of your knowledge have there been previously, any vent pipes, fill pipes, or access ways (etc.) indicating a fill pipe protruding from the ground on the property or adjacent to any structure located on the property?**	
	☒ Yes ☐ No ☐ Unknown	If Yes or Unknown, please describe
17)	**If the property is served by a private well or non-public water system, have contaminants been identified in the well or system that exceed guidelines applicable to the water system or has the well been designated as contaminated by any government agency?**	
	☐ Yes ☐ No ☒ Unknown	If Yes or Unknown, please describe
18)	**Are there currently or to the best of your knowledge have there been previously, any flooring, drains, or walls located within the facility that are stained by substances other than water or are emitting foul odors?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

Transaction Screen Questionnaire

Rincon Site Number 04-17840 – Buckley School, 3900 Stansbury, Sherman Oaks, California

19)	**To the best of your knowledge has your facility previously or does your facility currently, discharge wastewater on or adjacent to the property other than storm water into a sanitary sewer system?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

20)	**Have any of the following ever been dumped above grade, buried and/or burned on the property? (please check all that apply and describe if possible)**	
	☐ hazardous substances	no
	☐ petroleum products	no
	☐ unidentified waste materials	no
	☐ tires	
	☐ automotive or industrial batteries	no
	☐ other waste materials (please describe)	no

21)	**Are there currently or to the best of your knowledge have there been previously, a transformer, capacitor or any hydraulic equipment on the property?**	
	☒ Yes ☐ No ☐ Unknown	If Yes or Unknown, please describe We have hydraulic lift equipment - transformers are located throughout the campus

22)	**Are there currently or to the best of your knowledge have there been previously, any records indicating the presence of PCB's?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

23)	**Do your have any environmental liens or governmental notification relating to past or recurrent violations of environmental laws with respect to the property or any facility located on the property?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

Transaction Screen Questionnaire
Rincon Site Number 04-17840 – Buckley School, 3900 Stansbury, Sherman Oaks, California

24)	**Have you been informed of the past or current existence of hazardous substances, petroleum products, or environmental violations with respect to the property or any facility located on the property?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

25)	**Do you have any knowledge of any environmental site assessments of the property or facility that indicated the presence of hazardous substances or petroleum products on, or contamination of, the property or recommended further assessment of the property?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

26)	**Do you know of any past, threatened, or pending lawsuits or administrative proceedings concerning a release of any hazardous substances or petroleum products involving the property by any owner or occupant of the property?**	
	☐ Yes ☒ No ☐ Unknown	If Yes or Unknown, please describe

This questionnaire was completed by (please print)	
Name	CurTIS Covington
Title	Director of Plant Operations
Firm	The Buckley School
Street Address	3900 Stansbury Ave.
City, State, Zip Code	Sherman Oaks, C.A. 91423
Phone Number	(818) 461-6765
Fax Number	(818) 461-6712
What is the Preparer's relationship to the property (i.e., owner, occupant, property manager, employee, agent, consultant, etc.)?	Employee

Copies of the completed questionnaire should be faxed (preferably) or mailed to:

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, California 93001
Attention: Environmental Site Assessment Division
Fax: (805) 641 - 1072

Preparer represents that to the best of the preparer's knowledge the above statements and facts are true and correct and to the best of the preparer's knowledge no material facts have been suppressed or misstated.

Signature ______________ **Date** 12/6/04

Appendix 5

Geophysical Survey

GEOVision
geophysical services
a division of Blackhawk GeoServices

March 7, 2005

Project Number 5117

Ms. Tricia Aimsworth
Rincon Consultants, Inc.
790 East Santa Cara Street
Ventura, CA 93301

Subject: Geophysical Investigation at the Buckly School, Sherman Oaks, California

Dear Ms. Aimsworth:

A ground penetrating radar (GPR) survey was conducted on December 21, 2004 in a parking lot located at the Buckley School in Sherman Oaks , California. The purpose of the GPR survey was to screen an approximately 50 by 50-ft area for underground storage tanks believed to be on the property.

METHODOLOGY

GPR equipment used during this investigation consisted of a Geophysical Survey Systems Inc. (GSSI) SIR-3000 GPR system with a 400-MHz antenna (SIR-3000). Short duration EM pulses of high-frequency generated by a transmitting antenna propagate into the ground and are reflected from electrical discontinuities in the subsurface back to a receiving antenna. The propagation velocity of these EM waves in the subsurface is determined by the dielectric constant whereas the attenuation is primarily a function of ground conductivity and scattering. The dielectric constant is largely determined by water content, because the relative dielectric constant of water is 80 and that of rock and soil minerals typically is between 3 and 6. Attenuation is related to soil conductivity, which is primarily a function of clay content, moisture content, and dissolved solids in the pore water. Small percentages of clay in subsurface soils can rapidly increase the attenuation of GPR signals. Depth penetration is also a function of antenna frequency, and low frequency antennas can image to greater depths at the cost of resolution. At typical sites in Southern California, depth penetration of a 400-MHz antenna range from about 3 and 5 feet. High-amplitude, hyperbolic reflections are generally observed on GPR records over buried metallic objects such as pipes and tanks. Additional information on the GPR method can be found in the attached technical note.

1151Pomona Road, Suite P, Corona, CA 92882 phone 951-549-1234 fax 951-549-1236

FIELD PROCEDURES

Before conducting the GPR survey, a 5- by 5-foot grid was established with baselines marked on the ground with chalk. The survey grid was established immediately to the west of a large debris pile, which was adjacent to a possible UST vent.

GPR data were acquired semi-continuously (32 scans per second), as the 400-MHz antenna was hand-towed along south to north survey lines spaced 2.5 feet apart. Spatial control was maintained by the chalk markings. GPR data were viewed in real time on the SIR-3000's color monitor and saved to the instrument's hard disk for later archiving. All field copies of GPR data are retained in the project files.

DATA PROCESSING

Most GPR data acquired during this investigation were not processed; rather interpretation was made using the field records. The GPR profiles presented as figures in this report were processed using the RADAN™ for Windows software package developed by GSSI, Inc.

Data preparation and processing steps for the GPR profiles presented in the report included the following:

- Downloading data from the SIR-3000 hard disk to an office computer (all data)
- Trimming the ends of the line (data scans before the beginning and after the end of the survey line)
- File reversal as necessary
- Horizontal stacking, as necessary
- Vertical and horizontal high- and low-pass filtering
- Gain adjustment
- Horizontal distance normalization
- Importing GPR profiles into Corel Draw ™ 11
- Annotation of GPR records and plotting

All GPR data file names resulting from the various stages of processing were documented and data later archived.

RESULTS

There is one anomaly in the GPR data that warrants discussion. Figure 2 shows a high-amplitude GPR anomaly located at a depth of approximately 2 ft. Depth of investigation was about 3 feet due to the interference from the rebar in the concrete. This anomaly is in line with the exposed vent, and extends 8 ft to the west. There are two interpretations for this anomaly.

The first interpretation is that this anomaly is the result from a small underground storage tank. This tank would be considered quite shallow, and may have had its crown removed.

The second interpretation is that this anomaly results from the vent line itself, in which case the UST may be immediately west of the western termination of the anomaly. We recommend that the anomaly be uncovered at its western edge to determine its exact nature. Excavation at this location would reveal either the western edge of a small UST (i.e. the anomaly is caused by a UST), the termination of the vent line at the eastern edge of a UST, or the severed end of the vent line at a former UST location.

If you have any questions concerning this investigation, please call us at 951-549-1234.

Sincerely,
GEO*Vision* Geophysical Services

JB Shawver

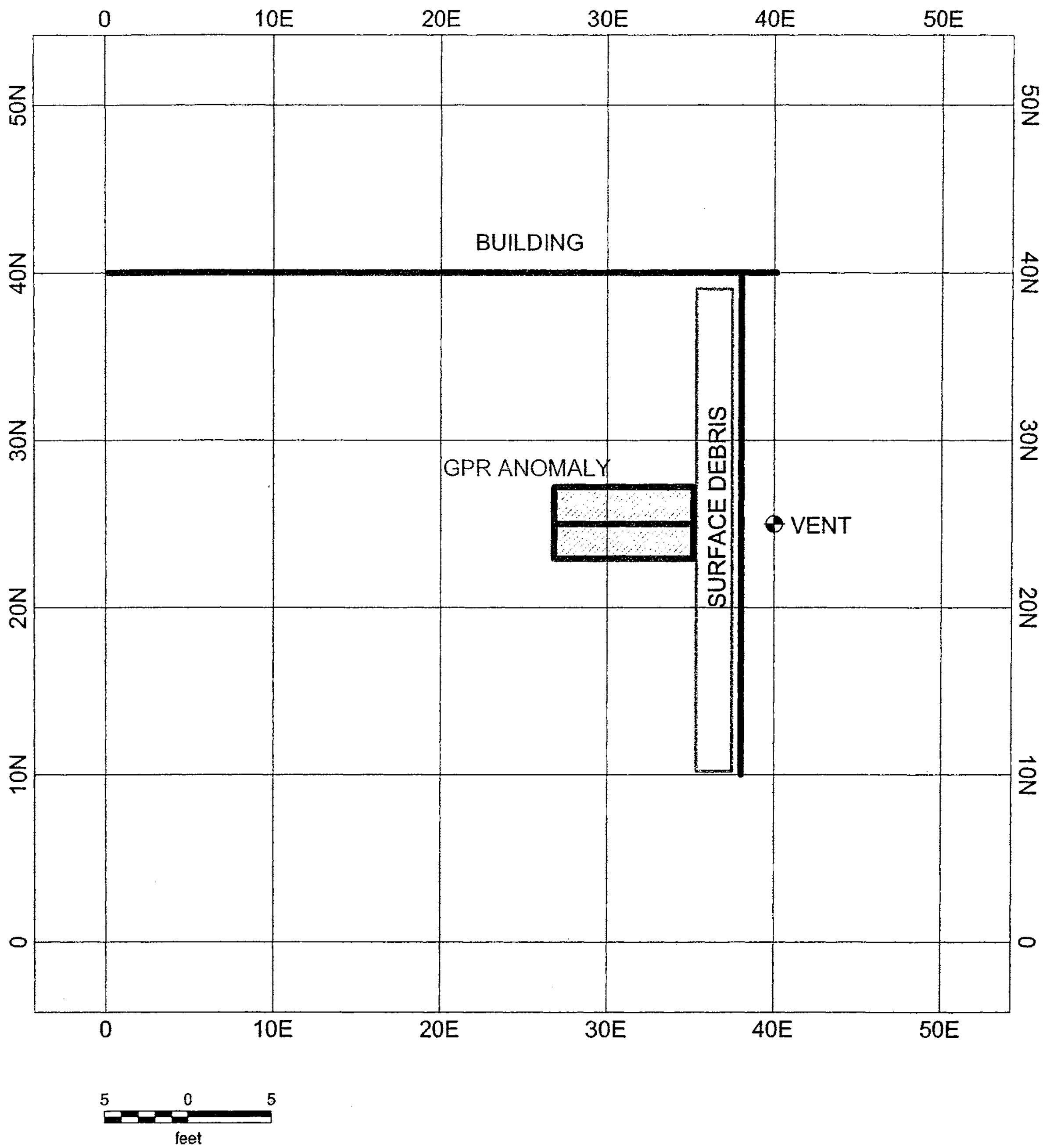
Submitted by:
JB Shawver
Project Geophysicist

Reviewed and Approved by:
Antony J. Martin, R. GP.
Technical Director

Attachments: Figure 1: Site Map
Figure 2: Example Ground Penetrating Radar Profile
Application Note – Geophysical Methods for Shallow Environmental Investigations

* This geophysical investigation was conducted under the supervision of a California Registered Geophysicist using industry standard methods and equipment. A high degree of professionalism was maintained during all aspects of the project from the field investigation and data acquisition, through data processing interpretation and reporting. All original field data files, field notes and observations, and other pertinent information are maintained in the project files and are available for the client to review for a period of at least one year.

A registered geophysicist's certification of interpreted geophysical conditions comprises a declaration of his/her professional judgment. It does not constitute a warranty or guarantee, expressed or implied, nor does it relieve any other party of its responsibility to abide by contract documents, applicable codes, standards, regulations or ordinances.



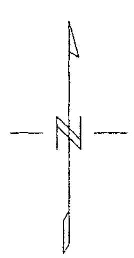
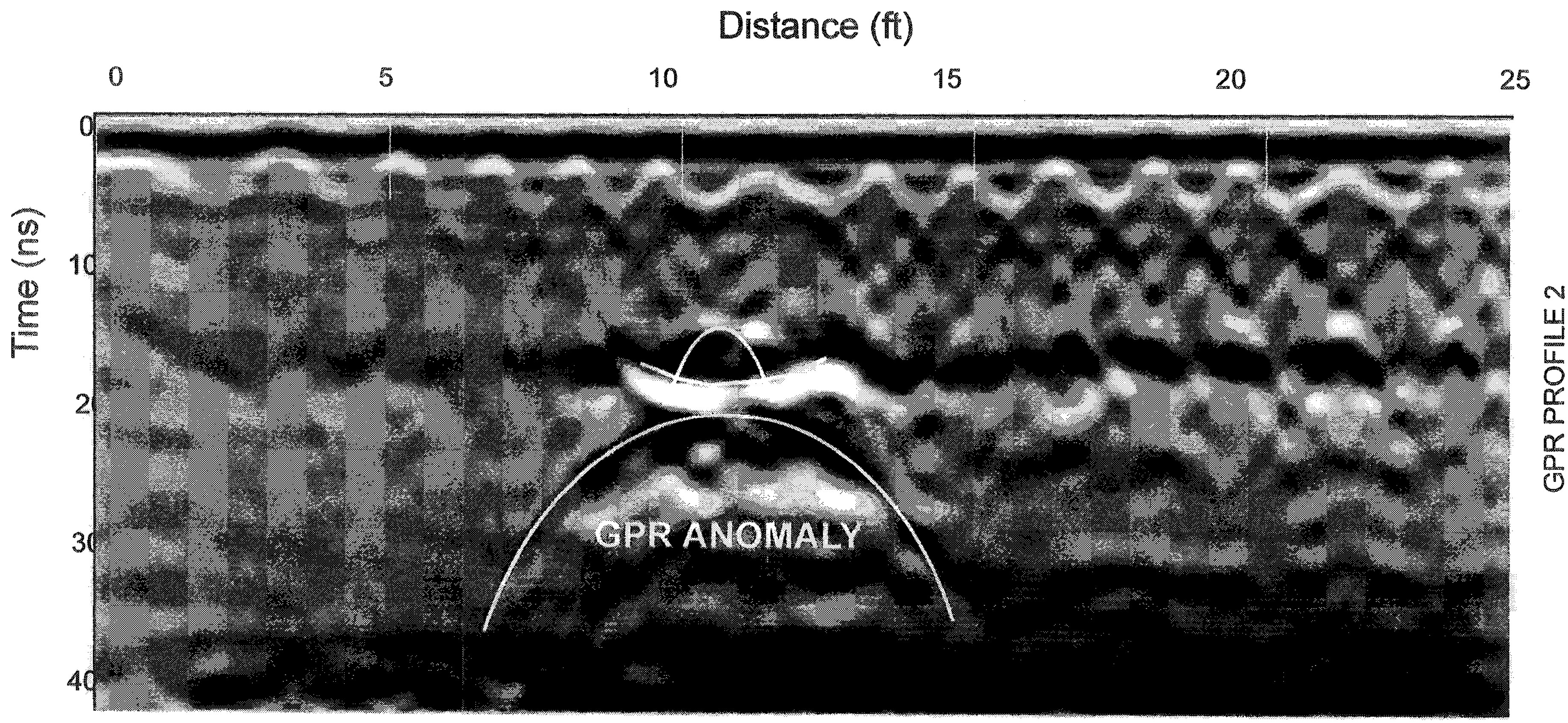


FIGURE 1

SITE MAP WITH GEOPHYSICAL INTERPRETATION

PROPERTY LOCATED AT
THE BUCKLY SCHOOL
VENTURA, CALIFORNIA

PREPARED FOR RINCON CONSULTANTS



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geophysical services
a division of Blackhawk GeoServices

Project # 5117	FIGURE 2 EXAMPLE GPR PROFILE 2
Date: March 7, 2005	THE BUCKLEY SCHOOL SHERMAN OAKS, CALIFORNIA
Drawn By: J SHAWVER	
Approved By:	PREPARED FOR RINCON CONSULTING, INC.
File C:\gvprojects\5117\f2.cdr	

Appendix 6

Soil Boring Logs

Rincon Consultants

LOG OF BORING B1

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: Former UST location
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion
Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Asphalt	
		CL		SANDY SILTY CLAY, some finer gravels, reddish brown, medium plasticity, moist	
5				becomes more dense	0.0
10				more reddish	0.0
15					0.0
				becomes gray to dark brown, sweet chemical odor	
20					24
		SL		SILTSTONE, light yellowish brown, moist, sweet chemical odor	
				becomes more dense	
25				siltstone had very strong gasoline odor refusal	985
30					

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B1.bor

Rincon Consultants

LOG OF BORING B2

(Page 1 of 1)

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: Former UST location
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion: ■ Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Asphalt	
		CL		SANDY SILTY CLAY, some finer gravels, reddish brown, medium plasticity, moist	
5	Sample			becomes more dense	0.0
10	Sample			more reddish	0.0
15	Sample				0.0
		SL		SILTSTONE	
20	Sample			light yellowish brown, moist, slight sweet chemical odor refusal	0.0
25					
30					

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B2.bor

Rincon Consultants

LOG OF BORING B3

(Page 1 of 1)

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: Former UST location
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion
Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Asphalt	
		CL		SANDY SILTY CLAY, some finer gravels, reddish brown, medium plasticity, moist	
5				becomes more dense	0.0
10					0.0
15					10
				becomes gray to dark brown, sweet chemical odor	
20				less sands and gravels, gray clay, dense, medium plasticity, petroleum odor	22
25					35
		SL		SILTSTONE, light yellowish brown, moist, slight petroleum odor	
30					11

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B3.bor

Rincon Consultants

LOG OF BORING B4

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: Former UST location
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion
Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Asphalt	
		CL		SANDY SILTY CLAY, some finer gravels, reddish brown, medium plasticity, moist	
				becomes less dense, less sand and gravel	
5					0.0
10					0.0
15					2
		SL		SILTSTONE	
20				yellowish brown, moist, slight sweet chemical odor refusal	16
25					
30					

Rincon Consultants

LOG OF BORING B5

(Page 1 of 1)

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: Waste Oil UST location
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion: Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Asphalt	
		CL		SANDY SILTY CLAY, some finer gravels, reddish brown, medium plasticity, moist	
5	Retained for Lab				0.0
		SL		SILTSTONE, light yellowish brown, moist refusal	
10	Retained for Lab				0.0
15					
20					
25					
30					

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B5.bor

Rincon Consultants

LOG OF BORING B6

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: Waste Oil UST location
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion

Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Asphalt	
		CL		SANDY SILTY CLAY, some finer gravels, reddish brown, medium plasticity, moist	
5					0.0
		SL		SILTSTONE, light yellowish brown, moist	
10					0.0
15				refusal	0.0
20					
25					
30					

Rincon Consultants

LOG OF BORING B7

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/27/04
Location	: End of hydraulic hoist
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion

Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Concrete	
		CL		SANDY SILTY CLAY, some fine gravels, reddish brown, medium plasticity, moist	0.0
		SL		SILTSTONE, light yellowish brown, moist	0.0

Depth scale: 0, 5, 10, 15, 20, 25, 30

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B7.bor

Rincon Consultants

LOG OF BORING B8

(Page 1 of 1)

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed : 12/30/04
Location : Adjacent to hoist piston
Method : Geoprobe
Drilled By : Core Probe
Logged By : J. Inch

Sample Portion
Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Concrete	
		CL		SILT, light brown, moderately dense, moist	0
		SL		SILTSTONE, light yellowish brown, moist refusal	0

Depth scale: 0, 5, 10, 15, 20, 25, 30

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Rincon Consultants

LOG OF BORING B9

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed : 12/30/04
Location : East end of former clairifier
Method : Geoprobe
Drilled By : Core Probe
Logged By : J. Inch

Sample Portion
Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Concrete	
		GP		Fill Pea Gravel, poorly graded, loose, moist	
				Concrete	
	Retained for Lab	SL		SILTSTONE, light yellowish brown, moist	0
10	Retained for Lab			darker brown	0

0
5
10
15
20
25
30

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B9.bor

Rincon Consultants

LOG OF BORING B10

Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA

Rincon Project #04-17841

Date Completed	: 12/30/04
Location	: Adjacent to the west end of former clairifier
Method	: Geoprobe
Drilled By	: Core Probe
Logged By	: J. Inch

Sample Portion
Retained for Lab

Depth in Feet	Samples	USCS	GRAPHIC	DESCRIPTION	PID
0				Concrete	
		GP		SILTY SANDY CLAY, medium plasticity, stiff, brown, moist	0
5		SL		SILTSTONE, light yellowish brown, moist	0
10					
15					
20					
25					
30					

02-04-2005 H:\Los Angeles County\Latham and Watkins\Buckley School\Phase II\Boring Logs\B10.bor

Appendix 7

Laboratory Analytical Reports

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Number of Pages 36
Date Received 12/28/2004
Date Reported 01/06/2005

Telephone (805)641-1000
Attn Joe Inch

Job Number	Ordered	Client
24245	12/28/2004	RINCON

Project ID: 04-17841
Project Name: Buckley School
Site: 3900 Stansbury Ave.
Sherman Oaks, CA

Enclosed are the results of analyses on 23 samples analyzed as specified on attached chain of custody.

Amolk MOLKY Brar
Laboratory Manager

Rojert G. Araghi
Laboratory Director

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

COC# № 28229 GLOBAL ID ______ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 24245

Company: Rincon Consultants	Report To: Rincon
Address: 790 E. Santa Clara, Ventura, CA 93001	Address:
Telephone: (805) 641-1000	Invoice To:
Fax: -1072	Address:
Special Instruction:	P.O.#: 04-17841
Project Name: Buckley School	
Site Address: 3900 Stansbury Ave, Sherman Oaks, CA	
Project ID: 04-17841	
Project Manager: Joe / Tricia	

ANALYSIS REQUESTED: 8260B TPH-g BTEX & oxygenates; 8015M TPH-DRO/TPH-ORO; 6010B Lead; 8260B VOCs; 6010B/7471A Metals

ITEM	Lab ID (LAB USE ONLY)	Sample ID	Date	Time	#	Type	Matrix	Preservation	8260B	8015M	6010B	8260B	6010B/7471A	Remarks
		B1-5	12/28/04	7:30	4	Soil | AQ	Brass | VOA	Meth / Sodium Bisulf						
1	141606	B1-10							X	X				
2	141607	B1-15							X	X	X			
3	141608	B1-20							X	~~X~~	X			
4	141609	B1-25							X	~~X~~	X			Sample for Dro Options
		B2-5												
		B2-10												
5	141610	B2-15							X	~~X X~~				
6	141611	B2-20			9:40				X	~~X X~~				

Collected By: Date 12/28/04 Time 10:00

Relinquished By: Date 12/28 Time 11:08

Relinquished By: C. Clara Date 12/28/04 Time 11:08

Received For Laboratory: Date 12/28/04 Time 11:08

Condition of Sample:

TAT: ☑ Normal ☐ Rush

CHAIN OF CUSTODY RECORD

White - Report, Yellow - Laboratory, Pink - Client

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

COC# № 28230 GLOBAL ID ____________ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 24245

Company:	Rincon Consultants
Address:	
Telephone:	
Fax:	
Special Instruction:	
Project Name:	Buckley School
Site Address:	3900 Stansbury Ave Sherman Oaks, CA
Project ID:	04-17841
Project Manager:	Joe Inch / Tricia
Report To:	Rincon
Address:	
Invoice To:	
Address:	
P.O.#:	04-17841

ANALYSIS REQUESTED

ITEM	LAB USE ONLY Lab ID	SAMPLE DESCRIPTION Sample ID	Date	Time	Container(s) #	Type	Matrix	Preservation	TPH-g, BTEX oxygenates 8260B	TPH-DRO/TPH-ORO 8015M	lead 6010B	VOCs 8260B	metals 6010B/7470A	Remarks
		B3-5	12/27/04	9:55	4	SS sleeve / VOA	Soil / AQ	Methanol / Sodium Bisul						
7	141612	B3-10							X	X				
8	141613	B3-15							X	X				
9	141614	B3-20							X	X	X			
10	141615	B3-25							X	X	X			
11	141616	B3-30							X					[illegible]
		B4-5												
12	141617	B4-10							X					
13	141618	B4-15							X					
14	141619	B4-20			12:30				X					

Collected By:		Date 12/28/04	Time 10:20	Relinquished By:	Date	Time
Relinquished By:	C. Clark	Date 12/28	Time 11:08	Received For Laboratory	Date 12/28/04	Time 11:08
Condition of Sample:						

TAT ☑ Normal ☐ Rush

CHAIN OF CUSTODY RECORD

White - Report, Yellow - Laboratory, Pink - Client

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Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

CHAIN OF CUSTODY RECORD

COC# № 28231 GLOBAL ID ______ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 24245

Company: Rincon Consultants
Address:
Telephone:
Fax:
Special Instruction:

Project Name: Buckley School
Site Address: 3900 Stansbury Ave, Sherman Oaks, CA
Project ID: 04-17841
Project Manager: Joe Inch / Tricia

Report To: Rincon
Address:
Invoice To:
Address:
P.O.#: 04-17841

ANALYSIS REQUESTED: VOCs 8260B; TPH-DRO / TPH-ORO 8015M; Metals 6010B/7470A; PCBs; TPAG BTEX, Oxy (8260B)

ITEM	Lab ID	Sample ID	Date	Time	#	Type	Matrix	Preservation	8260B	8015M	6010B/7470A			Remarks
15	141620	B5-5	12/27/04	1:10	4	SS sleeve / VOA	Soil / AQ	Methanol / Na bisulfate	X	X	X			
16	141621	B5-10							X	X	X			
17	141622	B5-15							X	X	X			
18	141623	B6-5							X	X	X			
19	141624	B6-10							X	X	X			
20	141625	B6-15							X	X	X			
21	141626	B7-5								X				
22	141627	B7-10		2:40						X	X	X		
23	141628	Pool Sump	12/27/04	3:10	4		AQ	—	X	X			X	

Collected By: Date Time
Relinquished By: C. Clark Date 12/28 Time 1108
Condition of Sample:

Relinquished By: Date Time
Received For Laboratory: [signature] Date 12/28/04 Time 1108

TAT: ☑ Normal ☐ Rush

White - Report, Yellow - Laboratory, Pink - Client

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

Page: 2
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8015M/DHSLUFT, TPH DRO AND ORO

Batch No: 010405-2

Our Lab I.D.		141606	141609	141612	141614	141621
Sample ID		B1-10	B1-25	B3-10	B3-20	B5-10
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	12/27/2004
Date Extracted		01/04/2005	01/04/2005	01/04/2005	01/04/2005	01/04/2005
Preparation Method						
Date Analyzed		01/05/2005	01/05/2005	01/05/2005	01/05/2005	01/05/2005
Matrix		Soil	Soil	Soil	Soil	Soil
Units		mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
Detection Limit Multiplier		1	1	1	1	1
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	**Results**
TPH DRO (C13-C22)	10	ND	ND	ND	ND	ND
TPH ORO (C22+)	50	ND	ND	ND	ND	ND

Our Lab I.D.		141606	141609	141612	141614	141621
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**
Surrogate Percent Recovery						
Chlorobenzene	70-120	101	119	120	97	101

QUALITY CONTROL REPORT

Batch No: 010405-2

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Diesel	99	108	8.7	75-120	15					

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Environmental Testing Services
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ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

Page: 3
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8015M/DHSLUFT, TPH DRO AND ORO

Batch No: 010405-2

Our Lab I.D.		**141622**	**141623**	**141624**	**141625**	**141626**
Sample ID		B5-15	B6-5	B6-10	B6-15	B7-5
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	12/27/2004
Date Extracted		01/04/2005	01/04/2005	01/04/2005	01/04/2005	01/04/2005
Preparation Method						
Date Analyzed		01/05/2005	01/05/2005	01/05/2005	01/05/2005	01/05/2005
Matrix		Soil	Soil	Soil	Soil	Soil
Units		mg/kg	mg/kg	mg/kg	mg/kg	mg/kg
Detection Limit Multiplier		1	1	1	1	1
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	**Results**
TPH DRO (C13-C22)	10	ND	ND	ND	ND	ND
TPH ORO (C22+)	50	ND	ND	ND	ND	ND

Our Lab I.D.		**141622**	**141623**	**141624**	**141625**	**141626**
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**
Surrogate Percent Recovery						
Chlorobenzene	70-120	120	100	114	99	118

QUALITY CONTROL REPORT

Batch No: 010405-2

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Diesel	99	108	8.7	75-120	15					

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Environmental Testing Services
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ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

Page: **4**
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8015M/DHSLUFT, TPH DRO AND ORO

Batch No: 010405-2

Our Lab I.D.		**141627**				
Sample ID		B7-10				
Date Sampled		12/27/2004				
Date Extracted		01/04/2005				
Preparation Method						
Date Analyzed		01/05/2005				
Matrix		Soil				
Units		mg/kg				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
TPH DRO (C13-C22)	10	ND				
TPH ORO (C22+)	50	ND				

Our Lab I.D.		**141627**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Chlorobenzene	70-120	120				

QUALITY CONTROL REPORT

Batch No: 010405-2

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Diesel	99	108	8.7	75-120	15					

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
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ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

Page: 5
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8015M/DHSLUFT, TPH DRO AND ORO

Batch No: 010505-1

Our Lab I.D.		141607	141613	141615	141620	
Sample ID		B1-15	B3-15	B3-25	B5-5	
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	
Date Extracted		01/04/2005	01/04/2005	01/04/2005	01/04/2005	
Preparation Method						
Date Analyzed		01/05/2005	01/05/2005	01/05/2005	01/05/2005	
Matrix		Soil	Soil	Soil	Soil	
Units		mg/kg	mg/kg	mg/kg	mg/kg	
Detection Limit Multiplier		1	1	1	1	
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	
TPH DRO (C13-C22)	10	ND	ND	ND	ND	
TPH ORO (C22+)	50	ND	ND	ND	ND	

Our Lab I.D.		141607	141613	141615	141620	
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**	
Surrogate Percent Recovery						
Chlorobenzene	70-120	92	87	88	98	

QUALITY CONTROL REPORT

Batch No: 010505-1

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Diesel	95	99	4.1	75-120	15					

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Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

Page: 6
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8015M/DHSLUFT, TPH as DRO and ORO

Batch No: 010405-2

Our Lab I.D.		**141628**				
Sample ID		Pool Sump				
Date Sampled		12/27/2004				
Date Extracted		01/03/2005				
Preparation Method						
Date Analyzed		01/05/2005				
Matrix		Water				
Units		mg/L				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
TPH DRO (C13-C22)	0.50	ND				
TPH ORO (C22+)	0.50	ND				

Our Lab I.D.		**141628**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Chlorobenzene	70-120	118				

QUALITY CONTROL REPORT

Batch No: 010405-2

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Diesel	99	108	8.7	75-120	15					

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223 9500

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

Page: 7
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010305-1C

Our Lab I.D.		141628				
Sample ID		Pool Sump				
Date Sampled		12/27/2004				
Date Extracted		01/03/2005				
Preparation Method						
Date Analyzed		01/03/2005				
Matrix		Water				
Units		ug/L				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
Acetone	5.00	ND				
Benzene	1.000	ND				
Bromobenzene (Phenyl bromide)	1.000	ND				
Bromochloromethane (Chlorobromomethane)	1.000	ND				
Bromodichloromethane (Dichlorobromomethane)	1.000	ND				
Bromoform (Tribromomethane)	5.000	ND				
Bromomethane (Methyl bromide)	3.000	ND				
2-Butanone (MEK, Methyl ethyl ketone)	5.00	ND				
n-Butylbenzene	1.000	ND				
sec-Butylbenzene	1.000	ND				
tert-Butylbenzene	1.000	ND				
Carbon disulfide	1.000	ND				
Carbon tetrachloride (Tetrachloromethane)	1.000	ND				
Chlorobenzene	1.000	ND				
Chloroethane	3.000	ND				
2-Chloroethyl vinyl ether	5.000	ND				
Chloroform (Trichloromethane)	1.000	ND				
Chloromethane (Methyl chloride)	3.000	ND				
4-Chlorotoluene (p-Chlorotoluene)	1.000	ND				
2-Chlorotoluene (o-Chlorotoluene)	1.000	ND				
1,2-Dibromo-3-chloropropane (DBCP)	5.000	ND				
Dibromochloromethane	1.000	ND				
1,2-Dibromoethane (EDB, Ethylene dibromide)	1.000	ND				
Dibromomethane	1.000	ND				
1,2-Dichlorobenzene (o-Dichlorobenzene)	1.000	ND				
1,3-Dichlorobenzene (m-Dichlorobenzene)	1.000	ND				

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010305-1C

Our Lab I.D.		**141628**				
Sample ID		Pool Sump				
Date Sampled		12/27/2004				
Analytes	**PQL**	**Results**				
1,4-Dichlorobenzene (p-Dichlorobenzene)	1.000	ND				
Dichlorodifluoromethane	3.000	ND				
1,1-Dichloroethane	1.000	ND				
1,2-Dichloroethane	1.000	ND				
1,1-Dichloroethene (1,1-Dichloroethylene)	1.000	ND				
cis-1,2-Dichloroethene	1.000	ND				
trans-1,2-Dichloroethene	1.000	ND				
1,2-Dichloropropane	1.000	ND				
1,3-Dichloropropane	1.000	ND				
2,2-Dichloropropane	1.000	ND				
1,1-Dichloropropene	1.000	ND				
cis-1,3-Dichloropropene	1.000	ND				
trans-1,3-Dichloropropene	1.000	ND				
Ethylbenzene	1.000	ND				
Hexachlorobutadiene (1,3-Hexachlorobutadiene)	3.000	ND				
2-Hexanone	5.000	ND				
Isopropylbenzene	1.000	ND				
p-Isopropyltoluene (4-Isopropyltoluene)	1.000	ND				
MTBE	2.000	ND				
4-Methyl-2-pentanone (MIBK, Methyl isobutyl ketone)	5.00	ND				
Methylene chloride (Dichloromethane, DCM)	5.00	ND				
Naphthalene	1.000	ND				
n-Propylbenzene	1.000	ND				
Styrene	1.000	ND				
1,1,1,2-Tetrachloroethane	1.000	ND				
1,1,2,2-Tetrachloroethane	1.000	ND				
Tetrachloroethene (Tetrachloroethylene)	1.000	ND				
Toluene (Methyl benzene)	1.000	ND				
1,2,3-Trichlorobenzene	1.000	ND				
1,2,4-Trichlorobenzene	1.000	ND				
1,1,1-Trichloroethane	1.000	ND				
1,1,2-Trichloroethane	1.000	ND				
Trichloroethene (TCE)	1.000	ND				
Trichlorofluoromethane	1.000	ND				
1,2,3-Trichloropropane	1.000	ND				
1,2,4-Trimethylbenzene	1.000	ND				
1,3,5-Trimethylbenzene	1.000	ND				
Vinyl acetate	5.00	ND				
Vinyl chloride (Chloroethene)	3.000	ND				
o-Xylene	1.000	ND				
m- & p-Xylenes	2.000	ND				

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ANALYTICAL RESULTS

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Our Lab I.D.		141628				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	116				
Dibromofluoromethane	70-120	117				
Toluene-d8	70-120	106				

QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	102	94	8.2	75-120	15					
Chlorobenzene	97	94	3.1	75-120	15					
1,1-Dichloroethene (1,1-Dichloroethylene)	114	112	1.8	75-120	15					
MTBE	116	108	7.1	75-120	15					
Toluene (Methyl benzene)	107	94	12.9	75-120	15					
Trichloroethene (TCE)	104	98	5.9	75-120	15					

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ANALYTICAL RESULTS

Ordered By

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790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Joe Inch

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010305-1C

Our Lab I.D.		141621	141622	141624	141625	
Sample ID		B5-10	B5-15	B6-10	B6-15	
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	
Date Extracted		01/03/2005	01/03/2005	01/03/2005	01/03/2005	
Preparation Method						
Date Analyzed		01/03/2005	01/03/2005	01/03/2005	01/03/2005	
Matrix		Soil	Soil	Soil	Soil	
Units		ug/kg	ug/kg	ug/kg	ug/kg	
Detection Limit Multiplier		1	1	1	1	
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	
Acetone	50.0	ND	ND	ND	ND	
Benzene	2.00	ND	ND	ND	ND	
Bromobenzene (Phenyl bromide)	10.00	ND	ND	ND	ND	
Bromochloromethane (Chlorobromomethane)	10.00	ND	ND	ND	ND	
Bromodichloromethane (Dichlorobromomethane)	10.00	ND	ND	ND	ND	
Bromoform (Tribromomethane)	50.00	ND	ND	ND	ND	
Bromomethane (Methyl bromide)	30.00	ND	ND	ND	ND	
2-Butanone (MEK, Methyl ethyl ketone)	50.00	ND	ND	ND	ND	
n-Butylbenzene	10.00	ND	ND	ND	ND	
sec-Butylbenzene	10.00	ND	ND	ND	ND	
tert-Butylbenzene	10.00	ND	ND	ND	ND	
Carbon disulfide	10.00	ND	ND	ND	ND	
Carbon tetrachloride (Tetrachloromethane)	10.00	ND	ND	ND	ND	
Chlorobenzene	10.00	ND	ND	ND	ND	
Chloroethane	30.00	ND	ND	ND	ND	
2-Chloroethyl vinyl ether	50.00	ND	ND	ND	ND	
Chloroform (Trichloromethane)	10.00	ND	ND	ND	ND	
Chloromethane (Methyl chloride)	30.00	ND	ND	ND	ND	
4-Chlorotoluene (p-Chlorotoluene)	10.00	ND	ND	ND	ND	
2-Chlorotoluene (o-Chlorotoluene)	10.00	ND	ND	ND	ND	
1,2-Dibromo-3-chloropropane (DBCP)	50.00	ND	ND	ND	ND	
Dibromochloromethane	10.00	ND	ND	ND	ND	
1,2-Dibromoethane (EDB, Ethylene dibromide)	10.00	ND	ND	ND	ND	
Dibromomethane	10.00	ND	ND	ND	ND	
1,2-Dichlorobenzene (o-Dichlorobenzene)	10.00	ND	ND	ND	ND	
1,3-Dichlorobenzene (m-Dichlorobenzene)	10.00	ND	ND	ND	ND	

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Environmental Testing Services
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ANALYTICAL RESULTS

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010305-1C

Our Lab I.D.		141621	141622	141624	141625	
Sample ID		B5-10	B5-15	B6-10	B6-15	
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	
1,4-Dichlorobenzene (p-Dichlorobenzene)	10.00	ND	ND	ND	ND	
Dichlorodifluoromethane	30.00	ND	ND	ND	ND	
1,1-Dichloroethane	10.00	ND	ND	ND	ND	
1,2-Dichloroethane	10.00	ND	ND	ND	ND	
1,1-Dichloroethene (1,1-Dichloroethylene)	10.00	ND	ND	ND	ND	
cis-1,2-Dichloroethene	10.00	ND	ND	ND	ND	
trans-1,2-Dichloroethene	10.00	ND	ND	ND	ND	
1,2-Dichloropropane	10.00	ND	ND	ND	ND	
1,3-Dichloropropane	10.00	ND	ND	ND	ND	
2,2-Dichloropropane	10.00	ND	ND	ND	ND	
1,1-Dichloropropene	10.00	ND	ND	ND	ND	
cis-1,3-Dichloropropene	10.00	ND	ND	ND	ND	
trans-1,3-Dichloropropene	10.00	ND	ND	ND	ND	
Ethylbenzene	2.00	ND	ND	ND	ND	
Hexachlorobutadiene (1,3-Hexachlorobutadiene)	30.00	ND	ND	ND	ND	
2-Hexanone	50.00	ND	ND	ND	ND	
Isopropylbenzene	10.00	ND	ND	ND	ND	
p-Isopropyltoluene (4-Isopropyltoluene)	10.00	ND	ND	ND	ND	
MTBE	5.00	ND	ND	ND	ND	
4-Methyl-2-pentanone (MIBK, Methyl isobutyl ketone)	50.00	ND	ND	ND	ND	
Methylene chloride (Dichloromethane, DCM)	50.00	ND	ND	ND	ND	
Naphthalene	10.00	ND	ND	ND	ND	
n-Propylbenzene	10.00	ND	ND	ND	ND	
Styrene	10.00	ND	ND	ND	ND	
1,1,1,2-Tetrachloroethane	10.00	ND	ND	ND	ND	
1,1,2,2-Tetrachloroethane	10.00	ND	ND	ND	ND	
Tetrachloroethene (Tetrachloroethylene)	10.00	ND	ND	ND	ND	
Toluene (Methyl benzene)	2.00	ND	ND	ND	ND	
1,2,3-Trichlorobenzene	10.00	ND	ND	ND	ND	
1,2,4-Trichlorobenzene	10.00	ND	ND	ND	ND	
1,1,1-Trichloroethane	10.00	ND	ND	ND	ND	
1,1,2-Trichloroethane	10.00	ND	ND	ND	ND	
Trichloroethene (TCE)	10.00	ND	ND	ND	ND	
Trichlorofluoromethane	10.00	ND	ND	ND	ND	
1,2,3-Trichloropropane	10.00	ND	ND	ND	ND	
1,2,4-Trimethylbenzene	10.00	ND	ND	ND	ND	
1,3,5-Trimethylbenzene	10.00	ND	ND	ND	ND	
Vinyl acetate	50.0	ND	ND	ND	ND	
Vinyl chloride (Chloroethene)	30.00	ND	ND	ND	ND	
o-Xylene	2.00	ND	ND	ND	ND	
m- & p-Xylenes	4.00	ND	ND	ND	ND	

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ANALYTICAL RESULTS

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Our Lab I.D.		141621	141622	141624	141625	
Surrogates	Con.Limit	% Rec.	% Rec.	% Rec.	% Rec.	
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	118	117	118	119	
Dibromofluoromethane	70-120	105	112	116	106	
Toluene-d8	70-120	104	108	108	106	

QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	102	94	8.2	75-120	15					
Chlorobenzene	97	94	3.1	75-120	15					
1,1-Dichloroethene (1,1-Dichloroethylene)	114	112	1.8	75-120	15					
MTBE	116	108	7.1	75-120	15					
Toluene (Methyl benzene)	107	94	12.9	75-120	15					
Trichloroethene (TCE)	104	98	5.9	75-120	15					

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ANALYTICAL RESULTS

Ordered By

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010405-1C

Our Lab I.D.		141620	141623			
Sample ID		B5-5	B6-5			
Date Sampled		12/27/2004	12/27/2004			
Date Extracted		01/04/2005	01/04/2005			
Preparation Method						
Date Analyzed		01/04/2005	01/04/2005			
Matrix		Soil	Soil			
Units		ug/kg	ug/kg			
Detection Limit Multiplier		1	1			
Analytes	**PQL**	**Results**	**Results**			
Acetone	50.0	106	120			
Benzene	2.00	ND	ND			
Bromobenzene (Phenyl bromide)	10.00	ND	ND			
Bromochloromethane (Chlorobromomethane)	10.00	ND	ND			
Bromodichloromethane (Dichlorobromomethane)	10.00	ND	ND			
Bromoform (Tribromomethane)	50.00	ND	ND			
Bromomethane (Methyl bromide)	30.00	ND	ND			
2-Butanone (MEK, Methyl ethyl ketone)	50.00	ND	ND			
n-Butylbenzene	10.00	ND	ND			
sec-Butylbenzene	10.00	ND	ND			
tert-Butylbenzene	10.00	ND	ND			
Carbon disulfide	10.00	ND	ND			
Carbon tetrachloride (Tetrachloromethane)	10.00	ND	ND			
Chlorobenzene	10.00	ND	ND			
Chloroethane	30.00	ND	ND			
2-Chloroethyl vinyl ether	50.00	ND	ND			
Chloroform (Trichloromethane)	10.00	ND	ND			
Chloromethane (Methyl chloride)	30.00	ND	ND			
4-Chlorotoluene (p-Chlorotoluene)	10.00	ND	ND			
2-Chlorotoluene (o-Chlorotoluene)	10.00	ND	ND			
1,2-Dibromo-3-chloropropane (DBCP)	50.00	ND	ND			
Dibromochloromethane	10.00	ND	ND			
1,2-Dibromoethane (EDB, Ethylene dibromide)	10.00	ND	ND			
Dibromomethane	10.00	ND	ND			
1,2-Dichlorobenzene (o-Dichlorobenzene)	10.00	ND	ND			
1,3-Dichlorobenzene (m-Dichlorobenzene)	10.00	ND	ND			

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010405-1C

Our Lab I.D.		**141620**	**141623**			
Sample ID		B5-5	B6-5			
Date Sampled		12/27/2004	12/27/2004			
Analytes	**PQL**	**Results**	**Results**			
1,4-Dichlorobenzene (p-Dichlorobenzene)	10.00	ND	ND			
Dichlorodifluoromethane	30.00	ND	ND			
1,1-Dichloroethane	10.00	ND	ND			
1,2-Dichloroethane	10.00	ND	ND			
1,1-Dichloroethene (1,1-Dichloroethylene)	10.00	ND	ND			
cis-1,2-Dichloroethene	10.00	ND	ND			
trans-1,2-Dichloroethene	10.00	ND	ND			
1,2-Dichloropropane	10.00	ND	ND			
1,3-Dichloropropane	10.00	ND	ND			
2,2-Dichloropropane	10.00	ND	ND			
1,1-Dichloropropene	10.00	ND	ND			
cis-1,3-Dichloropropene	10.00	ND	ND			
trans-1,3-Dichloropropene	10.00	ND	ND			
Ethylbenzene	2.00	ND	ND			
Hexachlorobutadiene (1,3-Hexachlorobutadiene)	30.00	ND	ND			
2-Hexanone	50.00	ND	ND			
Isopropylbenzene	10.00	ND	ND			
p-Isopropyltoluene (4-Isopropyltoluene)	10.00	ND	ND			
MTBE	5.00	ND	ND			
4-Methyl-2-pentanone (MIBK, Methyl isobutyl ketone)	50.00	ND	ND			
Methylene chloride (Dichloromethane, DCM)	50.00	ND	ND			
Naphthalene	10.00	ND	ND			
n-Propylbenzene	10.00	ND	ND			
Styrene	10.00	ND	ND			
1,1,1,2-Tetrachloroethane	10.00	ND	ND			
1,1,2,2-Tetrachloroethane	10.00	ND	ND			
Tetrachloroethene (Tetrachloroethylene)	10.00	18	27			
Toluene (Methyl benzene)	2.00	ND	ND			
1,2,3-Trichlorobenzene	10.00	ND	ND			
1,2,4-Trichlorobenzene	10.00	ND	ND			
1,1,1-Trichloroethane	10.00	ND	ND			
1,1,2-Trichloroethane	10.00	ND	ND			
Trichloroethene (TCE)	10.00	ND	ND			
Trichlorofluoromethane	10.00	ND	ND			
1,2,3-Trichloropropane	10.00	ND	ND			
1,2,4-Trimethylbenzene	10.00	ND	ND			
1,3,5-Trimethylbenzene	10.00	ND	ND			
Vinyl acetate	50.0	ND	ND			
Vinyl chloride (Chloroethene)	30.00	ND	ND			
o-Xylene	2.00	ND	ND			
m- & p-Xylenes	4.00	ND	ND			

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ANALYTICAL RESULTS

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Volatile Organic Compounds

Our Lab I.D.		141620	141623			
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**			
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	108	114			
Dibromofluoromethane	70-120	102	103			
Toluene-d8	70-120	100	98			

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	114	104	9.2	75-120	15					
Chlorobenzene	106	101	4.8	75-120	15					
1,1-Dichloroethene (1,1-Dichloroethylene)	118	106	10.7	75-120	15					
MTBE	120	112	6.9	75-120	15					
Toluene (Methyl benzene)	114	103	10.1	75-120	15					
Trichloroethene (TCE)	106	100	5.8	75-120	15					

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ANALYTICAL RESULTS

Ordered By

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790 East Santa Clara Street
Ventura, CA 93001

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010305-1C

Our Lab I.D.		141606	141607	141610	141611	141613
Sample ID		B1-10	B1-15	B2-15	B2-20	B3-15
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	12/27/2004
Date Extracted		01/03/2005	01/03/2005	01/03/2005	01/03/2005	01/03/2005
Preparation Method						
Date Analyzed		01/03/2005	01/03/2005	01/03/2005	01/03/2005	01/03/2005
Matrix		Soil	Soil	Soil	Soil	Soil
Units		ug/kg	ug/kg	ug/kg	ug/kg	ug/kg
Detection Limit Multiplier		1	1	1	1	1
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	**Results**
Benzene	2.00	2	ND	2	ND	7
DIPE	5.00	ND	ND	ND	ND	ND
ETBE	5.0	ND	ND	ND	ND	ND
Ethylbenzene	2.00	ND	ND	ND	ND	ND
MTBE	5.00	ND	ND	ND	ND	206
TAME	5.00	ND	ND	ND	ND	ND
TBA	20	ND	ND	ND	ND	320
Toluene (Methyl benzene)	2.00	2	ND	ND	ND	3
o-Xylene	2.00	ND	ND	ND	ND	ND
m- & p-Xylenes	4.0	ND	ND	ND	ND	ND
TPH as Gasoline (C4-C12)	500	ND	ND	ND	ND	646

Our Lab I.D.		141606	141607	141610	141611	141613
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	120	120	119	114	118
Dibromofluoromethane	70-120	114	110	116	120	116
Toluene-d8	70-120	104	107	106	106	106

QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	102	94	8.2	75-120	15					

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ANALYTICAL RESULTS

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates
QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	116	108	7.1	75-120	15					
Toluene (Methyl benzene)	107	94	12.9	75-120	15					

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ANALYTICAL RESULTS

Ordered By	Site
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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010305-1C

Our Lab I.D.		141616	141617			
Sample ID		B3-30	B4-10			
Date Sampled		12/27/2004	12/27/2004			
Date Extracted		01/03/2005	01/03/2005			
Preparation Method						
Date Analyzed		01/03/2005	01/03/2005			
Matrix		Soil	Soil			
Units		ug/kg	ug/kg			
Detection Limit Multiplier		1	1			
Analytes	**PQL**	**Results**	**Results**			
Benzene	2.00	13	ND			
DIPE	5.00	ND	ND			
ETBE	5.0	ND	ND			
Ethylbenzene	2.00	53	ND			
MTBE	5.00	1050	129			
TAME	5.00	ND	ND			
TBA	20	302	392			
Toluene (Methyl benzene)	2.00	ND	2			
o-Xylene	2.00	18	ND			
m- & p-Xylenes	4.0	36	ND			
TPH as Gasoline (C4-C12)	500	1930	550			

Our Lab I.D.		141616	141617			
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**			
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	114	120			
Dibromofluoromethane	70-120	115	96			
Toluene-d8	70-120	108	100			

QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	102	94	8.2	75-120	15					

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ANALYTICAL RESULTS

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	116	108	7.1	75-120	15					
Toluene (Methyl benzene)	107	94	12.9	75-120	15					

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ANALYTICAL RESULTS

Ordered By

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Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010305-2C

Our Lab I.D.		**141615**	**141619**			
Sample ID		B3-25	B4-20			
Date Sampled		12/27/2004	12/27/2004			
Date Extracted		01/03/2005	01/03/2005			
Preparation Method						
Date Analyzed		01/04/2005	01/04/2005			
Matrix		Soil	Soil			
Units		ug/kg	ug/kg			
Detection Limit Multiplier		5	5			
Analytes	**PQL**	**Results**	**Results**			
Benzene	10	295	27			
DIPE	25	ND	ND			
ETBE	25	ND	ND			
Ethylbenzene	10	670	53			
MTBE	25	2740	6950			
TAME	25	ND	ND			
TBA	100	ND	ND			
Toluene (Methyl benzene)	10	1980	54			
o-Xylene	10	1090	75			
m- & p-Xylenes	20	2700	170			
TPH as Gasoline (C4-C12)	2500	28500	10200			

Our Lab I.D.		**141615**	**141619**			
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**			
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	109	108			
Dibromofluoromethane	70-120	106	104			
Toluene-d8	70-120	105	105			

QUALITY CONTROL REPORT

Batch No: 010305-2C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit						
Benzene	102	92	10.3	75-120	15						

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 010305-2C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	99	96	3.1	75-120	15					
Toluene (Methyl benzene)	102	94	8.2	75-120	15					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010405-1C

Our Lab I.D.		141608	141614			
Sample ID		B1-20	B3-20			
Date Sampled		12/27/2004	12/27/2004			
Date Extracted		01/04/2005	01/04/2005			
Preparation Method						
Date Analyzed		01/04/2005	01/04/2005			
Matrix		Soil	Soil			
Units		ug/kg	ug/kg			
Detection Limit Multiplier		1	1			
Analytes	**PQL**	**Results**	**Results**			
Benzene	2.00	32	70			
DIPE	5.00	ND	ND			
ETBE	5.0	ND	ND			
Ethylbenzene	2.00	24	19			
MTBE	5.00	816	1050			
TAME	5.00	ND	ND			
TBA	20	798	792			
Toluene (Methyl benzene)	2.00	90	ND			
o-Xylene	2.00	67	ND			
m- & p-Xylenes	4.0	128	ND			
TPH as Gasoline (C4-C12)	500	2050	2550			

Our Lab I.D.		141608	141614			
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**			
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	108	106			
Dibromofluoromethane	70-120	106	108			
Toluene-d8	70-120	102	100			

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	114	104	9.2	75-120	15					

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24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	120	112	6.9	75-120	15					
Toluene (Methyl benzene)	114	103	10.1	75-120	15					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010405-1C

Our Lab I.D.		**141612**				
Sample ID		B3-10				
Date Sampled		12/27/2004				
Date Extracted		01/04/2005				
Preparation Method						
Date Analyzed		01/04/2005				
Matrix		Soil				
Units		ug/kg				
Detection Limit Multiplier		5				
Analytes	**PQL**	**Results**				
Benzene	10	ND				
DIPE	25	ND				
ETBE	25	ND				
Ethylbenzene	10	ND				
MTBE	25	ND				
TAME	25	ND				
TBA	100	ND				
Toluene (Methyl benzene)	10	ND				
o-Xylene	10	ND				
m- & p-Xylenes	20	ND				
TPH as Gasoline (C4-C12)	2500	93400				

Our Lab I.D.		**141612**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	116				
Dibromofluoromethane	70-120	99				
Toluene-d8	70-120	102				

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	114	104	9.2	75-120	15					

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Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	120	112	6.9	75-120	15					
Toluene (Methyl benzene)	114	103	10.1	75-120	15					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010405-1C

Our Lab I.D.		**141609**				
Sample ID		B1-25				
Date Sampled		12/27/2004				
Date Extracted		01/04/2005				
Preparation Method						
Date Analyzed		01/04/2005				
Matrix		Soil				
Units		ug/kg				
Detection Limit Multiplier		100				
Analytes	**PQL**	**Results**				
Benzene	200	8400				
DIPE	500	ND				
ETBE	500	ND				
Ethylbenzene	200	13700				
MTBE	500	3130				
TAME	500	ND				
TBA	2000	ND				
Toluene (Methyl benzene)	200	31000				
o-Xylene	200	32000				
m- & p-Xylenes	400	72200				
TPH as Gasoline (C4-C12)	50000	1080000				

Our Lab I.D.		**141609**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	105				
Dibromofluoromethane	70-120	101				
Toluene-d8	70-120	100				

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	114	104	9.2	75-120	15					

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Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	120	112	6.9	75-120	15					
Toluene (Methyl benzene)	114	103	10.1	75-120	15					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 010505-1C

Our Lab I.D.		**141618**				
Sample ID		B4-15				
Date Sampled		12/27/2004				
Date Extracted		01/05/2005				
Preparation Method						
Date Analyzed		01/05/2005				
Matrix		Soil				
Units		ug/kg				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
Benzene	2.00	4				
DIPE	5.00	ND				
ETBE	5.0	ND				
Ethylbenzene	2.00	ND				
MTBE	5.00	1270				
TAME	5.00	ND				
TBA	20	346				
Toluene (Methyl benzene)	2.00	2				
o-Xylene	2.00	ND				
m- & p-Xylenes	4.0	ND				
TPH as Gasoline (C4-C12)	500	2020				

Our Lab I.D.		**141618**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	106				
Dibromofluoromethane	70-120	99				
Toluene-d8	70-120	102				

QUALITY CONTROL REPORT

Batch No: 010505-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	113	113	<1	75-120	15					

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Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 010505-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	120	109	9.6	75-120	15					
Toluene (Methyl benzene)	109	114	4.5	75-120	15					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8260B, TPH as Gas

Batch No: 010305-1C

Our Lab I.D.		141628				
Sample ID		Pool Sump				
Date Sampled		12/27/2004				
Date Extracted		01/03/2005				
Preparation Method						
Date Analyzed		01/03/2005				
Matrix		Water				
Units		ug/L				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
TPH as Gasoline (C4-C12)	50	ND				

Our Lab I.D.		141628				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	116				
Dibromofluoromethane	70-120	117				
Toluene-d8	70-120	106				

QUALITY CONTROL REPORT

Batch No: 010305-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	102	94	8.2	75-120	15					
Chlorobenzene	97	94	3.1	75-120	15					
1,1-Dichloroethene (1,1-Dichloroethylene)	114	112	1.8	75-120	15					
Toluene (Methyl benzene)	107	94	12.9	75-120	15					
Trichloroethene (TCE)	104	98	5.9	75-120	15					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 8082, Polychlorinated Biphenyls(PCBs) by Gas Chromatography

Batch No:

Our Lab I.D.		**141627**				
Sample ID		B7-10				
Date Sampled		12/27/2004				
Date Extracted		12/30/2004				
Preparation Method						
Date Analyzed		12/30/2004				
Matrix		Soil				
Units		ug/kg				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
Aroclor-1016 (PCB-1016)	33.00	ND				
Aroclor-1221 (PCB-1221)	67.00	ND				
Aroclor-1232 (PCB-1232)	33.00	ND				
Aroclor-1242 (PCB-1242)	33.00	ND				
Aroclor-1248 (PCB-1248)	33.00	ND				
Aroclor-1254 (PCB-1254)	33.00	ND				
Aroclor-1260 (PCB-1260)	33.00	ND				

Our Lab I.D.		**141627**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Decachlorobiphenyl	43-169	114				

QUALITY CONTROL REPORT

Batch No:

Analytes	LCS % REC	LCS DUP % REC	LCS RPD % REC	LCS/LCSD % Limit	LCS RPD % Limit					
Aroclor-1260 (PCB-1260)	102	95	7.1	39-150	<30					

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Job Number	Order Date	Client
24245	12/28/2004	RINCON

Method: 6010B/7471A, CCR Title 22 Metals (TTLC)

Our Lab I.D.		**141620**	**141621**	**141622**	**141623**	**141624**
Sample ID		B5-5	B5-10	B5-15	B6-5	B6-10
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	12/27/2004
Date Extracted		01/04/2005	01/04/2005	01/04/2005	01/04/2005	01/04/2005
Preparation Method						
Date Analyzed		01/04/2005	01/04/2005	01/04/2005	01/04/2005	01/04/2005
Matrix		Soil	Soil	Soil	Soil	Soil
Units		mg/Kg	mg/Kg	mg/Kg	mg/Kg	mg/Kg
Detection Limit Multiplier		1	1	1	1	1
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	**Results**
AA Metals						
Mercury	0.20	ND	ND	ND	ND	ND
ICP Metals						
Antimony	0.50	1.03	ND	0.51	0.90	1.03
Arsenic	0.25	11.8	3.14	6.45	12.2	9.51
Barium	0.50	155	72.1	138	178	222
Beryllium	0.50	ND	ND	ND	ND	ND
Cadmium	0.50	0.50	0.91	1.88	0.57	1.72
Chromium	0.50	34.5	16.2	12.2	35.0	27.5
Cobalt	0.50	10.3	4.73	3.40	13.7	7.87
Copper	0.50	24.0	29.1	15.5	26.5	23.7
Lead	0.25	4.63	0.74	ND	4.25	2.31
Molybdenum	0.50	0.68	3.00	5.14	0.74	1.06
Nickel	0.50	25.6	38.9	22.3	28.6	26.6
Selenium	0.50	ND	ND	ND	ND	ND
Silver	0.50	ND	ND	ND	ND	ND
Thallium	0.50	ND	ND	ND	ND	ND
Vanadium	0.50	60.1	66.5	66.6	62.4	57.6
Zinc	0.50	55.9	69.3	47.3	61.0	57.7

QUALITY CONTROL REPORT

Analytes	LCS % REC	LCS/LCSD % Limit								
AA Metals										
Mercury	108	80-120								
ICP Metals										
Antimony	87	80-120								

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Method: 6010B/7471A, CCR Title 22 Metals (TTLC)

QUALITY CONTROL REPORT

Analytes	LCS % REC	LCS/LCSD % Limit								
ICP Metals										
Arsenic	89	80-120								
Barium	87	80-120								
Beryllium	91	80-120								
Cadmium	90	80-120								
Chromium	86	80-120								
Cobalt	91	80-120								
Copper	88	80-120								
Lead	85	80-120								
Molybdenum	85	80-120								
Nickel	92	80-120								
Selenium	89	80-120								
Silver	89	80-120								
Thallium	85	80-120								
Vanadium	87	80-120								
Zinc	92	80-120								

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24245	12/28/2004	RINCON

Method: 6010B/7471A, CCR Title 22 Metals (TTLC)

Our Lab I.D.		**141625**	**141627**			
Sample ID		B6-15	B7-10			
Date Sampled		12/27/2004	12/27/2004			
Date Extracted		01/04/2005	01/04/2005			
Preparation Method						
Date Analyzed		01/04/2005	01/04/2005			
Matrix		Soil	Soil			
Units		mg/Kg	mg/Kg			
Detection Limit Multiplier		1	1			
Analytes	**PQL**	**Results**	**Results**			
AA Metals						
Mercury	0.20	ND	ND			
ICP Metals						
Antimony	0.50	0.64	ND			
Arsenic	0.25	6.67	14.1			
Barium	0.50	113	50.8			
Beryllium	0.50	ND	ND			
Cadmium	0.50	2.76	1.24			
Chromium	0.50	23.9	11.3			
Cobalt	0.50	2.48	4.26			
Copper	0.50	20.0	17.5			
Lead	0.25	ND	0.58			
Molybdenum	0.50	5.61	3.82			
Nickel	0.50	29.7	24.2			
Selenium	0.50	ND	ND			
Silver	0.50	ND	ND			
Thallium	0.50	ND	ND			
Vanadium	0.50	76.6	71.5			
Zinc	0.50	60.4	36.0			

QUALITY CONTROL REPORT

Analytes	LCS % REC	LCS/LCSD % Limit								
AA Metals										
Mercury	108	80-120								
ICP Metals										
Antimony	87	80-120								

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Method: 6010B/7471A, CCR Title 22 Metals (TTLC)

QUALITY CONTROL REPORT

Analytes	LCS % REC	LCS/LCSD % Limit							
ICP Metals									
Arsenic	89	80-120							
Barium	87	80-120							
Beryllium	91	80-120							
Cadmium	90	80-120							
Chromium	86	80-120							
Cobalt	91	80-120							
Copper	88	80-120							
Lead	85	80-120							
Molybdenum	85	80-120							
Nickel	92	80-120							
Selenium	89	80-120							
Silver	89	80-120							
Thallium	85	80-120							
Vanadium	87	80-120							
Zinc	92	80-120							

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24245	12/28/2004	RINCON

Method: 6010B, Lead (ICP)

Batch No:

Our Lab I.D.		**141607**	**141608**	**141609**	**141614**	**141615**
Sample ID		B1-15	B1-20	B1-25	B3-20	B3-25
Date Sampled		12/27/2004	12/27/2004	12/27/2004	12/27/2004	12/27/2004
Date Extracted		01/04/2005	01/04/2005	01/04/2005	01/04/2005	01/04/2005
Preparation Method						
Date Analyzed		01/04/2005	01/04/2005	01/04/2005	01/04/2005	01/04/2005
Matrix		Soil	Soil	Soil	Soil	Soil
Units		mg/Kg	mg/Kg	mg/Kg	mg/Kg	mg/Kg
Detection Limit Multiplier		1	1	1	1	1
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	**Results**
ICP Metals						
Lead	0.25	1.40	2.14	ND	1.40	1.91

QUALITY CONTROL REPORT

Batch No:

Analytes	LCS % REC	LCS/LCSD % Limit								
ICP Metals										
Lead	85	80-120								

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Attn Tricia Bartholome

Job Number	Ordered	Client
24280	01/03/2005	RINCON

Project ID: 04-17841
Project Name: Buckley School
Site: 3900 Stansbury Ave.
Sherman Oaks, CA

Enclosed are the results of analyses on 3 samples analyzed as specified on attached chain of custody.

Amolk MOLKY Brar
Laboratory Manager

Rojert G. Araghi
Laboratory Director

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

COC# № 28232 GLOBAL ID ______ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 24280

CHAIN OF CUSTODY RECORD

Company: Rincon Consultants
Address: 790 E. Santa Clara, Ventura CA 93001
Telephone: (805) 641-1000
Fax: -1072
Special Instruction:

Project Name: Buckley School
Site Address: 3900 Stansbury Ave, Sherman Oaks, CA
Project ID: 04-17841
Project Manager: Tricia

Report To: Rincon
Address:
Invoice To:
Address:
P.O.#: 04-17841

ANALYSIS REQUESTED: TPH-DRO/ORO (8015M), PCBs (8080), VOCs (8260B), metals (6010B/7470A)

ITEM	Lab ID	Sample ID	Date	Time	#	Type	Matrix	Preservation	8015M	8080	8260B	6010B/7470A	Remarks
		B8-5	12/30/04		1	liner	soil	—					HOLD
		B8-5			3	VOAs		1 methanol 2 NaHSO4					↓
1	141805	B8-9			1	liner		—	X	X			
		B8-9			3	VOAs		1 methanol 2 NaHSO4					HOLD
		B9-8			1	liner		—					
		B9-8			3	VOAs		1 methanol 2 NaHSO4					↓
2	141806	B9-10			1	liner		—	X			X	
		B9-10			3	VOAs		1 methanol 2 NaHSO4			X		
		B10-5			1	liner		—					HOLD
		B10-5			3	VOAs		1 methanol 2 NaHSO4					↓

Collected By: Tricia Carsaleta (For Joe Irch) Date 12/30/04 Time
Relinquished By: Tricia Carsaleta Date 1/3/05 Time 1043
Relinquished By: Date Time
Received For Laboratory: Moser Date 1-3-05 Time 1043
TAT: ☒ Normal ☐ Rush
Condition of Sample:

White - Report, Yellow - Laboratory, Pink - Client

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COC# № 28233 GLOBAL ID ______ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 24280

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Project ID: 04-17841
Project Manager: Tricia

Report To: Rincon
Address:
Invoice To:
Address:
P.O.#: 04-17841

ANALYSIS REQUESTED: TPH-DRO/ORO (8015M); VOCs (8260B); metals (6010B/7470A)

ITEM	Lab ID	Sample ID	Date	Time	#	Type	Matrix	Preservation	8015M TPH-DRO/ORO	8260B VOCs	6010B/7470A metals									Remarks
3	141807	B10-10	12/30/04		1	liner	soil	—	X		X									
		B10-10	"		3	VOAs	"	1 methanol 2 NaHSO4		X										

Collected By: [signature] Date 12/30/04 Time
Relinquished By: [signature] Date 1/3/05 Time 1040
Condition of Sample:

Relinquished By: Date Time
Received For Laboratory: Moses Date 1-3-05 Time 1043

TAT ☑ Normal ☐ Rush

White - Report, Yellow - Laboratory, Pink - Client

CHAIN OF CUSTODY RECORD

AMERICAN SCIENTIFIC LABORATORIES, LLC

2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Ordered By	Site
Rincon Consultants, Inc. 790 East Santa Clara Street Ventura, CA 93001	3900 Stansbury Ave. Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Tricia Bartholome

Page: 2
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 8015M/DHSLUFT, TPH DRO AND ORO

Batch No: 010605-2

Our Lab I.D.		141805	141806	141807		
Sample ID		B8-9	B9-10	B10-10		
Date Sampled		12/30/2004	12/30/2004	12/30/2004		
Date Extracted		01/04/2005	01/04/2005	01/04/2005		
Preparation Method						
Date Analyzed		01/07/2005	01/07/2005	01/07/2005		
Matrix		Soil	Soil	Soil		
Units		mg/kg	mg/kg	mg/kg		
Detection Limit Multiplier		1	1	1		
Analytes	**PQL**	**Results**	**Results**	**Results**		
TPH DRO (C13-C22)	10	ND	ND	ND		
TPH ORO (C22+)	50	ND	ND	ND		

Our Lab I.D.		141805	141806	141807		
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**	**% Rec.**		
Surrogate Percent Recovery						
Chlorobenzene	70-120	91	87	84		

QUALITY CONTROL REPORT

Batch No: 010605-2

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Diesel	105	100	4.9	75-120	15					

AMERICAN SCIENTIFIC LABORATORIES, LLC

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Tricia Bartholome

Page: 3
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010405-1C

Our Lab I.D.		**141806**	**141807**		
Sample ID		B9-10	B10-10		
Date Sampled		12/30/2004	12/30/2004		
Date Extracted		01/04/2005	01/04/2005		
Preparation Method					
Date Analyzed		01/04/2005	01/04/2005		
Matrix		Soil	Soil		
Units		ug/kg	ug/kg		
Detection Limit Multiplier		1	1		
Analytes	**PQL**	**Results**	**Results**		
Acetone	50.0	ND	ND		
Benzene	2.00	ND	ND		
Bromobenzene (Phenyl bromide)	10.00	ND	ND		
Bromochloromethane (Chlorobromomethane)	10.00	ND	ND		
Bromodichloromethane (Dichlorobromomethane)	10.00	ND	ND		
Bromoform (Tribromomethane)	50.00	ND	ND		
Bromomethane (Methyl bromide)	30.00	ND	ND		
2-Butanone (MEK, Methyl ethyl ketone)	50.00	ND	ND		
n-Butylbenzene	10.00	ND	ND		
sec-Butylbenzene	10.00	ND	ND		
tert-Butylbenzene	10.00	ND	ND		
Carbon disulfide	10.00	ND	ND		
Carbon tetrachloride (Tetrachloromethane)	10.00	ND	ND		
Chlorobenzene	10.00	ND	ND		
Chloroethane	30.00	ND	ND		
2-Chloroethyl vinyl ether	50.00	ND	ND		
Chloroform (Trichloromethane)	10.00	ND	ND		
Chloromethane (Methyl chloride)	30.00	ND	ND		
4-Chlorotoluene (p-Chlorotoluene)	10.00	ND	ND		
2-Chlorotoluene (o-Chlorotoluene)	10.00	ND	ND		
1,2-Dibromo-3-chloropropane (DBCP)	50.00	ND	ND		
Dibromochloromethane	10.00	ND	ND		
1,2-Dibromoethane (EDB, Ethylene dibromide)	10.00	ND	ND		
Dibromomethane	10.00	ND	ND		
1,2-Dichlorobenzene (o-Dichlorobenzene)	10.00	ND	ND		
1,3-Dichlorobenzene (m-Dichlorobenzene)	10.00	ND	ND		

ANALYTICAL RESULTS

Page: 4
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 8260B, Volatile Organic Compounds

Batch No: 010405-1C

Our Lab I.D.		141806	141807			
Sample ID		B9-10	B10-10			
Date Sampled		12/30/2004	12/30/2004			
Analytes	**PQL**	**Results**	**Results**			
1,4-Dichlorobenzene (p-Dichlorobenzene)	10.00	ND	ND			
Dichlorodifluoromethane	30.00	ND	ND			
1,1-Dichloroethane	10.00	ND	ND			
1,2-Dichloroethane	10.00	ND	ND			
1,1-Dichloroethene (1,1-Dichloroethylene)	10.00	ND	ND			
cis-1,2-Dichloroethene	10.00	ND	ND			
trans-1,2-Dichloroethene	10.00	ND	ND			
1,2-Dichloropropane	10.00	ND	ND			
1,3-Dichloropropane	10.00	ND	ND			
2,2-Dichloropropane	10.00	ND	ND			
1,1-Dichloropropene	10.00	ND	ND			
cis-1,3-Dichloropropene	10.00	ND	ND			
trans-1,3-Dichloropropene	10.00	ND	ND			
Ethylbenzene	2.00	4	3			
Hexachlorobutadiene (1,3-Hexachlorobutadiene)	30.00	ND	ND			
2-Hexanone	50.00	ND	ND			
Isopropylbenzene	10.00	ND	ND			
p-Isopropyltoluene (4-Isopropyltoluene)	10.00	ND	ND			
MTBE	5.00	ND	ND			
4-Methyl-2-pentanone (MIBK, Methyl isobutyl ketone)	50.00	ND	ND			
Methylene chloride (Dichloromethane, DCM)	50.00	ND	ND			
Naphthalene	10.00	ND	ND			
n-Propylbenzene	10.00	ND	ND			
Styrene	10.00	ND	ND			
1,1,1,2-Tetrachloroethane	10.00	ND	ND			
1,1,2,2-Tetrachloroethane	10.00	ND	ND			
Tetrachloroethene (Tetrachloroethylene)	10.00	ND	ND			
Toluene (Methyl benzene)	2.00	ND	ND			
1,2,3-Trichlorobenzene	10.00	ND	ND			
1,2,4-Trichlorobenzene	10.00	ND	ND			
1,1,1-Trichloroethane	10.00	ND	ND			
1,1,2-Trichloroethane	10.00	ND	ND			
Trichloroethene (TCE)	10.00	ND	ND			
Trichlorofluoromethane	10.00	ND	ND			
1,2,3-Trichloropropane	10.00	ND	ND			
1,2,4-Trimethylbenzene	10.00	ND	ND			
1,3,5-Trimethylbenzene	10.00	ND	ND			
Vinyl acetate	50.0	ND	ND			
Vinyl chloride (Chloroethene)	30.00	ND	ND			
o-Xylene	2.00	ND	ND			
m- & p-Xylenes	4.00	ND	ND			

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ANALYTICAL RESULTS

Page: 5
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 8260B, Volatile Organic Compounds

Our Lab I.D.		141806	141807			
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**			
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	111	116			
Dibromofluoromethane	70-120	82	84			
Toluene-d8	70-120	102	104			

QUALITY CONTROL REPORT

Batch No: 010405-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	114	104	9.2	75-120	15					
Chlorobenzene	106	101	4.8	75-120	15					
1,1-Dichloroethene (1,1-Dichloroethylene)	118	106	10.7	75-120	15					
MTBE	120	112	6.9	75-120	15					
Toluene (Methyl benzene)	114	103	10.1	75-120	15					
Trichloroethene (TCE)	106	100	5.8	75-120	15					

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ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Tricia Bartholome

Page: 6
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 8082, Polychlorinated Biphenyls(PCBs) by Gas Chromatography

Batch No:

Our Lab I.D.		**141805**				
Sample ID		B8-9				
Date Sampled		12/30/2004				
Date Extracted		01/04/2005				
Preparation Method						
Date Analyzed		01/06/2005				
Matrix		Soil				
Units		ug/kg				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
Aroclor-1016 (PCB-1016)	33.00	ND				
Aroclor-1221 (PCB-1221)	67.00	ND				
Aroclor-1232 (PCB-1232)	33.00	ND				
Aroclor-1242 (PCB-1242)	33.00	ND				
Aroclor-1248 (PCB-1248)	33.00	ND				
Aroclor-1254 (PCB-1254)	33.00	ND				
Aroclor-1260 (PCB-1260)	33.00	ND				

Our Lab I.D.		**141805**				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Decachlorobiphenyl	43-169	90				

QUALITY CONTROL REPORT

Batch No:

Analytes	LCS % REC	LCS DUP % REC	LCS RPD % REC	LCS/LCSD % Limit	LCS RPD % Limit				
Aroclor-1260 (PCB-1260)	113	113	<1	39-150	<30				

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ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Tricia Bartholome

Page: 7
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 6010B/7471A, CCR Title 22 Metals (TTLC)

Batch No:

Our Lab I.D.		**141806**	**141807**			
Sample ID		B9-10	B10-10			
Date Sampled		12/30/2004	12/30/2004			
Date Extracted		01/06/2005	01/06/2005			
Preparation Method						
Date Analyzed		01/06/2005	01/06/2005			
Matrix		Soil	Soil			
Units		mg/Kg	mg/Kg			
Detection Limit Multiplier		1	1			
Analytes	**PQL**	**Results**	**Results**			
AA Metals						
Mercury	0.20	ND	ND			
ICP Metals						
Antimony	0.50	0.63	0.75			
Arsenic	0.25	0.90	3.57			
Barium	0.50	64.1	125			
Beryllium	0.50	ND	ND			
Cadmium	0.50	2.87	0.81			
Chromium	0.50	10.7	10.4			
Cobalt	0.50	3.23	4.31			
Copper	0.50	19.8	20.0			
Lead	0.25	0.38	2.18			
Molybdenum	0.50	1.92	1.58			
Nickel	0.50	22.8	19.4			
Selenium	0.50	ND	ND			
Silver	0.50	0.84	0.70			
Thallium	0.50	ND	ND			
Vanadium	0.50	40.1	44.6			
Zinc	0.50	55.5	51.8			

QUALITY CONTROL REPORT

Batch No:

Analytes	LCS % REC	LCS/LCSD % Limit								

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ANALYTICAL RESULTS

Page: 8
Project ID: 04-17841
Project Name: Buckley School

Job Number	Order Date	Client
24280	01/03/2005	RINCON

Method: 6010B/7471A, CCR Title 22 Metals (TTLC)

QUALITY CONTROL REPORT

Batch No:

Analytes	LCS % REC	LCS/LCSD % Limit								
AA Metals										
Mercury	90	80-120								
ICP Metals										
Antimony	84	80-120								
Arsenic	86	80-120								
Barium	86	80-120								
Beryllium	89	80-120								
Cadmium	87	80-120								
Chromium	86	80-120								
Cobalt	90	80-120								
Copper	87	80-120								
Lead	84	80-120								
Molybdenum	84	80-120								
Nickel	87	80-120								
Selenium	88	80-120								
Silver	92	80-120								
Thallium	83	80-120								
Vanadium	86	80-120								
Zinc	89	80-120								

Site Assessment Report

Buckley School
3900 Stansbury Avenue
Sherman Oaks, California

Submitted to:

Los Angeles Fire Department
Underground Storage Tank Program

Prepared by:

Rincon Consultants, Inc.
January 7, 2006

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, California 93001

805 641 1000
FAX 641 1072

info@rinconconsultants.com
www.rinconconsultants.com

January 7, 2006
Project Number 04-17842

Captain Frank Comfort
Los Angeles Fire Department
Underground Storage Tank Program
200 North Main Street, Rm. 1700
Los Angeles, CA 90012

Site Assessment Report
3900 Stansbury Avenue
Sherman Oaks, California
ID Number 916061598

Dear Captain Comfort:

This *Site Assessment Report* has been prepared for the Buckley School property located at 3900 Stansbury Avenue in Sherman Oaks, California. Services were provided in accordance with Rincon's *Site Assessment Workplan*, dated October 31, 2005, and the Los Angeles Fire Department's approval letter, dated December 9, 2005. The purpose of this assessment was to collect and analyze soil and groundwater samples from the vicinity of the former underground storage tank. The following report summarizes the work preformed, the findings, and provides conclusions and a recommendation.

Please contact us with any questions regarding this Report.

Sincerely,
RINCON CONSULTANTS, INC.

Geoffrey Frieman, MESM
Project Manager, Environmental Services

Walter Hamann, PG, CEG, REA II
Vice President, Environmental Services

REGISTERED GEOLOGIST
WALTER E. HAMANN
No. EG 1635
CERTIFIED ENGINEERING GEOLOGIST
STATE OF CALIFORNIA

EXECUTIVE SUMMARY

This report presents the findings of a soil and groundwater assessment conducted by Rincon Consultants on behalf of the Buckley School, located at 3900 Stansbury Avenue in Sherman Oaks, California (Figure 1). The site is approximately an 18-acre developed property with a private school (elementary through high school), located in an area that is comprised of residential land uses and open space. The Buckley School campus is currently developed with approximately 16 structures.

The purpose of the soil and groundwater assessment was to collect and analyze soil and groundwater samples from the vicinity of the former underground storage tank (UST). One soil boring was advanced to groundwater near the center of the former UST pit, and converted to a groundwater monitoring well.

On December 22, 2005, a hollow-stem auger drill rig was used to drill one soil boring at the former UST area (Figure 2). The soil boring was converted into a 2-inch diameter groundwater monitoring well (MW-1). MW-1 was installed to assess groundwater at the former UST area at the Site (Figure 2). During drilling of the soil boring, soil samples were collected at five-foot intervals. A total of ten soil samples were collected during this assessment.

No soil discoloration was noted, however, gasoline odor was noted in the soil samples collected between 20 and 25 feet below grade. The photoionization detector (PID) readings ranged from 0 to 64.4 parts per million by volume (ppmv) for the soil samples collected. Soil was predominately comprised of silty sands and sandy clays with layers of hard brittle siltstone at approximately 25, 45, and 55 feet below grade. Methyl tertiary butyl ether (MTBE) was detected in samples at 20 and 30 feet below grade. Total petroleum hydrocarbons (TPH) as gasoline range, carbon range C4- C12, was detected at 20 feet below the existing grade.

Groundwater was encountered in the boring at an approximate depth of 55 feet below grade. The boring was deepened to 70 feet below grade to enable installation of a groundwater monitoring well. However, groundwater was encountered during the sampling of the groundwater monitoring well at 41.19 feet below the top of casing. The analyzed groundwater sample did not have detectable levels of TPH-gasoline, benzene, ethylbenzene, total xylenes, or fuel oxygenates. Toluene was detected at 1.2 micrograms per liter (µg/L).

To evaluate the significance of TPH-gasoline and VOC levels in soil, the levels were compared to Maximum Soil Screening Levels (MSSL) established by the Regional Water Quality Control Board – Los Angeles Region (RWQCB) for TPH and VOCs above Drinking Water Aquifers (*Interim Site Assessment and Cleanup Guidebook*, dated May 1996). The Los Angeles RWQCB MSSL for TPH-gasoline at the site was determined to be 500 milligrams per kilogram (mg/kg). A concentration of 0.682 mg/kg TPH-gasoline was detected in the soil sample collected below the former UST at 20 feet below grade. This value is below the MSSL for this constituent. The screening level for benzene at 30 and 20 feet above groundwater was calculated to be 0.0079 mg/kg and 0.0082 mg/kg, respectively. Benzene was detected at a concentration of 0.006 mg/kg and 0.003 mg/kg in the soil at depths of 30 and 20 feet above groundwater, respectively. These values are below the MSSL for this constituent. The screening level for MTBE at 20 feet above

INTRODUCTION

This report presents the findings of a soil and groundwater assessment conducted by Rincon Consultants on behalf of the Buckley School located at 3900 Stansbury Avenue in Sherman Oaks, California (Figure 1). The site is approximately an 18-acre developed property with a private school (elementary through high school), located in an area that is comprised of residential land uses and open space. The Buckley School campus is currently developed with approximately 16 structures.

The following sections provide: an overview of the project history; the purpose and scope of the project; the physical setting, sampling and analytical testing methodologies; the results of the sampling and testing program; and conclusions and recommendations.

PROJECT HISTORY

Rincon performed a Phase I and Phase II Environmental Site Assessment (ESA), dated March 25, 2005, for the Buckley School property. As part of the March 25, 2005 report, an environmental database search and a site reconnaissance was performed. As a follow-up to the database search and the site reconnaissance, we filed a request with Los Angeles City Fire Department (LAFD) and the Regional Water Quality Control Board (RWQCB) to review documents pertaining to the subject site. The following is based on the document review conducted by Rincon for the subject site on December 2, 2004.

Review of LAFD Files

According to an LAFD Fire/Life Safety Violation notice, dated May 27, 1988, Buckley School was directed to remove product from the leaking underground storage tank (UST), monitor the groundwater sump (located beneath the swimming pool, downgradient of the UST area) for flammable vapors, provide an integrity test of the UST, and provide the LAFD with a report of analysis from soil borings to determine whether or not an unauthorized release has occurred.

According to a June 2, 1988 LAFD Fire/Life Safety Violation notice, Buckley School was required to provide a site assessment including the extent of contamination, location of groundwater, groundwater flow direction, and cleanup recommendations.

According to an Engineering Report on Soil Gas Investigation, prepared by Enviropro Inc. on October 31, 1988, one 10,000-gallon gasoline tank was removed in July of 1988. During the excavation of the tank (July 1998), two soil samples were collected and analyzed for total petroleum hydrocarbons (TPH). TPH was detected at a concentration of 46,600 milligrams per kilogram (mg/kg) in the soil sample collected from the north end of the excavation (Sample #1). A preliminary soil gas investigation was conducted by Enviropro Inc. on August 11, 1988 using a photoionization detector (PID). A total of 29 boreholes were drilled to depths from 1 to 1.5 feet below grade. The boreholes were covered with a plastic film and vapors were allowed to collect in the borehole. PID readings were collected from the boreholes by penetrating the plastic film with the PID sampling probe. The report states that the results of the soil gas investigation are only qualitative, because no direct measurement of soil or groundwater contamination has been provided. PID readings collected from various locations near the tank excavation area and the Pavilion area, downgradient of the former tank area, indicate the highest volatile organic compound (VOC) concentration was detected near the tank excavation to the east. The report proposes that a subsequent remedial investigation be conducted, including the installation of three groundwater monitoring wells.

A LAFD letter, dated April 12, 1989, states that groundwater beneath the site has been impacted and the case has been referred to the State Regional Water Quality Control Board (SRWQCB).

Review of RWQCB Files

A May 27, 1988 State of California Hazardous Substance Spill Report indicates that the LAFD notified the RWQCB of the gasoline UST release. The spill report indicates that the UST leaked an unknown quantity of gasoline into the swimming pool and school grounds sump pump, causing fuel to be pumped into a drainage ditch, which flows to the Los Angeles River.

According to a June 2, 1988 Underground Storage Tank Unauthorized Release (Leak) / Contamination Site Report, an unknown quantity of gasoline was released from the UST. The leak was discovered on May 27, 1988 during a tank test. The discharge was reportedly stopped by removal of tank contents. A piping leak was the determined source of discharge of the 10,000-gallon, 16 year-old steel tank.

A RWQCB case closure letter, dated July 22, 1996, indicates site closure was granted and no further action was required related to the UST release. A copy of the July 22, 1996 RWQCB letter is included in Appendix 1.

March 25, 2005 Phase II Environmental Site Assessment

The findings of the March 25, 2005 Phase I ESA indicated that the former presence of a UST and associated gasoline release on the subject site was a recognized environmental condition.

To evaluate the potential site impact associated with the former UST, a Phase II ESA was conducted at the site on December 27 and 30, 2004. The Phase II included the collection of subsurface soil samples (B1 through B4) from four locations in the vicinity of the former UST (Figure 3) and the analysis of select soil samples for the presence of TPH, benzene, toluene, ethylbenzene and xylenes (BTEX), lead, and fuel oxygenates.

The soil sample laboratory analytical results are summarized in Table 1. The findings of the Phase II indicate that the RWQCB MSSLs for TPH as gasoline (TPH-g) and benzene were exceeded in sample B1 at 25 feet below grade. BTEX and methyl tertiary butyl ether (MTBE) were detected in soil samples collected at various depths in borings B1, B3, and B4 at concentrations that could potentially exceed the MSSLs. Without actual depth to groundwater data for these locations, exact MSSLs cannot be calculated to determine whether these thresholds have been exceeded. The MSSL exceedence and potential exceedences were identified in the four borings advanced in the vicinity of the former UST area. Groundwater was not encountered in these borings during the Phase II ESA. Therefore, impact to groundwater and depth to groundwater could not be assessed.

On behalf of the Buckley School, Rincon submitted a Site Assessment Workplan (dated November 18, 2005) to the LAFD. The purpose of the workplan was to assess the impact to groundwater and the depth to groundwater at the former UST area. The LAFD approved the workplan in a letter dated December 9, 2005 (Appendix 2).

PURPOSE AND SCOPE

The purpose of the soil and groundwater assessment was to collect and analyze soil and groundwater samples from the vicinity of the former UST. One soil boring was advanced to groundwater near the center of the former UST pit, and converted to a groundwater monitoring well.

Our scope of work included the following:

- Provide advance notice of field sampling to the LAFD.
- Obtain a groundwater monitoring well permit.
- Conduct a geophysical survey of the proposed boring locations.
- Drill one soil boring to approximately 70 feet below grade using a hollow-stem auger drill rig near the center of the former UST location.
- Collect soil samples from the soil boring at 5-foot intervals starting at 5 feet below grade and ending at approximately 70 feel below grade for purposes of soil classification, field screening for VOCs, and retaining undisturbed samples for laboratory analysis.
- Convert the soil boring to groundwater monitoring well MW-1. Develop, purge, and sample groundwater monitoring well MW-1.
- Analyze soil and groundwater samples for BTEX, TPH-g, and fuel oxygenates (including MTBE) by EPA Method 8260B.
- Prepare this report documenting our findings.

GEOLOGIC AND HYDROGEOLOGIC SETTING

Topography

The current USGS topographic map (Van Nuys Quadrangle, 1966, photorevised 1972) indicates that the site is situated at an elevation ranging from about 800 to 900 feet above mean sea level with topography sloping downward to the west-northwest on the eastern portion of the site and to the east-southeast on the western portion of the site.

Geology and Hydrogeology

The project area is near the southern boundary of the San Fernando Valley alluvial basin. The sediments in the area are erosional remnants of the sedimentary rocks found along the southern boundary of the Santa Monica Mountains. These sedimentary rocks consist of claystones and siltstones. Erosion of these sediments generally results in fine-grained alluvial deposits.

According to the Geologic Map of the Beverly Hills and Van Nuys (South 1/2) Quadrangles (Dibblee, 1991), the site is underlain by Quaternary-age alluvium and Miocene-age unnamed shale and Monterey Formation. The alluvium is comprised of unconsolidated deposits of gravel, sand and silt-clay, derived mostly from Santa Monica Mountains and including gravel and sand from stream channels. The unnamed shale is comprised of soft, white-weathering diatomaceous shale to diatomite. The Monterey Formation is comprised of white-weathering, thin bedded, moderately hard, dark siliceous shale, and tan to light gray semi-friable bedded sandstone.

The GeoCheck summary report reviewed for the March 25, 2005 Phase I ESA indicates that the site is underlain by a Tertiary age stratified sequence. The USDA soil survey for the general area of the property indicates that the soil types present in the site vicinity are primarily gravelly loam. Based on the results of the soil sampling performed by Rincon for the December 27 and 30, 2004 Phase II ESA and as part of the current assessment, soil was comprised primarily of sandy, silty clay mixtures, and siltstone.

Hydrogeology

The site is located in the southern portion of the Los Angeles River Watershed. In the San Fernando Valley area, groundwater depths range from near land surface to 100 feet below ground surface. Based on the results of the groundwater monitoring well installation (MW-1), groundwater was encountered at an approximate depth of 55 feet below grade. During groundwater sampling on January 10, 2006, groundwater was encountered at 41.19 feet below the top of casing. Groundwater flow direction has not been established for this site. However, based on the assumption that the groundwater flow direction in the area parallels the topographic gradient, the general anticipated groundwater flow direction in the vicinity of the former UST would be to the east-northeast.

METHODOLOGY

GEOPHYSICAL SURVEY

On December 22, 2005, Spectrum Geophysics of Burbank, California conducted a geophysical survey at the Site under the oversight of Rincon Consultants. The purpose of the geophysical survey was to assess the presence of utilities at each of the boring locations. The survey included the use of ground-penetrating radar (GPR) and electromagnetic utility locating equipment.

UTILITY MARKING AND NOTIFICATION

Consistent with California law, Underground Service Alert was notified prior to the commencement of subsurface sampling. The utility marking service identifies known utility locations in the public right of way.

GROUNDWATER MONITORING WELL INSTALLATION

Prior to groundwater monitoring well installation, a groundwater monitoring well permit was obtained from the County of Los Angeles Department of Health Services. A copy of the permit is included in Appendix 3.

On December 22, 2005, Test America Drilling Corporation of Anaheim, California, used a hollow-stem auger drill rig to drill one soil boring at the former UST area (Figure 2). The soil boring was converted into a 2-inch diameter groundwater monitoring well (MW-1). MW-1 was installed to assess groundwater at the former UST area at the Site (Figure 2). The well was installed under the responsible oversight of Rincon's California Professional Geologist.

SOIL SAMPLING

During drilling of the soil boring, soil samples were collected at five-foot intervals. The samples were collected by driving a modified California Split Spoon sampler with brass liner inserts. Soil retained for laboratory analysis from select sample intervals was preserved onsite using EPA method 5035. Soil was collected from the brass liner using a disposable Lock N' Load sampling device. The Lock N' Load soil sample was then placed into 40-milliliter (ml) VOA vials containing either sodium bisulfate preservative or a methanol preservative, provided by the analytical laboratory. The samples were labeled, placed in a sealable plastic bag, and stored in a cooler with blue ice pending delivery to the analytical laboratory. In addition, a liner from each sample interval was sealed with Teflon, capped, labeled, placed in a sealable plastic bag, and stored in the cooler pending delivery to the analytical laboratory. The soil from the liners at each sample interval was used to screen for volatile organics using a PID and to classify the soil using the Unified Soil Classification System.

Groundwater was encountered in the boring at an approximate depth of 55 feet below grade. The boring was deepened to 70 feet below grade to enable installation of a groundwater monitoring well. Soil cuttings generated during drilling were stored onsite in a roll-off soil bin. Augers were decontaminated between uses by steam cleaning. Sampling equipment was decontaminated between uses by washing with a non-phosphate solution followed by a potable water rinse. The decontamination fluids were stored onsite in a 55-gallon DOT drum.

The field log of the boring is included as Appendix 4, Log of Boring/Monitoring Well.

GROUNDWATER MONITORING WELL DEVELOPMENT AND SAMPLING

On January 10, 2006, the well was developed and purged with a submersible pump. Prior to development and purging of the well, depth to water and total well depth were measured using an electronic water level indicator. The well was surged to suspend sediments in the well casing. A submersible pump was then used to purge and develop the well. A temperature-conductivity-pH meter was used to monitor aquifer parameters during development and purging. These parameters were monitored to verify that the aquifer conditions had stabilized and the sample to be collected is representative of the aquifer conditions at that location. Approximately 10 well volumes of water (37 gallons) were removed from MW-1 using the submersible pump. Purged water was pumped directly into labeled, 55-gallon DOT drum. The purging equipment was decontaminated between uses by washing with a non-phosphate solution followed by a potable water rinse.

After allowing the well to recover to within 80% of its original level, a groundwater sample was collected using a disposable bailer. The sample was retained in 40-ml VOA vials. Care was taken to ensure no headspace or bubbles were created within the vials. The sample was labeled, placed in a sealable plastic bag and stored in a cooler with blue ice pending delivery to an analytical laboratory. A copy of the groundwater sampling data sheet is included as Appendix 5, Groundwater Sampling/Purging Data Sheet.

LABORATORY ANALYSIS

The soil and groundwater samples were transported to American Scientific Laboratories of Los Angeles, a California Certified laboratory, under chain-of-custody documentation. Five soil samples (collected at 10, 20, 30, 40 and 50 feet below grade) and one groundwater sample were tested for TPH-g, BTEX, and fuel oxygenates by EPA Method 8260B.

RESULTS

SOIL SAMPLING

No soil discoloration was noted, however, gasoline odor was noted in the soil samples collected between 20 and 25 feet below grade. The PID readings ranged from 0 to 64.4 parts per million by volume (ppmv) for the soil samples collected. Soil was predominately comprised of silty sands and sandy clays with layers of hard brittle siltstone at approximately 25, 45, and 55 feet below grade. Groundwater was encountered in the boring at a depth of approximately 55 feet below grade. A copy of the soil boring log is included in Appendix 4.

A summary of the analytical testing program is included in Table 2. A copy of the laboratory analytical report is included in Appendix 6.

GROUNDWATER SAMPLING

Groundwater was encountered during drilling at a depth of approximately 55 feet below grade. However, groundwater was encountered at approximately 41.19 feet below grade during the sampling of the groundwater monitoring well.

Results of the groundwater analytical testing are summarized in Table 3, Groundwater Analytical Testing Summary. A copy of the laboratory analytical report is included in Appendix 6. The analyzed groundwater sample did not have detectable levels of TPH-gasoline, benzene, ethylbenzene, total xylenes, or fuel oxygenates. A level of 1.2 μg/L toluene was detected in the groundwater sample.

SOIL AND GROUNDWATER DISPOSAL

Soil cuttings generated during drilling were stored onsite in a roll-off bin. Purged groundwater generated during drilling and well development was stored onsite in properly labeled DOT approved 55-gallon drums. On December 30, 2005 BESI transported the soil cuttings to TPST Soil Recyclers of Adelanto, California, a licensed recycling facility. Copies of the records documenting the proper disposal of the soil cuttings are included in Appendix 7. Copies of the records documenting the proper disposal of the purge water will be forwarded upon receipt from the appropriate disposal facility.

CONCLUSIONS

To evaluate the significance of TPH-gasoline and VOC levels in soil, the levels were compared to MSSL established by RWQCB for TPH and VOCs above Drinking Water Aquifers (*Interim Site Assessment and Cleanup Guidebook*, dated May 1996). The guidance document has been used to determine when a site may require remedial action or to establish an acceptable clean up standard for a particular constituent. The document was developed to simplify the remediation process by facilitating the selection of soil cleanup levels for petroleum and VOC-impacted sites. The RWQCB soil threshold methodology was primarily developed for the protection of groundwater. Site-specific information used to select the appropriate RWQCB screening level includes the hydrocarbon range of the contaminant, soil lithology, and depth to shallow groundwater below the contaminated area. Groundwater is located between approximately 41 to 55 feet below grade, contaminated soil is primarily present between approximately 10 and 20 feet below grade, so the contaminated soil is 20 to 30 feet above ground water and the soils are comprised of interbedded silt, sand, and clay. To calculate the cleanup value, we have modeled the sediment at 10 feet below grade to be represented as 30% clay, 30% silt, and 40% sand; and at 20 feet below grade to be represented by 60% clay and 40% sand. Using the RWQCB table, the depth between contaminated soil and groundwater and soil type (30 feet - 30% clay, 30% silt, and 40% sand) and (20 feet - 40% sand and 60% clay) the attenuation factor (AF) were calculated to be of (7.9) and (8.2); respectively . The drinking water maximum contamination limit (MCL) for BTEX is b=0.001, t=0.15, e=0.007, x=1.75 milligrams per liter (mg/L). To calculate the soil cleanup screening levels at respective depths they multiply the AF by the MCL for the respective constituent.

TPH in Soil Samples

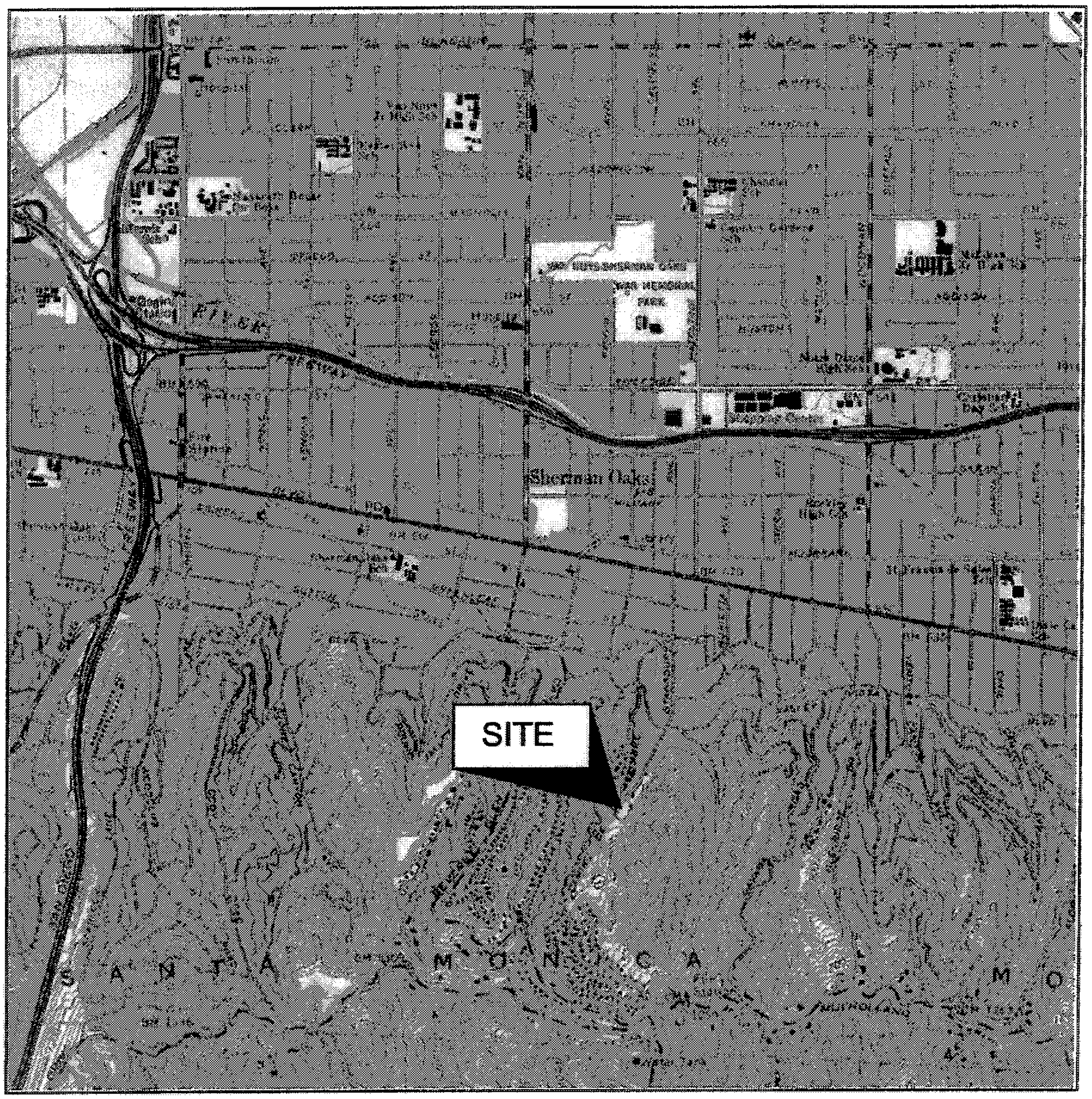
Los Angeles RWQCB MSSL for TPH-g is determined based on the distance between the soil contamination, at any given sample, and the underlying groundwater. TPH-gasoline was detected in the soil sample collected below the former UST at 20 feet below grade. Since groundwater is located between approximately 41 to 55 feet below grade, the MSSL for TPH-gasoline at the site was determined to be 500 mg/kg. TPH-g was detected in onsite alluvium at a maximum concentration of 0.682 mg/kg. This value is well below the calculated MSSL for TPH-g.

VOCs in Soil Samples

BTEX and MTBE were detected in the analyzed soil samples. The reported contaminant levels in the soil samples are well below the RWQCB action levels for these constituents, with the exception of benzene and MTBE. The level of BTEX and MTBE in soil were compared to their respective MSSL. Based on soil lithology, and depth to shallow groundwater below the contaminated area, the screening level for Benzene at 30 and 20 feet above groundwater was calculated to be 0.0079 mg/kg and 0.0082 mg/kg, respectively. Benzene was detected at a concentration of 0.006 mg/kg and 0.003 mg/kg in the soil at depths of 30 and 20 feet above groundwater, respectively. These values are well below the MSSL for this constituent. Based on Table 4.1 in the *Interim Site Assessment and Cleanup Guidebook*, dated May 1996, the screening level for MTBE at 20 feet above groundwater was calculated to be 0.0442 mg/kg. MTBE was detected at a concentration of 0.386 mg/kg in the soil at depths of 20, which exceeds the screening level.

Toluene in Groundwater Sample

To evaluate the significance of toluene in groundwater, the level was compared to MCLs established by Title 22 of the California Code of Regulations. The MCL for toluene in drinking water is 150 μg/L. Toluene was detected in groundwater samples collected during this assessment at 1.2 μg/L. The reported contaminant level is well below the MCL for this constituent.



Printed from TOPO!, 2001 National Geographic Holdings

0 1/2 1
Scale in Miles

North

Site Vicinity Map	
Buckley School 3900 Stansbury Avenue Sherman Oaks, California	Figure 1

Source: USGS - March 29, 2004

North

0 150 300

Approximate Scale in Feet

Groundwater Monitoring Well Location

Site Map	
Buckley School 3900 Stansbury Avenue Sherman Oaks, California	Figure 2

Table 1 - Analytical Testing Summary - TPH, BTEX, and Oxygenates
December 27 and 30, 2004

Boring	Depth (feet)	TPH (mg/kg) Gasoline (C4-C12)	DRO (C13-C22)	ORO (C22+)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	Oxygenates (mg/kg)	Lead (mg/kg)
B1	5	-	-	-	-	-	-	-	-	-
	10	ND	ND	ND	0.002	0.002	ND	ND	ND	-
	15	ND	ND	ND	ND	ND	ND	ND	ND	1.40
	20	2.05	-	-	0.032	0.09	0.024	0.195	MTBE - 0.816 TBA - 0.798	2.14
	25	1,080	ND	ND	8.4	31	13.7	104.2	MTBE - 3.13	ND
B2	5	-	-	-	-	-	-	-	-	-
	10	-	-	-	-	-	-	-	-	-
	15	ND	-	-	0.002	ND	ND	ND	ND	-
	20	ND	-	-	ND	ND	ND	ND	ND	-
B3	5	-	-	-	-	-	-	-	-	-
	10	93.4	ND	ND	ND	ND	ND	ND	ND	-
	15	0.646	ND	ND	0.007	0.003	ND	ND	MTBE - 0.206 TBA - 0.32	-
	20	2.55	ND	ND	0.07	ND	0.019	ND	MTBE - 1.05 TBA - 0.792	1.40
	25	28.5	ND	ND	0.295	1.98	0.67	3.79	MTBE - 2.74	1.91
	30	1.93	-	-	0.013	ND	0.053	0.054	MTBE - 1.05 TBA - 0.302	-
B4	5	-	-	-	-	-	-	-	-	-
	10	0.55	-	-	ND	0.002	ND	ND	MTBE - 0.129 TBA - 0.392	-
	15	2.02	-	-	0.004	0.002	ND	ND	MTBE - 1.27 TBA - 0.346	-
	20	10.2	-	-	0.027	0.054	0.053	0.245	MTBE - 6.95	-
Detection Limit		0.5-50	10	50	0.002-0.2	0.002-0.2	0.002-0.2	varies	varies	varies

- Not analyzed
ND - Not detected
mg/kg - milligrams per kilogram (parts per million)

Analyses:
TPH-G (total petroleum hydrocarbons, gasoline range) by EPA Method 8260B
TPH-DRO / TPH-ORO (total petroleum hydrocarbons, diesel range organics / oil range organics) by EPA Method 8015M
BTEX and Oxygenates by EPA Method 8260B
Lead by EPA Method 6010B

Table 2 - Analytical Testing Summary - TPH-g, BTEX, and Oxygenates
December 22, 2005

Boring	Depth (feet)	TPH-gasoline (C4-C12) (mg/kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethyl-benzene (mg/kg)	Total Xylenes (mg/kg)	Oxygenates (mg/kg)
MW-1	10	ND	0.003	0.003	ND	ND	ND
	20	0.682	0.006	0.004	0.008	0.008	MTBE-0.386
	30	ND	ND	0.015	0.004	0.025	MTBE-0.005
	40	ND	ND	0.005	0.004	0.006	ND
	50	ND	ND	0.002	ND	ND	ND
Detection Limit		0.500	0.002	0.002	0.002	varies	varies

mg/kg - milligrams per kilogram (parts per million)
ND - Not detected
TPH-gasoline (total petroleum hydrocarbons, gasoline range)

Analyses:

TPH-G (total petroleum hydrocarbons, gasoline range) by EPA Method 8260B
BTEX and Oxygenates by EPA Method 8260B

Table 3 - Water Analytical Testing Summary - TPH-g, BTEX, and Oxygenates

Sample Designation	TPH-gasoline (C4-C12) (µg/L)	Benzene (µg/L)	Toluene (µg/L)	Ethyl-benzene (µg/L)	Total Xylenes (µg/L)	Oxygenates (µg/L)
MW-1	ND	ND	1.2	ND	ND	ND
Detection Limit	50	1.0	1.0	1.0	varies	varies
MCL	NA	1.0	150.0	700.0	1750.0	varies

µg/L - micrograms per liter (parts per billion)
ND - not detected at or above detection limit
NA - not applicable
TPH-gasoline (total petroleum hydrocarbons, gasoline range)

Analyses:
TPH-G (total petroleum hydrocarbons, gasoline range) by EPA Method 8260B
BTEX and Oxygenates by EPA Method 8260B

Appendix 1

Los Angeles Regional Water Quality Control Board Letter
July 22, 1996

STATE OF CALIFORNIA—ENVIRONMENTAL PROTECTION AGENCY

PETE WILSON, Governor

CALIFORNIA REGIONAL WATER QUALITY CONTROL BOARD
LOS ANGELES REGION
101 CENTRE PLAZA DRIVE
MONTEREY PARK, CA 91754-2156
(213) 266-7500
FAX: (213) 266-7600

July 22, 1996

RECEIVED
JUL 30 19[illegible]
UNDERGROUND TANKS

Mr. Walter Baumhoff
Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA 91423

UNDERGROUND STORAGE TANK CASE CLOSURE
BUCKLEY SCHOOL
3900 STANSBURY AVENUE, SHERMAN OAKS (ID #916061598)

Dear Mr. Baumhoff

This letter confirms the completion of the site investigation and remedial action for the underground storage tank(s) formerly located at the above-described location.

Based on the available information and with the provision that the information provided to this agency was accurate and representative of site conditions, no further action related to the underground storage tank release is required.

This notice is issued pursuant to a regulation contained in Title 23, California Code of Regulations, Division 3, Chapter 16, Section 2721(e).

Please contact our office if you have any questions regarding this matter.

Sincerely,

ROBERT P. GHIRELLI, D. Env.
Executive Officer

DAVE DEANER
Acting Assistant Executive Officer
Underground Tanks

cc: Mr. Allan Patton, State Water Resources Control Board, Underground Storage Tank Program
Captain Jesse Pasos, Los Angeles City Fire Department, Underground Tanks

Appendix 2

Los Angeles Regional Water Quality Control Board Letter
December 9, 2005

CITY OF LOS ANGELES

CALIFORNIA

ANTONIO R. VILLARAIGOSA
MAYOR

DEPARTMENT OF FIRE

WILLIAM R. BAMATTRE
FIRE CHIEF

200 NORTH MAIN STREET
LOS ANGELES, CA 90012

(213) 978-3800
FAX: (213) 978-3815

http://www.lafd.org

December 9, 2005

Facility ID# 916061598

Elizabeth McGregor
Buckley School
3900 Stansbury Avenue
Sherman Oaks, CA 91423

Buckley School
3900 Stansbury Avenue
Sherman Oaks, California

Dear Elizabeth McGregor:

The Fire Department has reviewed the Site Assessment Workplan dated November 18, 2005, as submitted by Rincon Consultants, Incorporated.

Based on the information provided, this Department approves your Report.

Using the Site Address and Permit Number shown at the top of this letter, please label the title of your pending report to be submitted as **"SITE ASSESSMENT REPORT."**

In order to facilitate further processing of your pending report and other document submittals, please complete and return the attached "Required Information Form" with your future submittals, according to the instructions at the top of the form.

If you require additional information from the Los Angeles Fire Department, please contact Inspector II Neal Reitzell of the Environmental Unit, at (213) 482-6528.

Very truly yours,

WILLIAM R. BAMATTRE
Fire Chief

Frank K. Comfort

Frank K. Comfort, Captain I
Commander, Environmental Unit

FKC:NR:amo:3900StansburyAve#916061598air

cc: Walter Hamann, Rincon Consultants, Incorporated

Appendix 3

Groundwater Monitoring Well Permit

WELL PERMIT APPLICATION - NON-PRODUCTION WELLS

WATER & SEWAGE / MOUNTAIN & RURAL PROGRAMS - ENVIRONMENTAL HEALTH DIVISION
5050 COMMERCE DRIVE, BALDWIN PARK, CA 91706 (626) 430-5380 FAX (626) 813-3016

DATE: 12/6/05

X NEW WELL CONSTRUCTION	___ MONITORING	___ HEAT EXCHANGE
___ RECONSTRUCTION OR RENOVATION	___ CATHODIC	___ OTHER (Specify):
___ DECOMMISSIONING	___ INJECTION	
___ OTHER:	___ EXTRACTION	

WELL LOCATION

SITE ADDRESS: 3900 Stansbury Avenue	CITY: Sherman Oaks, CA		ZIP CODE: 90012
Township: 01W	Range: 15W	Section: 27	Map Book Page/ Grid: 562, A-6
NO. OF WELLS IN EACH PARCEL: 3	Attach site map with well locations		

WELL STRUCTURE

Type and Size of Production Casing	2" diam PVC casing, screen (85'-110') + solid (0'-85')
Sanitary / Annular Sealing Material	monterey sand, bentonite, volclay grout (screen) (solid) (solid)
Depth of Sanitary / Annular Seal	monterey sand (83'-110'), bentonite (2'-83'), grout (0-2')
Conductor Casing Seal	

CONSULTANT

Company	Rincon Consultants
Contact Person	Geoff Frieman
Address	790 E. Santa Clara St.
City, State Zip	Ventura, CA 93001
Telephone	(805) 641-1000

IF WELL AND GEOLOGIC CONDITIONS ENCOUNTERED IN THE FIELD ARE FOUND TO DIFFER FROM THE SCOPE OF WORK PRESENTED TO THIS OFFICE, WORK PLAN MODIFICATIONS MAY BE REQUIRED

OWNER / DRILLER INFORMATION

Well Owner	Buckley School
Address	3900 Stansbury Ave.
City / Zip Code	Sherman Oaks, CA 90012
Telephone	(818) 461-6720
Well Driller	Test America (For Rincon)
Address	1016 E. Katella Ave.
City / Zip Code	Anaheim, CA 92805
C-57 License No.	
Telephone	(714) 939-6850

DISPOSITION OF PERMIT (Department Use Only)

THIS PERMIT IS CONSIDERED COMPLETE WHEN THE WORK PLAN IS APPROVED AND WHEN THE WELL COMPLETION LOG IS RECEIVED. NO WELL CONSTRUCTION OR DECOMMISSIONING CAN BE INITIATED WITHOUT THE WORK PLAN APPROVAL FROM THIS DEPARTMENT.

WORK PLAN APPROVAL
This Approval is Valid for 180 Days

Date: 1-17-06 REHS: [signature]

Conditions

WELL DECOMMISSIONING

Well Depth log / records	
Method of Well Assessment	
Depth and Number of Perforations	
Type of Perforator Size of Perforations	
Type and Amount of Sealant	
Method of Upper Seal Pressure Application	

1-19-06 – VERIFIED THAT ONLY MW-1 WAS INSTALLED – PER GEOFF FRIEMAN, MW-2 & MW-3 WERE NOT NECESSARY AND WILL THEREFORE NOT BE INSTALLED

I hereby agree to comply in every respect with all the regulations of the County Environmental Health Division and with all ordinances and laws of the County of Los Angeles and the State of California pertaining to well construction, reconstruction and decommissioning. Upon completion of the well and within thirty days thereafter, I will furnish the Environmental Health office with a completion log of the well giving date drilled, depth of the well, perforations in the casing, and any other data deemed necessary by County Environmental Health Division.

[signature] for Rincon Consultants

Applicant's Signature

Applicant Name: (PRINT) Rincon Consultants
Telephone: (805) 641-1000

FINAL INSPECTION

Date: 1-19-06 REHS: [signature]

PERMIT ISSUED

The well log must be submitted to this Department prior to issuance of the final approval

Date: 1-19-06 REHS: [signature]

76A668-A
H-13 (Rev. 01/2001)

Appendix 4

Log of Boring/Monitoring Well

Rincon Consultants

LOG OF BORING/WELL DIAGRAM MW-1

Buckley School
3900 Stansbury Ave
Sherman Oaks, CA

04-17842

Date Completed	: 12/22/05
Drilling Method	: Hollow-Stem Auger
Driller	: Test America
Boring Location	: Buckely School
Logged By	: Bart Templeman

Well: MW1

Depth in Feet	USCS	DESCRIPTION	PID	Blow Count
0	SM	CLAYEY, SILTY SAND, brown, dry, slightly plastic, medium to coarse grained, firm, no odor		
5			1.7	6 5 4
10			2.0	9 10 11
15			2.5	8 10 12
20	CL	SANDY CLAY, light brown, dry, plastic, fine to medium grained, stiff, gasoline odor	4.4	7 8 10
25	ML	SILTSTONE, light brown and yellow, dry, non plastic, very fine grained, brittle, strong gasoline odor	64.4	50
30	ML	SANDY SILT, yellow and brown, dry, non plastic, very fine grained, hard, slight gasoline odor	7.0	40 50
35				35 50

Well construction: Grout (0–2 ft); Seal (Bentonite) (2–30 ft); Sand Pack (30–35 ft)

01-03-2006 P:\ESA Projects\Latham and Watkins\04-17840 Buckley School\GWM well install\boring logMW1.bor

Rincon Consultants

LOG OF BORING/WELL DIAGRAM MW-1

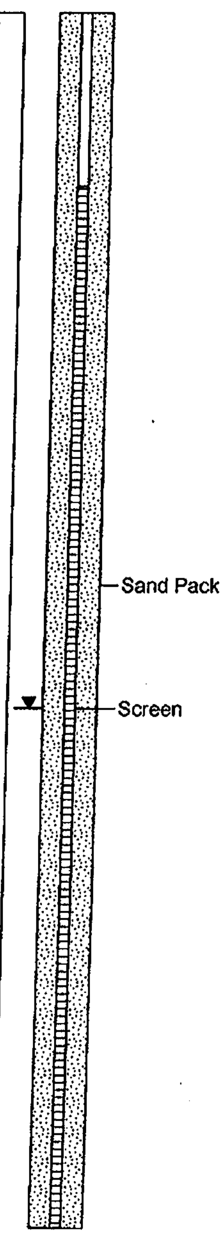
Buckley School
3900 Stansbury Ave
Sherman Oaks, CA

04-17842

Date Completed	: 12/22/05
Drilling Method	: Hollow-Stem Auger
Driller	: Test America
Boring Location	: Buckely School
Logged By	: Bart Templeman

Depth in Feet	USCS	DESCRIPTION	PID	Blow Count
35	ML	CLAYEY SILT, brown, dry, non plastic, fine grained, hard, very slight odor	3.4	
40		slightly plastic, firm, no odor	3.0	25 30 35
45	CL	CLAY/ROCK, dark brown, dry, non plastic, very fine grained, very hard, no odor	4.8	27 50
50	ML	SANDY SILT, dark brown, slightly moist, non plastic, medium to fine grained, loose, no odor	2.0	50
55	CL	CLAY/ROCK, dark brown, dry, non plastic, very fine grained, very hard, no odor	1.2	50
60			1.0	35 50
65			1.1	50
70				35 80

Well: MW1



01-03-2006 P:\ESA Projects\Latham and Watkins\04-17840 Buckley School\GWM well Install\boring logMW1.bor

Appendix 5

Groundwater Sampling/Purging Data Sheet

Rincon Consultants, Inc.

GROUND WATER SAMPLING/PURGING DATA SHEET

Job No: 04-17842	Date: 1-10-08
Project/Location Buckley School/Sherman Oaks	Well Number: MW1
Observation Period Start: Stop:	Survey Reference Point: North
Sampled By: SD	Witnessed By:

PURGING DATA

Type of Pump	Sub	Pump Inlet Depth (ft)	
Well Diameter (in)	2	Depth of Well (ft)	64.41
Depth to Water (ft)	41.19	Length of Water Column (ft)	23.22
Product Thickness (ft)	None	Volume Multiplier (gal/ft)	0.16
One Casing Volume (gal)	3.72	Three Casing Volumes (gal)	11.16
Purge Time, Start	11:20	Purge Time, Stop	11:50
Total Purge Time	30 minutes	Purge Rate (gpm)	1.2
Purge Volume (gal)	37	Drawdown (ft)	48.13

CASING OR BOREHOLE VOLUME =6.94

0.5-Inch Diameter = 0.010 gal/ft	4-Inch Diameter = 0.65 gal/ft
0.75-Inch Diameter = 0.023 gal/ft	6-Inch Diameter = 1.46 gal/ft
1-Inch Diameter = 0.041 gal/ft	9-Inch Diameter = 3.30 gal/ft
1.5-Inch Diameter = 0.092 gal/ft	12-Inch Diameter = 5.87 gal/ft
2-Inch Diameter = 0.16 gal/ft	15-Inch Diameter = 9.18 gal/ft

INDICATOR DATA

Volume Pumped (gal)	Before Purge	~~3.72~~ 7.44	14.88	22.32	29.76	33.48	37.2	
~~Parameter~~ TDS	632	1600	1684	1626	1606	1581	1562	At Sampling
Temperature (C)	19.0	19.3	19.1	19.1	18.2	18.6	18.9	
Conductivity (micromhos)	1264	3204	3371	3249	3190	3164	3124	
pH	6.80	6.68	6.66	6.64	6.64	6.66	6.65	
Dissolved Oxygen								
Comments:		x2	x4	x6	x8	x9	x10	

MISCELLANEOUS DATA

Condition of Traffic Box: Good

Drum Identification labeling: Non-Haz Waste

Weather Conditions: Clear

Comments:

Waited till 12:25 depth to water at 41.86

Sampled at 12:30

Appendix 6

Laboratory Analytical Reports

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Telephone (805) 641-1000
Attn Geoff Frieman

Number of Pages 5
Date Received 12/23/2005
Date Reported 01/03/2006

Job Number	Ordered	Client
28008	12/23/2005	RINCON

Project ID: 04-17842
Project Name: Buckley
Site: 3900 Stansbury Ave.
Sherman Oaks, CA

Enclosed are the results of analyses on 5 samples analyzed as specified on attached chain of custody.

Wendy Lu
Organics Supervisor

Rojert G. Araghi
Laboratory Director

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

CHAIN OF CUSTODY RECORD

COC# GLOBAL ID ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 28008

Company: Rincon Consultants, Inc.
Address: 790 E. Santa Clara Ventura CA 93001
Telephone: 805/641-1000
Fax: 805/641-1072
Special Instruction:

Project Name: Buckley
Site Address: 3900 Stansbury Ave Sherman Oaks CA
Project ID: 04-17842
Project Manager: Geoff F.

Report To: Bart
Address: 790 E Santa Clara
Invoice To: Rincon
Address: 790 E Santa Clara Ventura CA
P.O.#: 04-17842

ANALYSIS REQUESTED: BTEX + Oxy 8260B; TPH-G 8260B

ITEM	Lab ID	Sample ID	Date	Time	#	Type	Matrix	Preservation	BTEX + Oxy 8260B	TPH-G 8260B	Remarks
		MW1-5	12/22/05	12:00	4	6" Brass Voas	Solid	NaSO4 H2O CH3OH			
1	162376	MW1-10		12:10					X	X	Hold
		MW1-15		12:20							
2	162377	MW1-20		12:30					X	X	Hold
		MW1-25		12:40							
3	162378	MW1-30		12:50					X	X	Hold
		MW1-35		13:00							
4	162379	MW1-40		13:10					X	X	Hold
		MW1-45		13:20							
5	162380	MW1-50		13:30					X	X	Hold

Collected By: Date Time

Relinquished By: [signature] Date 12/23/05 Time 10:40

Condition of Sample:

Relinquished By: Date Time

Received For Laboratory: Bart K Date 12.23.05 Time 10:25

TAT ☐ Normal ☐ Rush

White - Report, Yellow - Laboratory, Pink - Client

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

COC# Nº 35289 GLOBAL ID ______ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 28008

CHAIN OF CUSTODY RECORD

Company: Rincon Consultants
Address: 790 E. Santa Clara
Ventura CA 93001
Telephone: 805/641-1000
Fax: 805/641-1072
Special Instruction:

Project Name: Buckley School
Site Address: 3900 Stansbury Ave
Sherman Oaks
Project ID: 04-17842
Project Manager: Geoff F.

Report To: Bart
Address: 790 E. Santa Clara
Invoice To: Rincon
Address: 790 E Santa Clara
Ventura CA
P.O.#: 04-17842

ANALYSIS REQUESTED: BTEX OXY 8260B; TPH-g 8260B

ITEM	Lab ID	Sample ID	Date	Time	#	Type	Matrix	Preservation	Remarks
		MW1-55	12/22/05	13:40	4	6" Brass VOAs	NaSO4 H2O CH3OH	Solid	Hold
		MW1-60		13:50					Hold
		MW1-65		14:00					Hold
		MW1-70		14:10					Hold
		MW1-75		14:20					Hold

Collected By:
Relinquished By: [signature] Date 12/23/05 Time 10:40
Condition of Sample:

Relinquished By: Date Time
Received For Laboratory: [signature] Date 12 23 05 Time 10:25

TAT ☐ Normal ☐ Rush

White - Report, Yellow - Laboratory, Pink - Client

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Geoff Frieman

Page: 2
Project ID: 04-17842
Project Name: Buckley

Job Number	Order Date	Client
28008	12/23/2005	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 122905-2C

Our Lab I.D.		162376	162378	162379	162380	
Sample ID		MW1-10	MW1-30	MW1-40	MW1-50	
Date Sampled		12/22/2005	12/22/2005	12/22/2005	12/22/2005	
Date Extracted		12/30/2006	12/30/2006	12/30/2006	12/30/2006	
Preparation Method						
Date Analyzed		12/30/2006	12/30/2006	12/30/2006	12/30/2006	
Matrix		Soil	Soil	Soil	Soil	
Units		ug/kg	ug/kg	ug/kg	ug/kg	
Detection Limit Multiplier		1	1	1	1	
Analytes	**PQL**	**Results**	**Results**	**Results**	**Results**	
Benzene	2.00	3	ND	ND	ND	
DIPE	5.00	ND	ND	ND	ND	
ETBE	5.0	ND	ND	ND	ND	
Ethylbenzene	2.00	ND	4	4	ND	
MTBE	5.00	ND	5	ND	ND	
TAME	5.00	ND	ND	ND	ND	
TBA	20	ND	ND	ND	ND	
Toluene (Methyl benzene)	2.00	3	15	5	2	
o-Xylene	2.00	ND	6	ND	ND	
m- & p-Xylenes	4.0	ND	19	6	ND	
TPH as Gasoline (C4-C12)	500	ND	ND	ND	ND	

Our Lab I.D.		162376	162378	162379	162380	
Surrogates	**Con.Limit**	**% Rec.**	**% Rec.**	**% Rec.**	**% Rec.**	
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	106	105	107	120	
Dibromofluoromethane	70-120	119	119	120	112	
Toluene-d8	70-120	107	106	110	96	

QUALITY CONTROL REPORT

Batch No: 122905-2C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	113	109	3.6	75-120	15					

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Page: 3
Project ID: 04-17842
Project Name: Buckley

Job Number	Order Date	Client
28008	12/23/2005	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 122905-2C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	108	112	3.6	75-120	15					
Toluene (Methyl benzene)	115	120	4.3	75-120	15					

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Site

3900 Stansbury Ave.
Sherman Oaks, CA

Telephone: (805)641-1000
Attn: Geoff Frieman

Page: 4
Project ID: 04-17842
Project Name: Buckley

Job Number	Order Date	Client
28008	12/23/2005	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 123005-1C

Our Lab I.D.		162377				
Sample ID		MW1-20				
Date Sampled		12/22/2005				
Date Extracted		12/30/2006				
Preparation Method						
Date Analyzed		12/30/2006				
Matrix		Soil				
Units		ug/kg				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
Benzene	2.00	6				
DIPE	5.00	ND				
ETBE	5.0	ND				
Ethylbenzene	2.00	8				
MTBE	5.00	386				
TAME	5.00	ND				
TBA	20	ND				
Toluene (Methyl benzene)	2.00	4				
o-Xylene	2.00	2				
m- & p-Xylenes	4.0	6				
TPH as Gasoline (C4-C12)	500	682				

Our Lab I.D.		162377				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	95				
Dibromofluoromethane	70-120	117				
Toluene-d8	70-120	107				

QUALITY CONTROL REPORT

Batch No: 123005-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	117	106	9.9	75-120	15					

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Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Page: 5
Project ID: 04-17842
Project Name: Buckley

Job Number	Order Date	Client
28008	12/23/2005	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 123005-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	101	90	11.5	75-120	15					
Toluene (Methyl benzene)	117	113	3.5	75-120	15					

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Telephone (805)641-1000
Attn Shawn Decker

Number of Pages 3
Date Received 01/11/2006
Date Reported 01/18/2006

Job Number	Ordered	Client
28135	01/11/2006	RINCON

Project ID: 04-17842
Project Name: Buckley School

Enclosed are the results of analyses on 1 sample analyzed as specified on attached chain of custody.

Wendy Lu
Organics Supervisor

Rojert G. Araghi
Laboratory Director

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Road, LA, CA 90065 Tel: (323) 223-9700 • Fax: (323) 223-9500

CHAIN OF CUSTODY RECORD

COC# № 35284 GLOBAL ID ________ ELECTRONIC REPORT: ☐ EDF ☐ EDD ASL JOB# 28135

Company: Rincon Consultants, Inc.
Address: 790 E. Santa Clara, Ventura, CA 93001
Telephone: 805/641-1000
Fax: 805 641-1072
Special Instruction:

Project Name: Buckley School
Site Address:
Project ID: 04-17842
Project Manager: Shawn Deikes

Report To: Rincon
Address:
Invoice To:
Address:
P.O.#:

ANALYSIS REQUESTED: 8260B TPH-g, BTEX, Fuel oxygenates

ITEM	Lab ID (LAB USE ONLY)	Sample ID	Date	Time	Container(s) #	Container(s) Type	Matrix	Preservation	8260B TPH-g, BTEX, Fuel oxygenates	Remarks
	163090	MW-1	1-10-06	12:30	3	VOA	H_2O	None	X	

Collected By: [signature] Date 1-10-06 Time 12:30
Relinquished By: [signature] Date 1-11-06 Time 11:00
Condition of Sample:

Relinquished By: Date Time
Received For Laboratory [signature] Date 1/11/06 Time 11:00

TAT: ☒ Normal ☐ Rush

White - Report, Yellow - Laboratory, Pink - Client

RECOMMENDATIONS

The analytical results from the soil and groundwater monitoring indicate the at all detected contaminants are below the respective screening levels for the detected constituents with the exception of MTBE at 20 feet below grade. The groundwater sample did no have any detected constituents that exceed its maximum contaminant level in drinking water. Due to the low levels and the impermeable soil lithology between the contamination and groundwater we recommend no further action for the site and we respectfully request that the RWQCB maintain case closure.

LIMITATIONS

This report has been prepared for and is intended for the exclusive use of Buckley School and its assignees. The contents of this report should not be relied upon by any other party without the written consent of Rincon Consultants, Inc.

Our conclusions regarding the site are based on the results of a limited subsurface sampling program. The results of this evaluation are qualified by the fact that only limited sampling and analytical testing was conducted during this assessment.

This scope was not intended to completely establish the quantities and distribution of contaminants present at the site or to determine the cost to remediate the site. The concentrations of contaminants measured at any given location may not be representative of conditions at other locations. Further, conditions may change at any particular location as a function of time in response to natural conditions, chemical reactions and other events. Conclusions regarding the condition of the site do not represent a warranty that all areas within the site are similar to those sampled.

groundwater was calculated to be 0.0442 mg/kg. MTBE was detected at a concentration of 0.386 mg/kg in the soil at depths of 20 which exceeds the screening level. The maximum contamination level (MCL), established by the RWQCB, for toluene in drinking water is 150 μg/L. Toluene was detected in groundwater samples collected during this assessment at 1.2 μg/L. The reported contaminant level is below the MCL for this constituent.

The analytical results from the soil and groundwater monitoring indicate the at all detected contaminants are below the respective screening levels for the detected constituents with the exception of MTBE at 20 feet below grade. The groundwater sample did no have any detected constituents that exceed its maximum contaminant level in drinking water. Due to the low levels and the impermeable soil lithology between the contamination and groundwater we recommend no further action for the site and we respectfully request that Los Angeles Fire Department (LAFD) maintain case closure.

AMERICAN SCIENTIFIC LABORATORIES, LLC
Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Ordered By

Rincon Consultants, Inc.
790 East Santa Clara Street
Ventura, CA 93001

Telephone: (805)641-1000
Attn: Shawn Decker

Page: 2
Project ID: 04-17842
Project Name: Buckley School

Job Number	Order Date	Client
28135	01/11/2006	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

Batch No: 011206-1C

Our Lab I.D.		163090				
Sample ID		MW-1				
Date Sampled		01/10/2006				
Date Extracted		01/12/2006				
Preparation Method						
Date Analyzed		01/12/2006				
Matrix		Water				
Units		ug/L				
Detection Limit Multiplier		1				
Analytes	**PQL**	**Results**				
Benzene	1.000	ND				
DIPE	2.000	ND				
ETBE	2.000	ND				
Ethylbenzene	1.000	ND				
MTBE	2.000	ND				
TAME	2.000	ND				
TBA	10.00	ND				
Toluene (Methyl benzene)	1.000	1.2				
o-Xylene	1.000	ND				
m- & p-Xylenes	2.000	ND				
TPH as Gasoline (C4-C12)	50	ND				

Our Lab I.D.		163090				
Surrogates	**Con.Limit**	**% Rec.**				
Surrogate Percent Recovery						
Bromofluorobenzene	70-120	103				
Dibromofluoromethane	70-120	97				
Toluene-d8	70-120	107				

QUALITY CONTROL REPORT

Batch No: 011206-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
Benzene	103	114	10.1	75-120	15					

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Environmental Testing Services
2520 N. San Fernando Rd., Los Angeles, CA 90065 Tel: (323) 223-9700 Fax: (323) 223-9500

ANALYTICAL RESULTS

Page: 3
Project ID: 04-17842
Project Name: Buckley School

Job Number	Order Date	Client
28135	01/11/2006	RINCON

Method: 8260B, Gas/BTEX and Oxygenates

QUALITY CONTROL REPORT

Batch No: 011206-1C

Analytes	MS % REC	MS DUP % REC	RPD %	MS/MSD % Limit	MS RPD % Limit					
MTBE	82	88	7.1	75-120	15					
Toluene (Methyl benzene)	118	120	1.7	75-120	15					

Appendix 7

Waste Manifest

Manifest

TPST Soil Recyclers of CA

Non-Hazardous Soils

Date of Shipment:	Responsible for Payment:	Transporter Truck #:	Facility #:	Given by TPST:	Load #
12 30 2005	BELSHIRE	707 / 733	A07	26305	11

Generator and/or Consultant

Generator's Name and Billing Address:	Generator's Phone #:	Generator's US EPA ID No.
BUCKLEY SCHOOL 3900 STANSBURY SHERMAN OAKS, CA	Person to Contact:	
	FAX#:	Customer Account Number with TPST:

Consultant's Name and Billing Address:	Consultant's Phone #:	
	Person to Contact:	
	FAX#:	Customer Account Number with TPST:

Generation Site (Transport from): *(name & address)*	Site Phone #:	BTEX Levels
BUCKLEY SCHOOL 3900 STANSBURY SHERMAN OAKS, CA	Person to Contact:	TPH Levels
	FAX#:	AVG. Levels

Designated Facility (Transport to): *(name & address)*	Facility Phone #: 800-862-8001	Facility Permit Numbers
TPST SOIL RECYCLERS OF CA 12328 HIBISCUS AVENUE ADELANTO, CA 92301	Person to Contact: DELLENA JEFFREY	
	FAX#: 760-246-8004	

Transporter Name and Mailing Address:	Transporter's Phone #: 949-450-1010	Transporter's US EPA ID No.: CAR000165175
B.E.S.I. 25971 TOWNE CENTRE DRIVE LAKE FOREST, CA 92610	Person to Contact: BRIAN CASS	Transporter's DOT No.: 450647
BESI# 120059.03	FAX#: 949-450-1177	Customer Account Number with TPST: 1000193

Description of Soil	Moisture Content	Contaminated by:	Approx. Qty:	Description of Delivery	Gross Weight	Tare Weight	Net Weight
Sand ☐ Organic ☐ Clay ☐ Other ☐	0 - 10% ☐ 10 - 20% ☐ 20% - over ☐	Gas ☐ Diesel ☐ Other ☐		soil	39900	36460	3440
Sand ☐ Organic ☐ Clay ☐ Other ☐	0 - 10% ☐ 10 - 20% ☐ 20% - over ☐	Gas ☐ Diesel ☐ Other ☐					1.72

List any exception to items listed above: Scale Ticket# 29323

Generator's and/or consultant's certification: I/We certify that the soil referenced herein is taken entirely from those soils described in the Soil Data Sheet completed and certified by me/us for the Generation Site shown above and nothing has been added or done to such soil that would alter it in any way.

Print or Type Name: Daniel Barrera Generator ☐ Consultant ☐ Signature and date: Month 12 Day 30 Year 05

Transporter

Transporter's certification: I/We acknowledge receipt of the soil described above and certify that such soil is being delivered in exactly the same condition as when received. I/We further certify that this soil is being directly transported from the Generation Site to the Designated Facility without off-loading, adding to, subtracting from or in any way delaying delivery to such site.

Print or Type Name: Frank Salazar (B# 2821640ML) Signature and date: Month 12 Day 30 Year 05

Recycling Facility

Discrepancies:

FAC# 39005TAN

ID# 122124

Recycling Facility certifies the receipt of the soil covered by this manifest except as noted above:

Print or Type Name: Signature and date: 12305

Please print or type

TRANSPORTER COPY